TIPTON STATION SUBDIVISION

Transportation Impact Analysis Tipton Station Road Knoxville, TN

A Transportation Impact Analysis for the Tipton Station Subdivision

Submitted to

Knoxville-Knox County Planning

Updated October 14, 2024 August 19, 2024 Ardurra Project No. 787.001

Submitted By:



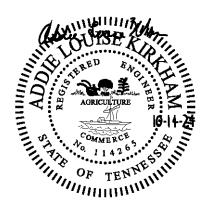


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Executive Summary

D.R. Horton - Knoxville is proposing a residential development. The project is located east of the two-way stop-controlled intersection of W Martin Mill Pike at Tipton Station Road in Knox County, Tennessee. The full buildout of the Tipton Station Subdivision proposes 343 single-family residential lots. Construction is proposed to take place this year and this study assumes full build out for the development will occur in 2027.

The Tipton Station Subdivision has a proposed single roadway connection to Tipton Station Road with a boulevard entrance.

Based on the results of the traffic analysis conducted to determine the impacts caused by the Tipton Station Subdivision on the studied intersections, the following observations have been made:

W Martin Mill Pike at Tipton Station Road

After the completion of the Tipton Station Road Subdivision the traffic conditions for the two-way stop-controlled intersection of W Martin Mill Pike at Tipton Station Road operates as follows: the northbound approach (Tipton Station Road) operate at a LOS A during both the AM and PM peak hours and the eastbound approach (Tipton Station Road) operates at a LOS C during both the AM and PM peak hours.

A northbound left turn lane is warranted during the AM peak hour per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

Maryville Pike (SR 33) at Tipton Station Road

After the completion of the Tipton Station Road Subdivision the overall traffic conditions for the two-way stop-controlled intersection of Maryville Pike (SR 33) at Tipton Station Road will operate as follows: the westbound approach (Tipton Station Road) will operate at a LOS F during the PM peak hour; however, the overall intersection delay will continue to operate at an acceptable LOS.

A southbound left turn lane is warranted during the existing, background and full buildout conditions. The warrant for a southbound left turn lane is an existing condition and not a result of the Tipton Station Subdivision.

Tipton Station Road at Roadway Connection

After the completion of the full buildout of the Tipton Station Subdivision the intersection of Tipton Station Road at Subdivision Roadway will operate as follows. The northbound approach (Subdivision Roadway) will operate at a LOS B during both

the AM and PM peak hours and the westbound approach (Tipton Station Road) will operate at a LOS A during both the AM and PM peak hours.

Recommendations

In order to maintain or provide an acceptable level-of-service for each of the intersections studied, some recommendations are presented.

- Recommended mitigation at W Martin Mill Pike at Tipton Station Road
 - o Install a northbound left turn lane with a minimum storage length of 50 feet.
- Recommended mitigation at Maryville Pike (SR 33) at Tipton Station Road
 - A southbound left turn lane is warranted during the existing conditions per the TDOT Highway System Access Manual.
 - There are no recommended improvements as a result of the Tipton Station Subdivision.
- Recommended mitigation at Tipton Station Road at Subdivision Connection
 - o Install a boulevard entrance between Tipton Station Road and the first internal intersection.
- Ardurra recommends that the intersection sight distance be certified by a land surveyor prior to construction in order to verify that Tipton Station Road has adequate intersection sight distance at the proposed subdivision roadway connection.
- Ardurra recommends that the signs and pavement markings be installed in accordance with the standards provided in the Manual on Uniform Traffic Control Devices (MUTCD).
- Any future improvements to the intersection or the various traffic management infrastructure, would need to be reviewed, coordinated, and approved by Knox County Engineering and Public Works.

1 Introduction

1.1 Project Description

This report provides a summary of a transportation impact analysis that was performed for the Tipton Station Subdivision residential development. The Tipton Station Subdivision proposes 343 single-family residential lots. The project is located east of the two-way stop-controlled intersection of W Martin Mill Pike at Tipton Station Road in Knox County, Tennessee. The location of the site is shown in Figure 1.

Construction is proposed to take place this year and this study assumes full build out for the subdivision and the future development area will occur in 2027.

The Tipton Station Subdivision has a proposed single roadway connection to Tipton Station Road with a boulevard entrance.

The standard practice for a residential development with 150 or more lots/units is to require at least two access points to provide alternative access opportunities in the event that one access is blocked by a fallen tree, crash, or other. For the Tipton Station Subdivision the roadway connection proposes a boulevard entrance with a single lane for entering and exiting traffic. The boulevard entrance extends from Tipton Station Road to the first internal intersection in order to provide an alternate access.

The proposed site layout is shown in Figure 2.

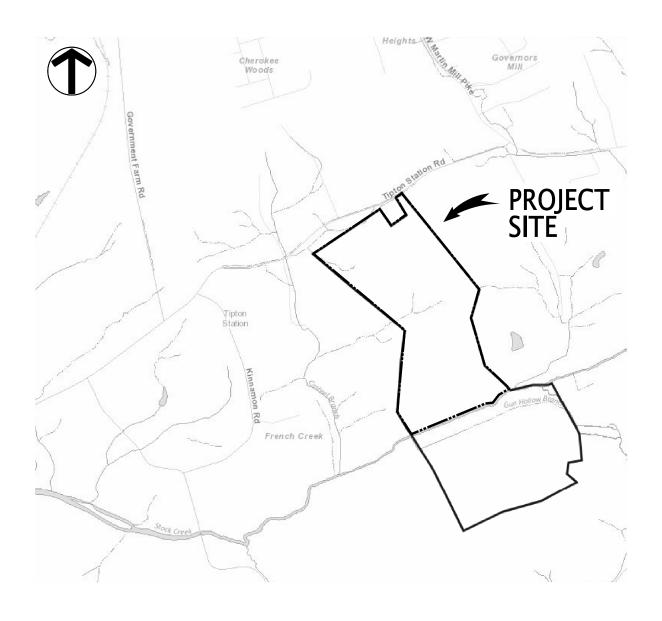


Figure 1: Location Map



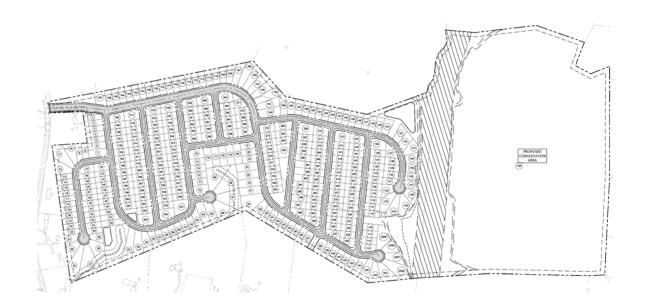


Figure 2: Site Plan

1.2 Study Area

The purpose of this study is to evaluate the impacts to the traffic conditions caused by the proposed development. Maryville Pike (SR 33) and Martin Mill Pike are considered north-south orientated roadways and Tipton Station Road is considered an east-west oriented roadway. The existing intersections and existing traffic control are summarized in Table 1.2-1 Study Area.

Table 1.2-1 Tipton Station Subdivision Study Area

Intersection	Existing Traffic Control
Maryville Pike (SR 33) at Tipton Station Road	TWSC
W Martin Mill Pike at Tipton Station Road	TWSC

1.3 Existing Site Conditions

Roadway geometry and posted speed limits were obtained by field observations. The Knoxville-Knox County Planning "2018 Major Road Plan" was used to determine road classification. This information is summarized in Table 1.3-1 Existing Site Conditions.

Table 1.3-1
Tipton Station Subdivision
Existing Site Conditions

Roadway	Speed Limit	Lanes	Road Width	Major Road Plan					
Maryville Pike (SR 33)	45 mph	2	~22 feet	Minor Arterial 88' ROW					
W Martin Mill Pike	40 mph	2	~20 feet	Minor Arterial 60' ROW					
Tipton Station Road	40 mph	2	~19.5 feet	Major Collector 60' ROW					
S Lake Blvd	25 mph	2	~26 feet	Local Street					

The intersection of Maryville Pike (SR 33) at Tipton Station Road / S Lake Blvd is a two-way stop-controlled intersection. S Lake Boulevard is the roadway connection to a residential subdivision with a boulevard entrance between Maryville Pike and S Creek Road. Tipton Station Road has a skewed intersection angle of approximately 60 degrees.

Tipton Station Road is classified as Major Collector per the Major Road Plan. The minimum intersection spacing required on a collector road is 300 feet per the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022. Goddard Road is located approximately 70 feet west of W Martin Mill Pike; therefore, the minimum separation on a collector is not met between the Goddard Road and W Martin Mill Pike.

There are no sidewalks or bike infrastructure in the vicinity of the proposed development.

An aerial photo of the intersection of Maryville Pike (SR 33) at Tipton Station Road / S Lake Boulevard and W Martin Mill Pike at Tipton Station Road are included in Attachment 1.

2 Existing Traffic Volumes

Ardurra conducted a turning movement count at the two-way stop-controlled intersection of Tipton Station Road at W Martin Mill Pike on Thursday May 16, 2024. The AM peak hour occurred between 7:15 a.m. and 8:15 a.m. with an AM PHF of 0.87 and an AM peak hour volume of 612 vph. The PM peak hour occurred between 5:00 p.m. and 6:00 p.m. with a PM PHF of 0.98 and a PM peak hour volume of 610 vph.

Ardurra conducted a turning movement count at the two-way stop-controlled intersection of Maryville Pike (SR 33) at Tipton Station Road / S Lake Boulevard on Thursday May 16, 2024. The AM peak hour occurred between 7:30 a.m. and 8:30 a.m. with an AM PHF of 0.89 and an AM peak hour volume of 763 vph. The PM peak hour occurred between 5:00 p.m. and 6:00 p.m. with a PM PHF of 0.88 and a PM peak hour volume of 1,029 vph.

The existing volumes including the AM and PM peak hour traffic volumes at the count locations are shown in Figure 3, and the count data collected is included in Attachment 2.

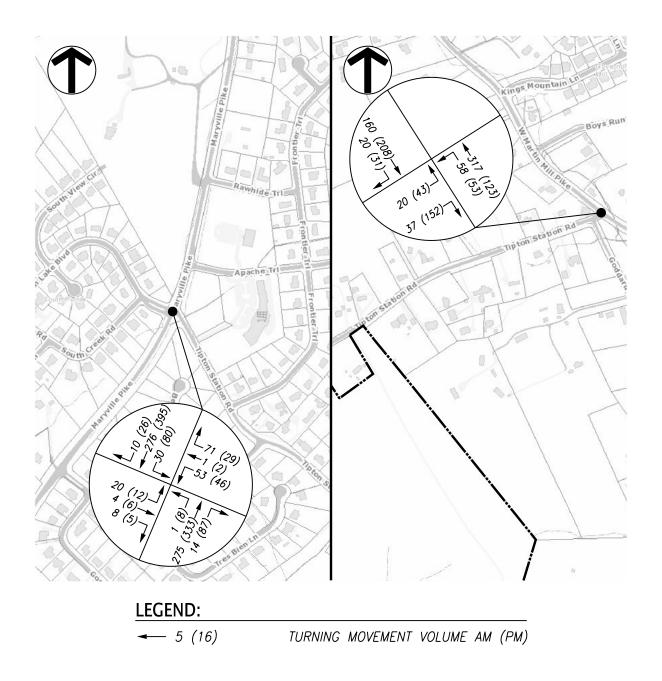


Figure 3: 2024 Existing Peak Hour Traffic

3 Background Growth

The Tennessee Department of Transportation (TDOT) maintains count stations in the vicinity of the proposed development.

TDOT count station ID 47000516 is located on Tipton Station Road east of Maryville Pike (SR 33) in Knoxville, TN. This count location was established in 2015 so the annual growth rate over the last eight years is approximately 0.30%. The 2023 ADT was 3,075 vehicles per day.

TDOT count station ID 47000117 is located on Maryville Pike (SR 33) near the Blount County Line and south of the intersection with Tipton Station Road. The annual growth rate for this station over the last ten years is approximately 0.95%. The 2023 ADT was 6,368 vehicles per day.

TDOT count station ID 47000496 is located on Martin Mill Pike south of W Governor John Sevier Highway (SR 168) and north of the intersection with Tipton Station Road. This count location was established in 2010 so the annual growth rate for this station over the last twelve years is approximately 0.52%. The 2022 ADT was 4,240 vehicles per day.

For the purpose of this study, an annual growth rate of 1.0% was assumed for traffic at the studied intersections until full occupancy is reached in 2027. Attachment 3 shows the trend line growth charts for the TDOT count stations.

Figure 4 demonstrates the projected background peak hour volumes at the studied intersections after applying the background growth rate to the existing conditions.

