# DUTCHTOWN ROAD SUBDIVISION <br> Traffic Impact Study <br> Dutchtown Road <br> Knoxville, TN 

## A Traffic Impact Study for the Proposed Dutchtown Road Subdivision

Submitted to

# Knoxville - Knox County Metropolitan Planning Commission 

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FMA Project No. 330.010

Submitted By:


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## Executive Summary

S \& E Properties, LLC proposes a residential development with single family homes. The project is located at east of Pellissippi Parkway (Highway 162) near the intersection of Dutchtown Road and Mabry Hood Road in West Knox County, Tennessee. The development will consist of 95 single family homes. Construction is proposed to take place this year and this study assumes full build out for the development will occur in 2018.

The driveway for the proposed development will tie into Dutchtown Road 385 -ft west of the intersection of Dutchtown Road and Rennboro Road. The proposed lane configuration is a single lane out of the development.

In order to maintain or provide an acceptable level-of-service for each of the intersections studied, some recommendations are presented.

## Dutchtown Road @ Project Entrance

The nearest road intersection to the project entrance is currently $385-\mathrm{ft}$ east at the intersection of Dutchtown Road and Rennboro Road, which does not meet the recommended minimum separation of 400 feet between roads on an arterial per the "Minimum Subdivision Regulations" for Knoxville and Knox County.

An eastbound left turn lane is warranted at the intersection of Dutchtown Road and the proposed project entrance. FMA recommends the two way left turn lane be restriped to include a break at the intersection of Dutchtown Road and the project entrance.

## Dutchtown Road @ Mabry Hood

The eastbound and westbound approach will continue to operate at a LOS B or higher after the completion of the Dutchtown Road Subdivision. The northbound and southbound approach will continue to operate at a LOS F after the completion of the Dutchtown Road Subdivision.

## Dutchtown Road @ Rennboro Road

The Unsignalized intersection capacity analyses shows a $95 \%$ queue length for the eastbound left turn lane of less than one car length during both the AM and PM peak hours; therefore, the existing left turn lane with a 150-ft storage length entering Rennboro Road will be adequate and will not interfere with the Dutchtown Road Subdivision.

## 1 Introduction

### 1.1 Project Description

This report provides a summary of a traffic impact study that was performed for the proposed Dutchtown Road Subdivision on Dutchtown Road. The project site is located east of Pellissippi Parkway (Highway 162) near the intersection of Mabry Hood Road and Dutchtown Road in west Knox County. The location of the site is shown in Figure 1.

The proposed Dutchtown Road Subdivision will consist of 95 single family lots. Full Buildout is expected to occur within three years, or by the year 2018. The proposed site layout is shown in Figure 2.

The purpose of this study is to evaluate the impacts to the traffic conditions caused by the development of the proposed subdivision.

### 1.2 Existing Site Conditions

The proposed subdivision site access will tie into Dutchtown Road approximately 871 feet east of the intersection of Dutchtown Road and Mabry Hood Road and approximately 385 feet west of the intersection of Dutchtown Road and Rennboro Road.

During a site visit it was determined that Dutchtown Road is a three-lane road with a two-way left turn lane at the proposed project entrance. The Knoxville-Knox County Metropolitan Planning Commission classifies Dutchtown Road as a minor arterial per the Major Road Plan. The posted speed limit on Dutchtown Road is 40 mph . The grade on Dutchtown Road at the proposed project entrance is approximately $3 \%$. The intersection sight distance at the proposed driveway was measured to be in excess of 400-ft east and west of the intersection.

Mabry Hood Road is a two-lane road and has a posted speed limit of 30 mph . The Knoxville-Knox County Metropolitan Planning Commission classifies Mabry Hood Road as a minor collector per the Major Road Plan. The grade on the southbound approach of Mabry Hood Road is approximately $5 \%$.

Rennboro Road is a two-lane road and has a posted speed limit of 25 mph . The Knoxville-Knox County Metropolitan Planning Commission classifies Rennboro Road as a local street per the Major Road Plan. There is an existing left turn lane with a 150 -ft storage length on Dutchtown Road at the intersection of Rennboro Road.

## FIGURE 1




FIGURE 2


## 2 Existing Traffic Volumes

FMA conducted an eight-hour turning movement count at the intersection of Dutchtown Road and Mabry Hood Road on Tuesday August 25, 2015. The existing volume including the AM and PM peak hour traffic volumes at the count locations are shown in Figure 3 and the count data collected is included in Attachment 1.

The current AM peak hour, and PM peak hour were determined using the eighthour turning movement count that FMA conducted. The AM peak hour occurred between 7:15 am and 8:15 am and the PM peak hour occurred between 5:00 pm and 6:00 pm.

Single-Family Detached Housing or Land Use 210 was used to calculate site trips for the existing single family housing on Rennboro Road using the fitted curve equations from The Trip Generation, $7^{\text {th }}$ Edition, published by the Institute of Transportation Engineers. The land use worksheets are included in Attachment 3.

The existing subdivision has 46 lots that enter and exit at the intersection of Dutchtown Road and Rennboro Road. The total number of trips generated by the existing single family housing was estimated to be 509 daily trips. During the peak hour the estimated trips are 42 trips during the AM peak hour and 53 trips during the PM peak hour. A trip generation summary is shown in Table 2-1.

Table 2-1
Trip Generation Summary

|  | Single-Family Detached Housing <br> (Land Use 210) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total Existing <br> Trips | \% Entering | \% Exiting | Number <br> Entering | Number <br> Exiting |
|  |  |  |  |  |  |
| Weekday | 509 | 50 | 50 | 255 | 255 |
| A.M. Peak | 42 | 25 | 75 | 11 | 32 |
| P.M. Peak | 53 | 63 | 37 | 33 | 20 |
|  |  |  |  |  |  |



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## 3 Background Growth

The Tennessee Department of Transportation (TDOT) maintains count Station \#000427 on Dutchtown Road near the Christian Academy of Knoxville. The annual traffic growth rate for Station \#000427 between 2000 and 2014 is approximately 0.50\%.

The Knoxville-Knox County Metropolitan Planning Commission (MPC) and the Transportation Planning Organization (TPO) maintain count station M56 on Dutchtown Road west of Mabry Hood Road. The annual traffic growth rate for Station M56 between 2010 and 2013 is approximately $6.32 \%$.

For the purpose of this study, an annual growth rate of $3 \%$ for traffic at the intersection of Dutchtown Road and Mabry Hood Road was assumed until full occupancy is reached in 2018.

Attachment 2 shows the trend line growth charts for the TDOT count stations and for the MPC/TPO count stations. Figure 4 demonstrates the projected future peak hour volumes at the intersections after applying this background growth rate to the existing conditions.


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| Project 330.010 | Proj. Mgr. |  | Designed By | Drown By | Reference | 2018 BACKGROUND PEAK HOUR TRAFFIC | $\frac{\text { DUTCHTOWN RD SUBDIVISION }}{\text { KNOX COUNTY, TN }}$ | FULGHUM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dote 9/1/15 | Q | ISSUED FOR REVIEW |  |  |  |  |  | $\cdots$ | SUITE 201 |

## 4 Trip Generation and Trip Distribution

Single-Family Detached Housing or Land Use 210 was used to calculate site trips for the proposed single family housing using the fitted curve equations from The Trip Generation, $7^{\text {th }}$ Edition, published by the Institute of Transportation Engineers. The land use worksheets are included in Attachment 3.

