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REVISION NO. 2SEPTEMBER 16

2024

EZ STOP CONCORD ROAD

KNOX COUNTY, TENNESSEE

TRAFFIC IMPACT STUDY

CONCORD ROAD KNOX COUNTY, TENNESSEE

CCI PROJECT NO. 01634-0010.000



REVISION 2 (09/16/2024)

This report replaces the previous version of the traffic impact study dated 05/23/2024 prepared for this project in its entirety. The associated changes are related to site plan modifications that reduced the overall building size of the proposed convenience store.

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EXECUTIVE SUMMARY

This report provides a summary of a traffic impact study that was performed for a proposed mixed-use development to be located at the northeast corner of Concord Road and 2nd Drive in Knox County, Tennessee. The project site is located on the east side of Concord Road and north side of 2nd Drive. The development plan for this site proposes an approximate 5,000 square-foot Convenience Store / Gas Station with 14 fueling stations, and two 2,800 square-foot retail buildings with unknown usage. For the purposes of this study, it was assumed that these retail buildings would both be fast food restaurants with drive through windows, to accommodate for the potential maximum amount of traffic to be generated. The proposed development will have one partial access on Concord Road approximately 390 feet north of 2nd Drive, where a driveway cut currently exists. The partial access will be a right-in / right-out only access on Concord Road. Additionally, the development will have one full access on 2nd Drive approximately 150 feet east of Concord Road.

The purpose of this study was the evaluation of the traffic operational and safety impacts of the proposed development upon roadways in the vicinity of the project site. Comments received from Knox County Engineering, Knoxville-Knox County Planning, and the Town of Farragut resulted in the existing intersections of Concord Road at Turkey Creek Road / Summerdale Drive, Concord Road at 2nd Drive, and Concord Road at Northshore Drive being identified for detailed study. Appropriate intersection evaluations such as capacity analyses, turn-lane warrants, and signal warrants were conducted at the study intersections for existing and future conditions, both with and without site generated traffic, in order to determine the anticipated impacts and to establish recommended measures to mitigate these impacts. Additionally, the proposed site accesses on Concord Road and 2nd Drive were evaluated for turn lane warrants and sight distance.

The primary conclusion of this study is that the traffic generated from the proposed development will have only minor impacts at the study intersections. However, some improvements are recommended to improve operations, safety, and capacity. The following is a list of recommendations developed with this traffic impact study:

- 1) A northbound right turn lane onto 2nd Drive from Concord Road should be constructed with a storage length of 50 feet and a taper length of 120 feet.
- 2) Ensure that grading, landscaping, signing, and other site features do not restrict lines of sight exiting the development. The sight distance looking left when exiting the site onto 2nd Drive should be improved to at least 250 feet.
- 3) The lanes on 2nd Drive should be widened to at least 10 feet per Knox County requirements.



INTRODUCTION & PURPOSE OF STUDY

This report provides a summary of a traffic impact study that was performed for a proposed mixed-use development to be located at the northeast corner of Concord Road and 2nd Drive in Knox County, Tennessee. The project site is located on the east side of Concord Road and the north side of 2nd Drive. FIGURE 1 is a location map showing the major roadways in the project site vicinity.

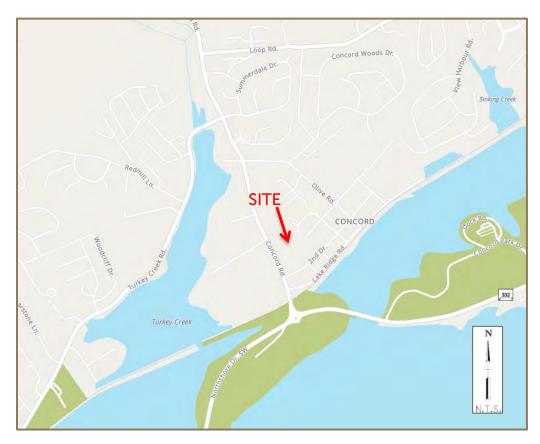


FIGURE 1 LOCATION MAP

The development plan for this site proposes an approximate 5,000 square-foot Convenience Store / Gas Station with 14 fueling stations, and two 2,800 square-foot retail buildings with unknown usage. For the purposes of this study, it was assumed that these retail buildings would both be fast food restaurants with drive through windows, to accommodate for the potential maximum amount of traffic to be generated. The proposed development will have one partial access on Concord Road approximately 390 feet north of 2nd Drive, where a driveway cut currently exists. The partial access will be a right-in / right-out only access on Concord Road. Additionally, the development will have one full access on 2nd Drive approximately 150 feet east of Concord Road. FIGURE 2 is a Conceptual Site Plan detailing the proposed site.



The purpose of this study was the evaluation of the traffic operational and safety impacts of the proposed development upon roadways in the vicinity of the project site. Comments received from Knox County Engineering, Knoxville-Knox County Planning, and the Town of Farragut resulted in the existing intersections of Concord Road at Turkey Creek Road / Summerdale Drive, Concord Road at 2nd Drive, and Concord Road at Northshore Drive being identified for detailed study. Appropriate intersection evaluations such as capacity analyses, turn-lane warrants, and signal warrants were conducted at the study intersections for existing and future conditions, both with and without site generated traffic, in order to determine the anticipated impacts and to establish recommended measures to mitigate these impacts. Additionally, the proposed site accesses on Concord Road and 2nd Drive were evaluated for turn lane warrants and sight distance.



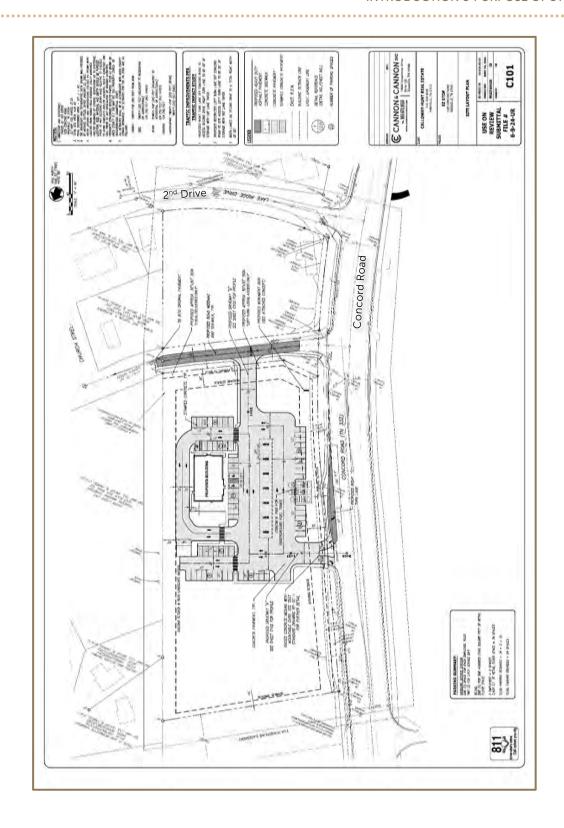


FIGURE 2
CONCEPTUAL SITE PLAN



EXISTING CONDITIONS

EXISTING ROADWAY CONDITIONS

Concord Road is classified as a Minor Arterial per the Tennessee Department of Transportation (TDOT) Functional Classification Maps and runs south to north from Northshore Drive to Kingston Pike. Within the study limits, Concord Road varies between a divided four-lane roadway with 2 travel lanes in each direction and an undivided five-lane roadway with two travel lanes in each direction and a center two-way left turn lane. In the study vicinity, Concord Road has 12-foot travel lanes and a posted speed limit of 40 mph. Concord Road has curb and gutter, bike lanes, and sidewalk on both sides of the roadway within the vicinity of the study

Turkey Creek Road is classified as a Major Collector per the TDOT Functional Classification Maps and runs west to east from Virtue Road to Concord Road. Turkey Creek Road is a two-lane road with one travel lane in each direction. Within this section, Turkey Creek Road has 12-foot travel lanes and a posted speed limit of 40 mph. Turkey Creek Road has curb and gutter on both sides and sidewalk on the north side in the study vicinity.

2nd Drive is a local road with no pavement markings except at the intersection with Concord Road, and one travel lane each direction ranging from 7 to 8 feet wide. 2nd Drive has a posted speed limit of 25 mph, and it does not have curb and gutter or sidewalk.

Northshore Drive is a west to east road running from Beals Chapel Road to Papermill Drive. East of Concord Road, Northshore Drive is classified as a Minor Arterial per the TDOT Functional Classification Maps; west of Concord Road it is classified as a Major Collector. In the study vicinity, Northshore Drive is a two-lane road with one travel lane in each direction, has no curb and gutter or sidewalk, and has a posted speed limit of 40 mph. Northshore Drive has 12-foot lane widths east of Concord Road and 11-foot lane widths west of Concord Road in the study vicinity.

The existing intersection of Concord Road at Turkey Creek Road / Summerdale Drive is a four-legged signalized intersection. Concord Road is considered the north-south street, and Turkey Creek Road / Summerdale Drive are considered the east-west streets. The southbound Concord Road approach contains one exclusive left turn lane, two exclusive through lanes, and one exclusive right turn lane. The left turn lane has storage of approximately 90 feet, and the right turn storage is 470 feet. The northbound Concord Road approach contains one exclusive left turn lane, one exclusive through lane, and a shared through / right turn lane. The left turn lane storage is approximately 70 feet. The eastbound approach, Turkey Creed Road, contains one exclusive left turn lane and one lane that services all movements with a storage length of approximately 165 feet. The westbound approach, Summerdale Drive, consists of one lane to service all movements. Marked crosswalks and actuated pedestrian signal phases exist crossing all legs of the intersection.

The existing intersection of Concord Road at 2nd Drive is a three-legged, side-street stop controlled intersection. Concord Road is the north-south street and 2nd Drive is the east-west street. The southbound approach of Concord Road contains one exclusive left turn lane and two exclusive through lanes. The left turn lane has a storage length of approximately 65 feet. The northbound approach of Concord Road contains one exclusive through lane and one shared through / right turn



lane. The westbound approach of 2nd Drive has one lane to service all movements. A marked crosswalk exists crossing the east leg of the intersection.

The existing intersection of Concord Road at Northshore Drive is a three-legged intersection controlled by a roundabout. Concord Road is considered the north-south street and Northshore Drive is considered the east-west street. The southbound approach of Concord Road contains one exclusive, yield controlled right turn bypass lane and an additional lane entering the roundabout. The eastbound approach of Northshore Drive has one lane entering the roundabout. The westbound approach of Northshore Drive contains one exclusive, free flowing right turn bypass lane and an additional lane entering the roundabout.

EXISTING SITE CONDITIONS

The project site is located at the intersection of Concord Road and 2nd Drive on the east side of Concord Road and the north side of 2nd Drive. The area of the site is approximately 20.6 acres, and it is currently zoned Neighborhood Commercial. The site is relatively flat and wooded throughout with no existing structures. A driveway cut currently exists on the west side of the site to Concord Road. FIGURE 3 provides an aerial view of the project site and the surrounding area.



FIGURE 3
EXISTING SITE CONDITIONS



EXISTING TRAFFIC DATA

Two types of traffic data were gathered for this study. The Tennessee Department of Transportation (TDOT) collects annual average daily traffic (AADT) data on roadways in the study area. Three count stations, located on Turkey Creek Road east of Brixworth Boulevard, Northshore Drive east of Concord Park Drive, and Concord Road at Clarity Pointe Lane, were found near the project site that were felt to have particular relevance for this study. The most currently available data from these stations can be found in TABLE 1.

TABLE 1: ANNUAL AVERAGE DAILY TRAFFIC COUNT SUMMARY

| COUNT YEAR | TDOT COUNT STATION 47000305 TURKEY CREEK ROAD | TDOT COUNT STATION 47000361 NORTHSHORE DRIVE | TDOT COUNT STATION 47000455 CONCORD ROAD |
|------------|---|--|--|
| 2018 | 2,889 | 13,682 | 10,070 |
| 2019 | 2,664 | 13,523 | 11,530 |
| 2020 | 2,264 | 13,793 | 11,464 |
| 2021 | 4,453 | 17,152 | 12,037 |
| 2022 | 4,404 | 15,495 | 11,905 |
| 2023 | 3,062 | 15,305 | 15,482 |

In addition to the available AADT data, intersection turning movement counts (TMC) were conducted at the existing study intersections to determine the current morning (AM) and evening (PM) peak hour operating volumes. These peak hour volumes are the traffic volumes with which the study's capacity analyses are based. The intersection TMC data were collected on March 20, 2024. The 2024 existing peak hour traffic volumes are summarized in FIGURE 4, and the raw data traffic count summary sheets are contained in APPENDIX A.

EXISTING CAPACITY ANALYSES

Capacity analyses employing the methods of the *Highway Capacity Manual* were conducted for the existing conditions at the study intersections. These analyses were performed with the 2024 existing traffic volumes, shown in FIGURE 4, and existing intersection geometry, traffic control, and signal timing. *Synchro 11* software was utilized for the capacity analyses for the intersection of Concord Road at Turkey Creek Road / Summerdale Drive. *HCS 2022* software was utilized for the capacity analysis for the intersections of Concord Road at 2nd Drive and Concord Road at Northshore Drive. The EVALUATIONS section of this report may be referenced for discussion and tabular summaries of these analyses, while more detailed summaries are presented on the computer printouts contained in APPENDIX C. Also contained in APPENDIX C is a section titled "Capacity and Level of Service Concepts," which provides a description of the utilized procedures.



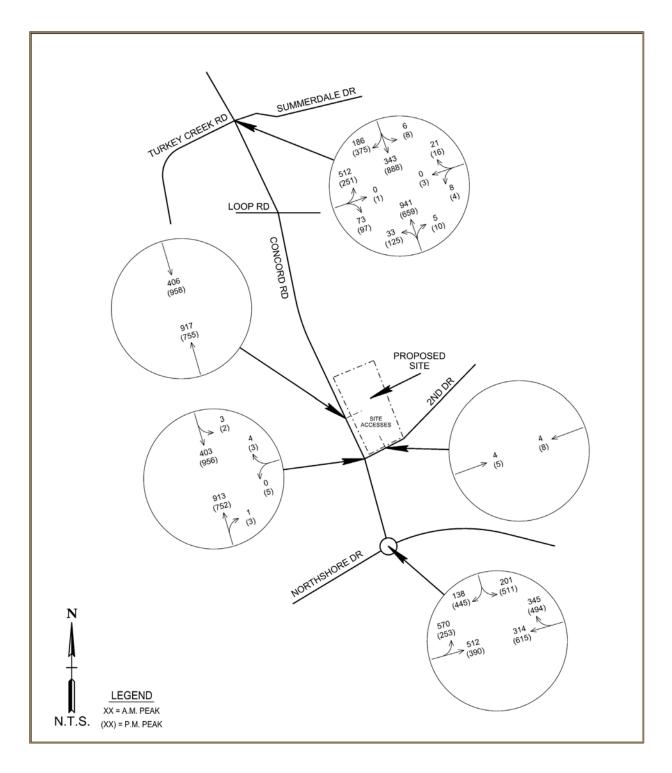


FIGURE 4
2024 EXISTING TRAFFIC VOLUMES



BACKGROUND CONDITIONS

BACKGROUND TRAFFIC GROWTH

The year for full buildout of the proposed development is unknown, however, the gas station / convenience store is anticipated to be completed in 2026. Therefore, Year 2026 was established as the appropriate design / analysis year for the study. In order to determine traffic volumes resulting solely from background traffic growth to Year 2026, it was necessary to establish an annual growth rate for existing traffic. The TDOT AADT values previously discussed, as well as knowledge of the area, were used to determine an approximate annual growth rate. Based on the available data, a background annual growth rate of 3.5% was assumed. FIGURE 5 contains the background traffic volumes that would result from this annual growth rate from Year 2024, when the counts were conducted to Year 2026.

BACKGROUND CAPACITY ANALYSES / LEVELS-OF-SERVICE

Capacity analyses as described in the EXISTING CONDITIONS section of this report were conducted utilizing the Year 2026 background volumes shown in FIGURE 5 and existing intersection geometry, traffic control, and signal timing. The EVALUATIONS section of this report may be referenced for discussion and tabular summaries of these analyses, while more detailed summaries are presented on the computer printouts contained in APPENDIX C.



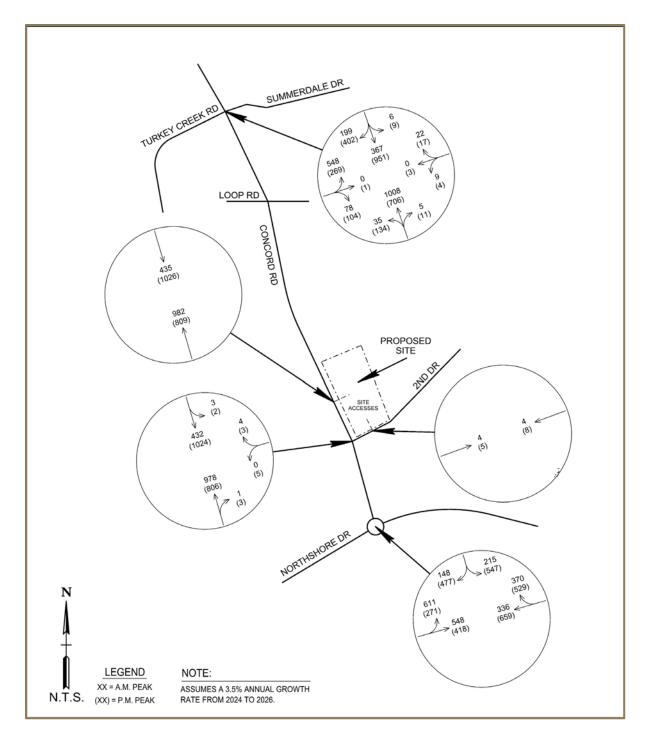


FIGURE 5
2026 BACKGROUND TRAFFIC VOLUMES



FUTURE CONDITIONS

TRIP GENERATION

In order to estimate the expected traffic volumes to be generated by the proposed development, the procedures recommended by the Institute of Transportation Engineers (ITE) were utilized. The proposed development will include a gas station / convenience store that is approximately 5,000 square feet and has 14 vehicle fueling stations, as well as two undetermined use retail buildings. These buildings are 2,800 square feet each, and were assumed to be fast food restaurants with drive throughs to account for the reasonable worst-case scenario traffic generated. A previous version of this study was performed for the originally-proposed convenience store building size of 7,015 square feet. A quick analysis of the effects of the reduced building size determined that the reduction would result in only minimally decreased generated trips and no changes to the study's recommendations. Therefore, the remainder of this report continues to reference the original building size of 7,015 square feet and associated evaluation results.

The ITE *Trip Generation Manual 11th Edition* was utilized for estimating traffic generated. The generated traffic volumes were determined based on the data for the peak hours of adjacent street traffic. Per guidance from a Knoxville-Knox County memorandum regarding pass-by rates for several land uses, a 65% pass-by rate was applied to the trip generation for the convenience market / gas station, and a 40% pass-by rate was applied to the trip generation for the fast-food restaurant. Pass-by trips are traffic volumes that are currently on the roadway and enter/exit the development as they "pass by" on their way to another destination. Additional trip generation information is contained in APPENDIX B. See TABLE 2 for a summary of the traffic generated for this development.



TABLE 2: TRIP GENERATION SUMMARY

| LAND USE | SIZE | WEEKDAY (TRIPS/DAY) | AM PEAK HOUR (TRIPS/HOUR) | PM PEAK HOUR (TRIPS/HOUR) |
|--|---------------------------|----------------------------|------------------------------|---------------------------------|
| Fast-Food Restaurant with Drive-Through Window LUC (934) | 2,800 sqft | 1,309 | 125 | 92 |
| Entering Trips Exiting Trips | | 655 (50%) 654 (50%) | 64 (51%) 61 (49%) | 48 (52%) 44 (48%) |
| Fast-Food Restaurant with Drive-Through Window LUC (934) | 2,800 sqft | 1,309 | 125 | 92 |
| Entering Trips Exiting Trips | | 654 (50%) 655 (50%) | 64 (51%) 61 (49%) | 48 (52%) 44 (48%) |
| Convenience Store / Gas Station LUC (945) | 7,015 Sqft 14 pumps | 4,841 | 442 | 377 |
| Entering Trips Exiting Trips | | 2,420 (50%) 2,421 (50%) | 221 (50%) 221 (50%) | 188 (50%) 189 (50%) |
| Total Trips | | 7,459 | 692 | 561 |
| Entering Trips Exiting Trips | | 3,729 3,730 | 349 343 | 284 277 |
| Internal Trips | | N/A | 90 | 129 |
| Entering Trips Exiting Trips | | N/A | 45 45 | 65 64 |
| Net External Trips | | 7,459 | 602 | 432 |
| Entering Trips Exiting Trips | | 3,729 3,730 | 304 298 | 219 213 |
| Pass-by Trips | | 4,194 | 387 | 319 |
| Entering Trips Exiting Trips | | 2,097 2,097 | 195 192 | 161 158 |
| Non-Pass-by Trips | | 3,265 | 215 | 113 |



| | , | | • |
|----------------|--------------|-----|----|
| Entering Trips | 1,632 | 109 | 58 |
| Exiting Trips | 1,633 | 106 | 55 |

A.M. Peak Hour trip generation is based on Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. P.M. Peak Hour trip generation is based on Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

TRIP DISTRIBUTION AND ASSIGNMENT

The proposed trip distribution for this development was determined through a review of existing travel patterns, local knowledge of the study area, proposed site location in relation to the surrounding roadway network, and engineering judgment. Primary trips and pass-by trips were separated based on the Knoxville-Knox County Metropolitan Planning Commission pass-by rates. FIGURES 6A and 6B provide a summary of how the above site generated trips would be assigned to the study intersections. FIGURES 7A-7C provide the proposed trip assignment volumes to the study intersections.

FUTURE TRAFFIC VOLUMES

Future projected traffic volumes for the study intersections were developed by adding the generated and assigned trips shown in FIGURE 7C to the 2026 background traffic volumes developed in the previous section and shown in FIGURE 5. These combined 2026 volumes reflect the existing traffic, the background traffic growth, and the generated traffic from the proposed development. These future volumes are shown on FIGURE 8 and are the combined volumes used in the analyses of future conditions with the proposed development.

FUTURE CAPACITY ANALYSES / LEVELS-OF-SERVICE

Capacity analyses as described in the EXISTING CONDITIONS section of this report were conducted utilizing the Year 2026 combined volumes shown in FIGURE 8 and existing intersection geometry, traffic control, and signal timing, as well as some improvement alternatives. Tabular summaries of the analyses results and associated discussion are also contained in the EVALUATIONS section. In addition, detailed computer printout summaries of the analyses are contained in APPENDIX C.