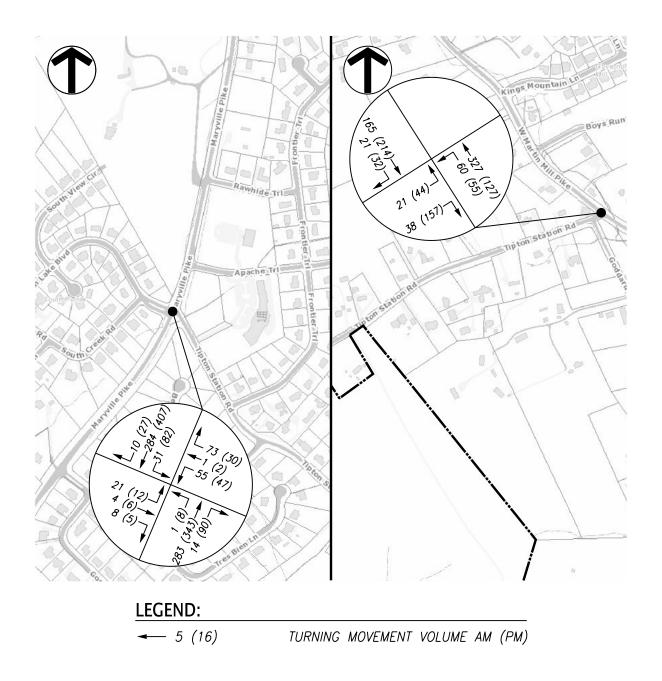


Figure 4: 2027 Background Peak Hour Traffic

4 Trip Generation and Trip Distribution

The Tipton Station Subdivision proposes 343 single-family residential lots. Single-Family Detached Housing or Land Use 210 was used to calculate site trips for the development using the fitted curve equations from the Trip Generation, 11th Edition, published by the Institute of Transportation Engineers.

The land use worksheets are included in Attachment 4. A trip generation summary is shown in Table 4-1.

Table 4-1 Tipton Station Subdivision Trip Generation Summary

Land Use	Density	Daily Trips	AM Peak Hour Enter Exit	PM Peak Hour Enter Exit		
Single Family Detached Housing (LUC	343 Lots	3,136	57 172	200 117		

The total combined new trips generated by the Tipton Station Subdivision were estimated to be 3,136 daily trips. The estimated trips are 229 trips during the AM peak hour and 317 trips during the PM peak hour.

Tipton Station Road at the proposed roadway connection has an existing trip distribution of 40% eastbound and 60% westbound during the AM peak hour and 70% eastbound and 30% westbound during the PM peak hour.

The directional distribution of the traffic generated by the Tipton Station Subdivision was determined using the existing traffic volumes in combination with the site plan layout. The entering/exiting traffic was assumed to be 60% eastbound Tipton Station Road to/from W Martin Mill Pike, 30% westbound Tipton Station Road to/from Maryville Pike (SR 33) and 10% westbound Tipton Station Road via Government Farm Road.

Figures 5 and 6 show the subdivision peak hour trip distribution and site trips. Figure 7 shows the 2027 full buildout peak hour traffic including the background growth and the peak hour site trips from both the future development area and the Tipton Station Road Subdivision.

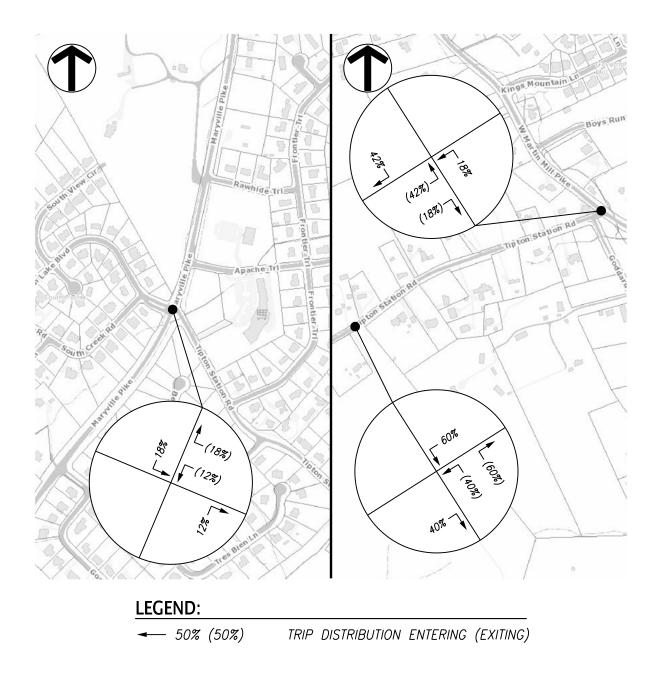


Figure 5: Subdivision Peak Hour Trip Distribution

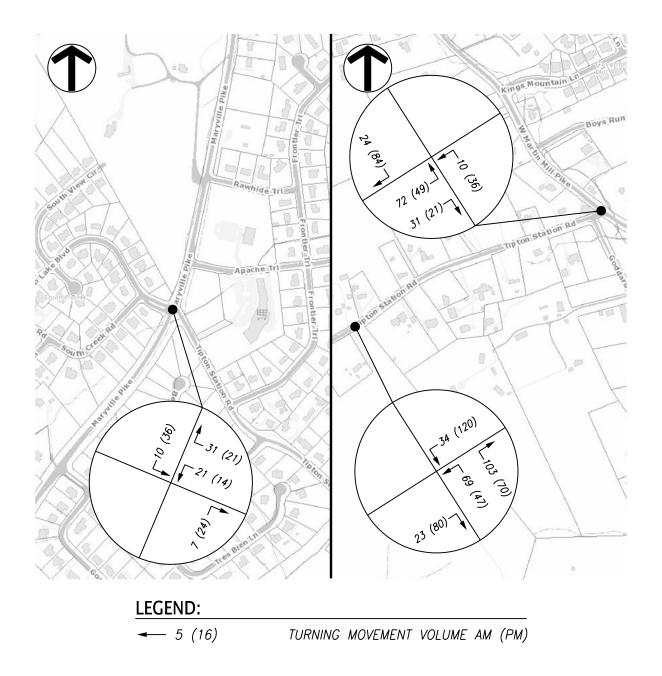


Figure 6: Subdivision Peak Hour Site Trips

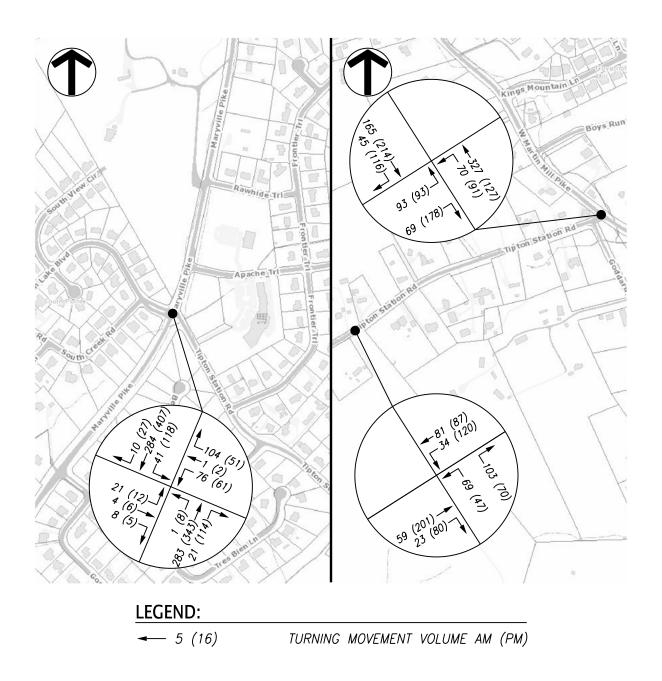


Figure 7: 2027 Full Buildout Peak Hour Traffic

5 Projected Capacity and Level of Service

Intersection capacity analyses were performed using the Synchro 11 at the two-way stop-controlled intersections in order to evaluate the AM and PM peak hours for existing, background and full buildout conditions.

Level of Service

The results from the analyses are expressed with a term "level of service" (LOS), which is based on the amount of delay experienced at the intersection. The LOS index ranges from LOS A, indicating excellent traffic conditions with minimal delay, to LOS F indicating very congested conditions with excessive delay. LOS D generally is considered the minimum acceptable condition in urban areas. Table 5-1 shows the LOS index range for signalized and unsignalized intersections as defined by the Highway Capacity Manual (HCM).

Table 5-1 Level of Service (LOS) Index

Level of Service	Signalized Intersection	Unsignalized Intersection
LOS A	≤ 10 sec	≤ 10 sec
LOS B	10 – 20 sec	10 – 15 sec
LOS C	20 – 35 sec	15 – 25 sec
LOS D	35 – 55 sec	25 – 35 sec
LOS E	55 – 80 sec	35 – 50 sec
LOS F	> 80 sec	> 50 sec

The Synchro 11 worksheets are included in Attachments 5, 6, and 7. Table 5-2 shows the results of the capacity analyses.

Table 5-2 Level of Service (LOS) Summary

			,	
Intersection	Time Period	Year 2024 Existing (Delay/LOS)	Year 2027 Background (Delay/LOS)	Year 2027 Full Buildout (Delay/LOS)
W Martin Mill Pike @	AM Peak			
Tipton Station Road	EB Approach	11.8 / B	12.0 / B	17.9 / C
•	NW Approach PM Peak	7.8 / A	7.8 / A	7.9 / A
	EB Approach	11.8 / B	12.0 / B	16.0 / C
	NW Approach	7.8 / A	7.9 / A	8.2 / A
Maryville Pike (SR 33) @	AM Peak			
Tipton Station Road	NB Approach	7.9 / A	7.9 / A	7.9 / A
•	EB Approach	16.6 / C	17.2 / C	18.8 / C
	WB Approach	15.6 / C	16.1 / C	19.2 / C
	SB Approach	8.0 / A	8.0 / A	8.1 / A
	PM Peak			
	NB Approach	8.4 / A	8.4 / A	8.4 / A
	EB Approach	26.3 / D	27.8 / D	35.0 / E
	WB Approach	30.1 / D	32.4 / D	53.3 / F
	SB Approach	8.6 / A	8.7 / A	8.9 / A
Tipton Station Road @	AM Peak			
Driveway	NB Approach			10.3 / B
,	WB Approach			7.5 / A
	PM Peak			12.2 / D
	NB Approach			13.2 / B
	WB Approach			8.2 / A

Notes:

^{1.} Whole intersection weighted average control delay expressed in second per vehicle for signalized intersections and all-way stop controlled intersections.

6 Turn Lane Warrant Analysis

Knox County Turn Lane Warrants

The intersection of W Martin Mill Pike at Tipton Station Road and Tipton Station Road at the proposed subdivision roadway connection were evaluated to determine if a right turn lane or a left turn lane are warranted. The Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy," was used to analyze the information.

At the intersection of Tipton Station Road at the proposed roadway connection to the subdivision neither an eastbound right turn lane nor a westbound left turn lane are warranted during the AM or PM peak hours after the completion of the Tipton Station Subdivision.

At the intersection of Tipton Station Road at W Martin Mill Pike a southbound right turn lane is not warranted during either the AM or PM peak hours and a northbound left turn lane is warranted during the AM peak hour after the completion of the Tipton Station Subdivision.

TDOT Turn Lane Warrants

The intersection of Maryville Pike (SR 33) at Tipton Station Road was evaluated to determine if a northbound right turn lane and southbound left turn lane on Maryville Pike (SR 33) are warranted. The TDOT Highway System Access Manual (HSAM) Volume 3: Geometric Design Criteria dated April 2021 was used to analyze the information. TDOT recommends that a turn lane be installed at an intersection when the turn lane warrants are met during both the AM and PM peak hours.

In order to evaluate a right turn lane warrant, the Major-Road Volume, (one direction), veh/h and Right-Turn Volume, veh/h were reference from Figure 7: 2027 Full Buildout Peak Hour Traffic. Per Figure 3-18: Right-Turn Warrant along Two-Lane Roadway (Unsignalized Intersection with Two-Way Stop-Control) the full buildout conditions at the intersection of Maryville Pike (SR 33) at Tipton Station Road will only warrant a right turn lane during the PM peak hour; therefore, a northbound right turn lane on Maryville Pike (SR 33) is not recommended.

In order to evaluate a left turn lane warrant, the Major Highway Volume (veh/h/ln) and the Left-Turn Volume (veh/h) were referenced from Figure 7: 2027 Full Buildout Peak Hour Traffic. Per Figure 3-15: Left-Turn Lane Warrant for Urban and Suburban Arterials (Unsignalized) the full buildout conditions at the intersection of Maryville Pike (SR 33) at Tipton Station Road will warrant a southbound left turn lane during both the AM and PM peak hours.

A southbound left turn lane is warranted during the existing, background and full buildout conditions. Per the TDOT HSAM "The volume-based warrants indicate situations where a left-turn would help mitigate traffic conflicts, not necessarily situations where a left-turn lane is required or must be constructed."

Per the TDOT HSAM Table 3-11: Lane Change and Deceleration Distance the recommended lane change and deceleration distance for a roadway with a speed limit of 45 mph is 340 feet and the minimum queue storage length for a turn lane is 50 feet. Therefore, the total recommended turn lane length is 390 feet.

The turn lane worksheets and TDOT Highway System Access Manual Figures are included in Attachment 8.

7 Conclusions and Recommendations

7.1 W Martin Mill Pike at Tipton Station Road

The existing, background and full buildout conditions at the two-way stop-controlled intersection of W Martin Mill Pike at Tipton Station Road were analyzed using the Synchro 11 software. The existing intersection is a three-legged stop-controlled intersection.

The existing and background traffic conditions for the two-way stop-controlled intersection of W Martin Mill Pike at Tipton Station Road operates as follows: the northbound approach (Tipton Station Road) operate at a LOS A during both the AM and PM peak hours and the eastbound approach (Tipton Station Road) operates at a LOS B during both the AM and PM peak hours.