The total number of trips generated by the proposed single family housing was estimated to be 992 daily trips. During the peak hour the estimated trips are 76 trips during the AM peak hour and 102 trips during the PM peak hour. A trip generation summary is shown in Table 4-1.

Table 4-1
Trip Generation Summary

|  |  | Single-Family Detached Housing <br> (Land Use 210) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total New | \% Entering | \% Exiting | Number <br> Entering | Number <br> Exiting |
|  | Trips |  |  | 496 | 496 |
| Weekday | 992 | 50 | 50 | 19 | 57 |
| A.M. Peak | 76 | 25 | 75 | 64 | 38 |
| P.M. Peak | 102 | 63 | 37 |  |  |
|  |  |  |  |  |  |

The directional distribution of the traffic generated by the proposed Dutchtown Road Subdivision was determined using the traffic data collected for the existing conditions. The typical weekday traffic pattern is for traffic to flow heavier in one direction in the morning peak period and then for the traffic to be heavier in the opposite direction during the evening peak period. Dutchtown Road at the proposed Project Entrance had a trip distribution of $55 \%$ Eastbound and $45 \%$ Westbound during the AM peak hour and 65\% Eastbound and 35\% Westbound during the PM peak hour. Mabry Hood Road had a trip distribution of 90\% Westbound right turns and $10 \%$ Eastbound left turns during the AM peak hour and $75 \%$ Westbound right turns and $25 \%$ Eastbound left turns during the PM peak hour. The trip distribution for the Dutchtown Road Subdivision is shown in Figure 5 and Figure 6.



Using the existing trip distribution the trips generated from the Dutchtown Road Subdivision are shown in Figure 7. Figure 8 shows the combined peak hour traffic from the background growth and the full build out of the Dutchtown Road Subdivision.

The existing trip distribution shown in Figure 5 and Figure 6 was used in combination with the trip generation to calculate the proposed traffic at the intersection of Rennboro Road and Dutchtown Road. Figure 9 shows the combined traffic of the Dutchtown Road Subdivision and the Rennboro Road Subdivision.

## 5 Projected Capacity and Level of Service

Unsignalized intersection capacity analyses were performed for the AM and PM peak hours to evaluate the traffic conditions at the intersections of Dutchtown Road and Mabry Hood Road, the intersection of Dutchtown Road and the proposed project entrance and the intersection of Dutchtown Road and Rennboro Road.

The results from the analyses are measured with a term "level of service" (LOS), which is based on the amount of delay experienced at the intersection. The LOS index ranges from LOS A, indicating excellent traffic conditions with minimal delay, to LOS F indicating very congested conditions with excessive delay. LOS D generally is considered the minimum acceptable condition in urban areas. Table 51 shows the results of the capacity analyses.


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## Table 5-1

Intersection Analysis
Level of Service (LOS) Summary

|  |  | Delay (sec |
| :---: | :---: | :---: |
|  | n Road | Hood Road |
| AM Peak | EB L | 9.5 / A |
|  | WB L | 10.1 / B |
|  | NB | 96.2 / F |
|  | SB | 132.5 / F |
| PM Peak | EB L | 9.5 / A |
|  | WB L | 8.8 / A |
|  | NB | 84.5 / F |
|  | SB | 189.6 / F |
|  | @ Ma | Road (Ba |
| AM Peak | EB L | 9.8 / A |
|  | WB L | 10.6 / B |
|  | NB | 280.8 / F |
|  | SB | 251.9 / F |
| PM Peak | EB L | 10.0 / A |
|  | WB L | 9.0 / A |
|  | NB | 148.7 / F |
|  | SB | 394.9 / F |
| Dutchtown Road @ Mabry Hood Road (Background Growth + Full Buildout 2018) |  |  |
| AM Peak | EB L | 10.2 / B |
|  | WB L | 10.7 / B |
|  | NB | 512.5 / F |
|  | SB | 327.9 / F |
| PM Peak | EB L | 10.2 / B |
|  | WB L | 9.1 / A |
|  | NB | 186.9 / F |
|  | SB | 539.1 / F |


| Dutchtown Road @ Project Entrance (Background Growth + Full Buildout 2018) |  |  |
| :--- | :---: | :--- |
| AM Peak | EB L | $9.4 / \mathrm{A}$ |
|  | SB LTR | $16.9 / \mathrm{C}$ |
| PM Peak | EB L | $8.5 / \mathrm{A}$ |
|  | SB LTR | $13.6 / \mathrm{B}$ |
| Dutchtown Road @ Rennboro Road (Background Growth + Full Buildout 2018) |  |  |
| AM Peak | EB L | $9.4 / \mathrm{A}$ |
|  | SB LTR | $18.7 / \mathrm{C}$ |
| PM Peak | EB L | $8.5 / \mathrm{A}$ |
|  | SB LTR | $15.4 / \mathrm{C}$ |

## 6 Turn Lane Warrant Analysis

The intersection of Dutchtown Road and the Project Entrance was evaluated to determine if a westbound right turn lane or an eastbound left turn on Dutchtown Road was warranted. The Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy," was used to analyze the information. A westbound right turn lane on Dutchtown Road is not warranted during the AM or PM peak hour. An eastbound left turn on Dutchtown Road is warranted during the PM peak hour. The turn lane warrant worksheets and analysis are included in Attachment 7.

## 7 Signal Warrant Analysis

The intersection of Dutchtown Road and the proposed project entrance was evaluated to determine if signalization was warranted for the proposed traffic generated by the Dutchtown Road Subdivision. Warrants for traffic signals can be found in Chapter 4C of the 2003 Manual on Uniform Traffic Control Devices (MUTCD), published by the Federal Highway Administration (FHWA). There are three volume-based warrants that were evaluated.

- Warrant 1, Eight-Hour Vehicular Volume
- Warrant 2, Four-Hour Vehicular Volume
- Warrant 3, Peak Hour

Signal Warrants 1 eight-hr vehicular volume, 2 four-hr vehicular volume and 3 peak hour were not met after the full build out of the Dutchtown Road Subdivision. The signal warrant worksheet is included in Attachment 8.

## 8 Conclusions and Recommendations

### 8.1 Dutchtown Road @ Mabry Hood Road

At the intersection of Dutchtown Road and Mabry Hood Road, all eastbound and westbound approaches currently operate at an acceptable LOS A or B during both the AM and PM peak hour. The eastbound and westbound approach will continue to operate at a LOS B or higher after the completion of the Dutchtown Road Subdivision.

At the intersection of Dutchtown Road and Mabry Hood Road, all northbound and southbound approaches currently operate at a LOS F during both the AM and PM peak hour. The northbound and southbound approach will continue to operate at a LOS F after the completion of the Dutchtown Road Subdivision.

FMA recommends that the crash data at this intersection be monitored.

### 8.2 Dutchtown Road @ Project Entrance

Dutchtown Road is classified as a minor arterial. The minimum intersection spacing required for an arterial is 400 feet per the "Minimum Subdivision Regulations" for Knoxville and Knox County. The nearest road intersection to the project entrance is currently 385 feet east at the intersection of Dutchtown Road and Rennboro Road. This intersection does not meet the recommended minimum separation of 400 feet between roads on an arterial.

An eastbound left turn lane is warranted at the intersection of Dutchtown Road and the proposed project entrance. The Unsignalized intersection capacity analyses shows a $95 \%$ queue length for the eastbound left turning movement of less than one car length during both the AM and PM peak hour; therefore, the existing two-way left turn lane has adequate storage. FMA recommends the two way left turn lane be restriped to include a break at the intersection of Dutchtown Road and the project entrance.