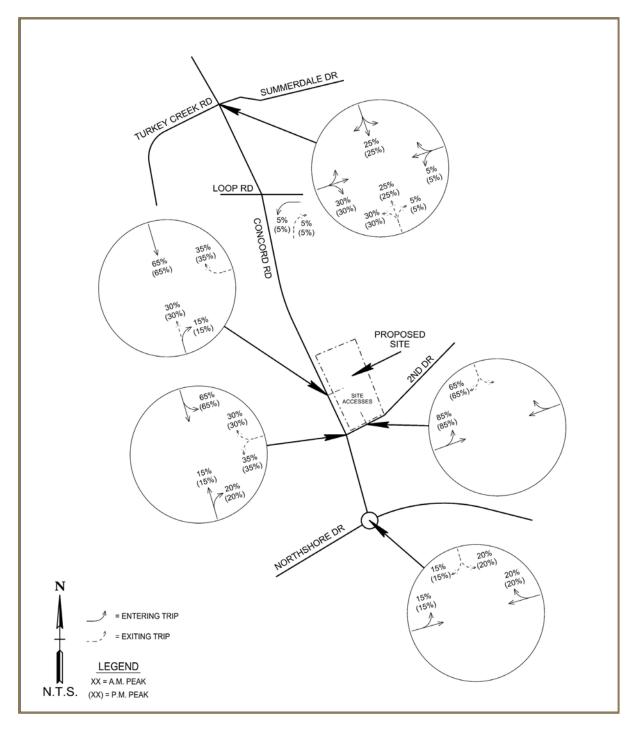


FIGURE 6A PRIMARY TRIP DISTRIBUTION



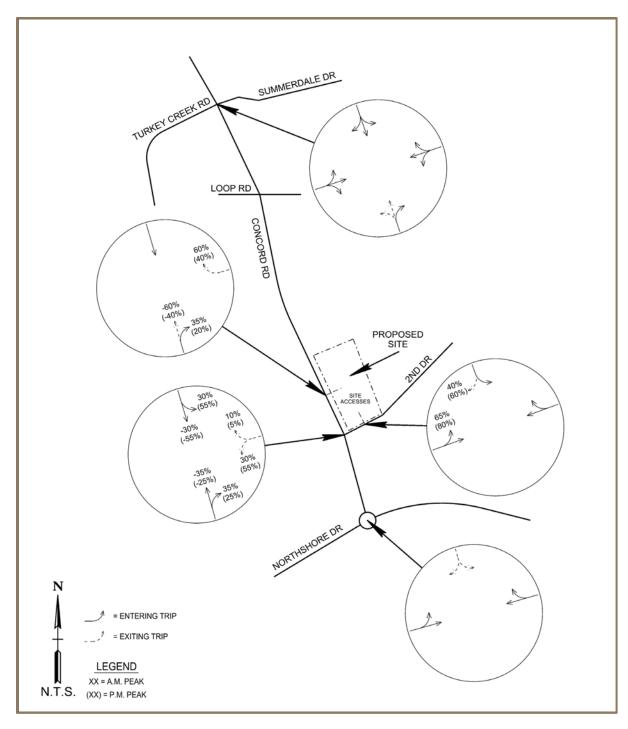


FIGURE 6B PASS-BY TRIP DISTRIBUTION



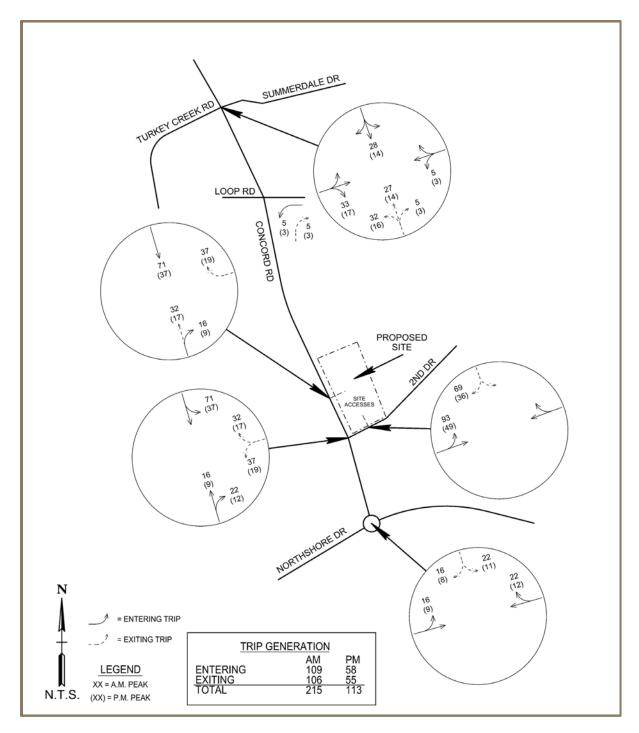


FIGURE 7A
PRIMARY TRIP ASSIGNMENT



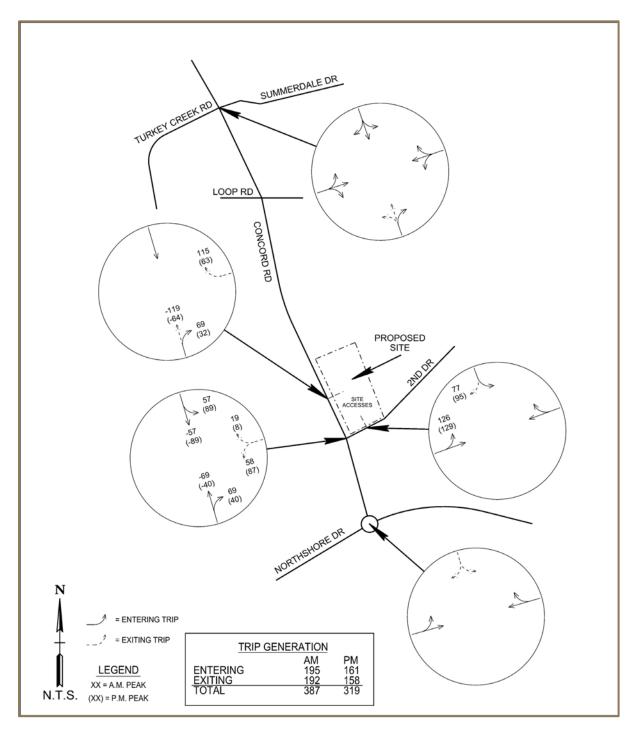


FIGURE 7B
PASS-BY TRIP ASSIGNMENT



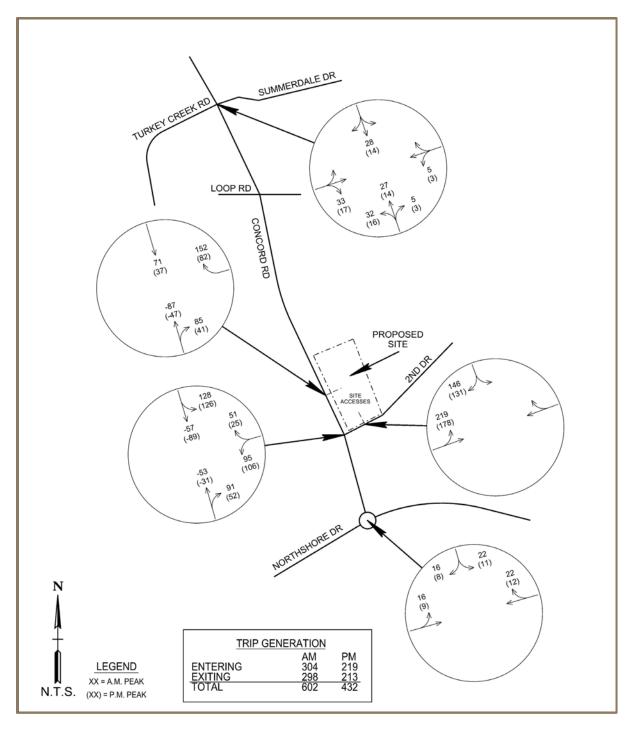


FIGURE 7C
TOTAL TRIP ASSIGNMENT



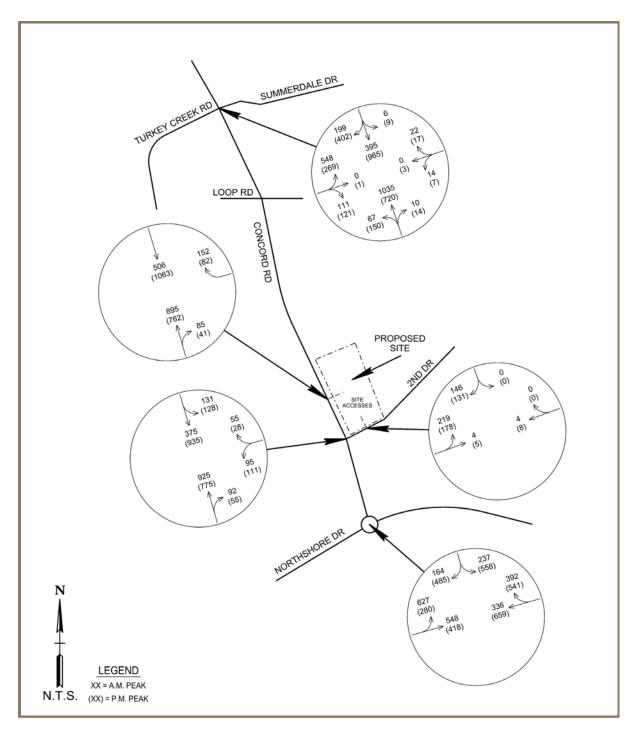


FIGURE 8
2026 COMBINED TRAFIC VOLUMES



EVALUATIONS

INTERSECTION CAPACITY ANALYSES

Intersection capacity analyses were performed for the study intersections. The capacity analyses employed the procedures of the *Highway Capacity Manual* utilizing *Synchro 11* software. A description of the fundamentals of these procedures is contained in the APPENDIX C section titled "Capacity and Level-of-Service Concepts." The results of these analyses for the existing, background and combined future traffic conditions are presented and discussed by individual intersection in the subsections below. Capacity analyses summaries are presented for each intersection in these individual subsections, which are accompanied by tables showing level-of-service (LOS) and queuing results. More detailed information is contained on the capacity software output summaries contained in APPENDIX C.

Potential mitigation measures were identified at intersections experiencing poor LOS or where vehicle queuing may become an issue. These mitigation strategies, where applicable, are described for each intersection in their respective subsections. The accompanying LOS and queue length tables show comparisons between the intersections under existing geometry, traffic control, and signal timing to these mitigation strategies in order to provide a quantitative measure of effectiveness of the mitigation.

Intersection #1: Concord Road at Turkey Creek Road / Summerdale Drive

As shown in TABLE 3, this intersection currently operates at overall LOS "C" during the peak hours. The intersection is expected to continue to operate at the same LOS under combined traffic conditions upon construction and full buildout of the proposed development. The eastbound shared left turn lane / through lane / right turn lane queue exceeds the current storage length in all scenarios, but lengthening the storage for this lane is not feasible due to the bridge. Queues for the northbound left turn lane may exceed the storage length; however, the two-way left turn lane provides plenty of spillback storage. Based on these analyses, the development will have only minimal impacts on intersection operations.



TABLE 3: CAPACITY ANALYSES SUMMARY - CONCORD ROAD AT TURKEY CREEK ROAD / SUMMERDALE DRIVE

| SCENARIO | | MOVEMENT/ APPROACH | AM PEAK (LOS/DELAY) | PM PEAK (LOS/DELAY) |
|-----------------|--|---------------------------------|---|--|
| 2024 Existing | Existing Geometry, Traffic Control & Signal Timing | EB WB NB SB Overall | C 28.0 A 0.7 C 26.5 B 16.4 C 24.0 | D 42.8 C 33.3 B 16.7 C 22.7 C 23.7 |
| 2026 Background | Existing Geometry, Traffic Control & Signal Timing | EB WB NB SB Overall | C 30.2 A 0.8 C 27.9 B 16.4 C 25.3 | D 45.4 C 34.0 B 17.2 C 24.2 C 25.1 |
| 2026 Combined | Existing Geometry, Traffic Control & Signal Timing | EB WB NB SB Overall | C 33.3 A 0.9 C 29.9 B 19.6 C 27.8 | D 45.8 D 37.6 B 17.8 C 25.7 C 26.1 |



TABLE 4: 95TH PERCENTIAL QUEUE SUMMARY – CONCORD ROAD AT TURKEY CREEK ROAD / SUMMERDALE DRIVE

| SCI | ENARIO | MOVEMENT/ APPROACH | AM PEAK | PM PEAK |
|-----------------|--|---|---|---|
| 2024 Existing | Existing Geometry, Traffic Control & Signal Timing | EBL EBL/T/R WBL/T/R NBL NBT/R SBL SBT SBR | 404' 178' 0' 31' 443' 10' 145' 19' | 248' 193' 36' 92' 293' 12' 468' 33' |
| 2026 Background | Existing Geometry, Traffic Control & Signal Timing | EBL EBL/T/R WBL/T/R NBL NBT/R SBL SBT SBR | 445' 206' 0' 32' 488' 10' 155' 20' | 271' 216' 37' 98' 320' 13' 532' 35' |
| 2026 Combined | Existing Geometry, Traffic Control & Signal Timing | EBL EBL/T/R WBL/T/R NBL NBT/R SBL SBT SBR | 483' 227' 0' 53' 508' 10' 172' 21' | 289' 220' 44' 115' 330' 12' 560' 38' |



Intersection #2: Concord Road at 2nd Drive

TABLE 3A indicates that the westbound approach of this intersection currently operates at overall LOS "B" during the AM peak hour and LOS "C" during the PM peak hour. The approach is anticipated to worsen to LOS "E" during the AM peak hour and "F" during the PM peak hour upon full buildout of the development under existing geometry and traffic control. The westbound approach currently experiences minimal traffic, with the resulting delay mainly affecting users of the development rather than other users. Several mitigation scenarios were evaluated, resulting in marginal improvements for the westbound approach but potentially worsening conditions for other approaches. Signalizing this intersection would cause unnecessary delays to Concord Road that would not exist even with the full buildout of this development. While separating the left and right lanes on the westbound approach would lead to slightly shorter delays and queue lengths, the benefits are not significant enough to justify the cost and effort involved. According to the charts by M.D. Harmelink in the *TDOT - Roadway Design Guidelines*, the storage warranted for the southbound left turn lane is 200 feet. However, as seen in TABLE 4A, the queue length for this movement is projected to be 25 feet under the 2026 Combined scenario.

TABLE 3A: CAPACITY ANALYSES SUMMARY - CONCORD ROAD AT 2ND DRIVE

| SC | ENARIO | MOVEMENT/ APPROACH | AM PEAK (LOS/DELAY) | PM PEAK (LOS/DELAY) |
|-----------------|--|---------------------------|-------------------------------------|-------------------------------------|
| 2024 Existing | Existing Geometry & | WB | B 12.2 | C 16.1 |
| | Traffic Control | SBL | B 12.5 | A 9.6 |
| 2026 Background | Existing Geometry & | WB | B 12.6 | C 17.0 |
| | Traffic Control | SBL | B 13.2 | A 9.8 |
| 2026 Combined | Existing Geometry & | WB | E 49.9 | F 56.6 |
| | Traffic Control | SBL | B 13.0 | B 11.1 |
| 2026 Combined | Exclusive Left & Right Turn Lanes On 2 nd Drive | WB SBL | E 35.2 B 13.0 | E 47.7 B 11.1 |
| 2026 Combined | Northbound Right Turn | WB | E 44.3 | F 53.6 |
| | Lane On Concord Road | SBL | B 13.0 | B 11.1 |
| 2026 Combined | Signalized | WB NB SB Overall | C 20.7 B 16.3 A 5.2 B 13.3 | C 34.2 B 13.0 A 5.6 B 10.5 |



TABLE 4A: 95TH PERCENTIAL QUEUE SUMMARY - CONCORD ROAD AT 2ND DRIVE

| SCE | ENARIO | MOVEMENT/ APPROACH | AM PEAK | РМ РЕАК |
|-----------------|------------------------|------------------------|---------------------------|-----------------------------|
| 2024 Existing | Existing Geometry & | WB | 0' | 3' |
| | Traffic Control | SBL | 0' | 0' |
| 2026 Background | Existing Geometry & | WB | 0' | 3' |
| | Traffic Control | SBL | 0' | 0' |
| 2026 Combined | Existing Geometry & | WB | 118' | 120' |
| | Traffic Control | SBL | 25' | 18' |
| 2026 Combined | Exclusive Left & Right | WBL | 78' | 100' |
| | Turn Lanes On | WBR | 13' | 5' |
| | 2 nd Drive | SBL | 25' | 18' |
| 2026 Combined | Northbound Right Turn | WB | 108' | 115' |
| | Lane On Concord Road | SBL | 25' | 18' |
| 2026 Combined | Signalized | WB NB SBL SBT | 79' 317' 41' 49' | 110' 222' 42' 148' |



Intersection #3: Concord Road at Northshore Drive

As indicated in TABLES 3B and 4B, the existing overall intersection LOS is an "F" during the AM peak hour, primarily due to significant delays and queues on the eastbound approach. This is projected to worsen to a more severe "F" through the background and combined scenarios. During the PM peak hour, the LOS is expected to worsen from "E" to "F" due to background traffic growth, with only a marginal increase in delay and queue length attributed to the development. The queue length and approach delay are anticipated to increase more significantly because of background conditions rather than the impact of the development.

TABLE 3B: CAPACITY ANALYSES SUMMARY – CONCORD ROAD AT NORTHSHORE DRIVE

| SCENARIO | | MOVEMENT/ APPROACH | AM PEAK (LOS/DELAY) | PM PEAK (LOS/DELAY) |
|-----------------|--|---------------------------|-------------------------------------|-------------------------------------|
| 2024 Existing | Existing Geometry & Traffic Control | EB WB SB Overall | F 103.1 A 6.5 A 6.1 F 56.7 | E 36.3 A 7.1 C 23.0 C 19.7 |
| 2026 Background | Existing Geometry & Traffic Control | EB WB SB Overall | F 145.4 A 7.7 A 6.5 F 79.1 | F 58.7 A 8.4 D 32.3 D 28.8 |
| 2026 Combined | Existing Geometry & Traffic Control | EB WB SB Overall | F 167.9 A 7.8 A 6.8 F 89.3 | F 65.7 A 8.5 D 34.3 D 31.2 |



.....

TABLE 4B: 95TH PERCENTIAL QUEUE SUMMARY – CONCORD ROAD AT NORTHSHORE DRIVE

| SCE | ENARIO | MOVEMENT/ APPROACH | АМ РЕАК | РМ РЕАК |
|-----------------|--|------------------------|-----------------------------|------------------------------|
| 2024 Existing | Existing Geometry & Traffic Control | EB WB SBL SBR | 880' 78' 25' 15' | 298' 120' 198' 135' |
| 2026 Background | Existing Geometry & Traffic Control | EB WB SBL SBR | 1148' 98' 28' 18' | 418' 150' 273' 178' |
| 2026 Combined | Existing Geometry & Traffic Control | EB WB SBL SBR | 1268' 100' 33' 20' | 450' 153' 290' 188' |

Intersection #4: Concord Road at Site Access

As shown in TABLES 3C and 4C, the site access on Concord Road with the proposed geometry has sufficient capacity for the development. The worst approach, westbound, has a LOS of "C" during the AM peak hour and "B" during the PM peak hour under the combined traffic scenario. The proposed condition analyzed a restricted access with right turn only from Concord Road into the site and a right turn only exiting the site onto Concord Road. There is currently a right turn flare at the driveway cut that exists where the proposed site access will be located.

TABLE 3C: CAPACITY ANALYSES SUMMARY - CONCORD ROAD AT SITE ACCESS

| SCE | ENARIO | MOVEMENT/ APPROACH | AM PEAK (LOS/DELAY) | PM PEAK (LOS/DELAY) |
|---------------|--|-----------------------|------------------------|------------------------|
| 2026 Combined | Proposed Geometry & Traffic Control | WB | C 16.7 | B 12.7 |



TABLE 4C: 95TH PERCENTIAL QUEUE SUMMARY - CONCORD ROAD AT SITE ACCESS

| SCENARIO | | MOVEMENT/ APPROACH | AM PEAK | PM PEAK |
|---------------|--|-----------------------|---------|---------|
| 2026 Combined | Proposed Geometry & Traffic Control | WBR | 40′ | 15′ |

Intersection #5: 2nd Drive at Site Access

As shown in TABLES 3D and 4D, the site access on 2nd Drive with the proposed geometry has sufficient capacity for the development. All approaches have a LOS "A" during both peak hours under the combined traffic scenario. The proposed condition analyzed one lane servicing all movements for each approach.

TABLE 3D: CAPACITY ANALYSES SUMMARY - 2ND DRIVE AT SITE ACCESS

| SCENARIO | | MOVEMENT/ | AM PEAK | PM PEAK |
|---------------|---------------------|-----------|-------------|-------------|
| | | APPROACH | (LOS/DELAY) | (LOS/DELAY) |
| 2026 Combined | Proposed Geometry & | EB | A 7.5 | A 7.4 |
| | Traffic Control | SB | A 8.9 | A 8.9 |

TABLE 4D: 95TH PERCENTIAL QUEUE SUMMARY - 2ND DRIVE AT SITE ACCESS

| SCE | ENARIO | MOVEMENT/ APPROACH | AM PEAK | РМ РЕАК |
|---------------|---------------------|-----------------------|---------|---------|
| 2026 Combined | Proposed Geometry & | EBL | 13′ | 10′ |
| | Traffic Control | SB | 13′ | 13′ |

TURN LANE WARRANT EVALUATIONS

Turn lane evaluations were conducted for a potential right lane entering the site from Concord Road and potential left and right lanes entering from 2nd Drive under combined volume scenarios, as well as a potential right turn lane from Concord Road onto 2nd Drive. The methods employed for the turn lane evaluation on 2nd Drive were those developed by M.D. Harmelink, as provided by in a series of tables from the Knox County publication *Access Control and Driveway Design Policy*. The results of these evaluations were that neither right nor left turn lanes are warranted on 2nd Drive entering the proposed development's access.



The methods used for determining if turn lanes are warranted on Concord Road are the tables provided in TDOT's *Highway Systems Access Manual Volume 3*. A right turn lane into the site access from Concord Road and a right turn lane onto 2nd Drive from Concord Road were found to be warranted. Additional information can be found on the turn lane evaluation worksheets contained in APPENDIX D. Because a left turn lane exists from Concord Road onto 2nd Drive, a left turn lane warrant was not analyzed at this location.

SIGNAL WARRANT EVALUATIONS

A signal warrant evaluation was performed for the intersection of Concord Road at 2nd Drive using the methods provided in the *Manual on Uniform Traffic Control Devices*. None of the four hours of traffic data collected meet the warrant for existing and background conditions at this intersection. Under the combined condition, both AM and PM peak hours meet the signal warrant for Concord Road at 2nd Drive. An 8-hour warrant has not been evaluated; however, due to not having enough data. Additional information can be found on the signal warrant evaluation worksheets contained in APPENDIX E.

SIGHT DISTANCE ASSESSMENT

Intersection sight distance was evaluated at the proposed intersections of Concord Road at the site access and 2nd Drive at the site access through field measurements. Measurements were taken looking right and left from the proposed site access approach at each location. According to AASHTO's *A Policy on Geometric Design of Highways and Streets* sight distance requirements for 40 mph roadways, 445 feet of sight distance is necessary when looking right and 385 feet is necessary when looking left from the proposed site access onto Concord Road. The sight distance looking left extends to the intersection with Northshore Drive. Sight distance looking right was not measured due to only having a right turn out of the site.

For 25 mph roadways, Knox County mandates 250 feet of sight distance looking left and right from the proposed site access onto 2nd Drive. The sight distance looking right onto 2nd Drive extends to the intersection of Concord Road. However, the sight distance looking left is obstructed to 225 feet due to a horizontal curve caused by vegetation and the current elevation of the corner of the proposed property. These issues can be mitigated by clearing and grading the proposed site to achieve a sight distance of at least 250 feet.



CONCLUSIONS & RECOMMENDATIONS

The primary conclusion of this study is that the traffic generated from the proposed development will have only minor impacts at the study intersections. Major congestion issues during peak hours do currently exist at the intersection of Concord Road at Northshore Drive, but the additional development impacts to this intersection would be marginal. The largest operational impacts would occur at the intersection of Concord Roat at 2nd Drive on the westbound 2nd Drive approach. This approach currently has very little traffic, and the majority of delay would be to users of the new development. The Knox County Engineering Department requested that the minimum width of 2nd Drive be increased to at least 20 feet. This width was deemed adequate, as heavy trucks are not expected to use this access into and out of the site. Turn lanes were warranted along Concord Road at the proposed site access and at 2nd Drive, and some were found to improve the operations of their respective intersections. Although a right turn lane is warranted into the site access from Concord Drive, there is currently a driveway flare that should be sufficient to serve the development. Furthermore, constructing of a right turn lane would require the relocation of a new large transmission pole. The signal warrant analysis at Concord Road at 2nd Drive determined that both peak hours meet the warrant under the combined scenario. However, because of the intersection's adequate performance as a side-street stop-controlled intersection, it is not recommended to install a signal at this time. Additionally, the southbound left turn volumes theoretically warrant an increase of the storage length to 200 feet, but the projected queue length is only around 25 feet. This being said, no changes to the existing turn lane are recommended.

Based on the above conclusions and other discussions throughout the report, the following is a list of recommendations developed with this traffic impact study:

- 1) A northbound right turn lane onto 2nd Drive from Concord Road should be constructed with a storage length of 50 feet and a taper length of 120 feet.
- 2) Ensure that grading, landscaping, signing, and other site features do not restrict lines of sight exiting the development. The sight distance looking left when exiting the site onto 2nd Drive should be improved to at least 250 feet.
- 3) The lanes on 2nd Drive should be widened to at least 10 feet per Knox County requirements.



APPENDIX

- A. TRAFFIC DATA
- **B. TRIP GENERATION INFORMATION**
- C. CAPACITY ANALYSES
- D. TURN LANE WARRANT EVALUATIONS
- **E. SIGNAL WARRANT EVALUATIONS**



APPENDIX A - TRAFFIC DATA



TRAFFIC GROWTH

| Source: | TDOT | |
|-------------|------------|--|
| Location: | Concord Rd | |
| | SR332 | |
| Route #: | | |
| Route Type: | | |
| Station: | 47000455 | |
| Capacity: | | |

| Count Year | Volume | Growth Rate |
|------------|--------|-------------|
| 2003 | | |
| 2004 | | #DIV/0! |
| 2005 | | #DIV/0! |
| 2006 | 9125 | #DIV/0! |
| 2007 | 9399 | 3.00 |
| 2008 | 13128 | 39.67 |
| 2009 | 8232 | -37.29 |
| 2010 | 9390 | 14.07 |
| 2011 | 9072 | -3.39 |
| 2012 | 9996 | 10.19 |
| 2013 | 10402 | 4.06 |
| 2014 | 11048 | 6.21 |
| 2015 | 11529 | 4.35 |
| 2016 | 11898 | 3.20 |
| 2017 | 12462 | 4.74 |
| 2018 | 10070 | -19.19 |
| 2019 | 11530 | 14.50 |
| 2020 | 11464 | -0.57 |
| 2021 | 12037 | 5.00 |
| 2022 | 11905 | -1.10 |
| 2023 | 15482 | 30.05 |

| Avg. 1 Year Rate 2003-2023 | #DIV/0! |
|----------------------------|---------|
| Avg. 1 Year Rate 2013-2023 | 4.72 |
| Avg. 1 Year Rate 2018-2023 | 9.57 |

| Source: | TDOT | | |
|-------------|----------------------|--|--|
| Location: | S. Northshore Dr. | | |
| | Southeast of Farrago | | |
| Route #: | | | |
| Route Type: | | | |
| Station: | 47000361 | | |
| Capacity: | | | |

| Count Year | Volume | Growth Rate |
|------------|--------|-------------|
| 2003 | 9036 | |
| 2004 | 8820 | -2.39 |
| 2005 | 10107 | 14.59 |
| 2006 | 9769 | -3.34 |
| 2007 | 9429 | -3.48 |
| 2008 | 9411 | -0.19 |
| 2009 | 8802 | -6.47 |
| 2010 | 9802 | 11.36 |
| 2011 | 9621 | -1.85 |
| 2012 | 9372 | -2.59 |
| 2013 | 10453 | 11.53 |
| 2014 | 11846 | 13.33 |
| 2015 | 12099 | 2.14 |
| 2016 | 12576 | 3.94 |
| 2017 | 13709 | 9.01 |
| 2018 | 13682 | -0.20 |
| 2019 | 13523 | -1.16 |
| 2020 | 13793 | 2.00 |
| 2021 | 17152 | 24.35 |
| 2022 | 15495 | -9.66 |
| 2023 | 15305 | -1.23 |

| Avg. 1 Year Rate 2003-2023 | 2.98 |
|----------------------------|------|
| Avg. 1 Year Rate 2013-2023 | 4.25 |
| Avg. 1 Year Rate 2018-2023 | 2.86 |

| Source: | TDOT |
|-------------|----------------------|
| Location: | Turkey Creek Rd |
| | Near Loudon Co. Line |
| Route #: | |
| Route Type: | |
| Station: | 47000305 |
| Capacity: | |