After the completion of the Tipton Station Road Subdivision the traffic conditions for the two-way stop-controlled intersection of W Martin Mill Pike at Tipton Station Road operates as follows: the northbound approach (Tipton Station Road) operate at a LOS A during both the AM and PM peak hours and the eastbound approach (Tipton Station Road) operates at a LOS C during both the AM and PM peak hours.

A northbound left turn lane is warranted during the AM peak hour and a southbound right turn lane is not warranted at the intersection of W Martin Mill Pike at Tipton Station Road per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

The northbound left turn lane has a recommended minimum storage length of 50 feet per the AASHTO Greenbook "A Policy on Geometric Design of Highways and Streets."

Per the recommendation of Knoxville-Knox County Planning an alternative intersection analysis was evaluated. The alternative design includes the installation of a roundabout at the existing stop-controlled intersection of W Martin Mill Pike at Tipton Station Road with Goddard Road as a fourth leg to proposed roundabout.

Goddard Road does not currently meet the minimum required separation on a collector; hence fore, the installation of a roundabout at the intersection would mitigate the intersection spacing between Goddard Road and W Martin Mill Pike.

Attachment 10 includes the Synchro 11 capacity analysis worksheets for the roundabout intersection. The results of the capacity analysis are that the intersection as a roundabout would operate at an overall LOS A during both the AM and PM peak hours after the completion of the Tipton Station Subdivision. The installation of a roundabout at this intersection would eliminate the need for a northbound left turn lane.

Ardurra recommends that any future intersection improvements be reviewed, coordinated and approved by Knox County Engineering and Public Works.

7.2 Maryville Pike (SR 33) at Tipton Station Road

The existing, background and full buildout conditions at the two-way stop-controlled intersection of Maryville Pike (SR 33) at Tipton Station Road were analyzed using the Synchro 11 software. The existing intersection is a four-legged stop-controlled intersection.

The existing and background traffic conditions for the two-way stop-controlled intersection of Maryville Pike (SR 33) at Tipton Station Road operates as follows: the northbound and southbound approaches (Maryville Pike) operate at a LOS A during both the AM and PM peak hours and the eastbound approach (S Lake Boulevard) operates at a LOS C during the AM peak hour and LOS D during the PM peak hour and the westbound approach (Tipton Station Road) operates at a LOS C during the AM peak hour and a LOS D during the PM peak hour.

After the completion of the Tipton Station Road Subdivision the traffic conditions for the two-way stop-controlled intersection of Maryville Pike (SR 33) at Tipton Station Road operates as follows: the northbound and southbound approaches (Maryville Pike) operate at a LOS A during both the AM and PM peak hours and the eastbound approach (S Lake Boulevard) operates at a LOS C during the AM peak hour and LOS E during the PM peak hour and the westbound approach (Tipton Station Road) operates at a LOS C during the AM peak hour.

The westbound approach (Tipton Station Road) will operate at a LOS F during the PM peak hour after the completion of the Tipton Station Road Subdivision; however, the overall intersection delay will continue to operate at an acceptable LOS.

The 95% queue length is defined as the queue length that has only a 5-percent probability of being exceeded during the analysis time period. The 95% queue length is typically used to determine the length of turning lanes in order to minimize the risk of blockage.

The westbound approach (Tipton Station Road) has an existing storage length of 200 feet before the queue from the intersection would block the driveway to the retail strip center. The unsignalized intersection capacity analysis shows the full buildout 95% queue length for the westbound approach (Tipton Station Road) of approximately 2.3 vehicles (58 feet) during the AM peak hour and 4 vehicles (100 feet) during the PM peak hour; therefore, the queue is not expected to block the nearest driveway intersection.

A southbound left turn lane is warranted during the existing, background and full buildout conditions. The warrant for a southbound left turn lane is an existing condition and not a result of the Tipton Station Subdivision.

Per the TDOT Highway System Access Manual (HSAM) Volume 3: Geometric Design Criteria dated April 2021. "The volume-based warrants indicate situations where a left-turn would help mitigate traffic conflicts, not necessarily situations where a left-turn lane is required or must be constructed."

Any future improvements to the intersection or the various traffic management infrastructure, would need to be reviewed, coordinated, and approved by both Tennessee Department of Transportation and Knox County Engineering and Public Works.

7.3 Tipton Station Road at Roadway Connection

The proposed full buildout conditions at the two-way stop-controlled intersection of Tipton Station Road at the Subdivision Roadway were analyzed using the Synchro 11 Software.

After the completion of the full buildout of the Tipton Station Subdivision the intersection of Tipton Station Road at Subdivision Roadway will operate as follows. The northbound approach (Subdivision Roadway) will operate at a LOS B during both the AM and PM peak hours and the westbound approach (Tipton Station Road) will operate at a LOS A during both the AM and PM peak hours.

The standard practice for a residential development with 150 or more lots/units is to require at least two access points to provide alternative access opportunities in the event that one access is blocked by a fallen tree, crash, or other. For the Tipton Station Subdivision the roadway connection proposes a boulevard entrance with a single lane for entering and exiting traffic. The boulevard entrance extends from Tipton Station Road to the first internal intersection in order to provide an alternate access.

Neither an eastbound right turn lane nor a westbound left turn lane is warranted at the intersection of Tipton Station Road at Subdivision Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

Tipton Station Road is classified as Major Collector per the Major Road Plan. The minimum intersection spacing required on a collector road is 300 feet per the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022. The Subdivision Roadway is located approximately 890 feet east of Galyon Lane and 1,635 feet west of Goddard Road; therefore, the minimum separation on a collector is met and no change is necessary.

The minimum required sight distance for a road with a posted speed limit of 40 mph is 400 feet in each direction in accordance with the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022.

At 15 feet from the edge of pavement the intersection sight distance is approximately 800 feet looking left (westbound) and 625 feet looking right (eastbound). Attachment 9 includes pictures of the intersection sight distance at the intersection of Tipton Station Road at Subdivision Roadway.

Ardurra recommends that the intersection sight distance be certified by a land surveyor prior to construction in order to verify that Tipton Station Road has adequate intersection sight distance at the proposed subdivision roadway connection to comply with Knox County Engineering and Public Works guidelines.

Ardurra recommends that the signs and pavement markings be installed in accordance with the standards provided in the *Manual on Uniform Traffic Control Devices* (MUTCD).

Any future improvements to the intersection or the various traffic management infrastructure, would need to be reviewed, coordinated, and approved by Knox County Engineering and Public Works.

Attachment 1 Aerial Photos



W Martin Mill Pike at Tipton Station Road - TWSC



Maryville Pike (SR 33) at Tipton Station Road – TWSC

Attachment 2 Traffic Counts

Intersection: Tipton Station Road at W Martin Mill Pike Date Conducted: Thursday May 16, 2024

Г	W	Martin	Mill Pi	ke				I	Tip	ton Sta	tion Roa	ad	Tipt	on Stat	ion Ro	ad	
	Southbound					Westb				Northk	ound			Eastbo	ound		
Start	Left	Thru	Right	Total	Left	Thru	Right	Total	Left	Thru		Total	Left		Right		Int. Total
7:00 AM 7:15 AM	0	26 35	6 4	32 39	0	0	0	0	8 15	48 82	0	56 97	6 3	0	4 13	10 16	98 152
7:30 AM	0	39	6	45	0	0	0	0	23	93	0	116	6	0	8	14	175
7:45 AM	0	29	5	34	0	0	0	0	13	93	0	106	5	0	10	15	155
Total	0	129	21	150	0	0	0	0	59	316	0	375	20	0	35	55	580
0.00 444 1	0		_	دما		0	0	ام	-	10	0	- c l		0	,	10	120
8:00 AM 8:15 AM	0	57 37	5 2	62 39	0	0	0	0	7 14	49 53	0	56 67	6 5	0	6 12	12 17	130 123
8:30 AM	0	17	5	22	0	0	0	0	6	40	0	46	7	0	4	11	79
8:45 AM	0	19	5	24	0	0	0	0	3	23	0	26	6	0	3	9	59
Total	0	130	17	147	0	0	0	0	30	165	0	195	24	0	25	49	391
0.00 444 1	0	1.1	2	1 -1		0	0	ام	4	2.1	0	2.5	2	0	2	-1	
9:00 AM 9:15 AM	0	14 16	3 2	1 <i>7</i> 18	0	0	0	0	4 1	31 19	0	35 20	2	0	3 1	5 4	57 42
9:30 AM	0	17	4	21	0	0	0	ő	4	27	0	31	4	0	5	9	61
9:45 AM	0	18	4	22	0	0	0	0	7	25	0	32	8	0	5	13	67
Total	0	65	13	78	0	0	0	0	16	102	0	118	1 <i>7</i>	0	14	31	227
10.00 AM I	0	1.1	0	22	_	0	0	ام	2	1.5	0	10	2	0	2	41	4.4
10:00 AM 10:15 AM	0	14 16	8 6	22 22	0	0	0	0	3 7	15 32	0	18 39	2	0	2 12	4 20	44 81
10:30 AM	0	14	3	17	0	0	0	0	4	27	0	31	5	0	5	10	58
10:45 AM	0	10	5	15	0	0	0	0	3	28	0	31	2	0	3	5	51
Total	0	54	22	76	0	0	0	0	17	102	0	119	17	0	22	39	234
11.00 AA I	0	20	-	ع د ا	0	0	0	ام	-	16	0	241	7	0	7	4.4	60
11:00 AM 11:15 AM	0	20 16	5 5	25 21	0	0	0	0	5 3	16 21	0	21 24	7 6	0	7 3	14 9	60 54
11:30 AM	0	15	6	21	0	0	0	ő	6	20	0	26	7	0	8	15	62
11:45 AM	0	15	2	17	0	0	0	0	4	21	0	25	4	0	8	12	54
Total	0	66	18	84	0	0	0	0	18	78	0	96	24	0	26	50	230
12.00 BM I	0	1.0	0	2.4	_	0	0	ام	-	20	0	221	4	0	,	10	67
12:00 PM 12:15 PM	0	16 20	8 7	24 27	0	0	0	0	5 3	28 1 <i>7</i>	0	33 20	4 10	0	6 6	10 16	67 63
12:30 PM	0	27	6	33	0	0	0	0	5	26	0	31	2	0	10	12	76
12:45 PM	0	17	3	20	0	0	0	0	3	27	0	30	5	0	6	11	61
Total	0	80	24	104	0	0	0	0	16	98	0	114	21	0	28	49	267
1:00 PM	0	17	4	21	0	0	0	ol	3	16	0	19	3	0	7	10	50
1:15 PM	0	27	2	29	0	0	0	0	6	18	0	24	1	0	5	6	59
1:30 PM	Ö	22	5	27	0	0	0	ő	9	23	0	32	6	0	11	17	76
1:45 PM	0	27	4	31	0	0	0	0	4	17	0	21	8	0	7	15	67
Total	0	93	15	108	0	0	0	0	22	74	0	96	18	0	30	48	252
2:00 PM	0	18	6	24	0	0	0	ol	2	29	0	31	3	0	10	13	68
2:15 PM	0	23	6	29	0	0	0	o	5	24	0	29	5	0	9	14	72
2:30 PM	0	21	5	26	0	0	0	0	2	15	0	1 <i>7</i>	7	0	7	14	57
2:45 PM	0	38	6	44	0	0	0	0	15	37	0	52	6	0	13	19	115
Total	0	100	23	123	0	0	0	0]	24	105	0	129	21	0	39	60	312
3:00 PM	0	34	4	38	0	0	0	ol	9	43	0	52	14	0	13	27	117
3:15 PM	0	38	9	47	0	0	0	0	8	17	0	25	5	0	15	20	92
3:30 PM	0	33	1	34	0	0	0	0	33	77	0	110	11	0	18	29	173
3:45 PM	0	37 142	11 25	48	0	0	0	0	<u>7</u> 57	22 159	0	29	36	0	11 57	17	94
Total	U	142	23	167	U	U	U	υĮ	37	159	U	216	36	U	37	93	476
4:00 PM	0	35	9	44	0	0	0	0	10	30	0	40	13	0	22	35	119
4:15 PM	0	44	10	54	0	0	0	0	10	30	0	40	13	0	22	35	129
4:30 PM	0	39	10	49	0	0	0	0	8	25	0	33	8	0	32	40	122
4:45 PM Total	0	52 170	11 40	63 210	0	0	0	0	10 38	33 118	0	43 156	43	0	28 104	37 147	143 513
TOTAL	U	170	+∪	10	J	U	U	۷Į	30	110	U	130	73	U	104	1-1/	515
5:00 PM	0	54	8	62	0	0	0	0	11	31	0	42	9	0	40	49	153
5:15 PM	0	50	8	58	0	0	0	0	15	32	0	47	9	0	40	49	154
5:30 PM	0	53	5	58	0	0	0	0	14	36	0	50	10	0	30	40	148
5:45 PM Total	0	208	10 31	61 239	0	0	0	0	13 53	123	0	37 176	15 43	0	42 152	57 195	155 610
Total	U	200	51	233		3	J	٧I	33	.23	U	170	73	Ü	132	155	0.0
Grand Total	0	1237	249	1486		0	0	0	350	1440	0	1790	284	0	532	816	4092
Approach %	0.0	83.2	16.8	26.0	#####				19.6	80.4	0.0	40 -	34.8	0.0	65.2	10.0	
Total %	0.0	30.2	6.1	36.3	0.0	0.0	0.0	0.0	8.6	35.2	0.0	43.7	6.9	0.0	13.0	19.9	