A westbound right turn lane is not warranted at the intersection of Dutchtown Road and the proposed project entrance.

The minimum required sight distance for a road with a posted speed limit of 40 mph is 400 feet in each direction in accordance with the "Minimum Subdivision Regulations" for Knoxville and Knox County. The proposed intersection of Dutchtown Road and the project entrance has a measured sight distance that exceeds 400 - ft east and west of the intersection, which meets the requirement. FMA recommends any necessary landscaping that may be involved to maintain this sight distance and continue to comply with Knox County Engineering \& Public Works.

The southbound approach of the proposed intersection of Dutchtown Road and the project entrance is expected to operate at a LOS C during the AM peak hour and a LOS B during PM peak hour after the completion of the Dutchtown Road Subdivision. The Unsignalized intersection capacity analyses shows a $95 \%$ queue length for the southbound approach of less than one car length during both the AM and PM peak hours; therefore, the proposed geometry of one $13-\mathrm{ft}$ lane exiting the subdivision will be adequate.

A signal is not warranted after the full build out of the Dutchtown Road Subdivision.

### 8.3 Dutchtown Road @ Rennboro Road

The intersection of Dutchtown Road and Rennboro Road is expected to operate at a LOS C or better during both the AM and PM peak hours after the full build out of the Dutchtown Road Subdivision. The Unsignalized intersection capacity analyses shows a $95 \%$ queue length for the eastbound left turn lane of less than one car length during both the AM and PM peak hours; therefore, the existing left turn lane with a 150-ft storage length entering Rennboro Road will be adequate and will not interfere with the Dutchtown Road Subdivision.

Attachment 1
Traffic Counts

Project: Dutchtown Road Subdivision
Date Conducted: 8/25/2015

|  | Dutchtown Road Eastbound |  |  |  | Dutchtown Road Westbound |  |  |  | Mabry Hood Road Northbound |  |  |  | Mabry Hood Road Southbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Int. Total |
| 7:00 AM | 6 | 52 | 2 | 60 | 0 | 50 | 2 | 52 | 1 | 0 | 1 | 2 | 4 | 2 | 72 | 78 | 192 |
| 7:15 AM | 7 | 110 | 0 | 117 | 2 | 96 | 5 | 103 | 1 | 0 | 0 | 1 | 17 | 5 | 84 | 106 | 327 |
| 7:30 AM | 9 | 211 | 2 | 222 | 2 | 116 | 7 | 125 | 3 | 0 | 1 | 4 | 18 | 4 | 123 | 145 | 496 |
| 7:45 AM | 15 | 241 | 0 | 256 | 5 | 172 | 7 | 184 | 1 | 0 | 6 | 7 | 13 | 6 | 122 | 141 | 588 |
| Total | 37 | 614 | 4 | 655 | 9 | 434 | 21 | 464 | 6 | 0 | 8 | 14 | 52 | 17 | 401 | 470 | 1603 |
| 8:00 AM | 20 | 121 | 1 | 142 | 1 | 154 | 11 | 166 | 2 | 1 | 0 | 3 | 7 | 9 | 110 | 126 | 437 |
| 8:15 AM | 18 | 101 | 3 | 122 | 2 | 97 | 6 | 105 | 1 | 0 | 1 | 2 | 4 | 7 | 78 | 89 | 318 |
| 8:30 AM | 14 | 68 | 1 | 83 | 2 | 70 | 5 | 77 | 0 | 0 | 0 | 0 | 4 | 4 | 67 | 75 | 235 |
| 8:45 AM | 11 | 40 | 0 | 51 | 0 | 84 | 6 | 90 | 2 | 0 | 0 | 2 | 1 | 4 | 45 | 50 | 193 |
| Total | 63 | 330 | 5 | 398 | 5 | 405 | 28 | 438 | 5 | 1 | 1 | 7 | 16 | 24 | 300 | 340 | 1183 |
| 11:00 AM | 13 | 40 | 0 | 53 | 1 | 32 | 3 | 36 | 2 | 2 | 0 | 4 | 1 | 2 | 8 | 11 | 104 |
| 11:15 AM | 21 | 39 | 0 | 60 | 0 | 26 | 5 | 31 | 0 | 1 | 0 | 1 | 1 | 2 | 20 | 23 | 115 |
| 11:30 AM | 28 | 56 | 0 | 84 | 1 | 45 | 4 | 50 | 0 | 1 | 1 | 2 | 2 | 5 | 21 | 28 | 164 |
| 11:45 AM | 21 | 51 | 2 | 74 | 2 | 49 | 6 | 57 | 3 | 3 | 2 | 8 | 1 | 0 | 28 | 29 | 168 |
| Total | 83 | 186 | 2 | 271 | 4 | 152 | 18 | 174 | 5 | 7 | 3 | 15 | 5 | 9 | 77 | 91 | 551 |
| 12:00 PM | 32 | 61 | 1 | 94 | 2 | 42 | 6 | 50 | 0 | 0 | 1 | 1 | 4 | 3 | 13 | 20 | 165 |
| 12:15 PM | 26 | 51 | 1 | 78 | 0 | 39 | 3 | 42 | 1 | 3 | 1 | 5 | 0 | 2 | 31 | 33 | 158 |
| 12:30 PM | 20 | 45 | 0 | 65 | 0 | 54 | 9 | 63 | 1 | 2 | 3 | 6 | 1 | 3 | 30 | 34 | 168 |
| 12:45 PM | 13 | 50 | 1 | 64 | 2 | 46 | 7 | 55 | 0 | 0 | 1 | 1 | 3 | 4 | 38 | 45 | 165 |
| Total | 91 | 207 | 3 | 301 | 4 | 181 | 25 | 210 | 2 | 5 | 6 | 13 | 8 | 12 | 112 | 132 | 656 |
| 2:00 PM | 19 | 56 | 4 | 79 | 0 | 45 | 4 | 49 | 1 | 1 | 1 | 3 | 5 | 6 | 26 | 37 | 168 |
| 2:15 PM | 19 | 66 | 2 | 87 | 0 | 45 | 2 | 47 | 3 | 1 | 0 | 4 | 6 | 0 | 24 | 30 | 168 |
| 2:30 PM | 23 | 90 | 1 | 114 | 0 | 37 | 7 | 44 | 0 | 1 | 1 | 2 | 2 | 4 | 30 | 36 | 196 |
| 2:45 PM | 24 | 111 | 1 | 136 | 2 | 51 | 10 | 63 | 0 | 0 | 3 | 3 | 4 | 3 | 21 | 28 | 230 |
| Total | 85 | 323 | 8 | 416 | 2 | 178 | 23 | 203 | 4 | 3 | 5 | 12 | 17 | 13 | 101 | 131 | 762 |
| 3:00 PM | 30 | 124 | 1 | 155 | 4 | 38 | 10 | 52 | 1 | 0 | 1 | 2 | 4 | 1 | 24 | 29 | 238 |
| 3:15 PM | 19 | 98 | 2 | 119 | 0 | 116 | 13 | 129 | 3 | 0 | 1 | 4 | 2 | 5 | 22 | 29 | 281 |
| 3:30 PM | 35 | 83 | 1 | 119 | 1 | 205 | 13 | 219 | 1 | 3 | 3 | 7 | 4 | 0 | 19 | 23 | 368 |
| 3:45 PM | 35 | 68 | 4 | 107 | 1 | 105 | 12 | 118 | 2 | 2 | 2 | 6 | 9 | 4 | 26 | 39 | 270 |
| Total | 119 | 373 | 8 | 500\| | 6 | 464 | 48 | 518 | 7 | 5 | 7 | 19 | 19 | 10 | 91 | 120 | 1157 |
| 4:00 PM | 42 | 71 | 1 | 114 | 1 | 62 | 7 | 70 | 1 | 2 | 2 | 5 | 5 | 7 | 20 | 32 | 221 |
| 4:15 PM | 36 | 73 | 1 | 110 | 4 | 43 | 12 | 59 | 2 | 6 | 2 | 10 | 7 | 4 | 20 | 31 | 210 |
| 4:30 PM | 56 | 95 | 4 | 155 | 1 | 59 | 8 | 68 | 0 | 0 | 4 | 4 | 9 | 2 | 32 | 43 | 270 |
| 4:45 PM | 56 | 108 | 0 | 164 | 0 | 60 | 10 | 70 | 0 | 2 | 1 | 3 | 7 | 1 | 28 | 36 | 273 |
| Total | 190 | 347 | 6 | 543 | 6 | 224 | 37 | 267 | 3 | 10 | 9 | 22 | 28 | 14 | 100 | 142 | 974 |
| 5:00 PM | 90 | 151 | 5 | 246 | 1 | 67 | 20 | 88 | 2 | 3 | 4 | 9 | 7 | 5 | 30 | 42 | 385 |
| 5:15 PM | 83 | 139 | 0 | 222 | 0 | 84 | 16 | 100 | 2 | 1 | 0 | 3 | 15 | 1 | 31 | 47 | 372 |
| 5:30 PM | 74 | 136 | 2 | 212 | 2 | 77 | 20 | 99 | 2 | 3 | 4 | 9 | 7 | 2 | 35 | 44 | 364 |
| 5:45 PM | 67 | 152 | 2 | 221 |  | 45 | 9 | 54 | 3 | 3 | 2 | 8 | 10 | 2 | 27 | 39 | 322 |
| Total | 314 | 578 | 9 | 901 | 3 | 273 | 65 | 341 | 9 | 10 | 10 | 29 | 39 | 10 | 123 | 172 | 1443 |