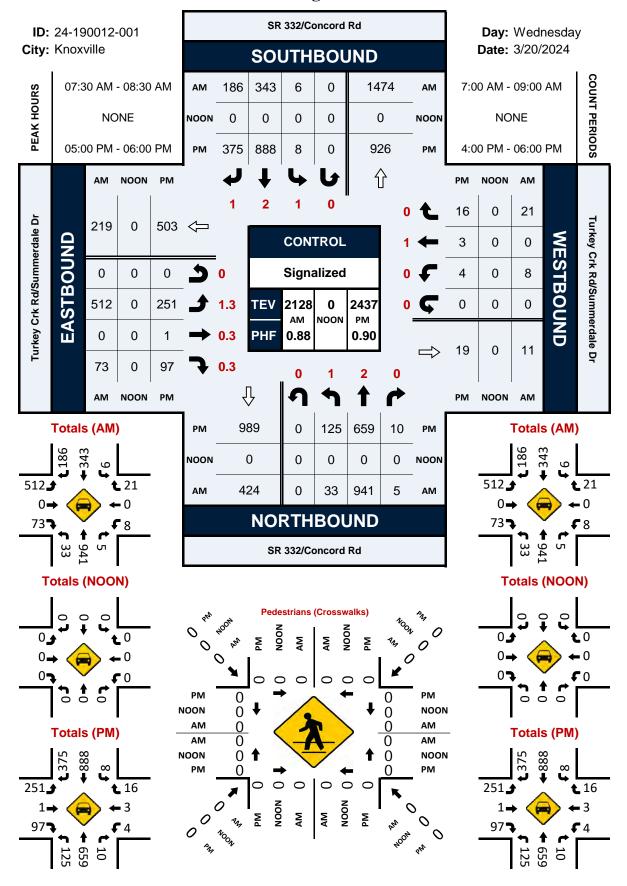
| Count Year | Volume | Growth Rate |
|------------|--------|-------------|
| 2003 | 1441 | |
| 2004 | 1484 | 2.98 |
| 2005 | 1629 | 9.77 |
| 2006 | 1487 | -8.72 |
| 2007 | 1708 | 14.86 |
| 2008 | 1828 | 7.03 |
| 2009 | 1526 | -16.52 |
| 2010 | 1676 | 9.83 |
| 2011 | 1831 | 9.25 |
| 2012 | 1915 | 4.59 |
| 2013 | 1823 | -4.80 |
| 2014 | 2050 | 12.45 |
| 2015 | 2213 | 7.95 |
| 2016 | 2423 | 9.49 |
| 2017 | 2969 | 22.53 |
| 2018 | 2889 | -2.69 |
| 2019 | 2664 | -7.79 |
| 2020 | 2264 | -15.02 |
| 2021 | 4453 | 96.69 |
| 2022 | 4404 | -1.10 |
| 2023 | 3062 | -30.47 |

| Avg. 1 Year Rate 2003-2023 | 6.02 |
|----------------------------|------|
| Avg. 1 Year Rate 2013-2023 | 7.93 |
| Avg. 1 Year Rate 2018-2023 | 8.46 |

| ·- | • | |
|----|---|--|

SR 332/Concord Rd & Turkey Crk Rd/Summerdale Dr

Peak Hour Turning Movement Count



National Data & Surveying Services

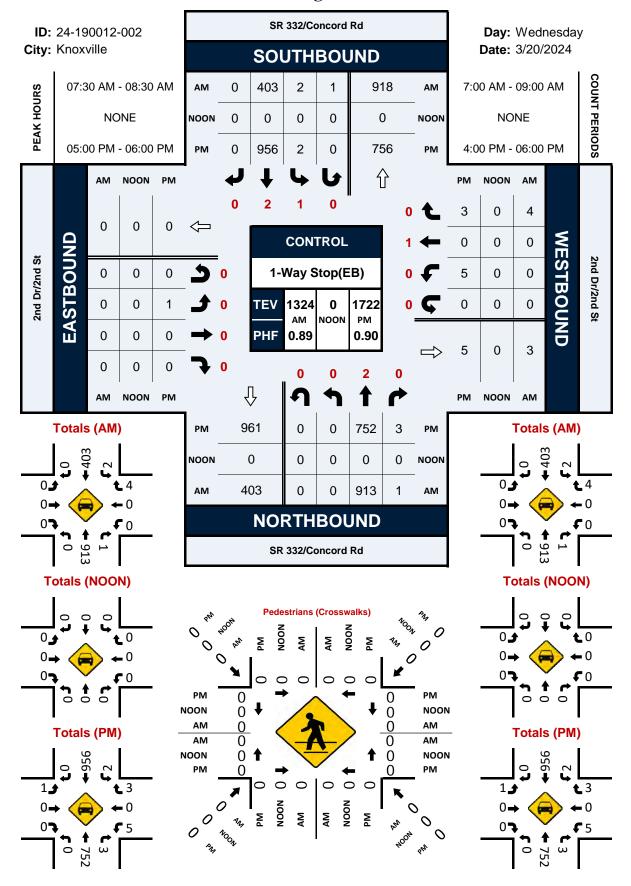
Intersection Turning Movement Count

Location: SR 332/Concord Rd & Turkey Crk Rd/Summerdale Dr City: Knoxville Control: Signalized Project ID: 24-190012-001 Date: 3/20/2024

| _ | | | | | | | | Data - | Totals | | | | | | | | |
|------------------|--------|------------|-------------|---------------------------|-------|--------|--------|-----------------------------|--------|-------|-------------|-----------------------------|-----------|-------|-------------|-------|-------|
| NS/EW Streets: | | SR 332/Co | ncord Rd | cord Rd SR 332/Concord Rd | | | Turke | Turkey Crk Rd/Summerdale Dr | | | | Turkey Crk Rd/Summerdale Dr | | | | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTE | OUND | | WESTBOUND | | | | |
| AM | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 1.3 | 0.3 | 0.3 | 0 | 0 | 1 | 0 | 0 | |
| 7 | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 3 | 117 | 0 | 0 | 0 | 38 | 15 | 0 | 100 | 0 | 10 | 0 | 3 | 0 | 4 | 0 | 290 |
| 7:15 AM | 5 | 166 | 0 | 0 | 0 | 42 | 33 | 0 | 132 | 0 | 16 | 0 | 0 | 0 | 7 | 0 | 401 |
| 7:30 AM | 8 | 252 | 0 | 0 | 2 | 66 | 30 | 0 | 123 | 0 | 8 | 0 | 0 | 0 | 13 | 0 | 502 |
| 7:45 AM | 5 | 271 | 1 | 0 | 2 | 88 | 55 | 0 | 149 | 0 | 24 | 0 | 4 | 0 | 4 | 0 | 603 |
| 8:00 AM | 11 | 213 | 1 | 0 | 1 | 92 | 53 | 0 | 125 | 0 | 22 | 0 | 2 | 0 | 3 | 0 | 523 |
| 8:15 AM | 9 | 205 | 3 | 0 | 1 | 97 | 48 | 0 | 115 | 0 | 19 | 0 | 2 | 0 | 1 | 0 | 500 |
| 8:30 AM | 4 | 195 | 0 | 0 | 2 | 115 | 43 | 0 | 106 | 0 | 12 | 0 | 0 | 0 | 3 | 0 | 480 |
| 8:45 AM | 6 | 159 | 0 | 0 | 1 | 83 | 34 | 0 | 84 | 0 | 12 | 0 | 1 | 0 | 2 | 0 | 382 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 51 | 1578 | 5 | 0 | 9 | 621 | 311 | 0 | 934 | 0 | 123 | 0 | 12 | 0 | 37 | 0 | 3681 |
| APPROACH %'s: | 3.12% | 96.57% | 0.31% | 0.00% | 0.96% | 65.99% | 33.05% | 0.00% | 88.36% | 0.00% | 11.64% | 0.00% | 24.49% | 0.00% | 75.51% | 0.00% | |
| PEAK HR : | | 07:30 AM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 33 | 941 | 5 | 0 | 6 | 343 | 186 | 0 | 512 | 0 | 73 | 0 | 8 | 0 | 21 | 0 | 2128 |
| PEAK HR FACTOR : | 0.750 | 0.868 | 0.417 | 0.000 | 0.750 | 0.884 | 0.845 | 0.000 | 0.859 | 0.000 | 0.760 | 0.000 | 0.500 | 0.000 | 0.404 | 0.000 | 0.882 |
| | | 0.88 | 34 | | | 0.91 | 6 | | | 0.8 | 45 | | | 0.5 | 58 | | 0.002 |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTE | OUND | | | WESTE | BOUND | | |
| PM | 1 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 1.3 | 0.3 | 0.3 | 0 | 0 | 1 | 0 | 0 | |
| • | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 23 | 138 | 1 | 0 | 1 | 203 | 115 | 0 | 49 | 0 | 15 | 0 | 4 | 0 | 1 | 0 | 550 |
| 4:15 PM | 34 | 148 | 2 | 0 | 1 | 169 | 76 | 0 | 45 | 0 | 20 | 0 | 0 | 0 | 1 | 0 | 496 |
| 4:30 PM | 24 | 135 | 3 | 0 | 8 | 217 | 94 | 0 | 58 | 0 | 23 | 0 | 1 | 0 | 2 | 0 | 565 |
| 4:45 PM | 20 | 155 | 1 | 0 | 2 | 197 | 89 | 0 | 82 | 0 | 14 | 0 | 0 | 0 | 2 | 0 | 562 |
| 5:00 PM | 30 | 143 | 4 | 0 | 0 | 229 | 93 | 0 | 60 | 0 | 21 | 0 | 0 | 1 | 6 | 0 | 587 |
| 5:15 PM | 35 | 188 | 4 | 0 | 2 | 243 | 101 | 0 | 70 | 1 | 29 | 0 | 2 | 0 | 2 | 0 | 677 |
| 5:30 PM | 37 | 161 | 0 | 0 | 5 | 216 | 93 | 0 | 51 | 0 | 23 | 0 | 1 | 0 | 4 | 0 | 591 |
| 5:45 PM | 23 | 167 | 2 | 0 | 1 | 200 | 88 | 0 | 70 | 0 | 24 | 0 | 1 | 2 | 4 | 0 | 582 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 226 | 1235 | 17 | 0 | 20 | 1674 | 749 | 0 | 485 | 1 | 169 | 0 | 9 | 3 | 22 | 0 | 4610 |
| APPROACH %'s: | 15.29% | 83.56% | 1.15% | 0.00% | 0.82% | 68.52% | 30.66% | 0.00% | 74.05% | 0.15% | 25.80% | 0.00% | 26.47% | 8.82% | 64.71% | 0.00% | |
| PEAK HR : | | 05:00 PM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 125 | 659 | 10 | 0 | 8 | 888 | 375 | 0 | 251 | 1 | 97 | 0 | 4 | 3 | 16 | 0 | 2437 |
| PEAK HR FACTOR : | 0.845 | 0.876 | 0.625 74 | 0.000 | 0.400 | 0.914 | 0.928 | 0.000 | 0.896 | 0.250 | 0.836 73 | 0.000 | 0.500 | 0.375 | 0.667 21 | 0.000 | 0.900 |

SR 332/Concord Rd & 2nd Dr/2nd St

Peak Hour Turning Movement Count



National Data & Surveying Services

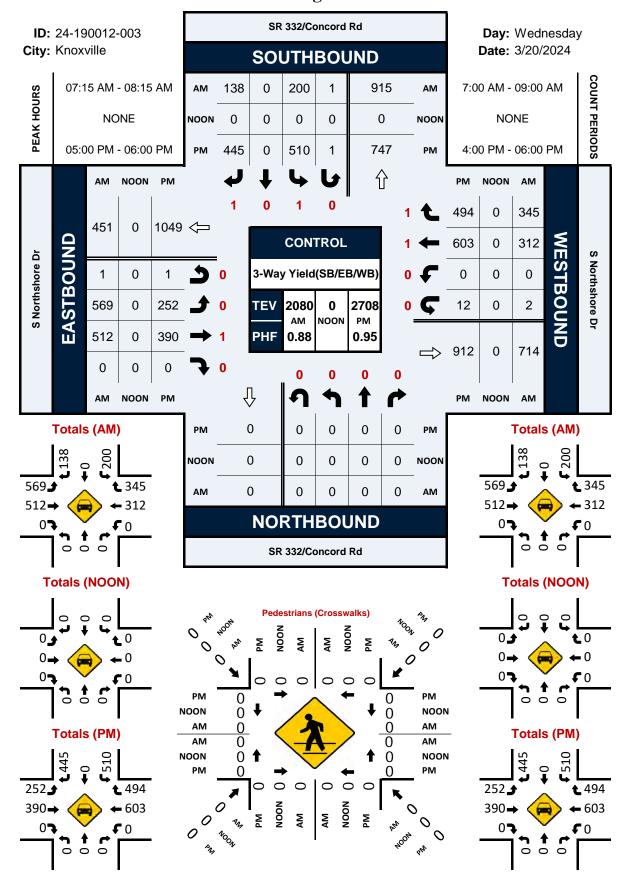
Intersection Turning Movement Count

Location: SR 332/Concord Rd & 2nd Dr/2nd St City: Knoxville Control: 1-Way Stop(EB) Project ID: 24-190012-002 Date: 3/20/2024

| | | (/ | | | | | | | | | | | | | | | |
|------------------|-------|------------|----------|--------|--------|-------------|----------|--------|----------|---------|--------|--------|---------|------------|---------|--------|-----|
| - | | | | | | | | Data - | Totals | | | | | | | | |
| NS/EW Streets: | | SR 332/Co | ncord Rd | | | SR 332/Co | ncord Rd | | | 2nd Dr/ | 2nd St | | | 2nd Dr/2 | 2nd St | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTB | OUND | | |
| AM | 0 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | |
| 7 | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TO |
| 7:00 AM | 0 | 106 | 0 | 0 | 0 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 15 |
| 7:15 AM | 0 | 151 | 0 | 0 | 0 | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 21 |
| 7:30 AM | 0 | 255 | 0 | 0 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 33 |
| 7:45 AM | 0 | 261 | 0 | 0 | 1 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 37 |
| 8:00 AM | 0 | 195 | 0 | 0 | 0 | 113 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 30 |
| 8:15 AM | 0 | 202 | 1 | 0 | 1 | 107 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 31 |
| 8:30 AM | 0 | 186 | 1 | 0 | 1 | 122 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 31 |
| 8:45 AM | 0 | 164 | 1 | 0 | 1 | 86 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 25 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TO |
| TOTAL VOLUMES: | 0 | 1520 | 3 | 0 | 4 | 717 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 9 | 0 | 22 |
| APPROACH %'s: | 0.00% | 99.80% | 0.20% | 0.00% | 0.55% | 99.31% | 0.00% | 0.14% | | | | | 18.18% | 0.00% | 81.82% | 0.00% | |
| PEAK HR : | | 07:30 AM - | 08:30 AM | | | | | | | | | | | | | | TO |
| PEAK HR VOL : | 0 | 913 | 1 | 0 | 2 | 403 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 13 |
| PEAK HR FACTOR : | 0.000 | 0.875 | 0.250 | 0.000 | 0.500 | 0.892 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 | 0.000 | 0.8 |
| | | 0.87 | 75 | | | 0.89 | 98 | | | | | | | 1.00 | 00 | | 0.0 |
| | | NODTU | DOLIND | | | COLUTIUS | DOLIND | | | EASTB | OLIND | | | MECTO | OLIND | | |
| PM | 0 | NORTH 2 | 0 | 0 | 1 | SOUTHI 2 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | WESTB 1 | 0 | 0 | |
| PIVI | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | то |
| 4:00 PM | 0 | 159 | 0 | 0 | 0 | 219 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 38 |
| 4:15 PM | 0 | 155 | 1 | 0 | 0 | 197 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 3! |
| 4:30 PM | 0 | 159 | 1 | 0 | 2 | 227 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 30 |
| 4:45 PM | 0 | 168 | Ö | 0 | 1 | 203 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 3 |
| 5:00 PM | 0 | 170 | 1 | 0 | 0 | 247 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 42 |
| 5:15 PM | 0 | 212 | i | 0 | 1 | 261 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | ò | 0 | 4 |
| 5:30 PM | 0 | 179 | i | 0 | 0 | 253 | 0 | 0 | o i | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 43 |
| 5:45 PM | Ö | 191 | ó | Ö | ĭ | 195 | Ö | Ö | 0 | Ö | Ö | Ö | 3 | Ö | 2 | ő | 39 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TO |
| TOTAL VOLUMES : | 0 | 1393 | 5 | 0 | 5 | 1802 | 0 | 1 | 1 | 0 | 0 | 0 | 6 | 0 | 8 | 0 | 32 |
| APPROACH %'s : | 0.00% | 99.64% | 0.36% | 0.00% | 0.28% | 99.67% | 0.00% | 0.06% | 100.00% | 0.00% | 0.00% | 0.00% | 42.86% | 0.00% | 57.14% | 0.00% | 32 |
| PEAK HR : | | 05:00 PM - | | 0.0070 | 0.2070 | | 0.0070 | 0.0070 | .00.0070 | 0.0070 | 0.0070 | 0.0070 | 12.0070 | 0.0070 | 37.1170 | 0.0070 | TO |
| PEAK HR VOL : | 0 | 752 | 3 | 0 | 2 | 956 | 0 | 0 | 1 | 0 | 0 | 0 | 5 | 0 | 3 | 0 | 17 |
| PEAK HR FACTOR : | 0.000 | 0.887 | 0.750 | 0.000 | 0.500 | 0.916 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.417 | 0.000 | 0.375 | 0.000 | |
| | | 0.007 | | | 3.000 | 0.710 | | 3.000 | 3.200 | 0.000 | | 2.000 | 3 | 0.000 | | 2.000 | 0.9 |

SR 332/Concord Rd & S Northshore Dr

Peak Hour Turning Movement Count



National Data & Surveying Services

Intersection Turning Movement Count

Location: SR 332/Concord Rd & S Northshore Dr City: Knoxville Control: 3-Way Yield(SB/EB/WB)

Project ID: 24-190012-003

| D | ate | э: | 3 | /2 | 0. | 1 | 2(|)2 | 24 | |
|---|-----|----|---|----|----|---|----|----|----|--|

| Control: | 3-Way Yi | eld(SB/EB/W | /B) | | | | | | | | | | | Date: 3 | 3/20/2024 | | |
|--------------------|----------|-------------|------------|-------|------------|-----------|------------|--------|------------|------------|---------|-------|-------|---------------|------------|-------|------------|
| Г | | | | | | | | Data - | Totals | | | | | | | | |
| NS/EW Streets: | | SR 332/C | oncord Rd | | | SR 332/Co | ncord Rd | | | S Northsh | nore Dr | | | S Northsi | nore Dr | | |
| | | NORT | HBOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| AM | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTA |
| 7:00 AM | 0 | 0 | 0 | 0 | 30 | 0 | 9 | 0 | 65 | 165 | 0 | 0 | 0 | 29 | 52 | 0 | 350 |
| 7:15 AM | 0 | 0 | 0 | 0 | 35 | 0 | 14 | 0 | 88 | 187 | 0 | 0 | 0 | 49 | 68 | 0 | 441 |
| 7:30 AM 7:45 AM | 0 | 0 | 0 | 0 | 52 52 | 0 | 34 44 | 1 | 153 159 | 113 120 | 0 | 1 | 0 | 92 98 | 102 120 | 1 | 549 594 |
| 8:00 AM | 0 | 0 | 0 | 0 | 61 | 0 | 46 | 0 | 169 | 92 | 0 | 0 | 0 | 73 | 55 | 0 | 496 |
| 8:15 AM | 0 | 0 | 0 | 0 | 60 | 0 | 38 | 0 | 80 | 96 | 0 | 0 | 0 | 74 | 88 | 0 | 436 |
| 8:30 AM | 0 | 0 | 0 | Ö | 72 | 0 | 57 | 0 | 75 | 108 | 0 | 0 | 0 | 72 | 93 | 0 | 477 |
| 8:45 AM | Ō | 0 | 0 | 0 | 39 | 0 | 48 | 1 | 81 | 113 | 0 | 0 | 0 | 71 | 79 | 0 | 432 |
| | | | | | | | | | | | | | | | | | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTA |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 401 | 0 | 290 | 2 | 870 | 994 | 0 | 1 | 0 | 558 | 657 | 2 | 3775 |
| APPROACH %'s: | | | | | 57.86% | 0.00% | 41.85% | 0.29% | 46.65% | 53.30% | 0.00% | 0.05% | 0.00% | 45.85% | 53.99% | 0.16% | |
| PEAK HR : | | | - 08:15 AM | | | | | | | | | | _ | | | _ | TOTA |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 200 | 0 | 138 | 1 | 569 | 512 | 0 | 1 | 0 | 312 | 345 | 2 | 2080 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.820 | 0.000 | 0.750 | 0.250 | 0.842 | 0.684 | 0.000 | 0.250 | 0.000 | 0.796 0.75 | 0.719 | 0.500 | 0.875 |
| | | | | | | 0.7 | 72 | | | 0.77 | 0 | | | 0.7 |)2 | | |
| | | NORT | HBOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| PM | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTA |
| 4:00 PM | 0 | 0 | 0 | 0 | 101 | 0 | 107 | 0 | 55 | 84 | 0 | 1 | 0 | 120 | 95 | 0 | 563 |
| 4:15 PM | 0 | 0 | 0 | 0 | 115 | 0 | 95 | 0 | 50 | 90 | 0 | 0 | 0 | 120 | 101 | 1 | 572 |
| 4:30 PM | 0 | 0 | 0 | 0 | 115 | 0 | 106 | 0 | 72 | 85 | 0 | 0 | 0 | 122 | 102 | 0 | 602 |
| 4:45 PM | 0 | 0 | 0 | 0 | 143 | 0 | 52 | 1 | 52 | 92 | 0 | 1 | 0 | 149 | 104 | 1 | 595 |
| 5:00 PM 5:15 PM | 0 | 0 | 0 | 0 | 129 133 | 0 | 117 136 | 0 | 63 71 | 98 81 | 0 | 0 | 0 | 153 157 | 116 127 | 1 3 | 677 709 |
| 5:30 PM | 0 | 0 | 0 | 0 | 147 | 0 | 100 | 0 | 53 | 109 | 0 | 0 | 0 | 157 | 130 | 7 | 697 |
| 5:45 PM | 0 | 0 | 0 | 0 | 101 | 0 | 92 | 1 | 65 | 109 | 0 | 0 | 0 | 142 | 121 | 1 | 625 |
| 3.43 T W | Ü | · · | · · | Ü | 101 | · | /2 | • | 05 | 102 | · · | · | · | 142 | 121 | ' | 023 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTA |
| TOTAL VOLUMES: | 0 | 0 | 0 | 0 | 984 | 0 | 805 | 2 | 481 | 741 | 0 | 3 | 0 | 1114 | 896 | 14 | 5040 |
| APPROACH %'s: | | | | | 54.94% | 0.00% | 44.95% | 0.11% | 39.27% | 60.49% | 0.00% | 0.24% | 0.00% | 55.04% | 44.27% | 0.69% | |
| PEAK HR : | | | - 06:00 PM | | | | | | | | | | | | | | TOTA |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 510 | 0 | 445 | 1 | 252 | 390 | 0 | 1 | 0 | 603 | 494 | 12 | 2708 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.867 | 0.000 | 0.818 | 0.250 | 0.887 | 0.894 | 0.000 | 0.250 | 0.000 | 0.960 | 0.950 | 0.429 | 0.955 |
| | | | | | | 0.88 | 38 | | | 0.96 | 3 | | | 0.96 | 53 | | 0.755 |

APPENDIX B - TRIP GENERATION INFORMATION



Land Use: 934 Fast-Food Restaurant with Drive-Through Window

Description

This land use includes any fast-food restaurant with a drive-through window. This type of restaurant is characterized by a large drive-through and large carry-out clientele, long hours of service (some are open for breakfast, all are open for lunch and dinner, some are open late at night or 24 hours a day) and high turnover rates for eat-in customers. The restaurant does not provide table service. A patron generally orders from a menu board and pays before receiving the meal. A typical duration of stay for an eat-in patron is less than 30 minutes. Fast casual restaurant (Land Use 930), high-turnover (sit-down) restaurant (Land Use 932), fast-food restaurant without drive-through window (Land Use 933), and fast-food restaurant with drive-through window and no indoor seating (Land Use 935) are related uses.

Additional Data

Users should exercise caution when applying statistics during the AM peak periods, as the sites contained in the database for this land use may or may not be open for breakfast. In cases where it was confirmed that the sites were not open for breakfast, data for the AM peak hour of the adjacent street traffic were removed from the database.

If the restaurant has outdoor seating, its area is not included in the overall gross floor area. For a restaurant that has significant outdoor seating, the number of seats may be more reliable than GFA as an independent variable on which to establish a trip generation rate.

The technical appendices provide supporting information on time-of-day distributions for this land use. The appendices can be accessed through either the ITETripGen web app or the trip generation resource page on the ITE website (https://www.ite.org/technical-resources/topics/trip-and-parking-generation/).

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in Alaska, Alberta (CAN), California, Colorado, Florida, Indiana, Kentucky, Maryland, Massachusetts, Minnesota, Montana, New Hampshire, New Jersey, New York, North Carolina, Ohio, Pennsylvania, South Dakota, Texas, Vermont, Virginia, Washington, and Wisconsin.