Intersection: Tipton Station Road at W Martin Mill Pike

Date Conducted: Thursday May 16, 2024

AM Peak Hour	7:15 AM - 8:15 AM	612
PM Peak Hour	5:00 PM - 6:00 PM	610

	W	Martin	Mill Pi	ke					Tip	ton Sta	tion Ro	ad	Tip	ton Stat	ion Ro	ad	
		South	oound			Westb	ound			North	bound			Eastbo	ound		
Start	Left	Thru	Right	Total	Left	Thru	Right	Total	Left	Thru	Right	Total	Left	Thru	Right	Total	Int. Total
Peak Hour Analysis from 7:00 AM to 9:00 AM																	
AM Peak Hour begins at 7:15 AM																	
7:15 AM	0	35	4	39	0	0	0	0	15	82	0	97	3	0	13	16	152
7:30 AM	0	39	6	45	0	0	0	0	23	93	0	116	6	0	8	14	175
7:45 AM	0	29	5	34	0	0	0	0	13	93	0	106	5	0	10	15	155
8:00 AM	0	57	5	62	0	0	0	0	7	49	0	56	6	0	6	12	130
Total Volume	0	160	20	180	0	0	0	0	58	317	0	375	20	0	37	57	612
Future (1.0% over 3 yrs)	0	165	21		0	0	0		60	327	0		21	0	38		631
PHF	-	0.70	0.83		-	-	-		0.63	0.85	-		0.83	-	0.71		0.87
Peak Hour Analysis from	3:00 PM	1 to 6:00) PM														
PM Peak Hour begins at	5:00 PM																
5:00 PM	0	54	8	62	0	0	0	0	11	31	0	42	9	0	40	49	153
5:15 PM	0	50	8	58	0	0	0	0	15	32	0	47	9	0	40	49	154
5:30 PM	0	53	5	58	0	0	0	0	14	36	0	50	10	0	30	40	148
5:45 PM	0	51	10	61	0	0	0	0	13	24	0	37	15	0	42	57	155
Total Volume	0	208	31	239	0	0	0	0	53	123	0	176	43	0	152	195	610
Future (1.0% over 3 yrs)	0	214	32		0	0	0		55	127	0		44	0	157		628
PHF	-	0.96	0.78		-	-	-		0.88	0.85	-		0.72	-	0.95		0.98

Intersection: Marvyille Pike at Tipton Station Rd/S Lake Blvd Date Conducted: Thursday May 16, 2024

[٨	<i>M</i> aryvil	le Pike		Tip	ton Stat	tion Roa	ad	1	Maryvil	le Pike		SI	ake Bo	oulevar	·d	
		Southk				Westb				Northk	ound			Eastbo			
Start	Left	Thru	Right	Total	Left		Right	Total	Left	Thru		Total	Left		Right		Int. Total
7:00 AM 7:15 AM	2 7	57 52	0	59 59	16 11	1 0	19 10	36 21	0 1	50 78	2 5	52 84	5 10	2	4 1	11 11	158 1 <i>7</i> 5
7:30 AM	3	70	2	75	18	0	29	47	0	80	5	85	7	0	1	8	215
7:45 AM	8	77	3	88	20	0	10	30	1	66	4	71	5	0	2	7	196
Total	20	256	5	281	65	1	68	134	2	274	16	292	27	2	8	37	744
8:00 AM	9	65	2	77	10	0	13	22	0	E.6	3	59	7	3	4	14	173
8:15 AM	10	64	3 2	76	5	1	19	23 25	0	56 73	2	75	7 1	3 1	1	3	173
8:30 AM	6	53	0	59	8	1	12	21	0	32	0	32	3	1	0	4	116
8:45 AM	4	53	5	62	2	0	9	11	0	41	1	42	3	1	0	4	119
Total	29	235	10	274	25	2	53	80	0	202	6	208	14	6	5	25	587
9:00 AM	4	37	1	42	_	0	13	18	0	37	3	40	8	1	0	9	109
9:15 AM	5	44	5	54	5 0	0	6	6	1	34	3 1	36	2	0	1	3	99
9:30 AM	4	44	4	52	5	2	5	12	1	33	3	37	6	0	2	8	109
9:45 AM	6	35	2	43	5	1	6	12	0	31	3	34	4	1	2	7	96
Total	19	160	12	191	15	3	30	48	2	135	10	147	20	2	5	27	413
10:00 AM	7	47	5	59	9	0	5	14	2	38	2	42	1	0	0	1	116
10:15 AM	11	48	5	64	8	0	8	16	1	38	4	43	2	1	1	4	127
10:30 AM	8	44	5	57	5	0	8	13	1	45	1	47	4	1	1	6	123
10:45 AM	7	40	4	51	2	0	8	10	0	50	9	59	1	0	1	2	122
Total	33	179	19	231	24	0	29	53	4	171	16	191	8	2	3	13	488
11:00 AM	9	34	2	45	3	0	3	6	0	64	6	70	4	1	0	5	126
11:15 AM	8	54	0	62	4	1	7	12	1	49	4	54	2	0	0	2	130
11:30 AM	5	43	5	53	3	0	8	11	0	40	6	46	2	0	0	2	112
11:45 AM	9	57	3	69	1	0	5	6	0	51	5	56	1	0	0	1	132
Total	31	188	10	229	11	1	23	35	1	204	21	226	9	1	0	10	500
12:00 PM	10	68	3	81	5	1	8	14	1	64	8	73	7	1	2	10	178
12:15 PM	9	51	4	64	5	1	8	14	1	52	5	58	2	1	2	5	141
12:30 PM	6	47	2	55	4	1	6	11	0	47	4	51	3	0	1	4	121
12:45 PM	8	54	3	65	4	0	7	11	0	41	6	47	1	0	2	3	126
Total	33	220	12	265	18	3	29	50	2	204	23	229	13	2	7	22	566
1:00 PM	6	54	3	63	6	0	2	8	0	47	5	52	7	0	3	10	133
1:15 PM	10	64	1	75	6	0	4	10	0	50	2	52	2	1	1	4	141
1:30 PM	10	58	0	68	3	0	12	15	2	56	2	60	2	1	1	4	147
1:45 PM	11	51	2	64	7	0	8	15	1	39	5	45	1	0	1	2	126
Total	37	227	6	270	22	0	26	48	3	192	14	209	12	2	6	20	547
2:00 PM	18	48	4	70	5	0	4	9	2	66	6	74	2	0	0	2	155
2:15 PM	10	55	2	67	4	0	8	12	2	59	8	69	2	1	0	3	151
2:30 PM	12	59	2	73	6	0	7	13	0	78	9	87	3	0	1	4	1 <i>77</i>
2:45 PM	14 54	63	11	80 290	21	0	8	14 48	<u>1</u> 5	267	13 36	78 308	1 8	0	0	10	173 656
Total	34	225	- 11	290	21	U	27	40	3	207	30	306	0	'	'	10	030
3:00 PM	10	54	5	69	7	0	5	12	2	65	9	76	5	0	0	5	162
3:15 PM	8	55	1	64	4	0	8	12	1	62	12	75	1	1	0	2	153
3:30 PM	10	72	5	87	4	4	13	21	0	82	13	95	2	1	0	3	206
3:45 PM Total	36	265	7 18	99 319	9 24	1 5	13 39	23 68	<u>2</u> 5	72 281	14 48	88 334	3 11	<u>2</u> 4	1 1	6 16	216 737
rotari	30	203		3.31		,	33	001	,	201	10	331	• • •			101	757
4:00 PM	17	60	5	82	10	2	5	17	0	82	16	98	3	2	1	6	203
4:15 PM	19	69	5	93	11	0	6	17	1	63	14	78	7	0	1	8	196
4:30 PM 4:45 PM	14 24	84 86	3 4	101 114	6 7	1 0	3 10	10 1 <i>7</i>	3 1	78 65	12 24	93 90	7 0	0	5 0	12 0	216 221
Total	74	299	17	390	34	3	24	61	5	288	66	359	17	2	7	26	836
·								·									
5:00 PM	18	94	5	117	10	1	5	16	3	118	29	150	4	3	2	9	292
5:15 PM	25	121	5	151	13	0	9	22	3	89 70	14	106	0	2	2	4	283
5:30 PM 5:45 PM	16 21	86 94	11 5	113 120	12 11	1 0	8 7	21 18	1 1	70 56	16 28	8 <i>7</i> 85	4 4	0 1	1 0	5 5	226 228
Total	80	395	26	501	46	2	29	77	8	333	87	428	12	6	5	23	1029
Grand Total	446	2649	146	3241	305	20	377	702	37	2551	343	2931	151	30	48	229	7103
Approach % Total %	13.8 6.3	81.7 37.3	4.5 2.1	45.6	43.4 4.3	2.8 0.3	53. <i>7</i> 5.3	9.9	1.3 0.5	87.0 35.9	11.7 4.8	41.3	65.9 2.1	13.1 0.4	21.0 0.7	3.2	
10141 /0	5.5	37.3	۷. ۱	15.01	7.5	5.5	5.5	5.5	5.5	55.5	7.0		4.1	5.4	5.7	5.4	

Intersection: Marvyille Pike at Tipton Station Rd/S Lake Blvd

Date Conducted: Thursday May 16, 2024

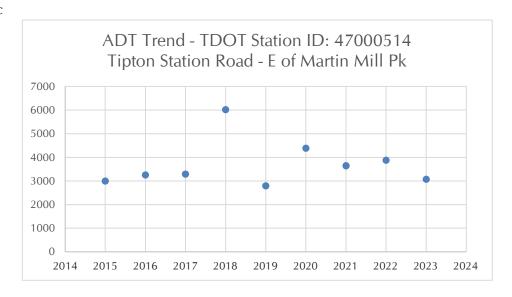
AM Peak Hour	7:30 AM - 8:30 AM	763
PM Peak Hour	7:30 AM - 8:30 AM 5:00 PM - 6:00 PM	1029

	Maryville Pike				Tipton Station Road				Maryville Pike				S Lake Boulevard				
	Southbound			Westbound				Northbound				Eastbound					
Start	Left	Thru	Right	Total	Left	Thru	Right	Total	Left	Thru	Right	Total	Left	Thru	Right	Total	Int. Total
Peak Hour Analysis from 7:00 AM to 9:00 AM																	
AM Peak Hour begins at	7:30 AN	1															
7:30 AM	3	70	2	75	18	0	29	47	0	80	5	85	7	0	1	8	215
7:45 AM	8	77	3	88	20	0	10	30	1	66	4	71	5	0	2	7	196
8:00 AM	9	65	3	77	10	0	13	23	0	56	3	59	7	3	4	14	173
8:15 AM	10	64	2	76	5	1	19	25	0	73	2	75	1	1	1	3	179
Total Volume	30	276	10	316	53	1	71	125	1	275	14	290	20	4	8	32	763
Future (1.0% over 3 yrs)	31	284	10		55	1	73		1	283	14		21	4	8		786
PHF	0.75	0.90	0.83		0.66	0.25	0.61		0.25	0.86	0.70		0.71	0.33	0.50		0.89
Peak Hour Analysis from 3:00 PM to 6:00 PM																	
PM Peak Hour begins at .	5:00 PM																
5:00 PM	18	94	5	117	10	1	5	16	3	118	29	150	4	3	2	9	292
5:15 PM	25	121	5	151	13	0	9	22	3	89	14	106	0	2	2	4	283
5:30 PM	16	86	11	113	12	1	8	21	1	70	16	87	4	0	1	5	226
5:45 PM	21	94	5	120	11	0	7	18	1	56	28	85	4	1	0	5	228
Total Volume	80	395	26	501	46	2	29	77	8	333	87	428	12	6	5	23	1029
Future (1.0% over 3 yrs)	82	407	27		47	2	30		8	343	90		12	6	5		1060
PHF	0.80	0.82	0.59		0.88	0.50	0.81		0.67	0.71	0.75		0.75	0.50	0.63		0.88

Attachment 3 ADT Trends

Adjusted Average Daily Traffic

Year	Daily Traff
2015	3000
2016	3258
2017	3291
2018	6017
2019	2798
2020	4389
2021	3647
2022	3881
2023	3075



Most Recent Trend Line Growth

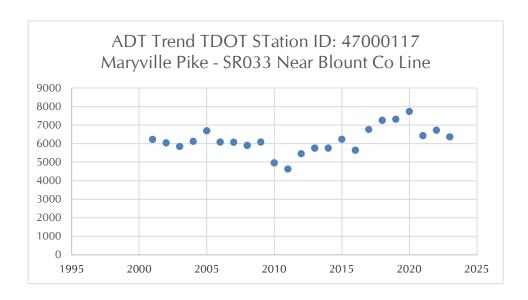
Year ADT 2015 3000 2023 3075

Annual Percent Growth

0.30%

Adjusted Average Daily Traffic

Year	Daily Traffic
2001	6227
2002	6040
2003	5850
2004	6120
2005	6689
2006	6081
2007	6074
2008	5906
2009	6083
2010	4964
2011	4626
2012	5459
2013	5760
2014	5754
2015	6238
2016	5645
2017	6763
2018	7262
2019	7314
2020	7736
2021	6431
2022	6723
2023	6368