| Grand Total | 982 | 2958 | 45 | 3985 | 39 | 2311 | 265 | 2615 | 41 | 41 | 49 | 131 | 184 | 109 | 1305 | 1598 | 8329 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Apprach \% | 24.6 | 74.2 | 1.1 |  | 1.5 | 88.4 | 10.1 |  | 31.3 | 31.3 | 37.4 |  | 11.5 | 6.8 | 81.7 | 19.2 |  |
| Total \% | 11.8 | 35.5 | 0.5 | 47.8 | 0.5 | 27.7 | 3.2 | 31.4 | 0.5 | 0.5 | 0.6 | 1.6 | 2.2 | 1.3 | 15.7 | 19.2 |  |

## Project: Dutchtown Road Subdivision

Date Conducted: 8/25/2015

| AM Peak Hour | $7: 15-8: 15$ | 1848 |
| :--- | :---: | ---: |
| Lunch Peak Hour | $11: 45-12: 45$ | 659 |
| PM Peak Hour | $5: 00-6: 00$ | 1443 |


|  | Dutchtown Road Eastbound |  |  |  | Dutchtown Road Westbound |  |  |  | Mabry Hood Road Northbound |  |  |  | Mabry Hood Road Southbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis from 7:00 AM to 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hour begins at 7:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:15 AM | 7 | 110 | 0 | 117 | 2 | 96 | 5 | 103 | 1 | 0 | 0 | 1 | 17 | 5 | 84 | 106 | 327 |
| 7:30 AM | 9 | 211 | 2 | 222 | 2 | 116 | 7 | 125 | 3 | 0 | 1 | 4 | 18 | 4 | 123 | 145 | 496 |
| 7:45 AM | 15 | 241 | 0 | 256 | 5 | 172 | 7 | 184 | 1 | 0 | 6 | 7 | 13 | 6 | 122 | 141 | 588 |
| 8:00 AM | 20 | 121 | 1 | 142 | 1 | 154 | 11 | 166 | 2 | 1 | 0 | 3 | 7 | 9 | 110 | 126 | 437 |
| Total Volume | 51 | 683 | 3 | 737 | 10 | 538 | 30 | 578 | 7 | 1 | 7 | 15 | 55 | 24 | 439 | 518 | 1848 |
| Future (3\% over 3 yrs) | 56 | 746 | 3 |  | 11 | 588 | 33 |  | 8 | 1 | 8 |  | 60 | 26 | 480 |  | 2019 |
| PHF | 0.64 | 0.71 | 0.38 |  | 0.50 | 0.78 | 0.68 |  | 0.58 | 0.25 | 0.29 |  | 0.76 | 0.67 | 0.89 |  | 0.79 |


| Peak Hour Analysis from 11:00 AM to 1:00 PM |
| :--- | :--- |

Lunch Peak Hour begins at 11:45 PM

| 11:45 AM | 21 | 51 | 2 | 74 | 2 | 49 | 6 | 57 | 3 | 3 | 2 | 8 | 1 | 0 | 28 | 29 | 168 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12:00 PM | 32 | 61 | 1 | 94 | 2 | 42 | 6 | 50 | 0 | 0 | 1 | 1 | 4 | 3 | 13 | 20 | 165 |
| 12:15 PM | 26 | 51 | 1 | 78 | 0 | 39 | 3 | 42 | 1 | 3 | 1 | 5 | 0 | 2 | 31 | 33 | 158 |
| 12:30 PM | 20 | 45 | 0 | 65 | 0 | 54 | 9 | 63 | 1 | 2 | 3 | 6 | 1 | 3 | 30 | 34 | 168 |
| Total Volume | 99 | 208 | 4 | 311 | 4 | 184 | 24 | 212 | 5 | 8 | 7 | 20 | 6 | 8 | 102 | 116 | 659 |
| Future (3\% over 3 yrs ) | 108 | 227 | 4 |  | 4 | 201 | 26 |  | 5 | 9 | 8 |  | 7 | 9 | 111 |  | 720 |
| PHF | 0.77 | 0.85 | 0.50 |  | 0.50 | 0.85 | 0.67 |  | 0.42 | 0.67 | 0.58 |  | 0.38 | 0.67 | 0.82 |  | 0.98 |

Peak Hour Analysis from 2:00 PM to 6:00 PM
PM Peak Hour begins at 5:00 PM

| 5:00 PM | 90 | 151 | 5 | 246 | 1 | 67 | 20 | 88 | 2 | 3 | 4 | 9 | 7 | 5 | 30 | 42 | 385 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5:15 PM | 83 | 139 | 0 | 222 | 0 | 84 | 16 | 100 | 2 | 1 | 0 | 3 | 15 | 1 | 31 | 47 | 372 |
| 5:30 PM | 74 | 136 | 2 | 212 | 2 | 77 | 20 | 99 | 2 | 3 | 4 | 9 | 7 | 2 | 35 | 44 | 364 |
| 5:45 PM | 67 | 152 | 2 | 221 | 0 | 45 | 9 | 54 | 3 | 3 | 2 | 8 | 10 | 2 | 27 | 39 | 322 |
| Total Volume | 314 | 578 | 9 | 901 | 3 | 273 | 65 | 341 | 9 | 10 | 10 | 29 | 39 | 10 | 123 | 172 | 1443 |
| Future (3\% over 3 yrs ) | 343 | 632 | 10 |  | 3 | 298 | 71 |  | 10 | 11 | 11 |  | 43 | 11 | 134 |  | 1577 |
| PHF | 0.87 | 0.95 | 0.45 |  | 0.38 | 0.81 | 0.81 |  | 0.75 | 0.83 | 0.63 |  | . 65 | 0.50 | 0.88 |  | 0.94 |