Source Numbers

163, 164, 168, 180, 181, 241, 245, 278, 294, 300, 301, 319, 338, 340, 342, 358, 389, 438, 502, 552, 577, 583, 584, 617, 640, 641, 704, 715, 728, 810, 866, 867, 869, 885, 886, 927, 935, 962, 977, 1050, 1053, 1054



Fast-Food Restaurant with Drive-Through Window (934)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday

Setting/Location: General Urban/Suburban

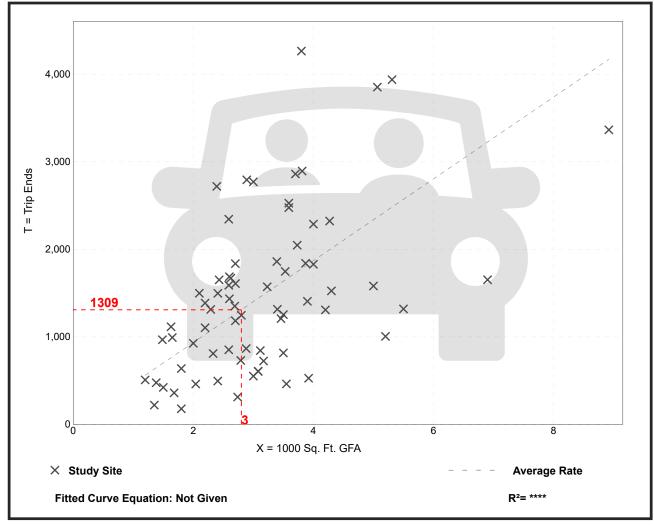
Number of Studies: 71 Avg. 1000 Sq. Ft. GFA: 3

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 467.48 | 98.89 - 1137.66 | 238.62 |

Data Plot and Equation



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Institute of Transportation Engineers

Fast-Food Restaurant with Drive-Through Window (934)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

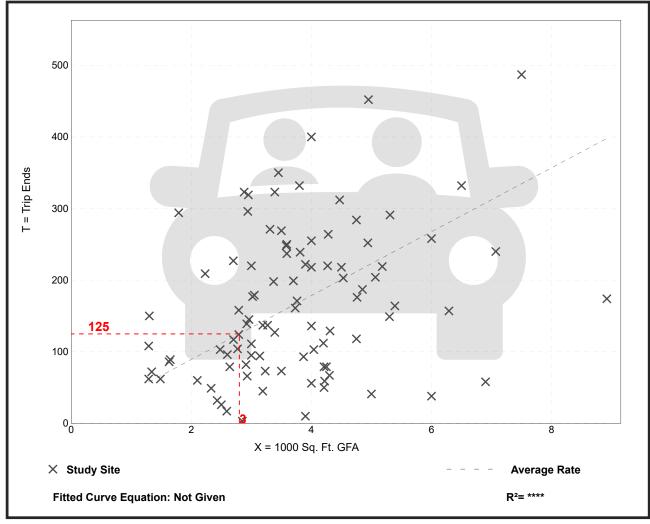
Number of Studies: 96 Avg. 1000 Sq. Ft. GFA: 4

Directional Distribution: 51% entering, 49% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 44.61 | 1.05 - 164.25 | 27.14 |

Data Plot and Equation



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Fast-Food Restaurant with Drive-Through Window (934)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

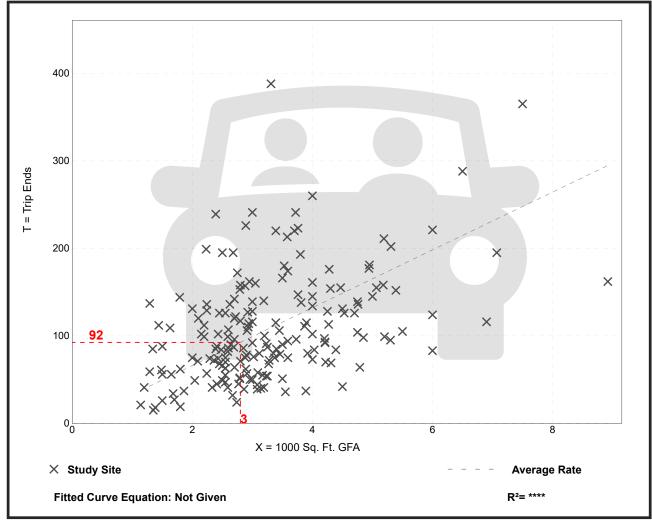
Number of Studies: 190 Avg. 1000 Sq. Ft. GFA: 3

Directional Distribution: 52% entering, 48% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 33.03 | 8.77 - 117.22 | 17.59 |

Data Plot and Equation



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Land Use: 945 **Convenience Store/Gas Station**

Description

A convenience store/gas station is a facility with a co-located convenience store and gas station. The convenience store sells grocery and other everyday items that a person may need or want as a matter of convenience. The gas station sells automotive fuels such as gasoline and diesel.

A convenience store/gas station is typically located along a major thoroughfare to optimize motorist convenience. Extended hours of operation (with many open 24 hours, 7 days a week) are common at these facilities.

The convenience store product mix typically includes pre-packaged grocery items, beverages, dairy products, snack foods, confectionary, tobacco products, over-the-counter drugs, and toiletries. A convenience store may sell alcohol, often limited to beer and wine. Coffee and premade sandwiches are also commonly sold at a convenience store. Made-to-order food orders are sometimes offered. Some stores offer limited seating.

The sites in this land use include both self-pump and attendant-pumped fueling positions and both pre-pay and post-pay operations.

Convenience store (Land Use 851), gasoline/service station (Land Use 944), and truck stop (Land Use 950) are related uses.

Land Use Subcategory

Multiple subcategories were added to this land use to allow for multi-variable evaluation of sites with single-variable data plots. All study sites are assigned to one of three subcategories, based on the number of vehicle fueling positions (VFP) at the site: between 2 and 8 VFP, between 9 and 15 VFP, and between 16 and 24 VFP. For each VFP range subcategory, data plots are presented with GFA as the independent variable for all time periods and trip types for which data are available. The use of both GFA and VFP (as the independent variable and land use subcategory, respectively) provides a significant improvement in the reliability of a trip generation estimate when compared to the single-variable data plots in prior editions of Trip Generation Manual.

Further, the study sites were also assigned to one of three other subcategories, based on the gross floor area (GFA) of the convenience store at the site: between 2,000 and 4,000 square feet, between 4,000 and 5,500 square feet, and between 5,500 and 10,000 square feet. For each GFA subcategory range, data plots are presented with VFP as the independent variable for all time periods and trip types for which data are available. The use of both VFP and GFA (as the independent variable and land use subcategory, respectively) provides a significant improvement in the reliability of a trip generation estimate when compared to the single-variable data plots in prior editions of *Trip Generation Manual*.



When analyzing the convenience store/gas station land use with each combination of GFA and VFP values as described above, the two sets of data plots will produce two estimates of sitegenerated trips. Both values can be considered when determining a site trip generation estimate.

Data plots are also provided for three additional independent variables: AM peak hour traffic on adjacent street, PM peak hour traffic on adjacent street, and employees. These independent variables are intended to be analyzed as single independent variables and do not have subcategories associated with them. Within the data plots and within the ITETripGen web app, these plots are found under the land use subcategory "none."

Additional Data

ITE recognizes there are existing convenience store/gas station sites throughout North America that are larger than the sites presented in the data plots. However, the ITE database does not include any site with more than 24 VFP or any site with gross floor area greater than 10,000 square feet. Submission of trip generation data for larger sites is encouraged.

The technical appendices provide supporting information on time-of-day distributions for this land use. The appendices can be accessed through either the ITETripGen web app or the trip generation resource page on the ITE website (https://www.ite.org/technical-resources/topics/tripand-parking-generation/).

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in Alberta (CAN), Arkansas, California, Connecticut, Delaware, Florida, Indiana, Iowa, Kentucky, Maryland, Massachusetts, Minnesota, Nevada, New Hampshire, New Jersey, Pennsylvania, Rhode Island, South Dakota, Texas, Utah, Vermont, Washington, and Wisconsin.

Source Numbers

221, 245, 274, 288, 300, 340, 350, 351, 352, 355, 359, 385, 440, 617, 718, 810, 813, 844, 850, 853, 864, 865, 867, 869, 882, 883, 888, 904, 926, 927, 936, 938, 954, 960, 962, 977, 1004, 1024, 1025, 1027, 1052



Convenience Store/Gas Station - GFA (5.5-10k)

(945)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday

Setting/Location: General Urban/Suburban

Number of Studies: 1

Avg. Num. of Vehicle Fueling Positions: 12

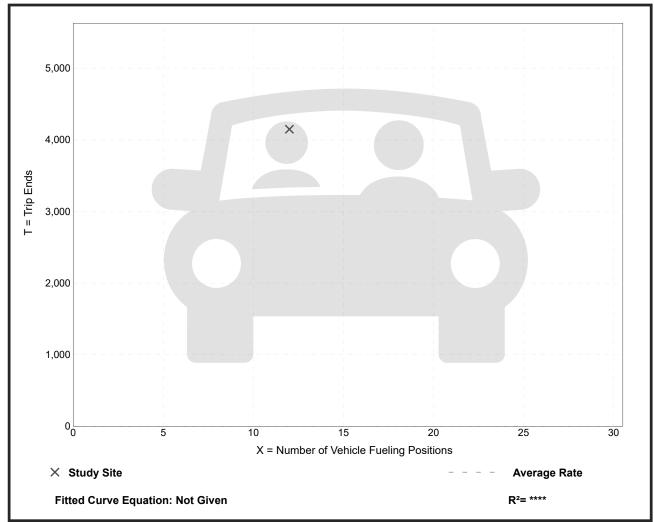
Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

| Average Rate | Range of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 345.75 | 345.75 - 345.75 | * |

Data Plot and Equation

Caution – Small Sample Size



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Convenience Store/Gas Station - GFA (5.5-10k) (945)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

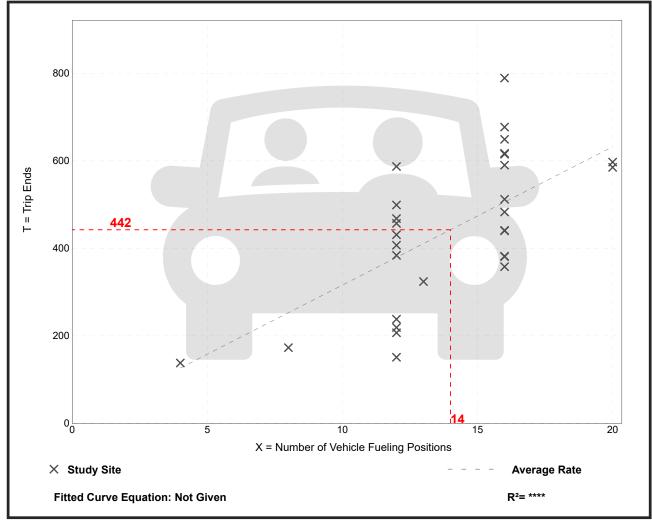
Number of Studies: 29 Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 31.60 | 12.58 - 49.31 | 9.10 |

Data Plot and Equation



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Convenience Store/Gas Station - GFA (5.5-10k) (945)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 29

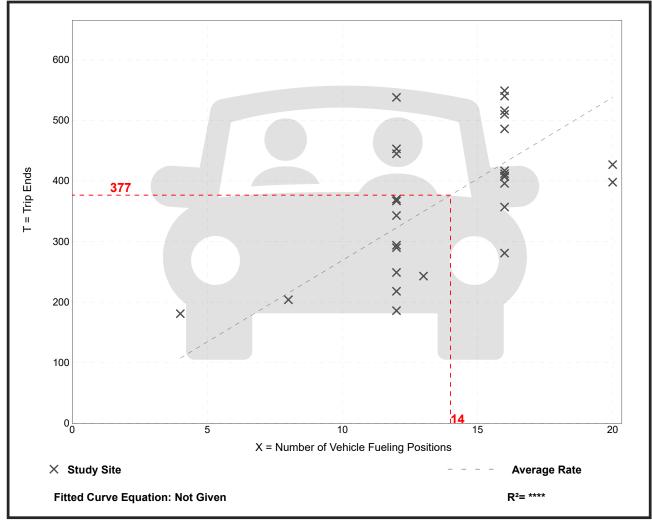
Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 26.90 | 15.50 - 45.25 | 6.87 |

Data Plot and Equation



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R-10

| NCHRP 684 Internal Trip Capture Estimation Tool | | | | | | | | |
|--|---------------------|---|---------------|-----------|--|--|--|--|
| Project Name: E-Z Stop Concord Organization: Cannon & Cannon, Inc. | | | | | | | | |
| Project Location: | Knoxville, TN | | Performed By: | WDR | | | | |
| Scenario Description: | Full Buildout | Ī | Date: | 4/10/2024 | | | | |
| Analysis Year: | 2026 | Ī | Checked By: | | | | | |
| Analysis Period: | AM Street Peak Hour | | Date: | | | | | |

| Table 1-A: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate) | | | | | | | |
|--|-----------|------------------|-----------------|--|-------|--------------------------------------|---------|
| 1 111 | Developm | ent Data (For In | formation Only) | | | Estimated Vehicle-Trips ³ | |
| Land Use | ITE LUCs1 | Quantity | Units | | Total | Entering | Exiting |
| Office | n/a | n/a | n/a | | 0 | 0 | 0 |
| Retail | 945 | 7,015sf | n/a | | 442 | 221 | 221 |
| Restaurant | 934 | 5,600sf | n/a | | 250 | 128 | 122 |
| Cinema/Entertainment | n/a | n/a | n/a | | 0 | 0 | 0 |
| Residential | n/a | n/a | n/a | | 0 | 0 | 0 |
| Hotel | n/a | n/a | n/a | | 0 | 0 | 0 |
| All Other Land Uses ² | n/a | n/a | n/a | | 0 | 0 | 0 |
| | | | | | 692 | 349 | 343 |

| Table 2-A: Mode Split and Vehicle Occupancy Estimates | | | | | | | |
|---|------------|-------------|-----------------|--|---------------|-----------|-----------------|
| Land Use | | Entering Tr | ips | | Exiting Trips | | |
| Land Use | Veh. Occ.4 | % Transit | % Non-Motorized | | Veh. Occ.4 | % Transit | % Non-Motorized |
| Office | | | | | | | |
| Retail | | | | | | | |
| Restaurant | | | | | | | |
| Cinema/Entertainment | | | | | | | |
| Residential | | | | | | | |
| Hotel | | | | | | | |
| All Other Land Uses ² | | | | | | | |

| Table 3-A: Average Land Use Interchange Distances (Feet Walking Distance) | | | | | | | |
|---|------------------|--------|------------|----------------------|-------------|-------|--|
| Origin (From) | Destination (To) | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | |
| Office | | | | | | | |
| Retail | | | | | | | |
| Restaurant | | | | | | | |
| Cinema/Entertainment | | | | | | | |
| Residential | | | | | | | |
| Hotel | | | | | | | |

| | | Table 4-A: Ir | nternal Person-Tri | o Origin-Destination Matrix | * | | | | |
|----------------------|------------------|---------------|--------------------|-----------------------------|-------------|-------|--|--|--|
| Origin (From) | Destination (To) | | | | | | | | |
| Oligin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | |
| Retail | 0 | | 29 | 0 | 0 | 0 | | | |
| Restaurant | 0 | 17 | | 0 | 0 | 0 | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | |
| Hotel | 0 | 0 | 0 | 0 | 0 | | | | |

| Table 5-A | : Computatio | ns Summary | | | | | | | |
|---|--------------|------------|-----|--|--|--|--|--|--|
| Total Entering Exiting | | | | | | | | | |
| All Person-Trips | 692 | 349 | 343 | | | | | | |
| Internal Capture Percentage | 13% | 13% | 13% | | | | | | |
| | | | | | | | | | |
| External Vehicle-Trips ⁵ | 600 | 303 | 297 | | | | | | |
| External Transit-Trips ⁶ | 0 | 0 | 0 | | | | | | |
| External Non-Motorized Trips ⁶ | | | | | | | | | |

| Table 6-A: Internal Trip Capture Percentages by Land Use | | | | | | |
|--|----------------|---------------|--|--|--|--|
| Land Use | Entering Trips | Exiting Trips | | | | |
| Office | N/A | N/A | | | | |
| Retail | 8% | 13% | | | | |
| Restaurant | 23% | 14% | | | | |
| Cinema/Entertainment | N/A | N/A | | | | |
| Residential | N/A | N/A | | | | |
| Hotel | N/A | N/A | | | | |

¹Land Use Codes (LUCs) from *Trip Generation Manual*, published by the Institute of Transportation Engineers.

²Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.

³Enter trips assuming no transit or non-motorized trips (as assumed in ITE *Trip Generation Manual*).

⁴Enter vehicle occupancy assumed in Table 1-A vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be made to Tables 5-A, 9-A (O and D). Enter transit, non-motorized percentages that will result with proposed mixed-use project complete.

Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A.

⁶Person-Trips

*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas A&M Transportation Institute - Version 2013.1

| Project Name: | E-Z Stop Concord | | | |
|------------------|---------------------|--|--|--|
| Analysis Period: | AM Street Peak Hour | | | |

| Table 7-A: Conversion of Vehicle-Trip Ends to Person-Trip Ends | | | | | | | | |
|--|-----------|-------------------------------|---------------|--|------------------------------|---------------|---------------|--|
| Lond Hoo | Tab | Table 7-A (D): Entering Trips | | | Table 7-A (O): Exiting Trips | | | |
| Land Use | Veh. Occ. | Vehicle-Trips | Person-Trips* | | Veh. Occ. | Vehicle-Trips | Person-Trips* | |
| Office | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | |
| Retail | 1.00 | 221 | 221 | | 1.00 | 221 | 221 | |
| Restaurant | 1.00 | 128 | 128 | | 1.00 | 122 | 122 | |
| Cinema/Entertainment | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | |
| Residential | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | |
| Hotel | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | |

| Table 8-A (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin) | | | | | | | | | | | |
|--|--------|------------------|------------|----------------------|-------------|-------|--|--|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | | | |
| Retail | 64 | | 29 | 0 | 31 | 0 | | | | | |
| Restaurant | 38 | 17 | | 0 | 5 | 4 | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | | | |
| Hotel | 0 | 0 | 0 | 0 | 0 | | | | | | |

| Table 8-A (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination) Destination (To) | | | | | | | | |
|---|--------|--------|------------|----------------------|-------------|-------|--|--|
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | |
| Office | | 71 | 29 | 0 | 0 | 0 | | |
| Retail | 0 | | 64 | 0 | 0 | 0 | | |
| Restaurant | 0 | 18 | | 0 | 0 | 0 | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | |
| Residential | 0 | 38 | 26 | 0 | | 0 | | |
| Hotel | 0 | 9 | 8 | 0 | 0 | | | |

| | Table 9-A (D): Internal and External Trips Summary (Entering Trips) | | | | | | | | | | |
|----------------------------------|---|-----------------------|-------|--|-----------------------|-------------------------|----------------------------|--|--|--|--|
| Destination Land Hea | | Person-Trip Estimates | | | | External Trips by Mode* | | | | | |
| Destination Land Use | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | | | |
| Office | 0 | 0 | 0 | | 0 | 0 | 0 | | | | |
| Retail | 17 | 204 | 221 | | 204 | 0 | 0 | | | | |
| Restaurant | 29 | 99 | 128 | | 99 | 0 | 0 | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | | | |
| Residential | 0 | 0 | 0 | | 0 | 0 | 0 | | | | |
| Hotel | 0 | 0 | 0 | | 0 | 0 | 0 | | | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | | | |

| Table 9-A (O): Internal and External Trips Summary (Exiting Trips) | | | | | | | | | |
|--|----------|------------------|-------|--|-------------------------|----------------------|----------------------------|--|--|
| Origin Land Use | ı | Person-Trip Esti | mates | | External Trips by Mode* | | | | |
| Origin Land Ose | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | |
| Office | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Retail | 29 | 192 | 221 | | 192 | 0 | 0 | | |
| Restaurant | 17 | 105 | 122 | | 105 | 0 | 0 | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Residential | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Hotel | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | |

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A ²Person-Trips

³Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator *Indicates computation that has been rounded to the nearest whole number.

| | NCHRP 684 Internal Trip Capture Estimation Tool | | | | | | | | |
|-----------------------|---|--|---------------|-----------------------|--|--|--|--|--|
| Project Name: | E-Z Stop Concord | | Organization: | Cannon & Cannon, Inc. | | | | | |
| Project Location: | Knoxville, TN | | Performed By: | WDR | | | | | |
| Scenario Description: | Full Buildout | | Date: | 4/10/2024 | | | | | |
| Analysis Year: | 2026 | | Checked By: | | | | | | |
| Analysis Period: | PM Street Peak Hour | | Date: | | | | | | |

| Table 1-P: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate) | | | | | | | | | |
|--|-----------|------------------|-----------------|--|--------------------------------------|----------|---------|--|--|
| Land Use | Developme | ent Data (For In | formation Only) | | Estimated Vehicle-Trips ³ | | | | |
| Land OSE | ITE LUCs1 | Quantity | Units | | Total | Entering | Exiting | | |
| Office | n/a | n/a | n/a | | 0 | 0 | 0 | | |
| Retail | 945 | 7,015sf | n/a | | 377 | 188 | 189 | | |
| Restaurant | 934 | 5,600sf | n/a | | 184 | 96 | 88 | | |
| Cinema/Entertainment | n/a | n/a | n/a | | 0 | 0 | 0 | | |
| Residential | n/a | n/a | n/a | | 0 | 0 | 0 | | |
| Hotel | n/a | n/a | n/a | | 0 | 0 | 0 | | |
| All Other Land Uses ² | n/a | n/a | n/a | | 0 | 0 | 0 | | |
| | | | | | 561 | 284 | 277 | | |

| Table 2-P: Mode Split and Vehicle Occupancy Estimates | | | | | | | | | |
|---|------------|-------------|-----------------|--|------------|---------------|-----------------|--|--|
| Land Use | | Entering Tr | ips | | | Exiting Trips | | | |
| Land USE | Veh. Occ.4 | % Transit | % Non-Motorized | | Veh. Occ.4 | % Transit | % Non-Motorized | | |
| Office | | | | | | | | | |
| Retail | | | | | | | | | |
| Restaurant | | | | | | | | | |
| Cinema/Entertainment | | | | | | | | | |
| Residential | | | | | | | | | |
| Hotel | | | | | | | | | |
| All Other Land Uses ² | | | | | | | | | |

| Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance) | | | | | | | | | |
|---|--------|------------------|------------|----------------------|-------------|-------|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | |
| Office | | | | | | | | | |
| Retail | | | | | | | | | |
| Restaurant | | | | | | | | | |
| Cinema/Entertainment | | | | | | | | | |
| Residential | | | | | | | | | |
| Hotel | | | | | | | | | |

| Table 4-P: Internal Person-Trip Origin-Destination Matrix* | | | | | | | | | | |
|--|--------|------------------|------------|----------------------|-------------|-------|--|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | | |
| Retail | 0 | | 28 | 0 | 0 | 0 | | | | |
| Restaurant | 0 | 36 | | 0 | 0 | 0 | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | | |
| Hotel | 0 | 0 | 0 | 0 | 0 | | | | | |

| Table 5-P: Computations Summary | | | | | | | | |
|---|-------|----------|---------|--|--|--|--|--|
| | Total | Entering | Exiting | | | | | |
| All Person-Trips | 561 | 284 | 277 | | | | | |
| Internal Capture Percentage | 23% | 23% | 23% | | | | | |
| | | | | | | | | |
| External Vehicle-Trips ⁵ | 433 | 220 | 213 | | | | | |
| External Transit-Trips ⁶ | 0 | 0 | 0 | | | | | |
| External Non-Motorized Trips ⁶ | 0 | 0 | 0 | | | | | |

| Table 6-P: Internal Trip Capture Percentages by Land Use | | | | | | | | |
|--|----------------|---------------|--|--|--|--|--|--|
| Land Use | Entering Trips | Exiting Trips | | | | | | |
| Office | N/A | N/A | | | | | | |
| Retail | 19% | 15% | | | | | | |
| Restaurant | 29% | 41% | | | | | | |
| Cinema/Entertainment | N/A | N/A | | | | | | |
| Residential | N/A | N/A | | | | | | |
| Hotel | N/A | N/A | | | | | | |

¹Land Use Codes (LUCs) from *Trip Generation Manual*, published by the Institute of Transportation Engineers.

²Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.

³Enter trips assuming no transit or non-motorized trips (as assumed in ITE *Trip Generation Manual*).

Enter vehicle occupancy assumed in Table 1-P vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be

Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P.

⁶Person-Trips

*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas A&M Transportation Institute - Version 2013.1

| Project Name: | E-Z Stop Concord |
|------------------|---------------------|
| Analysis Period: | PM Street Peak Hour |

| | Table 7-P: Conversion of Vehicle-Trip Ends to Person-Trip Ends | | | | | | | | | | | | |
|----------------------|--|-------------------|---------------|---|------------------------------|---------------|---------------|--|--|--|--|--|--|
| Land Use | Table | 7-P (D): Entering | g Trips | | Table 7-P (O): Exiting Trips | | | | | | | | |
| Land Use | Veh. Occ. | Vehicle-Trips | Person-Trips* | 1 | Veh. Occ. | Vehicle-Trips | Person-Trips* | | | | | | |
| Office | 1.00 | 1.00 0 0 | | 1 | 1.00 | 0 | 0 | | | | | | |
| Retail | 1.00 | 1.00 188 188 | | 1 | 1.00 | 189 | 189 | | | | | | |
| Restaurant | 1.00 | 96 | 96 | 1 | 1.00 | 88 | 88 | | | | | | |
| Cinema/Entertainment | 1.00 | 0 | 0 | 1 | 1.00 | 0 | 0 | | | | | | |
| Residential | 1.00 | 1.00 0 0 | | | 1.00 | 0 | 0 | | | | | | |
| Hotel | 1.00 | 0 | 0 | 1 | 1.00 | 0 | 0 | | | | | | |

| | Table 8-P (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin) | | | | | | | | | | | | |
|----------------------|--|------------------|------------|----------------------|-------------|-------|--|--|--|--|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Retail | 4 | | 55 | 8 | 49 | 9 | | | | | | | |
| Restaurant | 3 | 36 | | 7 | 16 | 6 | | | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | | | | | |
| Hotel | 0 | 0 | 0 | 0 | 0 | | | | | | | | |

| | Table 8-P (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination) | | | | | | | | | | | | |
|----------------------|---|--------|------------|----------------------|-------------|-------|--|--|--|--|--|--|--|
| Origin (From) | Destination (To) | | | | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | | | |
| Office | | 15 | 2 | 0 | 0 | 0 | | | | | | | |
| Retail | 0 | | 28 | 0 | 0 | 0 | | | | | | | |
| Restaurant | 0 | 94 | | 0 | 0 | 0 | | | | | | | |
| Cinema/Entertainment | 0 | 8 | 3 | | 0 | 0 | | | | | | | |
| Residential | 0 | 19 | 13 | 0 | | 0 | | | | | | | |
| Hotel | 0 | 4 | 5 | 0 | 0 | | | | | | | | |

| | Tab | ole 9-P (D): Interi | nal and External T | rips | Summary (Entering Tr | ips) | | | |
|----------------------------------|----------|---------------------|--------------------|------|-------------------------|----------------------|----------------------------|--|--|
| Destination Land Use | Pe | erson-Trip Estima | ites | | External Trips by Mode* | | | | |
| Destination Land Ose | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | |
| Office | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Retail | 36 | 152 | 188 | | 152 | 0 | 0 | | |
| Restaurant | 28 | 68 | 96 | | 68 | 0 | 0 | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Residential | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Hotel | 0 | 0 | 0 | | 0 0 | | 0 | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | |

| | Table 9-P (O): Internal and External Trips Summary (Exiting Trips) | | | | | | | | | | | | |
|----------------------------------|--|-------------------|-------|--|-------------------------|----------------------|----------------------------|--|--|--|--|--|--|
| Origin Land Use | Po | erson-Trip Estima | tes | | External Trips by Mode* | | | | | | | | |
| Origin Land Ose | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | | | | | |
| Office | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | | |
| Retail | 28 | 161 | 189 | | 161 0 0 | | | | | | | | |
| Restaurant | 36 | 52 | 88 | | 52 | 0 | 0 | | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | | |
| Residential | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | | |
| Hotel | 0 | 0 | 0 | | 0 0 | | 0 | | | | | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | | |

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P

²Person-Trips

³Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator

*Indicates computation that has been rounded to the nearest whole number.