Most Recent Trend Line Growth

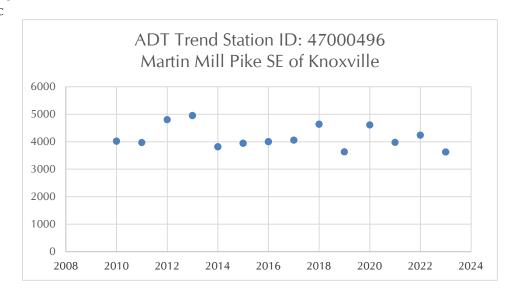
Year ADT 2013 5760 2023 6368

Annual Percent Growth

0.95%

Adjusted Average Daily Traffic

Year	Daily Traff
2010	4018
2011	3970
2012	4806
2013	4950
2014	3816
2015	3942
2016	4003
2017	4059
2018	4637
2019	3631
2020	4614
2021	3976
2022	4240
2023	3625



Most Recent Trend Line Growth

Year	ADT
2010	4018
2022	4240

Annual Percent Growth

0.52%

Attachment 4 Trip Generation

Project: Tipton Station Subdivision

Date Conducted: 7/9/2024

Single-Family Detached Housing (LUC 210) 343 Lots

Average Daily Traffic

$$Ln(T) = 0.92 Ln(X) + 2.68$$

$$Ln(T) = 0.92 Ln(343) + 2.68$$

$$T = 3136$$

Peak Hour of Adjacent Street Traffic One Hour Between 7 and 9 a.m.

$$Ln(T) = 0.91 Ln(X) + 0.12$$

 $Ln(T) = 0.91 Ln(343) + 0.12$
 $T = 229$

Peak Hour of Adjacent Street Traffic One Hour Between 4 and 6 p.m.

$$Ln(T) = 0.94 Ln(X) + 0.27$$

 $Ln(T) = 0.94 Ln(343) + 0.27$
 $T = 317$

		Per	cent	Nun	nber
Time Period	Total Trips	Enter	Exit	Enter	Exit
Weekday (24 hours)	3136	50%	50%	1568	1568
AM Peak Hour	229	25%	75%	57	172
PM Peak Hour	317	63%	37%	200	117

Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units On a: Weekday

Setting/Location: General Urban/Suburban

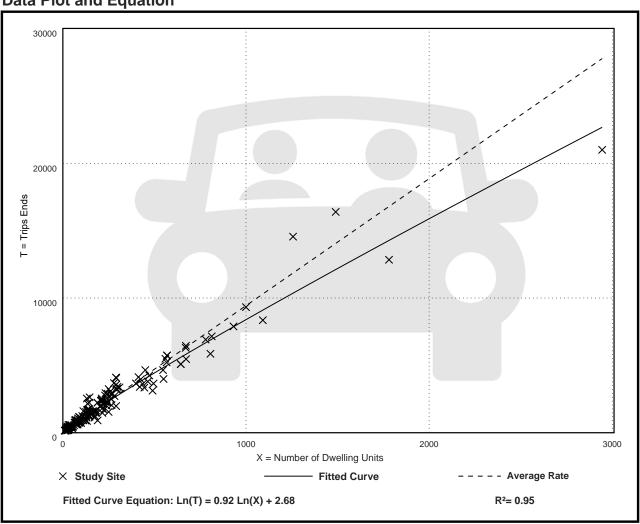
Number of Studies: 174 Avg. Num. of Dwelling Units: 246

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
9.43	4.45 - 22.61	2.13

Data Plot and Equation





Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

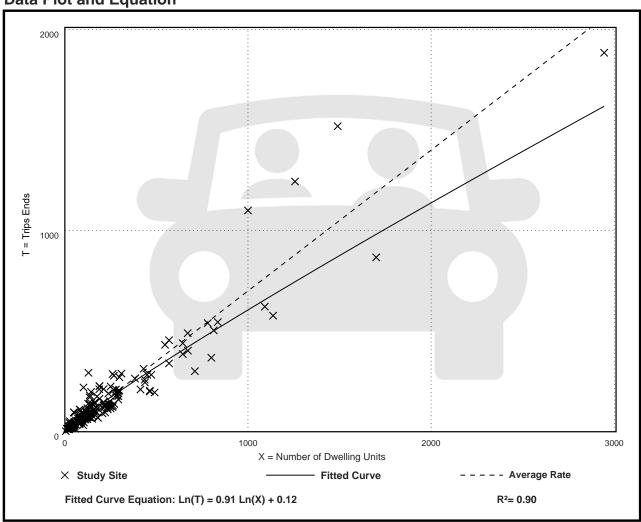
Number of Studies: 192 Avg. Num. of Dwelling Units: 226

Directional Distribution: 26% entering, 74% exiting

Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.70	0.27 - 2.27	0.24

Data Plot and Equation





Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

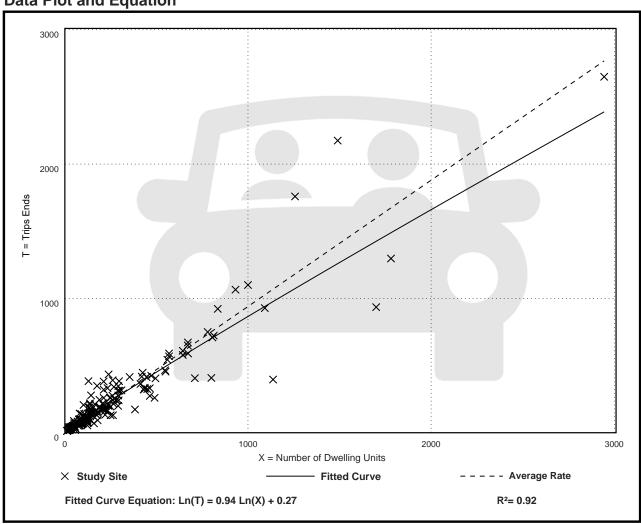
Number of Studies: 208 Avg. Num. of Dwelling Units: 248

Directional Distribution: 63% entering, 37% exiting

Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.94	0.35 - 2.98	0.31

Data Plot and Equation





Attachment 5 Intersection Worksheets – Existing AM/PM Peaks

Intersection						
Int Delay, s/veh	1.8					
Movement	EBL	EBR	SET	SER	NWL	NWT
Lane Configurations	N. W.		1			4
Traffic Vol, veh/h	20	37	160	20	58	317
Future Vol, veh/h	20	37	160	20	58	317
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e, # 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	87	87	87	87	87	87
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	23	43	184	23	67	364
mining i low	20	.0	101	20	V.	001
Major/Minor	Minor1		Major1	I	Major2	
Conflicting Flow All	694	196	0	0	207	0
Stage 1	196	-	-	-	-	-
Stage 2	498	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	_	-	2.218	-
Pot Cap-1 Maneuver	409	845	_	_	1364	-
Stage 1	837	-	_	_	-	_
Stage 2	611	_	_	_	_	_
Platoon blocked, %	011		_	_		
Mov Cap-1 Maneuver	384	845	_		1364	
Mov Cap-1 Maneuver	384			_		
•		-	-	-	-	-
Stage 1	837	-	-	-	-	-
Stage 2	573	-	-	-	-	-
Approach	EB		SE		NW	
HCM Control Delay, s	11.8		0		1.2	
HCM LOS	В					
Minor Lane/Major Mvr	nt	NWL	NWT I	EBLn1	SET	SER
Capacity (veh/h)		1364	-	595	-	-
HCM Lane V/C Ratio		0.049	-	0.11	-	-
HCM Control Delay (s)	7.8	0	11.8	-	-
HCM Lane LOS		Α	Α	В	-	-
HCM 95th %tile Q(veh)	0.2	-	0.4	-	-
	,					

Intersection												
Int Delay, s/veh	3.6											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	LDL	4	LDI	VVDL		WDI	NDL	4	NON	ODL	3B1	אומט
Traffic Vol, veh/h	20	4	8	53	↔ 1	71	1	275	14	30	276	10
Future Vol, veh/h	20	4	8	53	-	71		275	14	30	276	10
· · · · · · · · · · · · · · · · · · ·		0	0		1 0	0	1		0	0		
Conflicting Peds, #/hr	0			0				0			0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage		0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	89	89	89	89	89	89	89	89	89	89	89	89
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	22	4	9	60	1	80	1	309	16	34	310	11
Major/Minor	Minor2			Minor1			Major1			Major2		
Conflicting Flow All	744	711	316	709	708	317	321	0	0	325	0	0
Stage 1	384	384	-	319	319	-	-	-	-	-	-	-
Stage 2	360	327	_	390	389	_	_	_	_	_	_	_
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	_	_	4.12	_	_
Critical Hdwy Stg 1	6.12	5.52	0.22	6.12	5.52	0.22	7.14	_		4.12	_	_
Critical Hdwy Stg 1	6.12	5.52		6.12	5.52			_	_		_	
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2 212	_		2.218	_	-
Pot Cap-1 Maneuver	331	358	724	349	360	724	1239	-	-	400=	-	-
•	639	611		693	653	124	1233		-	1233		-
Stage 1	658	648	-	634	608	-	-	-	-	-	-	-
Stage 2	000	040	-	034	QUQ	-	-	-	-	-	-	-
Platoon blocked, %	200	245	704	220	247	704	1000	-	-	1005	-	-
Mov Cap-1 Maneuver	286	345	724	332	347	724	1239	-	-	1235	-	-
Mov Cap-2 Maneuver	286	345	-	332	347	-	-	-	-	-	-	-
Stage 1	638	590	-	692	652	-	-	-	-	-	-	-
Stage 2	584	647	-	600	587	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	16.6			15.6			0			0.8		
HCM LOS	C			C						3.0		
TOW LOO	J			J								
							0	05-	05-			
Minor Lane/Major Mvn	nt	NBL	NBT		EBLn1V		SBL	SBT	SBR			
Capacity (veh/h)		1239	-	-	346	480	1235	-	-			
HCM Lane V/C Ratio		0.001	-	-	0.104			-	-			
HCM Control Delay (s)		7.9	0	-	16.6	15.6	8	0	-			
HCM Lane LOS		Α	Α	-	С	С	Α	Α	-			
HCM 95th %tile Q(veh)	0	-	-	0.3	1.2	0.1	-	-			

Intersection						
	4.5					
Int Delay, s/veh						
Movement	EBL	EBR	SET	SER	NWL	NWT
Lane Configurations	**		1			सी
Traffic Vol, veh/h	43	152	208	31	53	123
Future Vol, veh/h	43	152	208	31	53	123
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		_	0	_	_	0
Grade, %	0	_	0	_	_	0
Peak Hour Factor	98	98	98	98	98	98
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	44	155	212	32	54	126
IVIVITIT FIOW	44	100	212	32	54	120
Major/Minor	Minor1	N	Major1	1	Major2	
Conflicting Flow All	462	228	0	0	244	0
Stage 1	228		_	_		_
Stage 2	234	_	_	_	_	_
Critical Hdwy	6.42	6.22	_		4.12	_
Critical Hdwy Stg 1	5.42	0.22	_	_	4.12	
	5.42	-	-	-	-	
Critical Hdwy Stg 2		2 240	-	-	- 0.40	
Follow-up Hdwy	3.518		-	-	2.218	-
Pot Cap-1 Maneuver	558	811	-	-	1322	-
Stage 1	810	-	-	-	-	-
Stage 2	805	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	533	811	-	-	1322	-
Mov Cap-2 Maneuver	533	-	-	-	-	-
Stage 1	810	-	-	-	-	-
Stage 2	770	-	-	-	-	-
Annroach	EB		SE		NW	
Approach						
HCM Control Delay, s	11.8		0		2.4	
HCM LOS	В					
Minor Lane/Major Mvn	nt	NWL	NWT	EBLn1	SET	SER
Capacity (veh/h)		1322		727	OLI	OLIV
HCM Lane V/C Ratio		0.041	-	0.274	-	-
	\				-	-
HCM Control Delay (s))	7.8	0	11.8	-	-
HCM Lane LOS	\	Α	Α	В	-	-
HCM 95th %tile Q(veh	1)	0.1	-	1.1	-	-

Intersection												
Int Delay, s/veh	3.6											
•		EDT	EDD	WDI	WDT	WDD	NDI	NDT	NDD	CDI	CDT	CDD
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	40	4	_	10	4	00	0	4	0.7	00	4	00
Traffic Vol, veh/h	12	6	5	46	2	29	8	333	87	80	395	26
Future Vol, veh/h	12	6	5	46	2	29	8	333	87	80	395	26
Conflicting Peds, #/hr	0	0	0	0	0	0	_ 0	0	0	0	0	_ 0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage	•	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	88	88	88	88	88	88	88	88	88	88	88	88
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	14	7	6	52	2	33	9	378	99	91	449	30
Major/Minor	Minor2			Minor1			Major1			Major2		
Conflicting Flow All	1109	1141	464	1099	1107	428	479	0	0	477	0	0
Stage 1	646	646	-	446	446	-	-	-	_	-	-	-
Stage 2	463	495	-	653	661	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	_	-	_	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	_	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.218	-	_	2.218	_	_
Pot Cap-1 Maneuver	187	201	598	190	210	627	1083	-	_	1085	_	_
Stage 1	460	467	-	591	574		-	_	_	-	-	_
Stage 2	579	546	_	456	460	_	_	_	_	-	-	_
Platoon blocked, %	3.0	3.3		.00	.00			_	_		_	_
Mov Cap-1 Maneuver	159	176	598	165	184	627	1083	_	_	1085	_	_
Mov Cap-2 Maneuver	159	176	-	165	184	-	-	_	_	-	_	_
Stage 1	455	413	_	584	568	_	_	_	_	_	_	_
Stage 2	540	540	_	393	407	<u>-</u>	_	_	_	_	_	_
Clayo L	3.0	3.0		300	101							
Approach	EB			WB			NB			SB		
HCM Control Delay, s	26.3			30.1			0.2			1.4		
HCM LOS	20.3 D			30.1 D			U.Z			1.4		
TOW LOG	U			U								
Minor Lane/Major Mvm	nt	NBL	NBT	NRD	EBLn1V	WRI n1	SBL	SBT	SBR			
	IX.	1083			195	229	1085	001	ODIN			
Capacity (veh/h)			-	-				-	-			
HCM Central Dalay (a)		0.008	-	-	0.134			-	-			
HCM Control Delay (s)		8.4	0	-	26.3	30.1	8.6	0	-			
HCM Lane LOS	\	A	Α	-	D	D	A	Α	-			
HCM 95th %tile Q(veh))	0	-	-	0.5	1.7	0.3	-	-			