Attachment 2
ADT Trends


Most Recent Trend Line Growth

| Year | ADT |
| :---: | :---: |
| 2000 | 6944 |
| 2014 | 7469 |

## Annual Average Daily Traffic County Summary

| Count Year | Count Station M56 <br> Dutchtown Rd <br> 200' W of Mabry Hood Rd | Count Station M271 <br> Mabry Hood Rd <br> S of Dutchtown Rd |
| :---: | :---: | :---: |
| 2010 | 10090 | 0 |
| 2011 | 10280 | 450 |
| 2012 | 10290 | 0 |
| 2013 | 12640 | 550 |

Growth Rate

Attachment 3
Trip Generation




Attachment 4
Intersection Worksheet
Existing AM/PM Peaks

| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :--- | :--- | :--- | :--- |
| General Information | Site Information |  |  |
| Analyst | Addie Kirkham | Intersection | Dutchtown @ Mabry Hood |
| Agency/Co. | FMA | Knox County |  |
| Jurisdiction | 2015 |  |  |
| Analysis Year |  |  |  |
| Date Performed | $8 / 27 / 2015$ |  |  |
| Analysis Time Period | AM Peak |  |  |
| Project Description 330.010 Dutchtown Road Subdivision |  |  |  |
| East/West Street: Dutchtown Road | North/South Street: | Mabry Hood Road |  |
| Intersection Orientation: East-West | Study Period (hrs): 0.25 |  |  |

Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 51 | 683 | 3 | 10 | 538 | 30 |
| Peak-Hour Factor, PHF | 0.64 | 0.71 | 0.38 | 0.50 | 0.78 | 0.68 |
| Hourly Flow Rate, HFR (veh/h) | 79 | 961 | 7 | 20 | 689 | 44 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 2 | 0 | 1 | 1 | 0 |
| Configuration | L | T | TR | L |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 7 | 1 | 7 | 55 | 24 |  |
| Peak-Hour Factor, PHF | 0.58 | 0.25 | 0.29 | 0.76 | 0.67 | 0.89 |
| Hourly Flow Rate, HFR (veh/h) | 12 | 4 | 24 | 72 | 35 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 1 |
| Lanes | 1 | 1 | 0 | 1 | 1 | 0 |
| Configuration | L |  | TR | L | T |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L | L | L |  | TR | L | T |  |
| $v$ (veh/h) | 79 | 20 | 12 |  | 28 | 72 | 35 |  |
| C (m) (veh/h) | 881 | 720 | 23 |  | 266 | 86 | 64 |  |
| v/c | 0.09 | 0.03 | 0.52 |  | 0.11 | 0.84 | 0.55 |  |
| 95\% queue length | 0.29 | 0.09 | 1.54 |  | 0.35 | 4.39 | 2.24 |  |
| Control Delay (s/veh) | 9.5 | 10.1 | 273.7 |  | 20.1 | 141.0 | 115.0 |  |
| LOS | A | B | F |  | C | $F$ | $F$ |  |
| Approach Delay (s/veh) | -- | -- | 96.2 |  |  | 132.5 |  |  |
| Approach LOS | -- | -- | F |  |  | $F$ |  |  |



Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 314 | 578 | 9 | 3 | 273 | 65 |
| Peak-Hour Factor, PHF | 0.87 | 0.95 | 0.45 | 0.38 | 0.81 | 0.81 |
| Hourly Flow Rate, HFR (veh/h) | 360 | 608 | 20 | 7 | 337 | 80 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 2 | 0 | 1 | 1 | 0 |
| Configuration | L | T | TR | L |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 9 | 10 | 10 | 39 | 10 |  |
| Peak-Hour Factor, PHF | 0.75 | 0.83 | 0.63 | 0.65 | 0.50 | 0.88 |
| Hourly Flow Rate, HFR (veh/h) | 12 | 12 | 15 | 60 | 20 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 1 | 0 | 1 | 1 | 0 |
| Configuration | L |  | TR | L | T |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L | L | L |  | TR | L | T |  |
| $v$ (veh/h) | 360 | 7 | 12 |  | 27 | 60 | 20 |  |
| C (m) (veh/h) | 1153 | 964 | 32 |  | 117 | 61 | 60 |  |
| v/c | 0.31 | 0.01 | 0.38 |  | 0.23 | 0.98 | 0.33 |  |
| 95\% queue length | 1.34 | 0.02 | 1.21 |  | 0.84 | 4.68 | 1.21 |  |
| Control Delay (s/veh) | 9.5 | 8.8 | 173.8 |  | 44.8 | 222.0 | 92.5 |  |
| LOS | A | A | $F$ |  | E | $F$ | $F$ |  |
| Approach Delay (s/veh) | -- | -- | 84.5 |  |  | 189.6 |  |  |
| Approach LOS | -- | -- | F |  |  | F |  |  |

Attachment 5
Intersection Worksheet Background AM/PM Peaks

| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | Addie Kirkham | Intersection | Dutchtown @ Mabry Hood |
| Agency/Co. | FMA | Jurisdiction | Knox County |
| Date Performed | 8/27/2015 | Analysis Year | 2018 |
| Analysis Time Period | Background AM Peak |  |  |
| Project Description 330.010 Dutchtown Road Subdivision |  |  |  |
| East/West Street: Dutchtown Road |  | North/South Street: Mabry Hood Road |  |
| Intersection Orientation: East-West |  | Study Period (hrs): 0.25 |  |

Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 56 | 746 | 3 | 11 | 588 | 33 |
| Peak-Hour Factor, PHF | 0.64 | 0.71 | 0.38 | 0.50 | 0.78 | 0.68 |
| Hourly Flow Rate, HFR (veh/h) | 87 | 1050 | 7 | 22 | 753 | 48 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 2 | 0 | 1 | 1 | 0 |
| Configuration | L | T | TR | L |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 8 | 1 | 8 | 60 | 26 |  |
| Peak-Hour Factor, PHF | 0.58 | 0.25 | 0.29 | 0.76 | 0.67 | 0.89 |
| Hourly Flow Rate, HFR (veh/h) | 13 | 4 | 27 | 78 | 38 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 1 | 0 | 1 | 1 | 0 |
| Configuration | L |  | TR | L | T |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L | L | L |  | TR | L | T |  |
| $v$ (veh/h) | 87 | 22 | 13 |  | 31 | 78 | 38 |  |
| C (m) (veh/h) | 831 | 667 | 10 |  | 235 | 66 | 48 |  |
| v/c | 0.10 | 0.03 | 1.30 |  | 0.13 | 1.18 | 0.79 |  |
| 95\% queue length | 0.35 | 0.10 | 2.40 |  | 0.45 | 6.21 | 3.20 |  |
| Control Delay (s/veh) | 9.8 | 10.6 | 896.3 |  | 22.6 | 275.6 | 203.2 |  |
| LOS | A | B | F |  | C | F | F |  |
| Approach Delay (s/veh) | -- | -- | 280.8 |  |  | 251.9 |  |  |
| Approach LOS | -- | -- | F |  |  | F |  |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :--- | :--- | :--- | :--- |
| General Information | Site Information |  |  |
| Analyst | Addie Kirkham | \|ntersection | Dutchtown @ Mabry Hood |
| Agency/Co. | FMA | Knox County |  |
| Jurisdiction | 2018 |  |  |
| Analysis Year |  |  |  |
| Date Performed | $8 / 27 / 2015$ |  |  |
| Analysis Time Period | Background PM Peak |  |  |
| Project Description 330.010 Dutchtown Road Subdivision |  |  |  |
| East/West Street: Dutchtown Road | North/South Street: | Mabry Hood Road |  |
| Intersection Orientation: East-West | Study Period (hrs): 0.25 |  |  |

Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 343 | 632 | 10 | 3 | 298 | 71 |
| Peak-Hour Factor, PHF | 0.87 | 0.95 | 0.45 | 0.38 | 0.81 | 0.81 |
| Hourly Flow Rate, HFR (veh/h) | 394 | 665 | 22 | 7 | 367 | 87 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 2 | 0 | 1 | 1 | 0 |
| Configuration | L | T | TR | L |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 10 | 11 | 11 | 43 | 11 |  |
| Peak-Hour Factor, PHF | 0.75 | 0.83 | 0.63 | 0.65 | 0.50 | 0.88 |
| Hourly Flow Rate, HFR (veh/h) | 13 | 13 | 17 | 66 | 22 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 1 | 0 | 1 | 1 | 0 |
| Configuration | L |  | TR | L | T |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L | L | L |  | TR | L | T |  |
| $v$ (veh/h) | 394 | 7 | 13 |  | 30 | 66 | 22 |  |
| C (m) (veh/h) | 1117 | 916 | 20 |  | 92 | 43 | 45 |  |
| v/c | 0.35 | 0.01 | 0.65 |  | 0.33 | 1.53 | 0.49 |  |
| 95\% queue length | 1.61 | 0.02 | 1.81 |  | 1.25 | 6.62 | 1.77 |  |
| Control Delay (s/veh) | 10.0 | 9.0 | 348.8 |  | 62.0 | 478.0 | 145.6 |  |
| LOS | A | A | $F$ |  | $F$ | $F$ | $F$ |  |
| Approach Delay (s/veh) | -- | -- | 148.7 |  |  | 394.9 |  |  |
| Approach LOS | -- | -- | F |  |  | $F$ |  |  |

## Attachment 6 <br> Intersection Worksheet <br> Background AM/PM Peaks + Development

| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | Addie Kirkham | Intersection | Dutchtown @ Mabry Hood |
| Agency/Co. | FMA | Jurisdiction | Knox County |
| Date Performed | 8/27/2015 | Analysis Year | 2018 |
| Analysis Time Period | Full Buildout AM Peak |  |  |
| Project Description 330.010 Dutchtown Road Subdivision |  |  |  |
| East/West Street: Dutchtown Road |  | North/South Street: Mabry Hood Road |  |
| Intersection Orientation: East-West |  | Study Period (hrs): 0.25 |  |

Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 56 | 755 | 3 | 11 | 636 | 36 |
| Peak-Hour Factor, PHF | 0.64 | 0.71 | 0.38 | 0.50 | 0.78 | 0.68 |
| Hourly Flow Rate, HFR (veh/h) | 87 | 1063 | 7 | 22 | 815 | 52 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 2 | 0 | 1 | 1 | 0 |
| Configuration | L | T | TR | L |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 8 | 1 | 8 | 61 | 26 |  |
| Peak-Hour Factor, PHF | 0.58 | 0.25 | 0.29 | 0.76 | 0.67 | 0.89 |
| Hourly Flow Rate, HFR (veh/h) | 13 | 4 | 27 | 80 | 38 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 1 | 0 | 1 | 1 | 0 |
| Configuration | L |  | TR | L | T |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L | L | L |  | TR | L | T |  |
| v (veh/h) | 87 | 22 | 13 |  | 31 | 80 | 38 |  |
| C (m) (veh/h) | 785 | 659 | 6 |  | 215 | 58 | 43 |  |
| v/c | 0.11 | 0.03 | 2.17 |  | 0.14 | 1.38 | 0.88 |  |
| 95\% queue length | 0.37 | 0.10 | 2.69 |  | 0.49 | 7.02 | 3.48 |  |
| Control Delay (s/veh) | 10.2 | 10.7 | 1676 |  | 24.5 | 366.4 | 246.9 |  |
| LOS | B | B | F |  | C | F | F |  |
| Approach Delay (s/veh) | -- | -- | 512.5 |  |  | 327.9 |  |  |
| Approach LOS | -- | -- | F |  |  | $F$ |  |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :--- | :--- | :--- | :--- |
| General Information | Site Information |  |  |
| Analyst | Addie Kirkham | Intersection | Dutchtown @ Mabry Hood |
| Agency/Co. | FMA | Knox County |  |
| Jurisdiction | 2018 |  |  |
| Analysis Year |  |  |  |
| Date Performed | $8 / 27 / 2015$ |  |  |
| Analysis Time Period | Full Buildout PM Peak |  |  |
| Project Description 330.010 Dutchtown Road Subdivision |  |  |  |
| East/West Street: Dutchtown Road | North/South Street: | Mabry Hood Road |  |
| Intersection Orientation: East-West | Study Period (hrs): 0.25 |  |  |

Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 343 | 670 | 10 | 3 | 321 | 77 |
| Peak-Hour Factor, PHF | 0.87 | 0.95 | 0.45 | 0.38 | 0.81 | 0.81 |
| Hourly Flow Rate, HFR (veh/h) | 394 | 705 | 22 | 7 | 396 | 95 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 2 | 0 | 1 | 1 | 0 |
| Configuration | L | T | TR | L |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 10 | 11 | 12 | 46 | 11 |  |
| Peak-Hour Factor, PHF | 0.75 | 0.83 | 0.63 | 0.65 | 0.50 | 0.88 |
| Hourly Flow Rate, HFR (veh/h) | 13 | 13 | 19 | 70 | 22 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 1 | 0 | 1 | 1 | 0 |
| Configuration | L |  | TR | L | T |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L | L | L |  | TR | L | T |  |
| $v$ (veh/h) | 394 | 7 | 13 |  | 32 | 70 | 22 |  |
| C (m) (veh/h) | 1083 | 886 | 16 |  | 87 | 37 | 40 |  |
| v/c | 0.36 | 0.01 | 0.81 |  | 0.37 | 1.89 | 0.55 |  |
| 95\% queue length | 1.68 | 0.02 | 2.03 |  | 1.44 | 7.59 | 1.96 |  |
| Control Delay (s/veh) | 10.2 | 9.1 | 477.7 |  | 68.7 | 653.8 | 174.1 |  |
| LOS | B | A | F |  | $F$ | $F$ | $F$ |  |
| Approach Delay (s/veh) | -- | -- | 186.9 |  |  | 539.1 |  |  |
| Approach LOS | -- | -- | F |  |  | $F$ |  |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  | Site Information |  |  |  |  |  |  |
| Analyst Addie Kirkham |  |  | Intersection |  |  | Dutchtown @ Project Entrance |  |  |  |
| Agency/Co. | FMA |  | Jurisdiction |  |  | Knox County |  |  |  |
| Date Performed | 8/27/2015 |  |  |  |  | 2018 |  |  |  |
| Analysis Time Period | AM Peak |  |  |  |  |  |  |  |  |
| Project Description 330.010 Dutchtown Road Subdivision |  |  |  |  |  |  |  |  |  |
| East/West Street: Dutchtown Road |  |  | North/South Street: Project Entrance |  |  |  |  |  |  |
| Intersection Orientation: East-West | East-West |  | Study Period (hrs): 0.25 |  |  |  |  |  |  |
| Vehicle Volumes and Adjustments |  |  |  |  |  |  |  |  |  |
| Major Street | Eastbound |  |  |  | Westbound |  |  |  |  |
| Movement | 1 | 2 | 3 |  | 4 | 5 |  | 6 |  |
|  | L | T | R |  | L | T |  | R |  |
| Volume (veh/h) | 10 | 814 |  |  |  | 683 |  | 9 |  |
| Peak-Hour Factor, PHF | 0.85 | 0.85 | 1.00 |  | 1.00 | 0.85 |  | 0.85 |  |
| Hourly Flow Rate, HFR (veh/h) | 11 | 957 | 0 |  | 0 | 803 |  | 10 |  |
| Percent Heavy Vehicles | 0 | -- | -- |  | 0 | -- |  | -- |  |
| Median Type | Two Way Left Turn Lane |  |  |  |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  |  |  | 0 |  |
| Lanes | 1 | 1 | 0 |  | 0 | 1 |  | 0 |  |
| Configuration | L | T |  |  |  |  |  | TR |  |
| Upstream Signal |  | 0 |  |  |  | 0 |  |  |  |
| Minor Street | Northbound |  |  |  | Southbound |  |  |  |  |
| Movement | 7 | 8 | 9 |  | 10 | 11 |  | 12 |  |
|  | L | T | R |  | L | T |  | R |  |
| Volume (veh/h) |  |  |  |  | 6 |  |  | 51 |  |
| Peak-Hour Factor, PHF | 1.00 | 1.00 | 1.00 |  | 0.85 | 1.00 |  | 0.85 |  |
| Hourly Flow Rate, HFR (veh/h) | 0 | 0 | 0 |  | 7 | 0 |  | 59 |  |
| Percent Heavy Vehicles | 0 | 0 | 0 |  | 0 | 0 |  | 0 |  |
| Percent Grade (\%) | 0 |  |  |  | 0 |  |  |  |  |
| Flared Approach | N |  |  |  |  | $N$ |  |  |  |
| Storage |  | 0 |  |  |  | 0 |  |  |  |
| RT Channelized |  |  | 0 |  |  |  |  | 0 |  |
| Lanes | 0 | 0 | 0 |  | 0 | 0 |  | 0 |  |
| Configuration |  |  |  |  |  | LR |  |  |  |
| Delay, Queue Length, and Level of Service |  |  |  |  |  |  |  |  |  |
| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |  |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 |  | 12 |
| Lane Configuration | L |  |  |  |  |  | LR |  |  |
| v (veh/h) | 11 |  |  |  |  |  | 66 |  |  |
| C (m) (veh/h) | 823 |  |  |  |  |  | 369 |  |  |
| v/c | 0.01 |  |  |  |  |  | 0.18 |  |  |
| 95\% queue length | 0.04 |  |  |  |  |  | 0.64 |  |  |
| Control Delay (s/veh) | 9.4 |  |  |  |  |  | 16.9 |  |  |
| LOS | A |  |  |  |  |  | C |  |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 16.9 |  |  |
| Approach LOS | -- | -- |  |  |  |  | C |  |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  | Site Information |  |  |  |  |  |  |
| Analyst Addie Kirkham |  |  | Intersection |  |  | Dutchtown @ Project Entrance |  |  |  |
| Agency/Co. | FMA |  | Jurisdiction |  |  | Knox County |  |  |  |
| Date Performed | 8/27/2015 |  | Analysis Year |  |  |  |  |  |  |
| Analysis Time Period | PM Pe |  | Analys | -ar |  | 2018 |  |  |  |
| Project Description 330.010 Dutchtown Road Subdivision |  |  |  |  |  |  |  |  |  |
| East/West Street: Dutchtown Road |  |  | North/South Street: Project Entrance |  |  |  |  |  |  |
| Intersection Orientation: East-West | East-West |  | Study Period (hrs): 0.25 |  |  |  |  |  |  |
| Vehicle Volumes and Adjustments |  |  |  |  |  |  |  |  |  |
| Major Street | Eastbound |  |  |  | Westbound |  |  |  |  |
| Movement | 1 | 2 | 3 |  | 4 | 5 |  | 6 |  |
|  | L | T | R |  | L | T |  | R |  |
| Volume (veh/h) | 42 | 868 |  |  |  | 401 |  | 22 |  |
| Peak-Hour Factor, PHF | 0.85 | 0.85 | 1.00 |  | 1.00 | 0.85 |  | 0.85 |  |
| Hourly Flow Rate, HFR (veh/h) | 49 | 1021 | 0 |  | 0 | 471 |  | 25 |  |
| Percent Heavy Vehicles | 0 | -- | -- |  | 0 | -- |  | -- |  |
| Median Type | Two Way Left Turn Lane |  |  |  |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  |  |  | 0 |  |
| Lanes | 1 | 1 | 0 |  | 0 | 1 |  | 0 |  |
| Configuration | L | T |  |  |  |  |  | TR |  |
| Upstream Signal |  | 0 |  |  |  | 0 |  |  |  |
| Minor Street | Northbound |  |  |  | Southbound |  |  |  |  |
| Movement | 7 | 8 | 9 |  | 10 | 11 |  | 12 |  |
|  | L | T | R |  | L | T |  | R |  |
| Volume (veh/h) |  |  |  |  | 9 |  |  | 29 |  |
| Peak-Hour Factor, PHF | 1.00 | 1.00 | 1.00 |  | 0.85 | 1.00 |  | 0.85 |  |
| Hourly Flow Rate, HFR (veh/h) | 0 | 0 | 0 |  | 10 | 0 |  | 34 |  |
| Percent Heavy Vehicles | 0 | 0 | 0 |  | 0 | 0 |  | 0 |  |
| Percent Grade (\%) | 0 |  |  |  | 0 |  |  |  |  |
| Flared Approach | N |  |  |  |  | N |  |  |  |
| Storage |  | 0 |  |  |  | 0 |  |  |  |
| RT Channelized |  |  | 0 |  |  |  |  | 0 |  |
| Lanes | 0 | 0 | 0 |  | 0 | 0 |  | 0 |  |
| Configuration |  |  |  |  |  | LR |  |  |  |
| Delay, Queue Length, and Level of Service |  |  |  |  |  |  |  |  |  |
| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |  |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 |  | 12 |
| Lane Configuration | L |  |  |  |  |  | LR |  |  |
| $v$ (veh/h) | 49 |  |  |  |  |  | 44 |  |  |
| C (m) (veh/h) | 1078 |  |  |  |  |  | 463 |  |  |
| v/c | 0.05 |  |  |  |  |  | 0.10 |  |  |
| 95\% queue length | 0.14 |  |  |  |  |  | 0.31 |  |  |
| Control Delay (s/veh) | 8.5 |  |  |  |  |  | 13.6 |  |  |
| LOS | A |  |  |  |  |  | B |  |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 13.6 |  |  |
| Approach LOS | -- | -- |  |  |  |  | B |  |  |



Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 6 | 814 |  |  | 692 | 5 |
| Peak-Hour Factor, PHF | 0.85 | 0.85 | 1.00 | 1.00 | 0.85 | 0.85 |
| Hourly Flow Rate, HFR (veh/h) | 7 | 957 | 0 | 0 | 814 | 5 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 1 | 0 | 0 | 1 | 0 |
| Configuration | L | T |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) |  |  |  | 3 |  | 29 |
| Peak-Hour Factor, PHF | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 0.85 |
| Hourly Flow Rate, HFR (veh/h) | 0 | 0 | 0 | 3 | 0 | 34 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  |  |  |  | LR |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L |  |  |  |  |  | LR |  |
| $v$ (veh/h) | 7 |  |  |  |  |  | 37 |  |
| C (m) (veh/h) | 818 |  |  |  |  |  | 300 |  |
| v/c | 0.01 |  |  |  |  |  | 0.12 |  |
| 95\% queue length | 0.03 |  |  |  |  |  | 0.42 |  |
| Control Delay (s/veh) | 9.4 |  |  |  |  |  | 18.7 |  |
| LOS | A |  |  |  |  |  | C |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 18.7 |  |
| Approach LOS | -- | -- |  |  |  |  | C |  |



Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 21 | 674 |  |  | 423 | 12 |
| Peak-Hour Factor, PHF | 0.85 | 0.85 | 1.00 | 1.00 | 0.85 | 0.85 |
| Hourly Flow Rate, HFR (veh/h) | 24 | 792 | 0 | 0 | 497 | 14 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 1 | 1 | 0 | 0 | 1 | 0 |
| Configuration | L | T |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) |  |  |  | 5 |  | 15 |
| Peak-Hour Factor, PHF | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 0.85 |
| Hourly Flow Rate, HFR (veh/h) | 0 | 0 | 0 | 5 | 0 | 17 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | $N$ |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  |  |  |  | LR |  |

Delay, Queue Length, and Level of Service

| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | L |  |  |  |  |  | LR |  |
| $v$ (veh/h) | 24 |  |  |  |  |  | 22 |  |
| C (m) (veh/h) | 1065 |  |  |  |  |  | 367 |  |
| v/c | 0.02 |  |  |  |  |  | 0.06 |  |
| 95\% queue length | 0.07 |  |  |  |  |  | 0.19 |  |
| Control Delay (s/veh) | 8.5 |  |  |  |  |  | 15.4 |  |
| LOS | A |  |  |  |  |  | C |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 15.4 |  |
| Approach LOS | -- | -- |  |  |  |  | C |  |

Attachment 7
Turn Lane Warrant Analysis

## Attachment 7

Turn Lane Warrant Analysis

## Project: Dutchtown Road Subdivision

Dutchtown Road at Project Entrance

LEFT TURN
AM
PM
Dutchtown Road at Project Entrance RIGHT TURN

AM
PM

VOLUMES

| Opposing | Thru | LT | LT MAX | Warrant Met |
| :---: | :---: | :---: | :---: | :---: |
| 692 | 814 | 10 | 15 | NO |
| 423 | 686 | 42 | 20 | YES |

VOLUMES

| Thru | RT | RT MAX | Warrant Met |
| :---: | :---: | :---: | :---: |
| 683 | 9 | 24 | NO |
| 401 | 22 | 149 | NO |

## TABLE 5A

LEFT-TURN LANE YOLUME TYRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH
(If the left-turn volume exceeds the table value a left -turn lane is needed)

| OPPOSING VOLUME | THROUGH VOLUNLE EXUS RIGET-TURIVOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-309 | 400-449 | 450-499 | 500-549 | 550-509 | $=1>600$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ | $\begin{aligned} & 70 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 2511-209 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & 45 \\ & 41) . \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ |  | 25 <br> $\mathbf{2 5}$ <br> 12 | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $20$ | 20 |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | 20 | 15 15 |
| $\begin{aligned} & 600-64 y \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | 20 ${ }_{\text {AM P }}$ | $\frac{20}{20} 10$ LT | 15 15 |
| $\begin{gathered} 700-749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | 15 15 | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ |

* Or through volume only if a right-turn lane exists


## TABLE 5B

RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVALLING SPEED OF 36 TO 45 MPH

| RIGHT-TURN <br> VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $<100$ | 100-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{gathered} \text { Fewer Than } 25 \\ 25-49 \\ 50-99 \end{gathered}$ |  |  |  |  |  |  |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  |  |  |  |  |  |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ |  |  |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Y'es } \end{aligned}$ |
| $\begin{aligned} & 309-349 \\ & 350-399 \end{aligned}$ |  |  | Y'es | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 400-459 \\ & 450-489 \end{aligned}$ |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Y'es } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 506-54 y \\ & 550-594 \end{aligned}$ | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { y'ts } \\ & \text { Yixs } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |


| RIGHT-TURN <br> VOLUME | THROUGH VOLUME PLUS LETE-TURN VOLUNEE * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | 400.449 | 450-499 | 500-549 | 550-600 | $+1>600$ |
|  |  | PM Peak 22 RT |  |  |  | Peak 9 |
| $\begin{gathered} \text { Frwer Tham } 25 \\ 25-49 \\ 50-99 \end{gathered}$ |  | PM Peak 22 RT |  | Yes | $\begin{aligned} & \text { yis } \\ & \text { Yes } \end{aligned}$ | Y's Yes |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  | Yes | Yes Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yos } \end{aligned}$ | $\begin{aligned} & \text { Yas } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & Y \in 5 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & Y_{\mathrm{Ps}} \\ & \mathrm{YeS}^{2} \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes Y'es | $\begin{aligned} & \text { Yes } \\ & \text { Yus } \end{aligned}$ |
| -600 or More | Yes | Yes | Yes | Yes | Yes | Yes |

* Or through volume only if a leth-turn lane exists.

Attachment 8
Signal Warrant Analysis

Attachment 8 Signal Warrant Analysis
Project: Dutchtown Road Subdivision

Dutchtown Road @ Project Entrance
2018 Peak Hour Traffic Full Buildout

| 7:00 AM | Dutchtown Road (Both Directions) | Project Entrance (Both Directions) | Warrant 1, Eight-Hr Vehicular Volume |  |  | Warrant 2, Four-Hr | Warrant 3, Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Condition A | Condition B | Condition A \& B |  |  |
|  | 1244 | 38 | NO | NO | NO | NO | NO |
| 8:00 AM | 858 | 38 | NO | NO | NO | NO | NO |
| 9:00 AM | - | - | - | - | - | - | - |
| 10:00 AM | - | - | - | - | - | - | - |
| 11:00 AM | 402 | 15* | NO | NO | NO | - | - |
| 12:00 PM | 471 | 15* | NO | NO | NO | - | - |
| 1:00 PM | - | - | - | - | - | - | - |
| 2:00 PM | 599 | 15* | NO | NO | NO | - | - |
| 3:00 PM | 1002 | 15* | NO | NO | NO | - | - |
| 4:00 PM | 711 | 57 | NO | NO | NO | NO | NO |
| 5:00 PM | 1058 | 57 | NO | NO | NO | NO | NO |

* Estimated Based on Generated ADT Number Exiting ((496 ADT Exiting Full Buildout) - (38 AM Peak) 2 - ( 57 PM Peak) ${ }^{*} 2$ )/ 20 hours $=15$ Trips $/ \mathrm{Hr}$