FULL BUILD-OUT TRIP GENERATION

| | | | Weekday | AM Peak Hour | PM Peak Hour |
|-----------------------------|----------|----------|---------------|--------------|--------------|
| Land Use | ITE Code | Size | (Trips / Day) | (Trips/HR) | (Trips/HR) |
| Convenience Store/Gas Stat | 945 | 7,015 sf | 4,841 | 442 | 377 |
| Entering Trips | 70% | Pass-by | 2,420 | 221 | 188 |
| Exiting Trips | | | 2,421 | 221 | 189 |
| Fast Food Restaurant with [| 934 | 5,600 sf | 2,618 | 250 | 184 |
| Entering Trips | 40% | Pass-by | 1,309 | 128 | 96 |
| Exiting Trips | | | 1,309 | 122 | 88 |
| n/a | n/a | n/a | | | |
| Entering Trips | | | | | |
| Exiting Trips | | | | | |
| n/a | n/a | n/a | | | |
| Entering Trips | | | | | |
| Exiting Trips | | | | | |
| n/a | n/a | n/a | | | |
| Entering Trips | | | | | |
| Exiting Trips | | | | | |
| n/a | n/a | n/a | | | |
| Entering Trips | | | | | |
| Exiting Trips | | | | | |
| TOTAL TRIPS | | | 7,459 | 692 | 561 |
| Entering Trips | | | 3,729 | 349 | 284 |
| Exiting Trips | | | 3,730 | 343 | 277 |
| INTERNAL TRIPS | | | | 90 | 129 |
| Entering Trips | | | | 45 | 65 |
| Exiting Trips | | | | 45 | 64 |
| NET EXTERNAL TRIPS | | | 7,459 | 602 | 432 |
| Entering Trips | | | 3,729 | 304 | 219 |
| Exiting Trips | | | 3,730 | 298 | 213 |
| NET EXTERNAL TRIPS | | | | | |
| Pass-by Trips | | | 4,194 | 387 | 319 |
| Entering Trips | | | 2,097 | 195 | 161 |
| Exiting Trips | | | 2,097 | 192 | 158 |
| Non-Pass-by Trips | | | 3,265 | 215 | 113 |
| Entering Trips | | | 1,632 | 109 | 58 |
| Exiting Trips | | | 1,633 | 106 | 55 |

APPENDIX C - CAPACITY ANALYSES



CAPACITY AND LEVEL-OF-SERVICE CONCEPTS

In a general sense, a roadway is similar to a pipeline or other material carrying conduit in that it has a certain capacity for the amount of material (vehicles) that it can efficiently carry. As the number of vehicles in a given time period gradually increases, the quality of traffic flow gradually decreases. On roadway sections this results in increasing turbulence in the traffic stream, and at intersections it results in increasing stops and delay. As the volumes begin to approach the capacity of the facility, these problems rapidly magnify, with resulting serious levels of congestion, stops, delay, excess fuel consumption, pollutant emissions, etc.

The Transportation Research Board has published the <u>Year 2010 Highway Capacity Manual (HCM2010)</u>, which establishes theoretical techniques to quantify the capacity conditions on all types of roadways, intersections, ramps, pedestrian facilities, etc. A basic concept that is applicable to most of these techniques is the idea of level of service (LOS). This concept establishes a rating system that quantifies the quality of traffic flow, as perceived by motorists and/or passengers. The general system is similar to a school grade scale, and is outlined as follows:

| Level of Service (LOS) | General Quality of Traffic Flow | Description of Corresponding Conditions |
|---------------------------|------------------------------------|---|
| А | Excellent | Roadways – Free flow, high maneuverability Intersections – Very few stops, very low delay |
| В | Very Good | Roadways – Free flow, slightly lower maneuverability Intersections – Minor stops, low delay |
| С | Good | Roadways – Stable flow, restricted maneuverability Intersections – Significant stops, significant delay |
| D | Fair | Roadways – Marginally stable flow, congestion seriously restricts maneuverability Intersections – High stops, long but tolerable delay |
| Е | Poor | Roadways – Unstable flow*, lower operating speeds, congestion severely restricts maneuverability Intersections – All vehicles stop, very long queues and very long intolerable delay |
| F | Very Poor | Roadways – Forced flow, stoppages may be lengthy, congestion severely restricts maneuverability Intersections – All vehicles stop, extensive queues and extremely long intolerable delay |

^{*}Unstable flow is such that minor fluctuations or disruptions can result in rapid degradation to LOS F.

LOS CRITERIA: SIGNALIZED & UNSIGNALIZED INTERSECTIONS

| LOS | CONTROL DELAY (S/VEH) | | | | | | | | | |
|-----|-----------------------|--------------|------------|--|--|--|--|--|--|--|
| LO3 | SIGNALIZED | UNSIGNALIZED | ROUNDABOUT | | | | | | | |
| A | ≤10 | ≤10 | ≤10 | | | | | | | |
| В | >10-20 | >10-15 | >10-15 | | | | | | | |
| С | >20-35 | >15-25 | >15-25 | | | | | | | |
| D | >35-55 | >25-35 | >25-35 | | | | | | | |
| E | >55-80 | >35-50 | >35-50 | | | | | | | |
| F | >80 | >50 | >50 | | | | | | | |

Another measure of intersection capacity that is often used in the evaluation of intersection operations is the volume to capacity (V/C) ratio. This ratio is defined as "the ratio of flow rate to capacity", and is a good measure of how much of an intersection's available capacity has been used up by the analysis volumes. Conversely, it also provides an indication of the reserve capacity available for future growth in traffic volumes.

The Intersection Capacity Utilization (ICU) is another measure that expresses a value similar to the V/C ratio. Specifically, the ICU method "sums the amount of the time required to serve all movements at saturation for a given cycle length and divides by that reference cycle length." The ICU is considered a more accurate measure of volume to capacity conditions for a signalized intersection, primarily because it accounts for the effects of the signal timing on intersection capacity.

Lanes, Volumes, Timings 1: Concord Drive & Turkey Creek Road/Summerdale Drive

| | • | - | • | • | ← | • | 4 | † | ~ | / | ţ | 4 |
|-------------------------|-------|-------|------|-------|----------|------|-------|------------|------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | 4 | | | 4 | | ሻ | ∱ } | | ሻ | ^ | 7 |
| Traffic Volume (vph) | 512 | 0 | 73 | 8 | 0 | 21 | 33 | 941 | 5 | 6 | 343 | 186 |
| Future Volume (vph) | 512 | 0 | 73 | 8 | 0 | 21 | 33 | 941 | 5 | 6 | 343 | 186 |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 |
| Frt | | 0.962 | | | 0.902 | | | 0.999 | | | | 0.850 |
| Flt Protected | 0.950 | 0.964 | | | 0.987 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1681 | 1641 | 0 | 0 | 1658 | 0 | 1770 | 3536 | 0 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.950 | 0.964 | | | 0.987 | | 0.478 | | | 0.149 | | |
| Satd. Flow (perm) | 1681 | 1641 | 0 | 0 | 1658 | 0 | 890 | 3536 | 0 | 278 | 3539 | 1583 |
| Satd. Flow (RTOR) | | 205 | | | 217 | | | | | | | 211 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Shared Lane Traffic (%) | 42% | | | | | | | | | | | |
| Lane Group Flow (vph) | 338 | 327 | 0 | 0 | 33 | 0 | 38 | 1075 | 0 | 7 | 390 | 211 |
| Turn Type | Split | NA | | Split | NA | | pm+pt | NA | | pm+pt | NA | pm+ov |
| Protected Phases | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Permitted Phases | | | | | | | 6 | | | 2 | | 2 |
| Detector Phase | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 6.0 | 6.0 | | 6.0 | 15.0 | | 6.0 | 15.0 | 8.0 |
| Minimum Split (s) | 16.0 | 16.0 | | 12.0 | 12.0 | | 14.0 | 24.0 | | 13.0 | 24.0 | 16.0 |
| Total Split (s) | 38.0 | 38.0 | | 16.0 | 16.0 | | 28.0 | 59.0 | | 17.0 | 59.0 | 38.0 |
| Total Split (%) | 27.0% | 27.0% | | 11.3% | 11.3% | | 19.9% | 41.8% | | 12.1% | 41.8% | 27.0% |
| Yellow Time (s) | 4.0 | 4.0 | | 3.5 | 3.5 | | 4.0 | 5.5 | | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | | 2.5 | 2.5 | | 3.5 | 3.5 | | 3.0 | 3.5 | 3.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.5 | | | 6.0 | | 7.5 | 9.0 | | 7.0 | 9.0 | 7.5 |
| Lead/Lag | Lead | Lead | | Lag | Lag | | Lead | Lag | | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | None | | None | None | | None | Min | | None | Min | None |
| Act Effct Green (s) | 28.2 | 28.2 | | | 6.4 | | 42.5 | 39.7 | | 39.4 | 34.1 | 75.9 |
| Actuated g/C Ratio | 0.30 | 0.30 | | | 0.07 | | 0.45 | 0.42 | | 0.42 | 0.36 | 0.81 |
| v/c Ratio | 0.67 | 0.51 | | | 0.11 | | 0.08 | 0.72 | | 0.03 | 0.30 | 0.16 |
| Control Delay | 40.0 | 15.6 | | | 0.7 | | 15.4 | 26.9 | | 15.2 | 24.7 | 1.1 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.0 | 15.6 | | | 0.7 | | 15.4 | 26.9 | | 15.2 | 24.7 | 1.1 |
| LOS | D | В | | | Α | | В | С | | В | С | Α |
| Approach Delay | | 28.0 | | | 0.7 | | | 26.5 | | | 16.4 | |
| Approach LOS | | С | | | Α | | | С | | _ | В | |
| Queue Length 50th (ft) | 198 | 62 | | | 0 | | 14 | 298 | | 2 | 107 | 0 |
| Queue Length 95th (ft) | #404 | 178 | | | 0 | | 31 | 443 | | 10 | 145 | 19 |
| Internal Link Dist (ft) | | 497 | | | 673 | | | 435 | | | 693 | |
| Turn Bay Length (ft) | | | | | | | 70 | | | 95 | | 475 |
| Base Capacity (vph) | 579 | 700 | | | 379 | | 616 | 2439 | | 291 | 2001 | 1312 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.58 | 0.47 | | | 0.09 | | 0.06 | 0.44 | | 0.02 | 0.19 | 0.16 |
| Intersection Summary | | | | | | | | | | | | |

Timing Plan: AM Cannon & Cannon, Inc.

Synchro 11 Report Page 1

1: Concord Drive & Turkey Creek Road/Summerdale Drive

Cycle Length: 141

Actuated Cycle Length: 93.6

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.72

Intersection Signal Delay: 24.0

Intersection Capacity Utilization 64.2%

ICU Level of Service C

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Concord Drive & Turkey Creek Road/Summerdale Drive



Lanes, Volumes, Timings 1: Concord Drive & Turkey Creek Road/Summerdale Drive

| | • | - | • | • | ← | • | 4 | † | <i>></i> | / | ţ | 4 |
|-------------------------|-------|-------|------|-------|----------|------|-------|------------|-------------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | 4 | | | 4 | | ሻ | ∱ } | | ሻ | ^ | 7 |
| Traffic Volume (vph) | 251 | 1 | 97 | 4 | 3 | 16 | 125 | 659 | 10 | 8 | 888 | 375 |
| Future Volume (vph) | 251 | 1 | 97 | 4 | 3 | 16 | 125 | 659 | 10 | 8 | 888 | 375 |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 |
| Frt | | 0.913 | | | 0.903 | | | 0.998 | | | | 0.850 |
| Flt Protected | 0.950 | 0.980 | | | 0.992 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1681 | 1583 | 0 | 0 | 1669 | 0 | 1770 | 3532 | 0 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.950 | 0.980 | | | 0.992 | | 0.157 | | | 0.370 | | |
| Satd. Flow (perm) | 1681 | 1583 | 0 | 0 | 1669 | 0 | 292 | 3532 | 0 | 689 | 3539 | 1583 |
| Satd. Flow (RTOR) | | 45 | | | 18 | | | 1 | | | | 417 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Shared Lane Traffic (%) | 28% | | | | | | | | | | | |
| Lane Group Flow (vph) | 201 | 187 | 0 | 0 | 25 | 0 | 139 | 743 | 0 | 9 | 987 | 417 |
| Turn Type | Split | NA | | Split | NA | | pm+pt | NA | | pm+pt | NA | pm+ov |
| Protected Phases | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Permitted Phases | | | | | | | 6 | | | 2 | | 2 |
| Detector Phase | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 6.0 | 6.0 | | 6.0 | 15.0 | | 6.0 | 15.0 | 8.0 |
| Minimum Split (s) | 16.0 | 16.0 | | 12.0 | 12.0 | | 14.0 | 24.0 | | 13.0 | 24.0 | 16.0 |
| Total Split (s) | 38.0 | 38.0 | | 16.0 | 16.0 | | 28.0 | 59.0 | | 17.0 | 59.0 | 38.0 |
| Total Split (%) | 27.0% | 27.0% | | 11.3% | 11.3% | | 19.9% | 41.8% | | 12.1% | 41.8% | 27.0% |
| Yellow Time (s) | 4.0 | 4.0 | | 3.5 | 3.5 | | 4.0 | 5.5 | | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | | 2.5 | 2.5 | | 3.5 | 3.5 | | 3.0 | 3.5 | 3.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.5 | | | 6.0 | | 7.5 | 9.0 | | 7.0 | 9.0 | 7.5 |
| Lead/Lag | Lead | Lead | | Lag | Lag | | Lead | Lag | | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | None | | None | None | | None | Min | | None | Min | None |
| Act Effct Green (s) | 19.9 | 19.9 | | | 7.0 | | 58.5 | 54.8 | | 47.6 | 38.9 | 68.5 |
| Actuated g/C Ratio | 0.20 | 0.20 | | | 0.07 | | 0.58 | 0.54 | | 0.47 | 0.38 | 0.68 |
| v/c Ratio | 0.61 | 0.54 | | | 0.19 | | 0.44 | 0.39 | | 0.02 | 0.72 | 0.35 |
| Control Delay | 48.7 | 36.4 | | | 33.3 | | 16.6 | 16.7 | | 13.2 | 31.7 | 1.5 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 48.7 | 36.4 | | | 33.3 | | 16.6 | 16.7 | | 13.2 | 31.7 | 1.5 |
| LOS | D | D | | | С | | В | В | | В | С | Α |
| Approach Delay | | 42.8 | | | 33.3 | | | 16.7 | | | 22.7 | |
| Approach LOS | | D | | | С | | | В | | _ | С | |
| Queue Length 50th (ft) | 134 | 92 | | | 5 | | 44 | 148 | | 3 | 302 | 0 |
| Queue Length 95th (ft) | 248 | 193 | | | 36 | | 92 | 293 | | 12 | 468 | 33 |
| Internal Link Dist (ft) | | 497 | | | 673 | | | 435 | | | 693 | |
| Turn Bay Length (ft) | | | | | | | 70 | | | 95 | | 475 |
| Base Capacity (vph) | 546 | 544 | | | 193 | | 491 | 2334 | | 468 | 1884 | 1356 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.37 | 0.34 | | | 0.13 | | 0.28 | 0.32 | | 0.02 | 0.52 | 0.31 |
| Intersection Summary | | | | | | | | | | | | |

Timing Plan: PM Cannon & Cannon, Inc.

Synchro 11 Report Page 1

1: Concord Drive & Turkey Creek Road/Summerdale Drive

Cycle Length: 141

Actuated Cycle Length: 101.1

Natural Cycle: 75

Control Type: Actuated-Uncoordinated

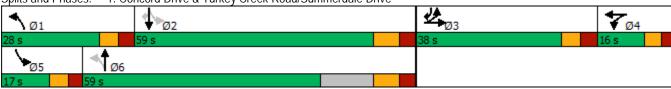
Maximum v/c Ratio: 0.72

Intersection Signal Delay: 23.7

Intersection Capacity Utilization 68.1%

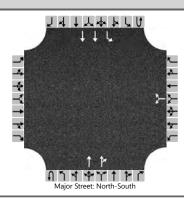
Analysis Period (min) 15

Splits and Phases: 1: Concord Drive & Turkey Creek Road/Summerdale Drive



| | HCS Two-Way Stop-Control Report | | | | | | | | | | |
|--------------------------|---------------------------------|----------------------------|---------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive | | | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut | | | | | | | | |
| Date Performed | 4/10/2024 | East/West Street | 2nd Drive | | | | | | | | |
| Analysis Year | 2024 | North/South Street | Concord Road | | | | | | | | |
| Time Analyzed | AM Peak | Peak Hour Factor | 0.89 | | | | | | | | |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 | | | | | | | | |
| Project Description | 2024 Existing AM Peak | | | | | | | | | | |

Lanes

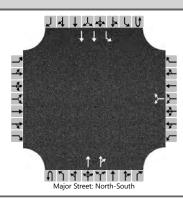


| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | |
|---|--------|---------------------|--------|----|------|------|------|------|------------|---|-----|----|-------|-------|-----|---|
| Approach | | Eastbound Westbound | | | | | | | Northbound | | | | South | bound | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 |
| Configuration | | | | | | | LR | | | | Т | TR | | L | Т | |
| Volume (veh/h) | | | | | | 0 | | 4 | | | 913 | 1 | 1 | 2 | 403 | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | Left Only | | | | | | | 1 | | | | | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | 6.4 | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | 6.46 | 4.16 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | 2.5 | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | 2.53 | 2.23 | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 4 | | | | | | | 3 | | |
| Capacity, c (veh/h) | | | | | | | 503 | | | | | | | 484 | | |
| v/c Ratio | | | | | | | 0.01 | | | | | | | 0.01 | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 0.0 | | | | | | | 0.0 | | |
| Control Delay (s/veh) | | | | | | | 12.2 | | | | | | | 12.5 | | |
| Level of Service (LOS) | | | | | | | В | | | | | | | В | | |
| Approach Delay (s/veh) | | | | | 12.2 | | | | | | 0.1 | | | | | |
| Approach LOS | | | | | | | В | | | | | A | | | | |

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| HCS Two-Way Stop-Control Report | | | | | | | | | | | |
|---------------------------------|-----------------------|----------------------------|---------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive | | | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut | | | | | | | | |
| Date Performed | 4/10/2024 | East/West Street | 2nd Drive | | | | | | | | |
| Analysis Year | 2024 | North/South Street | Concord Road | | | | | | | | |
| Time Analyzed | PM Peak | Peak Hour Factor | 0.90 | | | | | | | | |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 | | | | | | | | |
| Project Description | 2024 Existing PM Peak | | | | | | | | | | |

Lanes



| Approach | | Eastb | ound | | Westbound | | | | Northbound | | | | Southbound | | | | |
|---|--------|-----------|--------|----|-----------|------|------|------|------------|---|-----|----|------------|------|-----|---|--|
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 | |
| Configuration | | | | | | | LR | | | | Т | TR | | L | Т | | |
| Volume (veh/h) | | | | | | 5 | | 3 | | | 752 | 3 | 0 | 2 | 956 | | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (|) | | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | | |
| Median Type Storage | | Left Only | | | | | | | | | | | 1 | | | | |
| Critical and Follow-up Headways | | | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | | 4.1 | | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | | 4.16 | | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | | 2.23 | | | |
| Delay, Queue Length, an | d Leve | l of Se | ervice | | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 9 | | | | | | | 2 | | | |
| Capacity, c (veh/h) | | | | | | | 332 | | | | | | | 785 | | | |
| v/c Ratio | | | | | | | 0.03 | | | | | | | 0.00 | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 0.1 | | | | | | | 0.0 | | | |
| Control Delay (s/veh) | | | | | | | 16.1 | | | | | | | 9.6 | | | |
| Level of Service (LOS) | | | | | | | С | | | | | | | А | | | |
| Approach Delay (s/veh) | | | | | | 16.1 | | | | | | | 0.0 | | | | |
| Approach LOS | | | | | | С | | | | | | | | A | | | |

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| | | | | НС | S Ro | unda | abo | uts | Rep | ort | | | | | | | | |
|--|--------|-----------------------|-----------|----------|-------|----------|---------|--------|-----|-----------------|------------------|-----------|-------|--------------|--------|----------|--------|--|
| General Information | 1 | | | | | | Sit | te Inf | orn | natio | า | | | | | | | |
| Analyst | WDR | | | | L. | | | | | Intersection | | | | Nortl | nshore | Drive at | Concor | |
| Agency or Co. | Cann | on & Ca | nnon, Inc | i. | // | | + | 1 | T. | E/W Street Name | | | | Nortl | nshore | Drive | | |
| Date Performed | 3/28/ | 2024 | | | | | | | | N/S Street Name | | | | Concord Road | | | | |
| Analysis Year | 2024 | 2024 | | | | Ar W + E | | | | | sis Time l | Period, h | rs | 0.25 | | | | |
| Time Analyzed | AM P | AM Peak | | | | | | | | Peak | Peak Hour Factor | | | | 0.88 | | | |
| Project Description | 2024 | 2024 Existing AM Peak | | | | | | | | Jurisc | liction | | | Knox County | | | | |
| Volume Adjustment | s and | Site C | harac | teristic | s | | | | | | | | | | | | | |
| Approach | | EB | | | | ٧ | VB | | | | N | В | | | | SB | | |
| Movement | U | L | Т | R | U | L | Т | - | R | U | L | Т | R | U | L | Т | R | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | |
| Lane Assignment | | | L | .T | | | | Т | | | | | | | | | L | |
| Volume (V), veh/h | 1 | 569 | 512 | | 2 | | 31 | 2 3 | 45 | | | | | 1 | 200 | | 138 | |
| Percent Heavy Vehicles, % | 3 | 3 | 3 | | 3 | | 3 | 3 | 3 | | | | | 3 | 3 | | 3 | |
| Flow Rate (VPCE), pc/h | 1 | 666 | 599 | | 2 | | 36 | 55 4 | 04 | | | | | 1 | 234 | | 162 | |
| Right-Turn Bypass | | No | one | | | Non-\ | /ieldir | ng | | | No | ne | | Yielding | | | | |
| Conflicting Lanes | | 1 | | | | | 1 | | | | | | | | 1 | | | |
| Pedestrians Crossing, p/h | | | 0 | | | | 0 | | | | | | | | | 0 | | |
| Proportion of CAVs | | | | | | | | | (|) | | | | | | | | |
| Critical and Follow-U | Jp He | adway | / Adju | stmen | t | | | | | | | | | | | | | |
| Approach | | \neg | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s L | eft | Righ | t E | Bypass | Left | Right | Bypas | 5 L | _eft | Right | Bypass | |
| Critical Headway, s | | | | 4.9763 | | Т | | 4.976 | 3 | | | | | Т | | 4.9763 | 4.9763 | |
| Follow-Up Headway, s | | | | 2.6087 | | | | 2.608 | 7 | | | | | | | 2.6087 | 2.6087 | |
| Flow Computations, | Capa | city ar | nd v/c | Ratios | , | | | | Ė | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s L | eft | Righ | t E | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | |
| Entry Flow (v _e), pc/h | | | | 1266 | | Т | | 367 | T | 404 | | | | Т | | 235 | 162 | |
| Entry Volume, veh/h | | | | 1229 | | | 356 | | 392 | | | | | | 228 | 157 | | |
| Circulating Flow (v _c), pc/h | | | | 237 | | | | 668 | | | | 1503 | | | | 368 | | |
| Exiting Flow (vex), pc/h | | | | 835 | | Т | | 366 | | | | 667 | | Т | | 0 | | |
| Capacity (Cpce), pc/h | | | | 1084 | | | | 698 | | | | | | Т | | 948 | 950 | |
| Capacity (c), veh/h | | | | 1052 | | | | 678 | | | | | | | | 921 | 922 | |
| v/c Ratio (x) | | | | 1.17 | | | | 0.53 | | | | | | | | 0.25 | 0.17 | |
| Delay and Level of S | ervice | • | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | | WB | | | | NB | | | | SB | | |
| Lane | | | Left | Right | Bypas | s L | eft | Righ | t E | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | |
| Lane Control Delay (d), s/veh | | | | 103.1 | | | | 13.7 | | | | | | | | 6.4 | 5.6 | |
| Lane LOS | | | | F | | | | В | | Α | | | | | | Α | А | |
| 95% Queue, veh | | | | 35.2 | | | | 3.1 | | | | | | | | 1.0 | 0.6 | |
| Approach Delay, s/veh | | | | 103.1 | 6.5 | | | | | | | | | | 6.1 | | | |
| Approach LOS | | | | F | | | | Α | | | | | | | | Α | | |
| Intersection Delay, s/veh LC | S | | | | | 56.7 | | | | | | | | F | | | | |

| | | | | НС | S Ro | und | abc | outs | Rep | oort | | | | | | | | | |
|------------------------------------|--------|-----------------------|----------------|----------|---------------|------|---------|-------|-----------------|---------------------------|------------------|-------|--------------|-------------|--------|----------|--------|--|--|
| General Information | 1 | | | | | | Si | te In | forn | natio | n | | | | | | | | |
| Analyst | WDR | | | | J | | | | | Intersection | | | | North | nshore | Drive at | Concor | | |
| Agency or Co. | Cann | on & Ca | nnon, Ind | c. | // | | + | 1 | | E/W Street Name | | | | North | nshore | Drive | | | |
| Date Performed | 3/28/ | 2024 | | | | | | | N/S Street Name | | | | Concord Road | | | | | | |
| Analysis Year | 2024 | | | | | | | | Analy | Analysis Time Period, hrs | | | | 0.25 | | | | | |
| Time Analyzed | PM P | PM Peak | | | | | | | | | Peak Hour Factor | | | | 0.95 | | | | |
| Project Description | 2024 | 2024 Existing PM Peak | | | | | | | | Juriso | liction | | | Knox County | | | | | |
| Volume Adjustment | s and | Site C | harac | teristic | :s | | | | | | | | | | | | | | |
| Approach | Π | EB | | | | | WB | | | | N | В | T | | | SB | | | |
| Movement | U | L | Т | R | U | L | 1 | Г | R | U | L | Т | R | U | L | Т | R | | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | | |
| Lane Assignment | | | L | T | | | | Т | | | | | | | | | L | | |
| Volume (V), veh/h | 1 | 252 | 390 | | 12 | | 60 | 03 | 494 | | | | | 1 | 510 | | 445 | | |
| Percent Heavy Vehicles, % | 3 | 3 | 3 | | 3 | | 3 | 3 | 3 | | | | | 3 | 3 | | 3 | | |
| Flow Rate (VPCE), pc/h | 1 | 273 | 423 | | 13 | | 65 | 54 | 536 | | | | | 1 | 553 | | 482 | | |
| Right-Turn Bypass | | N | one | | | Non- | -Yieldi | ng | | | No | ne | | Yielding | | | | | |
| Conflicting Lanes | | 1 | | | | | 1 | | | | | | | | 1 | | | | |
| Pedestrians Crossing, p/h | | | 0 | | | | 0 | | | | | | | 0 | | | | | |
| Proportion of CAVs | | | | | | | | | (| 0 | | | | | | | | | |
| Critical and Follow-U | Jp He | adway | y Ad ju | stmen | t | | | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WI | 3 | | | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Bypas | SS | Left | Rig | nt I | Bypass | Left | Right | Bypass | 5 L | .eft | Right | Bypass | | |
| Critical Headway, s | | \neg | | 4.9763 | $\overline{}$ | | | 4.97 | 63 | | | | | Т | | 4.9763 | 4.9763 | | |
| Follow-Up Headway, s | | | | 2.6087 | | | | 2.60 | 87 | | | | | | | 2.6087 | 2.6087 | | |
| Flow Computations, | Capa | city a | nd v/c | Ratios | 5 | | | | | | | | | | | | | | |
| Approach | | П | | EB | | Т | | WI | 3 | | | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Bypas | SS | Left | Rig | nt I | Bypass | Left | Right | Bypass | 5 L | .eft | Right | Bypass | | |
| Entry Flow (v _e), pc/h | | | | 697 | | | | 66 | 7 | 536 | | | | Т | | 554 | 482 | | |
| Entry Volume, veh/h | | | | 677 | | | 648 | | 520 | | | | | | 538 | 468 | | | |
| Circulating Flow (v₀), pc/h | | | | 567 | • | | | 27 | 5 | | | 1264 | _ | | | 668 | | | |
| Exiting Flow (vex), pc/h | | | | 989 | | | | 65 | 5 | | | 274 | | | | 0 | | | |
| Capacity (c _{pce}), pc/h | | | | 774 | | | | 104 | 2 | | | | | | | 698 | 708 | | |
| Capacity (c), veh/h | | | | 751 | | | | 101 | 2 | | | | | | | 678 | 687 | | |
| v/c Ratio (x) | | | | 0.90 | | | | 0.6 | 4 | | | | | | | 0.79 | 0.68 | | |
| Delay and Level of S | ervice | , | | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | | WI | 3 | | | NB | | | | SB | | | |
| Lane | | | Left | Right | Bypas | SS | Left | Rig | nt I | Bypass | Left | Right | Bypass | S L | .eft | Right | Bypass | | |
| Lane Control Delay (d), s/veh | | | | 36.3 | | | | 12. | 8 | | | | | | | 26.5 | 19.1 | | |
| Lane LOS | | | | E | | | | В | | Α | | | | | | D | С | | |
| 95% Queue, veh | | | | 11.9 | | | | 4.8 | 3 | | | | | | | 7.9 | 5.4 | | |
| Approach Delay, s/veh | | | | 36.3 | | | | 7.1 | | | | | | | | 23.0 | | | |
| Approach LOS | | | | E | | | | Α | | | | | | | | С | | | |
| Intersection Delay, s/veh LC |)S | | | | | 19.7 | | | | | | | | С | | | | | |