Attachment 6 Intersection Worksheets – Background AM/PM Peaks

Intersection						
Int Delay, s/veh	1.9					
-						
Movement	EBL	EBR	SET	SER	NWL	NWT
Lane Configurations	Y		1>			सी
Traffic Vol, veh/h	21	38	165	21	60	327
Future Vol, veh/h	21	38	165	21	60	327
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e, # 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	87	87	87	87	87	87
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	24	44	190	24	69	376
	Minor1		Major1		Major2	
Conflicting Flow All	716	202	0	0	214	0
Stage 1	202	-	-	-	-	-
Stage 2	514	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	-	-	2.218	-
Pot Cap-1 Maneuver	397	839	-	-	1356	-
Stage 1	832	-	_	_	-	_
Stage 2	600	_	-	_	-	_
Platoon blocked, %	300		_	_		_
Mov Cap-1 Maneuver	372	839			1356	
Mov Cap-1 Maneuver	372	-	_	_	1000	
Stage 1	832	-	_	<u>-</u>		-
•	562		_	-	-	-
Stage 2	202	-	-	-	-	-
Approach	EB		SE		NW	
HCM Control Delay, s	12		0		1.2	
HCM LOS	В					
Minor Lane/Major Mvm	nt	NWL	NWT		SET	SER
Capacity (veh/h)		1356	-	580	-	-
HCM Lane V/C Ratio		0.051	-	0.117	-	-
HCM Control Delay (s)		7.8	0	12	-	-
HCM Lane LOS		Α	Α	В	-	-
HCM 95th %tile Q(veh)	0.2	-	0.4	-	-

Intersection												
Int Delay, s/veh	3.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			4	
Traffic Vol, veh/h	21	4	8	55	1	73	1	283	14	31	284	10
Future Vol, veh/h	21	4	8	55	1	73	1	283	14	31	284	10
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage	e,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	89	89	89	89	89	89	89	89	89	89	89	89
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	24	4	9	62	1	82	1	318	16	35	319	11
Major/Minor	Minor2			Minor1			Major1			Major2		
Conflicting Flow All	765	731	325	729	728	326	330	0	0	334	0	0
Stage 1	395	395	-	328	328	-	-	-	-	-	-	-
Stage 2	370	336	_	401	400	_	_	_	_	_	-	_
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	_	-	4.12	_	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	_	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	_	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	320	349	716	338	350	715	1229	-	-	1225	-	-
Stage 1	630	605	-	685	647	-	-	-	-	-	-	-
Stage 2	650	642	-	626	602	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	275	336	716	321	337	715	1229	-	-	1225	-	-
Mov Cap-2 Maneuver	275	336	-	321	337	-	-	-	-	-	-	-
Stage 1	629	584	-	684	646	-	-	-	-	-	-	-
Stage 2	574	641	-	592	581	-	-	-	-	-	-	-
-												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	17.2			16.1			0			0.8		
HCM LOS	С			С								
Minor Lane/Major Mvn	nt	NBL	NBT	NBR	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		1229			332	467	1225					
HCM Lane V/C Ratio		0.001	_	_	0.112		0.028	_	_			
HCM Control Delay (s)	7.9	0		17.2	16.1	8	0	_			
HCM Lane LOS		Α.5	A	_	C	C	A	A	<u>-</u>			
HCM 95th %tile Q(veh)	0	-		0.4	1.3	0.1	-	_			
TOWN JOHN JOHN Q(VEN	7	J			∪.→	1.0	0.1					

Intersection						
Int Delay, s/veh	4.5					
		EDD	OFT	OED	N IVA /I	N IVA /T
Movement	EBL	EBR	SET	SER	NWL	NWT
Lane Configurations	Y		ĵ,			र्स
Traffic Vol, veh/h	44	157	214	32	55	127
Future Vol, veh/h	44	157	214	32	55	127
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e,# 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	98	98	98	98	98	98
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	45	160	218	33	56	130
N	N 4: 4		1-11		4-10	
	Minor1		Major1		Major2	
Conflicting Flow All	477	235	0	0	251	0
Stage 1	235	-	-	-	-	-
Stage 2	242	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	-	-	2.218	-
Pot Cap-1 Maneuver	547	804	-	-	1314	-
Stage 1	804	-	-	-	-	-
Stage 2	798	-	-	-	-	-
Platoon blocked, %			_	_		-
Mov Cap-1 Maneuver	522	804	_	_	1314	_
Mov Cap-2 Maneuver	522	-	_	_	-	_
Stage 1	804	_	_	_	_	_
Stage 2	761	_	_	_	_	_
Olaye Z	701					
Approach	EB		SE		NW	
HCM Control Delay, s	12		0		2.4	
HCM LOS	В					
Minor Long/Maior M.	a b	NI\A/I	NI\A/T	CDL4	CET	CED
Minor Lane/Major Mvr	nt	NWL	NWT		SET	SER
Capacity (veh/h)		1314	-		-	-
HCM Lane V/C Ratio		0.043		0.285	-	-
HCM Control Delay (s)	7.9	0	12	-	-
HCM Lane LOS		Α	Α	В	-	-
HCM 95th %tile Q(veh	1)	0.1	-	1.2	-	-

Intersection												
Int Delay, s/veh	3.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4	LDIN	,,,,,,,	4	,, D, (1100	4	11511	UDL	4	UDIN
Traffic Vol, veh/h	12	6	5	47	2	30	8	343	90	82	407	27
Future Vol, veh/h	12	6	5	47	2	30	8	343	90	82	407	27
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	_	_	-	_	_	-	_	_	-	_	_	-
Veh in Median Storage	e.# -	0	-	_	0	_	_	0	_	_	0	_
Grade, %	-	0	-	-	0	-	_	0	-	-	0	_
Peak Hour Factor	88	88	88	88	88	88	88	88	88	88	88	88
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	14	7	6	53	2	34	9	390	102	93	463	31
Mai/Mi	N4: C			\ d: \ d			M-!. 4			M-1. C		
	Minor2	44		Minor1	4400		Major1			Major2		
Conflicting Flow All	1142	1175	479	1130	1139	441	494	0	0	492	0	0
Stage 1	665	665	-	459	459	-	-	-	-	-	-	-
Stage 2	477	510	-	671	680	-	- 4.40	-	-	1.10	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	<u>-</u>	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	2 240	6.12	5.52	2 240	0.040	-	-	0.040	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	177	192	587	181	201	616	1070	-	-	1071	-	-
Stage 1	449	458	-	582	566	-	-	-	-	-	-	-
Stage 2	569	538	-	446	451	-	-	-	-	-	-	-
Platoon blocked, %	140	167	E07	156	175	616	1070	-	-	1071	-	-
Mov Cap-1 Maneuver	149	167 167	587	156	175 175	616	1070	-	-	1071	-	-
Mov Cap-2 Maneuver	149 444		-	156		-	-	-	-	-	-	-
Stage 1	529	403 532	-	575 382	559 397	-	-	-		-	-	-
Stage 2	529	:J3Z	-	302	391	-	-	_	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	27.8			32.4			0.2			1.4		
HCM LOS	D			D								
Minor Lane/Major Mvn	nt	NBL	NBT	NRR	EBLn1V	VRI n1	SBL	SBT	SBR			
Capacity (veh/h)		1070	INDI	-	184	219	1071	051	ODIN			
HCM Lane V/C Ratio		0.008	<u> </u>		0.142		0.087	-	-			
HCM Control Delay (s	\	8.4	0	-	27.8	32.4	8.7	0	-			
HCM Lane LOS		0.4 A	A		27.0 D	J2.4	Α	A	<u>-</u>			
HCM 95th %tile Q(veh	1	0	-	_	0.5	1.9	0.3	-	_			
HOW JOHN JOHN GUILD WOLLD	7	- 0	_	_	0.0	1.0	0.0					

Attachment 7 Intersection Worksheets – Full Buildout AM/PM Peaks

Intersection						
	4.5					
Int Delay, s/veh	4.3					
Movement	EBL	EBR	SET	SER	NWL	NWT
Lane Configurations	M		f)			र्स
Traffic Vol, veh/h	93	69	165	45	70	327
Future Vol, veh/h	93	69	165	45	70	327
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	_	None	_	None	_	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		_	0	_	_	0
Grade, %	0	_	0	_	_	0
Peak Hour Factor	87	87	87	87	87	87
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	107	79	190	52	80	376
Major/Minor	Minor1	N	Major1		Major2	
Conflicting Flow All	752	216	0	0	242	0
Stage 1	216	210		U	242	-
Stage 2	536		-	-	_	-
		-	-	-		-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518		-	-	2.218	-
Pot Cap-1 Maneuver	378	824	-	-	1324	-
Stage 1	820	-	-	-	-	-
Stage 2	587	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	349	824	_	-	1324	-
Mov Cap-2 Maneuver	349		_	_		_
Stage 1	820	_	_	_	_	_
Stage 2	542				_	
Staye Z	J4Z	<u>-</u>	-	-	_	-
Approach	EB		SE		NW	
HCM Control Delay, s	17.9		0		1.4	
HCM LOS	C				- '''	
	<u> </u>					
Minor Lane/Major Mvr	nt	NWL	NWT	EBLn1	SET	SER
Capacity (veh/h)		1324	-	463	-	-
HCM Lane V/C Ratio		0.061	-	0.402	-	-
HCM Control Delay (s)	7.9	0	17.9	-	-
HCM Lane LOS		A	A	С	_	-
HCM 95th %tile Q(veh)	0.2	- '.	1.9	_	_
HOW JOHN JOHN & (VEI)	7	0.2		1.5		

Intersection												
Int Delay, s/veh	5.2											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			4	
Traffic Vol, veh/h	21	4	8	76	1	104	1	283	21	41	284	10
Future Vol, veh/h	21	4	8	76	1	104	1	283	21	41	284	10
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	_	-	None
Storage Length	_	_	-	-	-	-	_	-	-	_	-	-
Veh in Median Storage	e.# -	0	_	_	0	_	-	0	_	_	0	-
Grade, %	-	0	-	_	0	-	_	0	-	_	0	_
Peak Hour Factor	89	89	89	89	89	89	89	89	89	89	89	89
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	24	4	9	85	1	117	1	318	24	46	319	11
Major/Minor	Minor2			Minor1			Major1			Major2		
Conflicting Flow All	808	761	325	755	754	330	330	0	0	342	0	0
Stage 1	417	417	525	332	332	-	-	-	-	J4Z -	-	-
Stage 2	391	344	_	423	422	_	_	_			_	
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	_	_	4.12	_	
Critical Hdwy Stg 1	6.12	5.52	0.22	6.12	5.52	U.ZZ	T. 12	_	_	4 .12	_	_
Critical Hdwy Stg 1	6.12	5.52		6.12	5.52	_	_	_	_	_	_	_
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.218	<u>-</u>	_	2.218	_	_
Pot Cap-1 Maneuver	299	335	716	325	338	712	1229	_	_	1217	_	_
Stage 1	613	591	-	681	644	- 12		_	_	-	_	_
Stage 2	633	637	-	609	588	-	_	_	_	_	_	-
Platoon blocked, %				300	- 500			_	_		-	_
Mov Cap-1 Maneuver	240	319	716	306	322	712	1229	_	_	1217	-	_
Mov Cap-2 Maneuver	240	319	-	306	322	-	-	_	_	-	_	_
Stage 1	612	564	_	680	643	_	_	_	_	_	-	-
Stage 2	528	636	-	569	561	-	-	-	-	-	-	-
Ŭ												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	18.8			19.2			0			1		
HCM LOS	C			C								
Minor Lane/Major Mvn	nt	NBL	NBT	NBR	EBLn1\	WBLn1	SBL	SBT	SBR			
Capacity (veh/h)		1229	-	-	297	455	1217	-	-			
HCM Lane V/C Ratio		0.001	_	_		0.447		_	_			
HCM Control Delay (s)		7.9	0	_	18.8	19.2	8.1	0	-			
HCM Lane LOS		A	A	_	С	С	A	A	-			
HCM 95th %tile Q(veh)	0	-	-	0.4	2.3	0.1	-	-			
211 - 21112 - 2111	,											