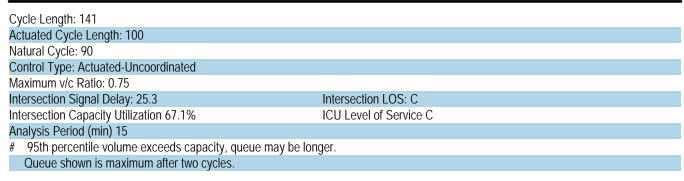
Lanes, Volumes, Timings 1: Concord Drive & Turkey Creek Road/Summerdale Drive

| | ۶ | → | • | • | ← | • | 1 | † | ~ | / | ↓ | -√ |
|-------------------------|-------|----------|------|-------|----------|------|-------|------------|------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 4 | | | 4 | | 7 | ∱ ∱ | | 7 | ^ | 7 |
| Traffic Volume (vph) | 548 | 0 | 78 | 9 | 0 | 22 | 35 | 1008 | 5 | 6 | 367 | 199 |
| Future Volume (vph) | 548 | 0 | 78 | 9 | 0 | 22 | 35 | 1008 | 5 | 6 | 367 | 199 |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 |
| Frt | | 0.962 | | | 0.904 | | | 0.999 | | | | 0.850 |
| Flt Protected | 0.950 | 0.964 | | | 0.986 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1681 | 1641 | 0 | 0 | 1660 | 0 | 1770 | 3536 | 0 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.950 | 0.964 | | | 0.986 | | 0.463 | | | 0.121 | | |
| Satd. Flow (perm) | 1681 | 1641 | 0 | 0 | 1660 | 0 | 862 | 3536 | 0 | 225 | 3539 | 1583 |
| Satd. Flow (RTOR) | | 205 | | | 217 | | | | | | | 226 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Shared Lane Traffic (%) | 42% | | | | | | | | | | | |
| Lane Group Flow (vph) | 361 | 351 | 0 | 0 | 35 | 0 | 40 | 1151 | 0 | 7 | 417 | 226 |
| Turn Type | Split | NA | | Split | NA | | pm+pt | NA | | pm+pt | NA | pm+ov |
| Protected Phases | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Permitted Phases | | | | | | | 6 | | | 2 | | 2 |
| Detector Phase | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 6.0 | 6.0 | | 6.0 | 15.0 | | 6.0 | 15.0 | 8.0 |
| Minimum Split (s) | 16.0 | 16.0 | | 12.0 | 12.0 | | 14.0 | 24.0 | | 13.0 | 24.0 | 16.0 |
| Total Split (s) | 38.0 | 38.0 | | 16.0 | 16.0 | | 28.0 | 59.0 | | 17.0 | 59.0 | 38.0 |
| Total Split (%) | 27.0% | 27.0% | | 11.3% | 11.3% | | 19.9% | 41.8% | | 12.1% | 41.8% | 27.0% |
| Yellow Time (s) | 4.0 | 4.0 | | 3.5 | 3.5 | | 4.0 | 5.5 | | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | | 2.5 | 2.5 | | 3.5 | 3.5 | | 3.0 | 3.5 | 3.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.5 | | | 6.0 | | 7.5 | 9.0 | | 7.0 | 9.0 | 7.5 |
| Lead/Lag | Lead | Lead | | Lag | Lag | | Lead | Lag | | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | None | | None | None | | None | Min | | None | Min | None |
| Act Effct Green (s) | 30.9 | 30.9 | | | 6.2 | | 46.4 | 43.5 | | 43.1 | 37.7 | 81.5 |
| Actuated g/C Ratio | 0.31 | 0.31 | | | 0.06 | | 0.46 | 0.44 | | 0.43 | 0.38 | 0.82 |
| v/c Ratio | 0.70 | 0.54 | | | 0.11 | | 0.09 | 0.75 | | 0.04 | 0.31 | 0.17 |
| Control Delay | 42.5 | 17.5 | | | 8.0 | | 15.2 | 28.3 | | 15.0 | 24.8 | 1.0 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 42.5 | 17.5 | | | 8.0 | | 15.2 | 28.3 | | 15.0 | 24.8 | 1.0 |
| LOS | D | В | | | Α | | В | С | | В | С | Α |
| Approach Delay | | 30.2 | | | 8.0 | | | 27.9 | | | 16.4 | |
| Approach LOS | | С | | | Α | | | С | | | В | |
| Queue Length 50th (ft) | 229 | 81 | | | 0 | | 15 | 330 | | 2 | 116 | 0 |
| Queue Length 95th (ft) | #445 | 206 | | | 0 | | 32 | 488 | | 10 | 155 | 20 |
| Internal Link Dist (ft) | | 497 | | | 673 | | | 435 | | | 693 | |
| Turn Bay Length (ft) | | | | | | | 70 | | | 95 | | 475 |
| Base Capacity (vph) | 527 | 655 | | | 365 | | 599 | 2219 | | 260 | 1820 | 1312 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.69 | 0.54 | | | 0.10 | | 0.07 | 0.52 | | 0.03 | 0.23 | 0.17 |
| Intersection Summary | | | | | | | | | | | | |

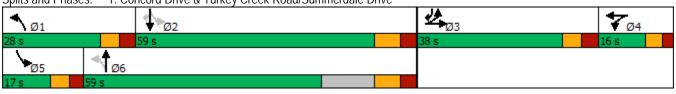
Timing Plan: AM Cannon & Cannon, Inc.

Synchro 11 Report Page 1

1: Concord Drive & Turkey Creek Road/Summerdale Drive



Splits and Phases: 1: Concord Drive & Turkey Creek Road/Summerdale Drive



Lanes, Volumes, Timings 1: Concord Drive & Turkey Creek Road/Summerdale Drive

| 1. Concord Drive 8 | ve & Turkey Creek Road/Summerdale Drive | | | | | | | | | 2020 Backyrounu | | | | |
|-------------------------|---|----------|------|--------|----------|------|-------|------------|------|-----------------|----------|-------|--|--|
| | ۶ | → | • | • | ← | • | 4 | † | / | > | ţ | 4 | | |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | |
| Lane Configurations | ሻ | 4 | | | 4 | | * | ↑ ↑ | | Ť | ^ | 7 | | |
| Traffic Volume (vph) | 269 | 1 | 104 | 4 | 3 | 17 | 134 | 706 | 11 | 9 | 951 | 402 | | |
| Future Volume (vph) | 269 | 1 | 104 | 4 | 3 | 17 | 134 | 706 | 11 | 9 | 951 | 402 | | |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | | |
| Frt | | 0.913 | | | 0.901 | | | 0.998 | | | | 0.850 | | |
| Flt Protected | 0.950 | 0.980 | | | 0.992 | | 0.950 | | | 0.950 | | | | |
| Satd. Flow (prot) | 1681 | 1583 | 0 | 0 | 1665 | 0 | 1770 | 3532 | 0 | 1770 | 3539 | 1583 | | |
| Flt Permitted | 0.950 | 0.980 | | | 0.992 | | 0.135 | | | 0.351 | | | | |
| Satd. Flow (perm) | 1681 | 1583 | 0 | 0 | 1665 | 0 | 251 | 3532 | 0 | 654 | 3539 | 1583 | | |
| Satd. Flow (RTOR) | | 44 | | | 19 | | | 1 | | | | 447 | | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | | |
| Shared Lane Traffic (%) | 28% | | | | | | | | | | | | | |
| Lane Group Flow (vph) | 215 | 201 | 0 | 0 | 26 | 0 | 149 | 796 | 0 | 10 | 1057 | 447 | | |
| Turn Type | Split | NA | | Split | NA | | pm+pt | NA | | pm+pt | NA | pm+ov | | |
| Protected Phases | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 | | |
| Permitted Phases | | | | • | | | 6 | | | 2 | _ | 2 | | |
| Detector Phase | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 | | |
| Switch Phase | | | | • | | | | | | | _ | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 6.0 | 6.0 | | 6.0 | 15.0 | | 6.0 | 15.0 | 8.0 | | |
| Minimum Split (s) | 16.0 | 16.0 | | 12.0 | 12.0 | | 14.0 | 24.0 | | 13.0 | 24.0 | 16.0 | | |
| Total Split (s) | 38.0 | 38.0 | | 16.0 | 16.0 | | 28.0 | 59.0 | | 17.0 | 59.0 | 38.0 | | |
| Total Split (%) | 27.0% | 27.0% | | 11.3% | 11.3% | | 19.9% | 41.8% | | 12.1% | 41.8% | 27.0% | | |
| Yellow Time (s) | 4.0 | 4.0 | | 3.5 | 3.5 | | 4.0 | 5.5 | | 4.0 | 5.5 | 4.0 | | |
| All-Red Time (s) | 3.5 | 3.5 | | 2.5 | 2.5 | | 3.5 | 3.5 | | 3.0 | 3.5 | 3.5 | | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 2.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | |
| Total Lost Time (s) | 7.5 | 7.5 | | | 6.0 | | 7.5 | 9.0 | | 7.0 | 9.0 | 7.5 | | |
| Lead/Lag | Lead | Lead | | Lag | Lag | | Lead | Lag | | Lead | Lag | Lead | | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | Yes | | |
| Recall Mode | None | None | | None | None | | None | Min | | None | Min | None | | |
| Act Effct Green (s) | 21.5 | 21.5 | | 110110 | 7.0 | | 62.3 | 58.6 | | 50.6 | 42.0 | 73.1 | | |
| Actuated g/C Ratio | 0.20 | 0.20 | | | 0.07 | | 0.58 | 0.55 | | 0.48 | 0.39 | 0.69 | | |
| v/c Ratio | 0.63 | 0.57 | | | 0.20 | | 0.50 | 0.41 | | 0.03 | 0.76 | 0.36 | | |
| Control Delay | 51.2 | 39.2 | | | 34.0 | | 17.9 | 17.1 | | 13.4 | 33.9 | 1.6 | | |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | |
| Total Delay | 51.2 | 39.2 | | | 34.0 | | 17.9 | 17.1 | | 13.4 | 33.9 | 1.6 | | |
| LOS | D | D | | | C | | В | В | | В | C | A | | |
| Approach Delay | J | 45.4 | | | 34.0 | | D | 17.2 | | J | 24.2 | , , | | |
| Approach LOS | | D | | | C | | | В | | | C | | | |
| Queue Length 50th (ft) | 155 | 111 | | | 5 | | 49 | 167 | | 3 | 342 | 0 | | |
| Queue Length 95th (ft) | 271 | 216 | | | 37 | | 98 | 320 | | 13 | 532 | 35 | | |
| Internal Link Dist (ft) | 2/1 | 497 | | | 673 | | 70 | 435 | | 10 | 693 | 00 | | |
| Turn Bay Length (ft) | | 777 | | | 073 | | 70 | 433 | | 95 | 073 | 475 | | |
| Base Capacity (vph) | 512 | 513 | | | 183 | | 458 | 2225 | | 447 | 1769 | 1343 | | |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 | | |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 | | |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 | | |
| Reduced v/c Ratio | 0.42 | 0.39 | | | 0.14 | | 0.33 | 0.36 | | 0.02 | 0.60 | 0.33 | | |
| Reduced We Railo | 0.42 | 0.37 | | | 0.14 | | 0.33 | 0.50 | | 0.02 | 0.00 | 0.55 | | |

Timing Plan: PM Cannon & Cannon, Inc.

Intersection Summary

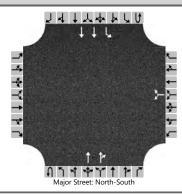
Synchro 11 Report Page 1

2026 Background

| Cycle Length: 141 | |
|---|------------------------|
| Actuated Cycle Length: 106.5 | |
| Natural Cycle: 80 | |
| Control Type: Actuated-Uncoordinated | |
| Maximum v/c Ratio: 0.76 | |
| Intersection Signal Delay: 25.1 | Intersection LOS: C |
| Intersection Capacity Utilization 71.0% | ICU Level of Service C |
| Analysis Period (min) 15 | |
| | |
| Splits and Phases: 1: Concord Drive & Turkey Creek Road/S | Summerdale Drive |

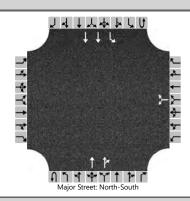
Timing Plan: PM Cannon & Cannon, Inc.

| HCS Two-Way Stop-Control Report | | | | | | | | | | |
|---------------------------------|--|--------------------|---------------------------|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive | | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut | | | | | | | |
| Date Performed | 4/16/2024 | East/West Street | 2nd Drive | | | | | | | |
| Analysis Year | 2026 | North/South Street | Concord Road | | | | | | | |
| Time Analyzed | AM Peak | Peak Hour Factor | 0.89 | | | | | | | |
| Intersection Orientation | tersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | |
| Project Description | Project Description 2026 Background AM Peak | | | | | | | | | |



| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | | |
|---|--------|--------|--------|------|------|-------|-------|------|----|-------|-------|----|------|-------|-------|---|--|
| Approach | | Eastk | ound | | | Westl | bound | | | North | bound | | | South | bound | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 | |
| Configuration | | | | | | | LR | | | | Т | TR | | L | Т | | |
| Volume (veh/h) | | | | | | 0 | | 4 | | | 978 | 1 | 1 | 2 | 432 | | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | 6.4 | 4.1 | | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | 6.46 | 4.16 | | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | 2.5 | 2.2 | | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | 2.53 | 2.23 | | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 4 | | | | | | | 3 | | | |
| Capacity, c (veh/h) | | | | | | | 476 | | | | | | | 444 | | | |
| v/c Ratio | | | | | | | 0.01 | | | | | | | 0.01 | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 0.0 | | | | | | | 0.0 | | | |
| Control Delay (s/veh) | | | | | | | 12.6 | | | | | | | 13.2 | | | |
| Level of Service (LOS) | | | | | | | В | | | | | | | В | | | |
| Approach Delay (s/veh) | | | | | 12.6 | | | | | | 0.1 | | | | | | |
| Approach LOS | | | | | В | | | | | | | | А | | | | |

| HCS Two-Way Stop-Control Report | | | | | | | | | | | |
|--|-----------------------|--------------------|---------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive | | | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut | | | | | | | | |
| Date Performed | 4/16/2024 | East/West Street | 2nd Drive | | | | | | | | |
| Analysis Year | 2026 | North/South Street | Concord Road | | | | | | | | |
| Time Analyzed | PM Peak | Peak Hour Factor | 0.90 | | | | | | | | |
| Intersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | | | |
| Project Description 2026 Background PM Peak | | | | | | | | | | | |



| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | | |
|---|-------|---------|--------|------|------|-------|-------|------|----|-------|-------|----|-----|-------|-------|---|--|
| Approach | | Eastb | ound | | | Westl | bound | | | North | bound | | | South | bound | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 | |
| Configuration | | | | | | | LR | | | | T | TR | | L | T | | |
| Volume (veh/h) | | | | | | 5 | | 3 | | | 806 | 3 | 0 | 2 | 1024 | | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | | 0 | | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | 1 | | | | | | | | |
| Critical and Follow-up He | eadwa | ys | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | | 4.1 | | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | | 4.16 | | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | | 2.23 | | | |
| Delay, Queue Length, and | Leve | l of Se | ervice | | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | Π | | | | | | 9 | | | | | | | 2 | | | |
| Capacity, c (veh/h) | | | | | | | 309 | | | | | | | 745 | | | |
| v/c Ratio | | | | | | | 0.03 | | | | | | | 0.00 | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 0.1 | | | | | | | 0.0 | | | |
| Control Delay (s/veh) | | | | | | | 17.0 | | | | | | | 9.8 | | | |
| Level of Service (LOS) | | | | | | | С | | | | | | | Α | | | |
| Approach Delay (s/veh) | | | | | | 17.0 | | | | | | | 0.0 | | | | |
| Approach LOS | | | | | | (| С | | | | | | А | | | | |

| | | | | НС | S Rou | ındak | oout | s Re | port | | | | | | | | | |
|--|-----------------|---------|-----------|----------|--------------|----------|--------|-------------------------------|--------|------------|-----------|--------|----------|---------|----------|--------|--|--|
| General Information | | | | | | | Site I | nfor | matio | n | | | | | | | | |
| Analyst | WDR | | | | | <u> </u> | 1 | | Inters | section | | T | North | shore | Drive at | Concor | | |
| Agency or Co. | Cann | on & Ca | nnon, Inc | <u> </u> | | · | 1 | | E/W | Street Na | me | | North | shore | Drive | | | |
| Date Performed | 4/16/ | 2024 | | | | N | | 1. | N/S S | Street Nar | ne | | Conce | ord Roa | ad | | | |
| Analysis Year | 2026 | | | | ▲ ↓ . | W ÷ | E | 1 | Analy | sis Time I | Period, h | irs | 0.25 | | | | | |
| Time Analyzed | AM P | eak | | | | | | 1 | Peak | Hour Fact | tor | | 0.88 | | | | | |
| Project Description | 2026 | Backgro | und AM | Peak | | V | 1 | | Juriso | liction | | | Knox | County | / | | | |
| Volume Adjustment | s and | Site C | haract | teristic | ics | | | | | | | | | | | | | |
| Approach | | [| EΒ | | | WE | 3 | | | N | В | | | | SB | | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | | |
| Lane Assignment | | | L | т | | | 1 | | | | | | | | | L | | |
| Volume (V), veh/h | 1 | 610 | 548 | | 2 | | 334 | 370 | | | | | 1 | 214 | | 148 | | |
| Percent Heavy Vehicles, % | 3 | 3 | 3 | | 3 | | 3 | 3 | | | | | 3 | 3 | | 3 | | |
| Flow Rate (VPCE), pc/h | 1 | 714 | 641 | | 2 | | 391 | 433 | | | | | 1 | 250 | | 173 | | |
| Right-Turn Bypass | | N | one | | | Non-Yie | lding | | | No | ne | | Yielding | | | | | |
| Conflicting Lanes | | | 1 | | | 1 | | | | | | | 1 | | | | | |
| Pedestrians Crossing, p/h | | | 0 | | | 0 | | | | | | | 0 | | | | | |
| Proportion of CAVs | | | | | | | | | 0 | | | | | | | | | |
| Critical and Follow-U | Jp He | adway | y Adju | stmen | t | | | | | | | | | | | | | |
| Approach | proach EB WB NB | | | | | | | | | Т | | SB | | | | | | |
| Lane | | | Left | Right | Bypass | Left | : R | ight | Bypass | Left | Right | Bypass | L | eft | Right | Bypass | | |
| Critical Headway, s | | | | 4.9763 | | | 4.9 | 9763 | | | | | Т | | 4.9763 | 4.9763 | | |
| Follow-Up Headway, s | | | | 2.6087 | | | 2.6 | 6087 | | | | | | | 2.6087 | 2.6087 | | |
| Flow Computations, | Capa | city aı | nd v/c | Ratios | ; | | | | | | | | _ | | | | | |
| Approach | | Ī | | EB | | Т | ١ | WB | | | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Bypass | Left | : R | ight | Bypass | Left | Right | Bypass | L | eft | Right | Bypass | | |
| Entry Flow (v _e), pc/h | | | | 1356 | | | 3 | 393 | 433 | | | | \top | | 251 | 173 | | |
| Entry Volume, veh/h | | | | 1317 | | | 3 | 382 | 420 | | | | | | 244 | 168 | | |
| Circulating Flow (v _c), pc/h | | | | 253 | | | 7 | 716 | | | 1609 | | т | | 394 | | | |
| Exiting Flow (vex), pc/h | | | | 893 | | | 3 | 392 | | | 715 | | | | 0 | | | |
| Capacity (c _{pce}), pc/h | | \neg | | 1066 | | | 6 | 665 | | | | Т | Т | | 923 | 925 | | |
| Capacity (c), veh/h | | | | 1035 | | | 6 | 545 | | | | | | | 896 | 898 | | |
| v/c Ratio (x) | | | | 1.27 | | | C |).59 | | | | | Т | | 0.27 | 0.19 | | |
| Delay and Level of S | ervice | | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | ١ | WB | | | NB | | | | SB | | | |
| Lane | | | Left | Right | Bypass | Left | : R | ight Bypass Left Right Bypass | | | | L | eft | Right | Bypass | | | |
| Lane Control Delay (d), s/veh | 1 | | | 145.4 | | | 1 | 6.3 | | | | | | | 6.9 | 5.9 | | |
| Lane LOS | | | | F | | | | С | Α | | | | | | Α | А | | |
| 95% Queue, veh | | | | 45.9 | | | | 3.9 | | | | | | | 1.1 | 0.7 | | |
| Approach Delay, s/veh | | | | 145.4 | | | | 7.7 | | | | | | | 6.5 | | | |
| Approach LOS | | | | F | | | | Α | | | | | | | Α | | | |
| Intersection Delay, s/veh LC | | | | | | 79.1 | | | | | | | F | | | | | |

| | | | | НС | S Ro | unda | abo | uts F | Rep | ort | | | | | | | | |
|--|-------|---------|-----------|---|--------------|-------|---------|--------|---------|--------|------------|-----------|--------|----------|-------------|----------|--------|--|
| General Information | | | | | | | Sit | te Inf | orn | natio | 1 | | | | | | | |
| Analyst | WDR | | | | 1 | 15 | | | | Inters | ection | | | North | nshore | Drive at | Concor | |
| Agency or Co. | Cann | on & Ca | nnon, Inc | i. | // | | - | 1 | ī. | E/W S | Street Na | me | | North | nshore | Drive | | |
| Date Performed | 4/16/ | 2024 | | | | | N | | 1 | N/S S | treet Nar | ne | | Conc | ord Ro | ad | | |
| Analysis Year | 2026 | | | | ⋠ ↓ | W | † E | 1 | H | Analy | sis Time l | Period, h | rs | 0.25 | | | | |
| Time Analyzed | PM P | eak | | | | | | | | Peak | Hour Fact | tor | | 0.95 | | | | |
| Project Description | 2026 | Backgro | und PM | Peak | Jurisdiction | | | | | | sdiction | | | | Knox County | | | |
| Volume Adjustment | s and | Site C | harac | acteristics | | | | | - | | | | | | | | | |
| Approach | | E | B | | ٧ | WB | | | | N | В | | | | SB | | | |
| Movement | U | L | Т | R | U | L | Т | - | R | U | L | Т | R | U | L | Т | R | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | |
| Lane Assignment | | | L | .T | | | | T | | | | | | | | | Ĺ | |
| Volume (V), veh/h | 1 | 270 | 418 | | 13 | | 64 | 16 5 | 29 | | | | | 1 | 546 | | 477 | |
| Percent Heavy Vehicles, % | 3 | 3 | 3 | | 3 | | 3 | 3 | 3 | | | | | 3 | 3 | | 3 | |
| Flow Rate (VPCE), pc/h | 1 | 293 | 453 | | 14 | | 70 | 00 5 | 74 | | | | | 1 | 592 | | 517 | |
| Right-Turn Bypass | | No | one | | | Non-Y | /ieldir | ng | | | No | ne | | Yielding | | | | |
| Conflicting Lanes | | | 1 | | | | 1 | | | | | | | | | 1 | | |
| Pedestrians Crossing, p/h | | | 0 | | | | 0 | | | | | 0 | | | | | | |
| Proportion of CAVs | | | | | | | | | (|) | | | | | | | | |
| Critical and Follow-U | Jp He | adway | / Adju | stmen | t | | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | E | Bypass | Left | Right | Bypas | 5 L | .eft | Right | Bypass | |
| Critical Headway, s | | | | 4.9763 | | | | 4.976 | 3 | | | | | | | 4.9763 | 4.9763 | |
| Follow-Up Headway, s | | | | 2.6087 | | | | 2.608 | 7 | | | | | | | 2.6087 | 2.6087 | |
| Flow Computations, | Capa | city a | nd v/c | Ratios | ; | | | | | | | | | | | | | |
| Approach | | П | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | E | Bypass | Left | Right | Bypas | 5 L | _eft | Right | Bypass | |
| Entry Flow (v _e), pc/h | | \neg | | 747 | | | | 714 | T | 574 | | | | Т | | 593 | 517 | |
| Entry Volume, veh/h | | | | 725 | | | | 693 | | 557 | | | | | | 576 | 502 | |
| Circulating Flow (v _c), pc/h | | | | 607 | | | | 295 | | | | 1354 | | | | 715 | | |
| Exiting Flow (vex), pc/h | | | | 1059 | | | | 701 | | | | 294 | | | | 0 | | |
| Capacity (Cpce), pc/h | | | | 743 | | | | 1021 | | | | | | | | 666 | 675 | |
| Capacity (c), veh/h | | | | 721 | | | | 992 | | | | | | | | 646 | 655 | |
| v/c Ratio (x) | | | | 1.01 | | | | 0.70 | | | | | | | | 0.89 | 0.77 | |
| Delay and Level of Service | | | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | | WB | | | | NB | | | | SB | | |
| Lane | | | Left | eft Right Bypass Left Right Bypass Left | | | | Right | Bypas | S L | _eft | Right | Bypass | | | | | |
| Lane Control Delay (d), s/veh | | | | 58.7 | | | | 15.1 | | | | | | | | 38.8 | 25.0 | |
| Lane LOS F | | | | | | С | | Α | | | | | | E | С | | | |
| 95% Queue, veh | | | | 16.7 | | | | 6.0 | \prod | | | | | | | 10.9 | 7.1 | |
| Approach Delay, s/veh | | | | 58.7 | | | | 8.4 | | | | | | | | 32.3 | | |
| Approach LOS | | | | F | | | | Α | | | | | | | | D | | |
| Intersection Delay, s/veh LC | S | | | | | 28.8 | | | | | | | | D | | | | |

Lanes, Volumes, Timings 1: Concord Drive & Turkey Creek Road/Summerdale Drive

| | ۶ | → | • | • | + | • | 4 | † | <i>></i> | / | ţ | </th |
|-------------------------|-------|----------|------|-------|----------|------|-------|------------|-------------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | Ť | 4 | | | 4 | | ۲ | ∱ } | | 7 | ^ | 7 |
| Traffic Volume (vph) | 548 | 0 | 111 | 14 | 0 | 22 | 67 | 1035 | 10 | 6 | 395 | 199 |
| Future Volume (vph) | 548 | 0 | 111 | 14 | 0 | 22 | 67 | 1035 | 10 | 6 | 395 | 199 |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 |
| Frt | | 0.949 | | | 0.918 | | | 0.999 | | | | 0.850 |
| Flt Protected | 0.950 | 0.968 | | | 0.981 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1681 | 1626 | 0 | 0 | 1678 | 0 | 1770 | 3536 | 0 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.950 | 0.968 | | | 0.981 | | 0.407 | | | 0.112 | | |
| Satd. Flow (perm) | 1681 | 1626 | 0 | 0 | 1678 | 0 | 758 | 3536 | 0 | 209 | 3539 | 1583 |
| Satd. Flow (RTOR) | | 205 | | | 217 | | | 1 | | | | 226 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Shared Lane Traffic (%) | 39% | | | | | | | | | | | |
| Lane Group Flow (vph) | 380 | 369 | 0 | 0 | 41 | 0 | 76 | 1187 | 0 | 7 | 449 | 226 |
| Turn Type | Split | NA | | Split | NA | | pm+pt | NA | | pm+pt | NA | pm+ov |
| Protected Phases | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Permitted Phases | | | | | | | 6 | | | 2 | | 2 |
| Detector Phase | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 6.0 | 6.0 | | 6.0 | 15.0 | | 6.0 | 15.0 | 8.0 |
| Minimum Split (s) | 16.0 | 16.0 | | 12.0 | 12.0 | | 14.0 | 24.0 | | 13.0 | 24.0 | 16.0 |
| Total Split (s) | 38.0 | 38.0 | | 16.0 | 16.0 | | 28.0 | 59.0 | | 17.0 | 59.0 | 38.0 |
| Total Split (%) | 27.0% | 27.0% | | 11.3% | 11.3% | | 19.9% | 41.8% | | 12.1% | 41.8% | 27.0% |
| Yellow Time (s) | 4.0 | 4.0 | | 3.5 | 3.5 | | 4.0 | 5.5 | | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | | 2.5 | 2.5 | | 3.5 | 3.5 | | 3.0 | 3.5 | 3.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.5 | | | 6.0 | | 7.5 | 9.0 | | 7.0 | 9.0 | 7.5 |
| Lead/Lag | Lead | Lead | | Lag | Lag | | Lead | Lag | | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | None | | None | None | | None | Min | | None | Min | None |
| Act Effct Green (s) | 31.2 | 31.2 | | | 6.1 | | 47.5 | 44.3 | | 41.1 | 34.5 | 76.8 |
| Actuated g/C Ratio | 0.30 | 0.30 | | | 0.06 | | 0.46 | 0.43 | | 0.40 | 0.33 | 0.74 |
| v/c Ratio | 0.75 | 0.58 | | | 0.14 | | 0.18 | 0.79 | | 0.04 | 0.38 | 0.18 |
| Control Delay | 46.7 | 19.6 | | | 0.9 | | 16.6 | 30.7 | | 15.2 | 28.9 | 1.2 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 46.7 | 19.6 | | | 0.9 | | 16.6 | 30.7 | | 15.2 | 28.9 | 1.2 |
| LOS | D | В | | | А | | В | С | | В | С | Α |
| Approach Delay | | 33.3 | | | 0.9 | | | 29.9 | | | 19.6 | |
| Approach LOS | | С | | | Α | | | С | | | В | |
| Queue Length 50th (ft) | 253 | 97 | | | 0 | | 28 | 345 | | 2 | 128 | 0 |
| Queue Length 95th (ft) | #483 | 227 | | | 0 | | 53 | 508 | | 10 | 172 | 21 |
| Internal Link Dist (ft) | | 497 | | | 673 | | | 435 | | | 693 | |
| Turn Bay Length (ft) | | | | | | | 70 | | | 95 | | 475 |
| Base Capacity (vph) | 505 | 632 | | | 361 | | 555 | 2126 | | 242 | 1743 | 1231 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.75 | 0.58 | | | 0.11 | | 0.14 | 0.56 | | 0.03 | 0.26 | 0.18 |
| Intersection Summary | | | | | | | | | | | | |

Timing Plan: AM Cannon & Cannon, Inc.

Synchro 11 Report Page 1

Cycle Length: 141

Actuated Cycle Length: 103.7

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.79

Intersection Signal Delay: 27.8

Intersection Capacity Utilization 78.7%

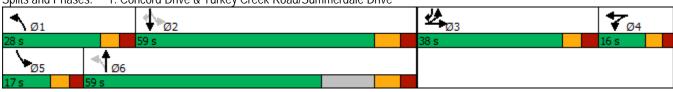
ICU Level of Service D

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Concord Drive & Turkey Creek Road/Summerdale Drive



Lanes, Volumes, Timings 1: Concord Drive & Turkey Creek Road/Summerdale Drive

| | ۶ | → | • | • | ← | • | 1 | † | <i>></i> | / | ţ | -√ |
|---------------------------------------|-----------|-----------|------|-------|----------|------|-------|------------|-------------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 4 | | | 4 | | 7 | ∱ ∱ | | Ţ | ^ | 7 |
| Traffic Volume (vph) | 269 | 1 | 121 | 7 | 3 | 17 | 150 | 720 | 14 | 9 | 965 | 402 |
| Future Volume (vph) | 269 | 1 | 121 | 7 | 3 | 17 | 150 | 720 | 14 | 9 | 965 | 402 |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 |
| Frt | | 0.904 | | | 0.914 | | | 0.997 | | | | 0.850 |
| Flt Protected | 0.950 | 0.982 | | | 0.987 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1681 | 1571 | 0 | 0 | 1680 | 0 | 1770 | 3529 | 0 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.950 | 0.982 | | | 0.987 | | 0.127 | | | 0.344 | | |
| Satd. Flow (perm) | 1681 | 1571 | 0 | 0 | 1680 | 0 | 237 | 3529 | 0 | 641 | 3539 | 1583 |
| Satd. Flow (RTOR) | | 57 | | | 19 | | | 2 | | | | 447 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Shared Lane Traffic (%) | 25% | | | | | | | | | | | |
| Lane Group Flow (vph) | 224 | 210 | 0 | 0 | 30 | 0 | 167 | 816 | 0 | 10 | 1072 | 447 |
| Turn Type | Split | NA | | Split | NA | | pm+pt | NA | | pm+pt | NA | pm+ov |
| Protected Phases | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Permitted Phases | | | | | | | 6 | | | 2 | | 2 |
| Detector Phase | 3 | 3 | | 4 | 4 | | 1 | 6 | | 5 | 2 | 3 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 6.0 | 6.0 | | 6.0 | 15.0 | | 6.0 | 15.0 | 8.0 |
| Minimum Split (s) | 16.0 | 16.0 | | 12.0 | 12.0 | | 14.0 | 24.0 | | 13.0 | 24.0 | 16.0 |
| Total Split (s) | 38.0 | 38.0 | | 16.0 | 16.0 | | 28.0 | 59.0 | | 17.0 | 59.0 | 38.0 |
| Total Split (%) | 27.0% | 27.0% | | 11.3% | 11.3% | | 19.9% | 41.8% | | 12.1% | 41.8% | 27.0% |
| Yellow Time (s) | 4.0 | 4.0 | | 3.5 | 3.5 | | 4.0 | 5.5 | | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | | 2.5 | 2.5 | | 3.5 | 3.5 | | 3.0 | 3.5 | 3.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.5 | | | 6.0 | | 7.5 | 9.0 | | 7.0 | 9.0 | 7.5 |
| Lead/Lag | Lead | Lead | | Lag | Lag | | Lead | Lag | | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | None | | None | None | | None | Min | | None | Min | None |
| Act Effct Green (s) | 22.4 | 22.4 | | | 7.2 | | 64.5 | 60.8 | | 51.6 | 43.0 | 75.0 |
| Actuated g/C Ratio | 0.20 | 0.20 | | | 0.07 | | 0.59 | 0.55 | | 0.47 | 0.39 | 0.68 |
| v/c Ratio | 0.65 | 0.58 | | | 0.24 | | 0.55 | 0.42 | | 0.03 | 0.77 | 0.37 |
| Control Delay | 53.2 | 37.9 | | | 37.6 | | 19.9 | 17.3 | | 13.9 | 35.9 | 1.7 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 |
| Total Delay | 53.2 | 37.9 | | | 37.6 | | 19.9 | 17.3 | | 13.9 | 35.9 | 1.7 |
| LOS | D | D | | | D | | В | B | | В | D | A |
| Approach Delay | | 45.8 | | | 37.6 | | | 17.8 | | | 25.7 | |
| Approach LOS | 171 | D | | | D | | ГО | B 101 | | 2 | C | 0 |
| Queue Length 50th (ft) | 171 | 114 | | | 8 44 | | 58 | 181 | | 3 | 370 | 0 |
| Queue Length 95th (ft) | 289 | 220 | | | | | 115 | 330 | | 12 | 560 | 38 |
| Internal Link Dist (ft) | | 497 | | | 673 | | 70 | 435 | | 95 | 693 | 475 |
| Turn Bay Length (ft) | 407 | EOE | | | 100 | | 70 | 2205 | | | 1717 | 475 |
| Base Capacity (vph) | 497 | 505 | | | 180 | | 444 | 2205 | | 435 | 1717 | 1327 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | | 0 | 0 | 0 |
| Storage Cap Reductn Reduced v/c Ratio | 0 0.45 | 0 0.42 | | | 0.17 | | 0.38 | 0 0.37 | | 0.02 | 0.62 | 0.34 |
| Intersection Summary | 0.40 | 0.42 | | | 0.17 | | 0.30 | 0.37 | | 0.02 | 0.02 | 0.34 |
| intersection Summary | | | | | | | | | | | | |

Timing Plan: PM Cannon & Cannon, Inc.

Synchro 11 Report Page 1

Cycle Length: 141
Actuated Cycle Length: 109.8
Natural Cycle: 80
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.77
Intersection Signal Delay: 26.1 Intersection LOS: C
Intersection Capacity Utilization 72.8% ICU Level of Service C
Analysis Period (min) 15

Splits and Phases: 1: Concord Drive & Turkey Creek Road/Summerdale Drive

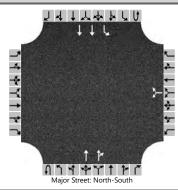
 Ø1
 Ø2

 28 s
 59 s

 Ø5
 Ø6

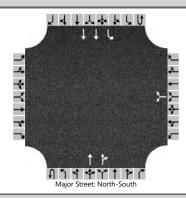
 17 s
 59 s

| HCS Two-Way Stop-Control Report | | | | | | | | | | |
|---------------------------------|---|--------------------|---------------------------|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive | | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut | | | | | | | |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive | | | | | | | |
| Analysis Year | 2026 | North/South Street | Concord Road | | | | | | | |
| Time Analyzed | AM Peak | Peak Hour Factor | 0.89 | | | | | | | |
| Intersection Orientation | ersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | |
| Project Description | Project Description 2026 Combined AM Peak | | | | | | | | | |



| Vehicle Volumes and Ad | justme | nts | | | | | | | | | | | | | | |
|---|--------|--------|--------|------|------|-------|-------|------|----|-------|-------|----|------|-------|-------|---|
| Approach | T | Eastb | ound | | | Westl | bound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 |
| Configuration | | | | | | | LR | | | | Т | TR | | L | Т | |
| Volume (veh/h) | | | | | | 95 | | 55 | | | 925 | 92 | 1 | 130 | 375 | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | | 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | T | | | | | 7.5 | | 6.9 | | | | | 6.4 | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | 6.46 | 4.16 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | 2.5 | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | 2.53 | 2.23 | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | Т | | | | | | 169 | | | | | | | 147 | | |
| Capacity, c (veh/h) | | | | | | | 238 | | | | | | | 594 | | |
| v/c Ratio | | | | | | | 0.71 | | | | | | | 0.25 | | |
| 95% Queue Length, Q ₉₅ (veh) | | Ì | Ì | | | Ì | 4.7 | | Ì | | Ì | | | 1.0 | | |
| Control Delay (s/veh) | | | | | | | 49.9 | | | | | | | 13.0 | | |
| Level of Service (LOS) | | | | | | | E | | | | | | | В | | |
| Approach Delay (s/veh) | | 49.9 | | | | | | | | | • | | 3 | .4 | | |
| Approach LOS | | | | E | | | | | | A | | | | | | |

| HCS Two-Way Stop-Control Report | | | | | | | | | | |
|---------------------------------|---|--------------------|---------------------------|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive | | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut | | | | | | | |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive | | | | | | | |
| Analysis Year | 2026 | North/South Street | Concord Road | | | | | | | |
| Time Analyzed | PM Peak | Peak Hour Factor | 0.90 | | | | | | | |
| Intersection Orientation | ction Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | |
| Project Description | Project Description 2026 Combined PM Peak | | | | | | | | | |

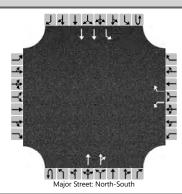


| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | |
|---|--------|---------|--------|------|------|-------|-------|------|----|-------|-------|----|----|-------|-------|---|
| Approach | | Eastb | ound | | | Westl | oound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 |
| Configuration | | | | | | | LR | | | | T | TR | | L | Т | |
| Volume (veh/h) | | | | | | 111 | | 28 | | | 775 | 55 | 0 | 128 | 935 | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | |
| Critical and Follow-up He | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | | 4.16 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | | 2.23 | | |
| Delay, Queue Length, and | d Leve | l of Se | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 154 | | | | | | | 142 | | |
| Capacity, c (veh/h) | | | | | | | 213 | | | | | | | 730 | | |
| v/c Ratio | | | | | | | 0.72 | | | | | | | 0.19 | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 4.8 | | | | | | | 0.7 | | |
| Control Delay (s/veh) | | | | | | | 56.6 | | | | | | | 11.1 | | |
| Level of Service (LOS) | | | | | | | F | | | | | | | В | | |
| Approach Delay (s/veh) | | | | | | 56 | 5.6 | | | | | | | 1 | .3 | |
| Approach LOS | | | | | | | F | | | | | | | , | A | |

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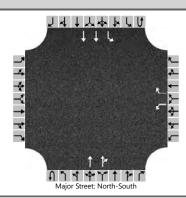
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| | HCS Two-Way Stop | -Control Report | |
|--------------------------|---|----------------------------|---------------------------|
| General Information | | Site Information | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive |
| Analysis Year | 2026 | North/South Street | Concord Road |
| Time Analyzed | AM Peak | Peak Hour Factor | 0.89 |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 |
| Project Description | 2026 Combined AM Peak Exclusive Left and Ri | ght | |



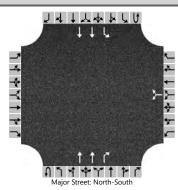
| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | |
|---|--------|---------|--------|------|------|-------|-------|------|----|-------|-------|----|------|-------|-------|---|
| Approach | | Eastb | ound | | | Westl | oound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | Т | R | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 |
| Configuration | | | | | | L | | R | | | Т | TR | | L | Т | |
| Volume (veh/h) | | | | | | 95 | | 55 | | | 925 | 92 | 1 | 130 | 375 | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (|) | | | | | | | | | |
| Right Turn Channelized | | | | | | Ν | lo | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | 6.4 | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | 6.46 | 4.16 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | 2.5 | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | 2.53 | 2.23 | | |
| Delay, Queue Length, an | d Leve | l of Se | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | T | | | | | 107 | | 62 | | | | | | 147 | | |
| Capacity, c (veh/h) | | | | | | 186 | | 461 | | | | | | 594 | | |
| v/c Ratio | | | | | | 0.57 | | 0.13 | | | | | | 0.25 | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | 3.1 | | 0.5 | | | | | | 1.0 | | |
| Control Delay (s/veh) | | | | | | 47.5 | | 14.0 | | | | | | 13.0 | | |
| Level of Service (LOS) | | | | | | Е | | В | | | | | | В | | |
| Approach Delay (s/veh) | | | | | | 3: | 5.2 | | | | | | | 3 | .4 | |
| Approach LOS | | | | | | | E | | | | | | | , | 4 | |

| | HCS Two-Way Stop | -Control Report | |
|--------------------------|--|----------------------------|---------------------------|
| General Information | | Site Information | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive |
| Analysis Year | 2026 | North/South Street | Concord Road |
| Time Analyzed | PM Peak | Peak Hour Factor | 0.90 |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 |
| Project Description | 2026 Combined PM Peak Exclusive Left and Rig | ght | |



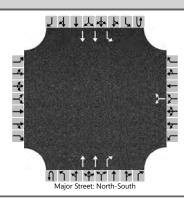
| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | | |
|---|--------|--------|--------|------|------|-------|-------|------|----|-------|-------|----|----|-------|--|---|--|
| Approach | T | Eastk | ound | | | Westl | oound | | | North | bound | | | South | bound | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | |
| Number of Lanes | | 0 | 0 | 0 | | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 0 | |
| Configuration | | | | | | L | | R | | | Т | TR | | L | Т | | |
| Volume (veh/h) | | | | | | 111 | | 28 | | | 775 | 55 | 0 | 128 | 935 | | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (|) | | | | | | | | | | |
| Right Turn Channelized | | | | | | N | lo | | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | | 4.1 | | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | | 4.16 | | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | | 2.23 | | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | T | | | | | 123 | | 31 | | | | | | 142 | | | |
| Capacity, c (veh/h) | | | | | | 185 | | 545 | | | | | | 730 | | | |
| v/c Ratio | | | | | | 0.67 | | 0.06 | | | | | | 0.19 | | | |
| 95% Queue Length, Q ₉₅ (veh) | | Ì | Ì | | | 4.0 | | 0.2 | Ì | | Ì | | | 0.7 | | | |
| Control Delay (s/veh) | | | | | | 56.7 | | 12.0 | | | | | | 11.1 | | | |
| Level of Service (LOS) | | | | | | F | | В | | | | | | В | | | |
| Approach Delay (s/veh) | | | | | | 47 | 7.7 | | | | | | | 1 | 4.16 2.2 2.23 142 730 0.19 0.7 11.1 | | |
| Approach LOS | | | | | | ı | E | | | | | | | | | | |

| | HCS Two-Way Stop | -Control Report | |
|--------------------------|--|----------------------------|---------------------------|
| General Information | | Site Information | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive |
| Analysis Year | 2026 | North/South Street | Concord Road |
| Time Analyzed | AM Peak | Peak Hour Factor | 0.89 |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 |
| Project Description | 2026 Combined AM Peak Northbound Right | | |



| Vehicle Volumes and Ad | , | | | | | | | | | | | | | 0 11 1 | | |
|---|--------|--------|--------|------|------|-------|-------|------|----|-------|-------|----|------|----------|-------|---|
| Approach | | Eastb | ound | | | Westl | oound | | | North | bound | | | South | bound | |
| Movement | U | L | T | R | U | L | Т | R | U | L | T | R | U | L | T | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 1 | 2 | 0 |
| Configuration | | | | | | | LR | | | | Т | R | | L | Т | |
| Volume (veh/h) | | | | | | 95 | | 55 | | | 925 | 92 | 1 | 130 | 375 | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | Ν | lo | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | |
| Critical and Follow-up H | leadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.5 | | 6.9 | | | | | 6.4 | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | 6.46 | 4.16 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | 2.5 | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | 2.53 | 2.23 | | |
| Delay, Queue Length, ar | d Leve | l of S | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 169 | | | | | | | 147 | | |
| Capacity, c (veh/h) | | | | | | | 251 | | | | | | | 596 | | |
| v/c Ratio | | | | | | | 0.67 | | | | | | | 0.25 | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 4.3 | | | | | | | 1.0 | | |
| Control Delay (s/veh) | | | | | | | 44.3 | | | | | | | 13.0 | | |
| Level of Service (LOS) | | | Ì | | | | E | | | | | | | В | | |
| Approach Delay (s/veh) | | | - | | | 44 | 4.3 | • | | | • | • | 3.4 | | | |
| Approach LOS | 1 | | | | | | E | | | | | | | 3.4 A | | |

| | HCS Two-Way Stop | -Control Report | |
|--------------------------|--|----------------------------|---------------------------|
| General Information | | Site Information | |
| Analyst | WDR | Intersection | Concord Road at 2nd Drive |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive |
| Analysis Year | 2026 | North/South Street | Concord Road |
| Time Analyzed | PM Peak | Peak Hour Factor | 0.90 |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 |
| Project Description | 2026 Combined PM Peak Northbound Right | | |



| Approach | Т | Easth | ound | | | Westk | ound | | | North | bound | | | Southbound | | | |
|---|--------|---------|--------|------|------|-------|------|------|----|-------|-------|----|-----|------------|-----|---|--|
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Priority | + | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 1 | 2 | 0 | |
| Configuration | | | | | | | LR | | | | Т | R | | L | Т | | |
| Volume (veh/h) | | | | | | 111 | | 28 | | | 775 | 55 | 0 | 128 | 935 | | |
| Percent Heavy Vehicles (%) | | | | | | 3 | | 3 | | | | | 3 | 3 | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (|) | | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | N | lo | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | T | | | | | 7.5 | | 6.9 | | | | | | 4.1 | | | |
| Critical Headway (sec) | | | | | | 6.86 | | 6.96 | | | | | | 4.16 | | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | | |
| Follow-Up Headway (sec) | | | | | | 3.53 | | 3.33 | | | | | | 2.23 | | | |
| Delay, Queue Length, an | d Leve | l of Se | ervice | | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 154 | | | | | | | 142 | | | |
| Capacity, c (veh/h) | | | | | | | 218 | | | | | | | 730 | | | |
| v/c Ratio | | | | | | | 0.71 | | | | | | | 0.19 | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 4.6 | | | | | | | 0.7 | | | |
| Control Delay (s/veh) | | | | | | | 53.6 | | | | | | | 11.1 | | | |
| Level of Service (LOS) | | | | | | | F | | | | | | | В | | | |
| Approach Delay (s/veh) | | | | | | 53 | 3.6 | | | | | | 1.3 | | | | |
| Approach LOS | | | 53.6 F | | | | | | | | | Α | | | | | |

| | • | • | † | / | > | ļ |
|-------------------------|--------|------|------------|------|-------------|----------|
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | W | | ∱ % | | * | ^ |
| Traffic Volume (vph) | 95 | 55 | 925 | 92 | 131 | 375 |
| Future Volume (vph) | 95 | 55 | 925 | 92 | 131 | 375 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 |
| Frt | 0.950 | 1.00 | 0.986 | 0.70 | 1.00 | 0.70 |
| Flt Protected | 0.969 | | 0.700 | | 0.950 | |
| Satd. Flow (prot) | 1715 | 0 | 3490 | 0 | 1770 | 3539 |
| Flt Permitted | 0.969 | U | 3470 | U | 0.146 | 3339 |
| | 1715 | 0 | 3490 | 0 | 272 | 3539 |
| Satd. Flow (perm) | | U | | U | 212 | 3339 |
| Satd. Flow (RTOR) | 50 | 0.00 | 19 | 0.00 | 0.02 | 0.00 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Shared Lane Traffic (%) | | | 445- | | | |
| Lane Group Flow (vph) | 163 | 0 | 1105 | 0 | 142 | 408 |
| Turn Type | Prot | | NA | | pm+pt | NA |
| Protected Phases | 8 | | 2 | | 1 | 6 |
| Permitted Phases | | | | | 6 | |
| Detector Phase | 8 | | 2 | | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | | 15.0 | | 5.0 | 15.0 |
| Minimum Split (s) | 23.5 | | 23.5 | | 10.5 | 23.5 |
| Total Split (s) | 23.5 | | 25.9 | | 10.6 | 36.5 |
| Total Split (%) | 39.2% | | 43.2% | | 17.7% | 60.8% |
| Yellow Time (s) | 37.270 | | 3.5 | | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | | 2.0 | | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | | 5.5 | | 5.5 | 5.5 |
| | 5.5 | | | | | 5.5 |
| Lead/Lag Ontimize? | | | Lag | | Lead | |
| Lead-Lag Optimize? | NI | | Yes | | Yes | C 14- |
| Recall Mode | None | | C-Max | | None | C-Max |
| Act Effct Green (s) | 10.1 | | 32.1 | | 41.6 | 42.7 |
| Actuated g/C Ratio | 0.17 | | 0.54 | | 0.69 | 0.71 |
| v/c Ratio | 0.50 | | 0.59 | | 0.38 | 0.16 |
| Control Delay | 20.7 | | 16.3 | | 7.6 | 4.4 |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Delay | 20.7 | | 16.3 | | 7.6 | 4.4 |
| LOS | С | | В | | Α | Α |
| Approach Delay | 20.7 | | 16.3 | | | 5.2 |
| Approach LOS | C C | | В | | | A |
| Queue Length 50th (ft) | 38 | | 156 | | 15 | 24 |
| Queue Length 95th (ft) | 79 | | #317 | | 41 | 49 |
| 0 , , | 739 | | | | 41 | |
| Internal Link Dist (ft) | / 39 | | 696 | | / [| 696 |
| Turn Bay Length (ft) | F 40 | | 107/ | | 65 | 2510 |
| Base Capacity (vph) | 549 | | 1876 | | 371 | 2519 |
| Starvation Cap Reductn | 0 | | 0 | | 0 | 0 |
| Spillback Cap Reductn | 0 | | 0 | | 0 | 0 |
| Storage Cap Reductn | 0 | | 0 | | 0 | 0 |
| Reduced v/c Ratio | 0.30 | | 0.59 | | 0.38 | 0.16 |
| Intersection Summary | | | | | | |