Intersection						
Int Delay, s/veh	5.5					
	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	1			4	M	
Traffic Vol, veh/h	59	23	34	81	69	103
Future Vol, veh/h	59	23	34	81	69	103
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control F	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	<i>‡</i> 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	64	25	37	88	75	112
	•		Ψ.			
				_		
	ajor1		Major2		Minor1	
Conflicting Flow All	0	0	89	0	239	77
Stage 1	-	-	-	-	77	-
Stage 2	-	-	-	-	162	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	-	-	2.218	-	3.518	3.318
Pot Cap-1 Maneuver	_	_	1506	_	749	984
Stage 1	-	-	-	_	946	-
Stage 2	_	_	_	_	867	_
Platoon blocked, %	_	_		_		
Mov Cap-1 Maneuver	_	_	1506	-	730	984
Mov Cap-2 Maneuver	_	_	-	_	730	-
Stage 1	_				946	
Stage 2		-	_	-	844	-
Slaye 2	-	-	-	-	044	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		2.2		10.3	
HCM LOS					В	
NA' 1 /NA - ' NA ()		IDL 4	CDT	EDD	MDI	WDT
Minor Lane/Major Mvmt	ľ	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		863	-		1506	-
HCM Lane V/C Ratio		0.217	-	-	0.025	-
HCM Control Delay (s)		10.3	-	-	7.5	0
HCM Lane LOS		В	-	-	Α	Α
HCM 95th %tile Q(veh)		0.8			0.1	

Intersection						
Int Delay, s/veh	6.2					
Movement	EBL	EBR	SET	SER	NWL	NWT
Lane Configurations	N.		₽			4
Traffic Vol, veh/h	93	178	214	116	91	127
Future Vol, veh/h	93	178	214	116	91	127
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	, # 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	98	98	98	98	98	98
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	95	182	218	118	93	130
		_		_		
	Minor1		/lajor1		Major2	
Conflicting Flow All	593	277	0	0	336	0
Stage 1	277	-	-	-	-	-
Stage 2	316	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	_
Follow-up Hdwy	3.518	3.318	_	-	2.218	-
Pot Cap-1 Maneuver	468	762	_	-	1223	-
Stage 1	770	-	_	_	-	_
Stage 2	739	_	_	_	_	_
Platoon blocked, %	700		_	_		_
Mov Cap-1 Maneuver	430	762	_	_	1223	_
Mov Cap-1 Maneuver	430	702	_	_	1223	_
•	770	-	-	-		-
Stage 1			-	-		
Stage 2	678	-	-	-	-	-
Approach	EB		SE		NW	
HCM Control Delay, s	16		0		3.4	
HCM LOS	С					
Minor Lane/Major Mvm	<u>it</u>	NWL	NWT		SET	SER
Capacity (veh/h)		1223	-	602	-	-
HCM Lane V/C Ratio		0.076	-	0.459	-	-
HCM Control Delay (s)		8.2	0	16	-	-
HCM Lane LOS HCM 95th %tile Q(veh)		A 0.2	Α	C 2.4	-	-

Intersection												
Int Delay, s/veh	6.9											
•		EDT	EDD	WDI	WDT	WDD	NDL	NDT	NDD	CDI	CDT	CDD
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	10	4	F	64	4	51	0	242	111	110	407	07
Traffic Vol, veh/h	12 12	6	5	61 61	2	51	8	343 343	114 114	118 118	407 407	27 27
Future Vol, veh/h Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	407	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	Stop -	Stop	None	Stop -	Stop -	None	-	-	None	-	-	None
Storage Length		_	INUITE	_	_	INUITE	_	_	INUITE	_	_	INUITE
Veh in Median Storage		0	_		0	_	_	0	_		0	_
Grade, %	-, π -	0		_	0	_	_	0	_	_	0	_
Peak Hour Factor	88	88	88	88	88	88	88	88	88	88	88	88
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mymt Flow	14	7	6	69	2	58	9	390	130	134	463	31
WIVING LIOW	17	1	- 0	- 03		- 50	J	000	100	107	700	01
N.A ' (N.A.	N 41						M			M. 1		
	Minor2	1005		Minor1	465-		Major1			Major2		
Conflicting Flow All	1250	1285	479	1226	1235	455	494	0	0	520	0	0
Stage 1	747	747	-	473	473	-	-	-	-	-	-	-
Stage 2	503	538	-	753	762	-	-	-	-	- 4.40	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.12	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	2.040	0.040	-	-	0.040	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.218	-	-	2.218	-	-
Pot Cap-1 Maneuver	150	165	587	155	176	605	1070	-	-	1046	-	-
Stage 1	405	420	-	572	558	-	-	-	-	-	-	-
Stage 2	551	522	-	402	414	-	-	-	-	-	-	-
Platoon blocked, %	115	101	E07	400	1.10	COF	1070	-	-	1040	-	-
Mov Cap-1 Maneuver	115	134	587	126	143	605	1070	-	-	1046	-	-
Mov Cap-2 Maneuver	115	134	-	126	143	-	-	-	-	-	-	-
Stage 1	400	346	-	565	551	-	-	-	-	-	-	-
Stage 2	490	516	-	321	341	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	35			53.3			0.1			1.9		
HCM LOS	Е			F								
Minor Lane/Major Mvm	nt	NBL	NBT	NBR	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		1070	-	-	146	196	1046					
HCM Lane V/C Ratio		0.008	_		0.179			_	_			
HCM Control Delay (s)		8.4	0	_	35	53.3	8.9	0	_			
HCM Lane LOS		Α	A	<u>-</u>	E	55.5	Α	A	_			
HCM 95th %tile Q(veh)	0	-	_	0.6	4	0.4	-	_			
TOTAL OCAL TOTAL Q(VOIL	1	J			0.0		υ. τ					

Intersection						
Int Delay, s/veh	4.2					
		EDD	MDI	WOT	ND	NDD
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	1		400	र्स	, A	
Traffic Vol, veh/h	201	80	120	87	47	70
Future Vol, veh/h	201	80	120	87	47	70
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	218	87	130	95	51	76
N. 1. /N. 1	1		4		M	
	/lajor1		Major2		Minor1	
Conflicting Flow All	0	0	305	0	617	262
Stage 1	-	-	-	-	262	-
Stage 2	-	-	-	-	355	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	-	-	2.218	-	3.518	3.318
Pot Cap-1 Maneuver	-	-	1256	-	453	777
Stage 1	-	-	-	-	782	-
Stage 2	-	-	-	-	710	-
Platoon blocked, %	-	_		_		
Mov Cap-1 Maneuver	_	_	1256	-	404	777
Mov Cap-2 Maneuver	_	_		_	404	-
Stage 1					782	_
Stage 2		_			633	_
Slaye 2	_	_	_	_	000	<u>-</u>
Approach	EB		WB		NB	
HCM Control Delay, s	0		4.8		13.2	
HCM LOS					В	
N. 1 (N. 1 N. 1		IDL 4	БОТ	EDD	MAIDI	MOT
Minor Lane/Major Mvmt	<u> </u>	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		567	-		1256	-
HCM Lane V/C Ratio		0.224	-	-	0.104	-
HCM Control Delay (s)		13.2	-	-	8.2	0
HCM Lane LOS		В	-	-	Α	Α
HCM 95th %tile Q(veh)		0.9	-	-	0.3	-

Attachment 8 Turn Lane Warrants

Project: Tipton Station Subdivision

 PM

Tipton Station Road at Subdi	vision Roadw	ay			
Tipton Station Road	VOLUMES				
at Subdivision Roadway					
LEFT TURN	Opposing	Thru	LT	LT MAX	Warrant Met
AM	82	81	34	250	NO
PM	281	87	120	130	NO
Tipton Station Road	VOLUMES				
at Subdivision Roadway					
RIGHT TURN		Thru	RT	RT MAX	Warrant Met
AM	_	59	23	549	NO
PM		201	80	349	NO
Tipton Station Road at W Ma	rtin Mill Pike				
Tipton Station Road	VOLUMES				
at W Martin Mill Pike					
LEFT TURN	Opposing	Thru	LT	LT MAX	Warrant Met
AM	210	327	70	65	YES
PM	330	127	91	110	NO
Tipton Station Road	VOLUMES				
at W Martin Mill Pike					
RIGHT TURN		Thru	RT	RT MAX	Warrant Met
AM	_	165	45	449	NO

214

116

349

NO

TABLE 5A

LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH

(If the left-turn volume exceeds the table value a left -turn lane is needed)

OPPOSING	THROU	GH VOLUME	PLUS RIGH	T-TURN V	OLUME	
VOLUME	100 - 149	150 - 199	200 - 249	250 - 299	300 - 349	350 - 399
100 - 149	250	180	140	110	80	70
150 - 199	200	140	105	90	70	60
200 - 249	160	115	85	AM Peak 70 I	T 65	55
250 - 299	130	100	75	65		50
300 - 349 350 - 399	110 PM	Peak 91 LT	70 65	60 55	55 50	45 40
400 - 449	90	70	60	50	45	35
450 - 499	80	65	55	45	40	30
500 - 549	70	60	45	35	35	25
550 - 599	65	55	40	35	30	25
600 - 649	60	45	35	30	25	25
650 - 699	55	35	35	30	25	20
700 - 749	50	35	30	25	20	20
750 or More	45	35	25	25	20	20

OPPOSING	THROU	GH VOLUME	PLUS RIGH	T-TURGN	A OPOINT	
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 599	=/ > 600
100 - 149	70	60	50	45	40	35
150 - 199	60	55	45	40	35	30
200 - 249	55	50	40	35	30	30
250 - 299	50	45	35	30	30	30
300 - 349	45	40	35	30	25	25
350 - 399	40 ·	35	30	25	25	20
400 - 449	35	30	30	25	20	20
450 - 499	30	25	25	20	20	20
500 - 549	25	25	20	20	20	15
550 - 599	25	20	20	20	20	15
600 - 649	25	20	20	20	20	15
650 - 699	20	20	20	20	20	15
700 - 749	20	20	. 20	15	15	15
750 or More	20	20	20	15	15	15

^{*} Or through volume only if a right-turn lane exists

TABLE 5B

RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH

RIGHT-TURN	THRO	UGH VOLUM	E PLUS LEI	T-TURN	VOLUME	; *
VOLUME	< 100	100 - 199	200 - 249	250 - 299	300 - 349	350 - 399
Fewer Than 25 25 - 49 50 - 99	AM Peak	45 RT				
100 - 149 150 - 199		PM Peak 11	6 RT			
200 - 249 250 - 299					Yes	Yes Yes
300 - 349 350 - 399			Yes	Yes Yes	Yes Yes	Yes Yes
400 - 449 450 - 499		Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
500 - 549 550 - 599	Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
600 or More	Yes	Yes	Yes	Yes	Yes	Yes

RIGHT-TURN	THR	OUGH VOLU	ME PLUS LE	FT-TURN	VOLUM	E *
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 600	+ / > 600
Fewer Than 25 25 - 49 50 - 99				Yes	Yes Yes	Yes Yes
100 - 149 150 - 199		Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
200 - 249 250 - 299	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
300 - 349 350 - 399	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
400 - 449 450 - 499	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
500 - 549 550 - 599	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
600 or More	Yes	Yes	Yes	Yes	Yes	Yes

^{*} Or through volume only if a left-turn lane exists.

TABLE 5A

LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH

(If the left-turn volume exceeds the table value a left -turn lane is needed)

OPPOSING	THROU	GH VOLUME	PLUS RIGH	T-TURN V	i	
VOLUME	100 - 149	150 - 199	200 - 249	250 - 299	300 - 349	350 - 399
100 - 149 150 - 199	250 AM	Peak 34 LT	140 105	110 90	80 70	70 60
200 - 249	160	115	85	75	65	55
250 - 299		Peak 120 LT	75	65	60	50
300 - 349	110	90	70	60	55	45
350 - 399		80	65	55	50	40
400 - 449	90	70	60	50	45	35
450 - 499	80	65	55	45	40	30
500 - 549	70	60	45	35	35	25
550 - 599	65	55	40	35	30	25
600 - 649	60	45	35	30	25	25
650 - 699	55	35	35	30	25	20
700 - 749	50	35	30	25	20	20
750 or More	45	35	25	25	20	20

OPPOSING	THROU	GH VOLUME	PLUS RIGH	T-TURN	VOLUME	*
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 599	=/ > 600
100 - 149	70	60	50	45	40	35
150 - 199	60	55	45	40	35	30
200 - 249	55	50	40	35	30	30
250 - 299	50	45	35	30	30	30
300 - 349	45	40	35	30	25	25
350 - 399	40 ·	35	30	25	25	20
400 - 449	35	30	30	25	20	20
450 - 499	30	25	25	20	20	20
500 - 549	25	25	20	20	20	15
550 - 599	25	20	20	20	20	15
600 - 649	25	20	20	20	20	15
650 - 699	20	20	20	20	20	15
700 - 749	20	20	. 20	15	15	15
750 or More		20	20	15	15	15

^{*} Or through volume only if a right-turn lane exists

TABLE 5B

RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH

RIGHT-TURN	THRO	UGH VOLUM	E PLUS LEI	T-TURN	VOLUME	<u> </u>
VOLUME	<100	100 - 199	200 - 249	250 - 299	300 - 349	350 - 399
Fewer Than 25 25 - 49 50 - 99	AM F	Peak 23 RT	PN	Peak 80 RT		
100 - 149 150 - 199						
200 - 249 250 - 299					Yes	Yes Yes
300 - 349 350 - 399			Yes	Yes Yes	Yes Yes	Yes Yes
400 - 449 450 - 499		Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
500 - 549 550 - 599	Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
600 or More	Yes	Yes	Yes	Yes	Yes	Yes

RIGHT-TURN	THR	OUGH VOLU	ME PLUS LE	FT-TURN	VOLUM	E *
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 600	+ / > 600
Fewer Than 25 25 - 49 50 - 99				Yes	Yes Yes	Yes Yes
100 - 149 150 - 199		Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
200 - 249 250 - 299	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
300 - 349 350 - 399	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
400 - 449 450 - 499	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
500 - 549 550 - 599	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
600 or More	Yes	Yes	Yes	Yes	Yes	Yes

^{*} Or through volume only if a left-turn lane exists.

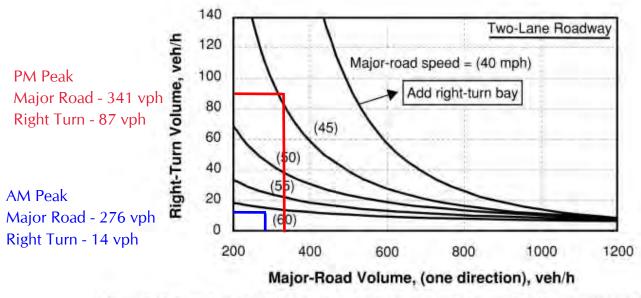


Figure 3-18: Right-Turn Lane Warrant along Two-Lane Roadway (Unsignalized Intersection with Two-Way Stop-Control)²⁴

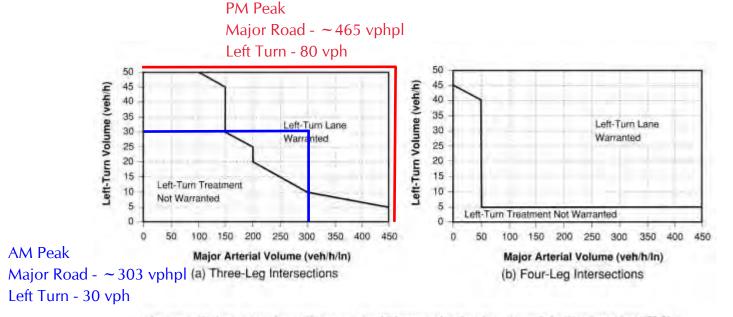


Figure 3-15: Left-Turn Lane Warrant for Urban and Suburban Arterials (Unsignalized)^{20, 21}

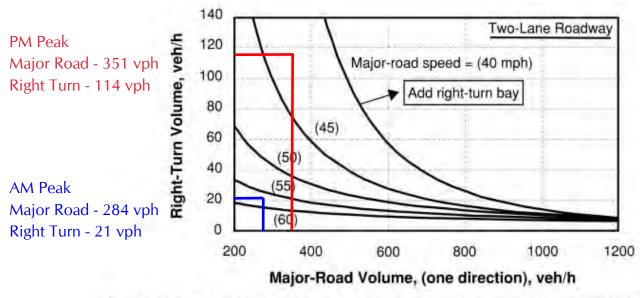


Figure 3-18: Right-Turn Lane Warrant along Two-Lane Roadway (Unsignalized Intersection with Two-Way Stop-Control)²⁴

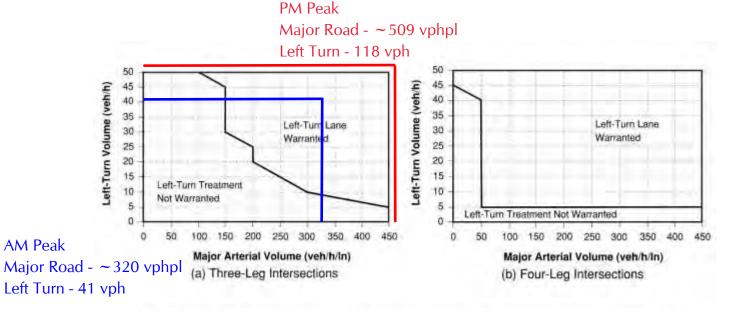


Figure 3-15: Left-Turn Lane Warrant for Urban and Suburban Arterials (Unsignalized)^{20, 21}

Attachment 9 Sight Distance



Tipton Station Road at Subdivision Roadway – Looking Left (Westbound)



Tipton Station Road at Subdivision Roadway – Looking Right (Eastbound)

Attachment 10 Alternative Analysis

4: Goddard Road & Tipton Station Road & W Martin Mill Pike

Intersection				
Intersection Delay, s/veh	5.7			
Intersection LOS	А			
Approach	EB	NB	SE	NW
Entry Lanes	1	1	1	1
Conflicting Circle Lanes	1	1	1	1
Adj Approach Flow, veh/h	186	0	242	456
Demand Flow Rate, veh/h	190	0	247	466
Vehicles Circulating, veh/h	194	384	82	109
Vehicles Exiting, veh/h	135	0	493	275
Ped Vol Crossing Leg, #/h	0	0	0	0
Ped Cap Adj	1.000	1.000	1.000	1.000
Approach Delay, s/veh	4.7	0.0	4.6	6.7
Approach LOS	Α	-	A	Α
	1 6			
Lane	Left	Left	Left	Left
Designated Moves	Left LR	Left LR	Left TR	Left LT
Designated Moves	LR	LR	TR	LT
Designated Moves Assumed Moves	LR	LR	TR	LT
Designated Moves Assumed Moves RT Channelized	LR LR	LR LR	TR TR	LT LT
Designated Moves Assumed Moves RT Channelized Lane Util	LR LR 1.000	LR LR 1.000	TR TR 1.000	LT LT 1.000
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s	LR LR 1.000 2.609	LR LR 1.000 2.609	TR TR 1.000 2.609	LT LT 1.000 2.609
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s	LR LR 1.000 2.609 4.976	LR LR 1.000 2.609 4.976	TR TR 1.000 2.609 4.976	LT LT 1.000 2.609 4.976
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor	LR LR 1.000 2.609 4.976 190 1132 0.979	LR LR 1.000 2.609 4.976 0	TR TR 1.000 2.609 4.976 247	LT LT 1.000 2.609 4.976 466 1235 0.980
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h	LR LR 1.000 2.609 4.976 190 1132	LR LR 1.000 2.609 4.976 0 933	TR TR 1.000 2.609 4.976 247 1269 0.981 242	LT LT 1.000 2.609 4.976 466 1235
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h Cap Entry, veh/h	LR LR 1.000 2.609 4.976 190 1132 0.979 186 1108	LR LR 1.000 2.609 4.976 0 933 1.000	TR TR 1.000 2.609 4.976 247 1269 0.981 242 1244	LT LT 1.000 2.609 4.976 466 1235 0.980 456 1209
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h	LR LR 1.000 2.609 4.976 190 1132 0.979 186 1108 0.168	LR LR 1.000 2.609 4.976 0 933 1.000 0 933	TR TR 1.000 2.609 4.976 247 1269 0.981 242 1244 0.195	LT LT 1.000 2.609 4.976 466 1235 0.980 456 1209 0.377
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h Cap Entry, veh/h V/C Ratio Control Delay, s/veh	LR LR 1.000 2.609 4.976 190 1132 0.979 186 1108	LR LR 1.000 2.609 4.976 0 933 1.000 0	TR TR 1.000 2.609 4.976 247 1269 0.981 242 1244	LT LT 1.000 2.609 4.976 466 1235 0.980 456 1209
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h Cap Entry, veh/h V/C Ratio	LR LR 1.000 2.609 4.976 190 1132 0.979 186 1108 0.168	LR LR 1.000 2.609 4.976 0 933 1.000 0 933	TR TR 1.000 2.609 4.976 247 1269 0.981 242 1244 0.195	LT LT 1.000 2.609 4.976 466 1235 0.980 456 1209 0.377

4: Goddard Road & Tipton Station Road & W Martin Mill Pike

Intersection				
Intersection Delay, s/veh	5.3			
Intersection LOS	Α			
Approach	EB	NB	SE	NW
Entry Lanes	1	1	1	1
Conflicting Circle Lanes	1	1	1	1
Adj Approach Flow, veh/h	277	0	336	223
Demand Flow Rate, veh/h	283	0	342	228
Vehicles Circulating, veh/h	222	505	95	97
Vehicles Exiting, veh/h	215	0	230	408
Ped Vol Crossing Leg, #/h	0	0	0	0
Ped Cap Adj	1.000	1.000	1.000	1.000
Approach Delay, s/veh	5.8	0.0	5.4	4.5
Approach LOS	Α	-	А	Α
Lane	Left	Left	Left	1 -44
Lano	LEIL	Leit	Leit	Left
Designated Moves	LR	LR	TR	Lett LT
Designated Moves	LR	LR	TR	LT
Designated Moves Assumed Moves	LR	LR	TR	LT
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s	LR LR	LR LR	TR TR	LT LT
Designated Moves Assumed Moves RT Channelized Lane Util	LR LR 1.000	LR LR 1.000	TR TR 1.000	LT LT 1.000
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s	LR LR 1.000 2.609 4.976 283	LR LR 1.000 2.609	TR TR 1.000 2.609	LT LT 1.000 2.609
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s	LR LR 1.000 2.609 4.976	LR LR 1.000 2.609 4.976	TR TR 1.000 2.609 4.976	LT LT 1.000 2.609 4.976 228 1250
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor	LR LR 1.000 2.609 4.976 283 1100 0.979	LR LR 1.000 2.609 4.976 0	TR TR 1.000 2.609 4.976 342	LT LT 1.000 2.609 4.976 228 1250 0.980
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h	LR LR 1.000 2.609 4.976 283 1100 0.979	LR LR 1.000 2.609 4.976 0 824 1.000	TR TR 1.000 2.609 4.976 342 1252 0.981 336	LT LT 1.000 2.609 4.976 228 1250 0.980 223
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h Cap Entry, veh/h	LR LR 1.000 2.609 4.976 283 1100 0.979 277	LR LR 1.000 2.609 4.976 0 824 1.000	TR TR 1.000 2.609 4.976 342 1252 0.981 336 1229	LT LT 1.000 2.609 4.976 228 1250 0.980 223 1225
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h	LR LR 1.000 2.609 4.976 283 1100 0.979 277 1077	LR LR 1.000 2.609 4.976 0 824 1.000 0 824	TR TR 1.000 2.609 4.976 342 1252 0.981 336 1229 0.273	LT LT 1.000 2.609 4.976 228 1250 0.980 223 1225 0.182
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h Cap Entry, veh/h V/C Ratio Control Delay, s/veh	LR LR 1.000 2.609 4.976 283 1100 0.979 277	LR LR 1.000 2.609 4.976 0 824 1.000 0 824 0.000 4.4	TR TR 1.000 2.609 4.976 342 1252 0.981 336 1229	LT LT 1.000 2.609 4.976 228 1250 0.980 223 1225
Designated Moves Assumed Moves RT Channelized Lane Util Follow-Up Headway, s Critical Headway, s Entry Flow, veh/h Cap Entry Lane, veh/h Entry HV Adj Factor Flow Entry, veh/h Cap Entry, veh/h V/C Ratio	LR LR 1.000 2.609 4.976 283 1100 0.979 277 1077	LR LR 1.000 2.609 4.976 0 824 1.000 0 824	TR TR 1.000 2.609 4.976 342 1252 0.981 336 1229 0.273	LT LT 1.000 2.609 4.976 228 1250 0.980 223 1225 0.182



Date: October 14, 2024

To: Knoxville Knox County Planning

Subject: Tipton Station Road TIS Comments (10-SB-24-C / 10-C-24-DP)

Dear City of Knoxville staff,

The following comment response document is submitted to address comments dated September 6, 2024:

1. Reviewer Comment: There are a few instances where the TIS refers to the northbound leg of the Tipton Station Rd at Martin Mill Pk intersection as being Martin Mill Pk however this leg is actually named Tipton Station Rd – please review and revise as necessary throughout the document.

<u>Response:</u> Updated TIA Report with the correct name of the northbound leg at the intersection of Tipton Station Rd at Martin Mill Pk.

2. Reviewer Comment: The turn lane warrant sheets provided in the appendix need to be more clearly labeled to show the specific scenario and volumes being reported, particularly for the TDOT warrant scenarios for each set of volumes (existing, background and build) so that it can be discerned at what point the warrant has been met and to support the claim that the Maryville Pk at Tipton Station Rd intersection warrants a northbound left turn lane with the existing volumes.

Response: Updated the TDOT Turn Lane Warrants in Attachment 8 to include the vehicle volumes and to add TDOT Turn Lane Warrants for the existing conditions at the intersection of Maryville Pike at Tipton Station Road.

3. **Reviewer Comment:** Please revise the recommendations included on Page 4 in the Executive Summary to add a bullet point for the Maryville Pk at Tipton Station Rd mitigation to reference that the TIS did determine that a southbound left turn lane has been found to be warranted based on existing conditions.

Response: Added the following bullet item to Page 4. "A southbound left turn lane is warranted during the existing conditions per the TDOT Highway System Access Manual."

4. **Reviewer Comment:** Please provide evaluation of an alternative mitigation scenario where a roundabout would be installed at the intersection of Tipton Station Rd and Martin Mill Pk, which may also allow a tie-in of the closely spaced Goddard Rd intersection. The evaluation should include a brief assessment of the feasibility of this mitigation and the expected level-of-service.

<u>Response:</u> Added the evaluation of the installation of a roundabout at the existing intersection of W Martin Mill Pike at Tipton Station Road to Section 7.1. and the roundabout capacity analysis reports to Attachment 10 – Alternative Analysis.

Sincerely,



Addie Kirkham, P.E.