Timing Plan: AM Peak Cannon & Cannon, Inc. Synchro 11 Report Page 1

| Cycle Length: 60 | |
|---|------------------------|
| Actuated Cycle Length: 60 | |
| Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start (| of Green |
| Natural Cycle: 60 | |
| Control Type: Actuated-Coordinated | |
| Maximum v/c Ratio: 0.59 | |
| Intersection Signal Delay: 13.3 | Intersection LOS: B |
| Intersection Capacity Utilization 58.1% | ICU Level of Service B |
| Analysis Period (min) 15 | |
| # 95th percentile volume exceeds capacity, queue may be lo | nger. |
| Queue shown is maximum after two cycles. | |
| | |
| Splits and Phases: 2: Concord Rd & 2nd Dr | |
| Ø1 Ø2 (R) | |

| | • | 4 | † | ~ | > | ţ |
|-------------------------|-------|------|------------|------|-------------|----------|
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | W | | ∱ % | | ች | ^ |
| Traffic Volume (vph) | 111 | 28 | 775 | 55 | 128 | 935 |
| Future Volume (vph) | 111 | 28 | 775 | 55 | 128 | 935 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 |
| Frt | 0.973 | | 0.990 | 0.70 | | 3.73 |
| Flt Protected | 0.961 | | 3.770 | | 0.950 | |
| Satd. Flow (prot) | 1742 | 0 | 3504 | 0 | 1770 | 3539 |
| Flt Permitted | 0.961 | J | 5501 | | 0.232 | 5557 |
| Satd. Flow (perm) | 1742 | 0 | 3504 | 0 | 432 | 3539 |
| Satd. Flow (RTOR) | 21 | | 9 | | 102 | 3307 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Shared Lane Traffic (%) | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |
| Lane Group Flow (vph) | 151 | 0 | 902 | 0 | 139 | 1016 |
| Turn Type | Prot | U | NA | U | pm+pt | NA |
| Protected Phases | 8 | | 2 | | риі+рі 1 | 6 |
| Permitted Phases | U | | ۷ | | 6 | U |
| Detector Phase | 8 | | 2 | | 1 | 6 |
| Switch Phase | Ŏ | | Z | | ı | 0 |
| Minimum Initial (s) | 8.0 | | 15.0 | | 5.0 | 15.0 |
| | 43.5 | | 23.5 | | 10.5 | 23.5 |
| Minimum Split (s) | | | | | | |
| Total Split (s) | 43.5 | | 25.9 | | 10.6 | 36.5 |
| Total Split (%) | 54.4% | | 32.4% | | 13.3% | 45.6% |
| Yellow Time (s) | 3.5 | | 3.5 | | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | | 2.0 | | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | | 5.5 | | 5.5 | 5.5 |
| Lead/Lag | | | Lag | | Lead | |
| Lead-Lag Optimize? | N. | | Yes | | Yes | 0.14 |
| Recall Mode | None | | C-Max | | None | C-Max |
| Act Effct Green (s) | 11.8 | | 43.6 | | 57.2 | 57.2 |
| Actuated g/C Ratio | 0.15 | | 0.54 | | 0.72 | 0.72 |
| v/c Ratio | 0.55 | | 0.47 | | 0.31 | 0.40 |
| Control Delay | 34.2 | | 13.0 | | 6.0 | 5.5 |
| Queue Delay | 0.0 | | 0.0 | | 0.0 | 0.0 |
| Total Delay | 34.2 | | 13.0 | | 6.0 | 5.5 |
| LOS | С | | В | | Α | Α |
| Approach Delay | 34.2 | | 13.0 | | | 5.6 |
| Approach LOS | С | | В | | | Α |
| Queue Length 50th (ft) | 61 | | 130 | | 17 | 85 |
| Queue Length 95th (ft) | 110 | | 222 | | 42 | 148 |
| Internal Link Dist (ft) | 739 | | 696 | | | 696 |
| Turn Bay Length (ft) | | | | | 65 | |
| Base Capacity (vph) | 838 | | 1913 | | 444 | 2531 |
| Starvation Cap Reductn | 0 | | 0 | | 0 | 0 |
| Spillback Cap Reductn | 0 | | 0 | | 0 | 0 |
| Storage Cap Reductn | 0 | | 0 | | 0 | 0 |
| Reduced v/c Ratio | 0.18 | | 0.47 | | 0.31 | 0.40 |
| Intersection Summary | | | | | | |

Timing Plan: PM Peak Cannon & Cannon, Inc.

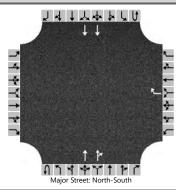
Synchro 11 Report Page 1

| Cycle Length: 80 | |
|--|------------------------|
| Actuated Cycle Length: 80 | |
| Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of | of Green |
| Natural Cycle: 80 | |
| Control Type: Actuated-Coordinated | |
| Maximum v/c Ratio: 0.55 | |
| Intersection Signal Delay: 10.5 | Intersection LOS: B |
| Intersection Capacity Utilization 51.9% | ICU Level of Service A |
| Analysis Period (min) 15 | |
| | |
| Splits and Phases: 2: Concord Rd & 2nd Dr | |
| Ø1 Ø2 (R) | |
| 10.6 s 25.9 s | |
| k | l - |

| | | | | НС | S Ro | unda | abo | uts | Rep | ort | | | | | | | | |
|--|--------|---------|-----------|----------|------------|-------|----------|--------|-----|--------|-------------|-----------|-------|-------------|--------|----------|--------|--|
| General Information | | | | | | | Sit | te Inf | orn | natio | า | | | | | | | |
| Analyst | WDR | | | | 1 | 15 | | | | Inters | ection | | | Nortl | nshore | Drive at | Concor | |
| Agency or Co. | Cann | on & Ca | nnon, Inc | i. | // | | - | 1 | ī. | E/W S | Street Na | me | | Nortl | nshore | Drive | | |
| Date Performed | 4/16/ | 2024 | | | | | N | , | 1 | N/S S | treet Nar | ne | | Conc | ord Ro | ad | | |
| Analysis Year | 2026 | | | | ▼ ↓ | W | ∯ E S | 1 | H | Analy | rsis Time I | Period, h | rs | 0.25 | | | | |
| Time Analyzed | AM P | eak | | | | | | | | Peak | Hour Fact | tor | | 0.88 | | | | |
| Project Description | 2026 | Combin | ed AM Pe | eak | | | , | 1 | | Jurisc | liction | | | Knox County | | | | |
| Volume Adjustment | s and | Site C | harac | teristic | S | | | | | | | | | | | | | |
| Approach | | E | B | | | ٧ | VB | | | | N | В | | | | SB | | |
| Movement | U | L | Т | R | U | L | Т | - | R | U | L | Т | R | U | L | Т | R | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | |
| Lane Assignment | | | L | .T | | | | Т | | | | | | | | | L | |
| Volume (V), veh/h | 1 | 626 | 548 | | 2 | | 33 | 4 3 | 92 | | | | | 1 | 236 | | 164 | |
| Percent Heavy Vehicles, % | 3 | 3 | 3 | | 3 | | 3 | | 3 | | | | | 3 | 3 | | 3 | |
| Flow Rate (VPCE), pc/h | 1 | 733 | 641 | | 2 | | 39 | 1 4 | 59 | | | | | 1 | 276 | | 192 | |
| Right-Turn Bypass | | No | one | | | Non-Y | /ieldir | ng | | | No | ne | | | Yi | ielding | | |
| Conflicting Lanes | | | 1 | | | | 1 | | | | | | | | | 1 | | |
| Pedestrians Crossing, p/h | | | 0 | | | | 0 | | | | | | | | | 0 | | |
| Proportion of CAVs | | | | | | | | | (|) | | | | | | | | |
| Critical and Follow-U | Jp He | adway | / Adju | stmen | t | | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | E | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | |
| Critical Headway, s | | | | 4.9763 | | | | 4.976 | 3 | | | | | | | 4.9763 | 4.9763 | |
| Follow-Up Headway, s | | | | 2.6087 | | | | 2.608 | 7 | | | | | Т | | 2.6087 | 2.6087 | |
| Flow Computations, | Capa | city ar | nd v/c | Ratios | ; | | | | | | | | | | | | | |
| Approach | | \neg | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | E | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | |
| Entry Flow (v _e), pc/h | | | | 1375 | | | | 393 | T | 459 | | | | т | | 277 | 192 | |
| Entry Volume, veh/h | | | | 1335 | | | | 382 | | 446 | | | | | | 269 | 186 | |
| Circulating Flow (v _c), pc/h | | | | 279 | | | | 735 | | | | 1654 | | | | 394 | | |
| Exiting Flow (vex), pc/h | | | | 919 | | | | 392 | | | | 734 | | | | 0 | | |
| Capacity (Cpce), pc/h | | | | 1038 | | | | 652 | | | | | | Т | | 923 | 925 | |
| Capacity (c), veh/h | | | | 1008 | | | | 633 | | | | | | | | 896 | 898 | |
| v/c Ratio (x) | | | | 1.32 | | | | 0.60 | | | | | | | | 0.30 | 0.21 | |
| Delay and Level of S | ervice | • | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | | WB | | | | NB | | | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | E | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | |
| Lane Control Delay (d), s/veh | | | | 167.9 | | | | 16.9 | | | | | | | | 7.2 | 6.1 | |
| Lane LOS | | | | F | | | | С | | Α | | | | | | А | А | |
| 95% Queue, veh | | | | 50.7 | | | | 4.0 | | | | | | | | 1.3 | 0.8 | |
| Approach Delay, s/veh | | | | 167.9 | | | | 7.8 | | | | | | | | 6.8 | | |
| Approach LOS | | | | F | | | | Α | | | | | | | | Α | | |
| Intersection Delay, s/veh LC | S | | | | | 89.3 | | | | | | | | F | | | | |

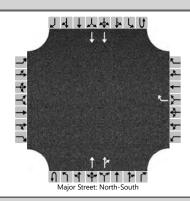
| | | | | НС | S Ro | un <u>d</u> a | abo | uts l | Rep | ort | | | | | | | | |
|--|--------|----------|-----------|----------|-------|---------------|----------|-------|-----|--------|------------|-----------|--------|-------------|--------|----------|--------|--|
| General Information | | | | | | | | | | natior | 1 | | | | | | | |
| Analyst | WDR | | | | | Jι | A | 1 | | Inters | ection | | Т | North | nshore | Drive at | Concor | |
| Agency or Co. | Cann | on & Cai | nnon, Inc | | // | | + | 1 | ī. | _ | Street Na | me | | North | nshore | Drive | | |
| Date Performed | 4/16/ | 2024 | | | / | 4 | | 1 | H | N/S S | treet Nar | me | | Conc | ord Ro | ad | | |
| Analysis Year | 2026 | | | | ∢ ↓ | W | † E | 1 | H | Analy | sis Time I | Period, h | rs | 0.25 | | | | |
| Time Analyzed | PM P | eak | | | * | | | | | Peak | Hour Fact | tor | | 0.95 | | | | |
| Project Description | 2026 | Combine | ed PM Pe | eak | | | - | 1 | | Juriso | liction | | | Knox County | | | | |
| Volume Adjustments | s and | Site C | harac | teristic | s | | | | | | | | | | | | | |
| Approach | | E | :B | | | ١ | WB | | | | N | В | | | | SB | | |
| Movement | U | L | Т | R | U | L | T | - | R | U | L | Т | R | U | L | Т | R | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | |
| Lane Assignment | | | L | T | | | | T | | | | | | | | | L | |
| Volume (V), veh/h | 1 | 279 | 418 | | 13 | | 64 | 16 5 | 41 | | | | | 1 | 557 | | 485 | |
| Percent Heavy Vehicles, % | 3 | 3 | 3 | | 3 | | 3 | 3 | 3 | | | | | 3 | 3 | | 3 | |
| Flow Rate (VPCE), pc/h | 1 | 302 | 453 | | 14 | | 70 | 00 5 | 87 | | | | | 1 | 604 | | 526 | |
| Right-Turn Bypass | | No | ne | | | Non- | Yieldii | ng | | | No | ne | | | Yi | elding | | |
| Conflicting Lanes | | | 1 | | | | 1 | | | | | | | | | 1 | | |
| Pedestrians Crossing, p/h | | | 0 | | | | 0 | | | | | | | | | 0 | | |
| Proportion of CAVs | | | | | | | | | (|) | | | | | | | | |
| Critical and Follow-L | Jp He | adway | / Adju | stmen | t | | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | ss L | .eft | Right | E | Bypass | Left | Right | Bypass | L | .eft | Right | Bypass | |
| Critical Headway, s | | | | 4.9763 | | | | 4.976 | 3 | | | | | Т | | 4.9763 | 4.9763 | |
| Follow-Up Headway, s | | | | 2.6087 | | | | 2.608 | 7 | | | | | | | 2.6087 | 2.6087 | |
| Flow Computations, | Capac | city ar | nd v/c | Ratios | , | | | | | | | | | | | | | |
| Approach | | Ī | | EB | | Т | | WB | | | | NB | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | ss L | .eft | Right | E | Bypass | Left | Right | Bypass | L | .eft | Right | Bypass | |
| Entry Flow (v _e), pc/h | | | | 756 | | | | 714 | T | 587 | | | | Т | | 605 | 526 | |
| Entry Volume, veh/h | | | | 734 | | | | 693 | | 570 | | | | | | 587 | 511 | |
| Circulating Flow (v _c), pc/h | | | | 619 | | | | 304 | | | | 1375 | | Т | | 715 | | |
| Exiting Flow (vex), pc/h | | | | 1071 | | | | 701 | | | | 303 | | | | 0 | | |
| Capacity (c _{pce}), pc/h | | | | 734 | | | | 1012 | Τ | | | | | Т | | 666 | 675 | |
| Capacity (c), veh/h | | | | 713 | | | | 983 | | | | | | | | 646 | 655 | |
| v/c Ratio (x) | | | | 1.03 | | | | 0.71 | T | | | | | Т | | 0.91 | 0.78 | |
| Delay and Level of S | ervice | | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | | | NB | | Π | | SB | | |
| Lane | | | Left | Right | Bypas | ss L | .eft | Right | E | Bypass | Left | Right | Bypass | L | .eft | Right | Bypass | |
| Lane Control Delay (d), s/veh | | | | 65.7 | | | | 15.5 | | | | | | | | 41.6 | 26.0 | |
| Lane LOS | | | | F | | | | С | | Α | | | | | | E | D | |
| 95% Queue, veh | | | | 18.0 | | | | 6.1 | | | | | | | | 11.6 | 7.5 | |
| Approach Delay, s/veh | | | | 65.7 | | | | 8.5 | | | | | | | , | 34.3 | | |
| Approach LOS | | | | F | | | | А | | | | | | Т | | D | | |
| Intersection Delay, s/veh LO | S | | | | | 31.2 | | | | | | | | D | | | | |

| | HCS Two-Way Stop | -Control Report | | | | | | | |
|--------------------------|-----------------------|----------------------------|-----------------------------|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | |
| Analyst | WDR | Intersection | Concord Road at Site Access | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut | | | | | | |
| Date Performed | 5/20/2024 | East/West Street | Site Access | | | | | | |
| Analysis Year | 2026 | North/South Street | Concord Road | | | | | | |
| Time Analyzed | AM Peak | Peak Hour Factor | 0.89 | | | | | | |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 | | | | | | |
| Project Description | 2026 Combined AM Peak | | | | | | | | |



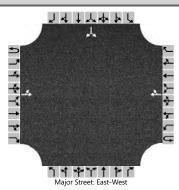
| Vehicle Volumes and Ad | justme | nts | | | | | | | | | | | | | | |
|---|--------|------------|--------|------|------|-------|-------|------|----|-------|-------|---|----|-------|-------|---|
| Approach | | Eastb | oound | | | Westl | bound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 |
| Configuration | | R T | | | | | | TR | | | Т | | | | | |
| Volume (veh/h) | | 152 895 85 | | | | | | 85 | | | 506 | | | | | |
| Percent Heavy Vehicles (%) | | | | | | | | 3 | | | | | | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | Ν | lo | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | | | 6.9 | | | | | | | | |
| Critical Headway (sec) | | | | | | | | 6.96 | | | | | | | | |
| Base Follow-Up Headway (sec) | | | | | | | | 3.3 | | | | | | | | |
| Follow-Up Headway (sec) | | | | | | | | 3.33 | | | | | | | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | | 171 | | | | | | | | |
| Capacity, c (veh/h) | | | | | | | | 476 | | | | | | | | |
| v/c Ratio | | | | | | | | 0.36 | | | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | | 1.6 | | | | | | | Ì | |
| Control Delay (s/veh) | | | | | | | | 16.7 | | | | | | | | |
| Level of Service (LOS) | | C | | | | | | | | | | | | | | |
| Approach Delay (s/veh) | | 16.7 | | | | | • | | | | • | | • | • | | |
| Approach LOS | | С | | | | | | | | | | | | | | |

| | HCS Two-Way Stop | -Control Report | |
|--------------------------|-----------------------|----------------------------|-----------------------------|
| General Information | | Site Information | |
| Analyst | WDR | Intersection | Concord Road at Site Access |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Town of Farragut |
| Date Performed | 5/20/2024 | East/West Street | Site Access |
| Analysis Year | 2026 | North/South Street | Concord Road |
| Time Analyzed | PM Peak | Peak Hour Factor | 0.90 |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 |
| Project Description | 2026 Combined PM Peak | | |



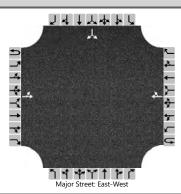
| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | |
|---|--------|---------|--------|------|------|-------|-------|------|----|-------|-------|----|----|-------|-------|---|
| Approach | | Eastb | ound | | | Westl | oound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 |
| Configuration | | | | | | | | R | | | Т | TR | | | Т | |
| Volume (veh/h) | | | | | | | | 82 | | | 762 | 41 | | | 1063 | |
| Percent Heavy Vehicles (%) | | | | | | | | 3 | | | | | | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | Ν | lo | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | |
| Critical and Follow-up He | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | | | 6.9 | | | | | | | | |
| Critical Headway (sec) | | | | | | | | 6.96 | | | | | | | | |
| Base Follow-Up Headway (sec) | | | | | | | | 3.3 | | | | | | | | |
| Follow-Up Headway (sec) | | | | | | | | 3.33 | | | | | | | | |
| Delay, Queue Length, and | d Leve | l of Se | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | T | | | | | | | 91 | | | | | | | | |
| Capacity, c (veh/h) | | | | | | | | 557 | | | | | | | | |
| v/c Ratio | | | | | | | | 0.16 | | | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | | 0.6 | | | | | | | | |
| Control Delay (s/veh) | | | | | | | | 12.7 | | | | | | | | |
| Level of Service (LOS) | | | | | | | | В | | | | | | | | |
| Approach Delay (s/veh) | | | | | | 12 | 2.7 | | | | | | | | | |
| Approach LOS | | В | | | | | | | | | | | | | | |

| | HCS Two-Way Stop-Control Report | | | | | | | | | | | |
|--------------------------|---------------------------------|----------------------------|--------------------------|--|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | | |
| Analyst | WDR | Intersection | 2nd Drive at Site Access | | | | | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Knox County | | | | | | | | | |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive | | | | | | | | | |
| Analysis Year | 2026 | North/South Street | Site Access | | | | | | | | | |
| Time Analyzed | AM Peak | Peak Hour Factor | 0.89 | | | | | | | | | |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 | | | | | | | | | |
| Project Description | 2026 Combined AM Peak | | | | | | | | | | | |



| Vehicle Volumes and Ad | T | | | | П | | | | П | N 1 -1 | | | T | 6 11 | | |
|---|--------|---------|--------|------|------|-------|-------|----|---|---------------|-------|---|---|-------|-------|------|
| Approach | | Eastb | ound | | | Westl | oound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | | 7 | 8 | 9 | | 10 | 11 | 12 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 |
| Configuration | | LT | | | | | | TR | | | | | | | LR | |
| Volume (veh/h) | | 219 | 4 | | | | 4 | 0 | | | | | | 0 | | 146 |
| Percent Heavy Vehicles (%) | | 3 | | | | | | | | | | | | 3 | | 3 |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | | | | | | | | | (| 0 | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | | | Left | Only | | | | | | | | 1 | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | 4.1 | | | | | | | | | | | | 7.1 | | 6.2 |
| Critical Headway (sec) | | 4.13 | | | | | | | | | | | | 6.43 | | 6.23 |
| Base Follow-Up Headway (sec) | | 2.2 | | | | | | | | | | | | 3.5 | | 3.3 |
| Follow-Up Headway (sec) | | 2.23 | | | | | | | | | | | | 3.53 | | 3.33 |
| Delay, Queue Length, an | d Leve | l of Se | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | T | 246 | | | | | | | | | | | | | 164 | |
| Capacity, c (veh/h) | | 1610 | | | | | | | | | | | | | 1076 | |
| v/c Ratio | | 0.15 | | | | | | | | | | | | | 0.15 | |
| 95% Queue Length, Q ₉₅ (veh) | | 0.5 | | | | | | | | | | | | | 0.5 | |
| Control Delay (s/veh) | | 7.6 | 1.2 | | | | | | | | | | | | 8.9 | |
| Level of Service (LOS) | | А | А | | | | | | | | | | | | А | |
| Approach Delay (s/veh) | | 7 | .5 | | | | | | | | | | | 8 | .9 | |
| Approach LOS | | A A | | | | | | | | | | | | | | |

| | HCS Two-Way Stop | -Control Report | | | | | | |
|--------------------------|-----------------------|----------------------------|--------------------------|--|--|--|--|--|
| General Information | | Site Information | | | | | | |
| Analyst | WDR | Intersection | 2nd Drive at Site Access | | | | | |
| Agency/Co. | Cannon & Cannon, Inc. | Jurisdiction | Knox County | | | | | |
| Date Performed | 5/20/2024 | East/West Street | 2nd Drive | | | | | |
| Analysis Year | 2026 | North/South Street | Site Access | | | | | |
| Time Analyzed | PM Peak | Peak Hour Factor | 0.90 | | | | | |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 | | | | | |
| Project Description | 2026 Combined PM Peak | | | | | | | |



| Vehicle Volumes and Ad | justme | nts | | | | | | | | | | | | | | |
|---|--------|---------|--------|------|-------|-------|-------|----|---|-------|-------|---|---|-------|-------|------|
| Approach | T | Eastb | ound | | | Westl | bound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | | 7 | 8 | 9 | | 10 | 11 | 12 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 |
| Configuration | | LT | | | | | | TR | | | | | | | LR | |
| Volume (veh/h) | | 178 | 5 | | | | 8 | 0 | | | | | | 0 | | 131 |
| Percent Heavy Vehicles (%) | | 3 | | | | | | | | | | | | 3 | | 3 |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | | | | | | | | | | 0 | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | | | Undi | vided | | | | | | | | | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | T | 4.1 | | | | | | | | | | | | 7.1 | | 6.2 |
| Critical Headway (sec) | | 4.13 | | | | | | | | | | | | 6.43 | | 6.23 |
| Base Follow-Up Headway (sec) | | 2.2 | | | | | | | | | | | | 3.5 | | 3.3 |
| Follow-Up Headway (sec) | | 2.23 | | | | | | | | | | | | 3.53 | | 3.33 |
| Delay, Queue Length, an | d Leve | l of Se | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | T | 198 | | | | | | | | | | | | | 146 | |
| Capacity, c (veh/h) | | 1605 | | | | | | | | | | | | | 1070 | |
| v/c Ratio | | 0.12 | | | | | | | | | | | | | 0.14 | |
| 95% Queue Length, Q ₉₅ (veh) | | 0.4 | | | | | | | | | | | | | 0.5 | |
| Control Delay (s/veh) | | 7.6 | 0.9 | | | | | | | | | | | | 8.9 | |
| Level of Service (LOS) | | А | А | | | | | | | | | | | | А | |
| Approach Delay (s/veh) | | 7 | .4 | | | | | | | | | | | . 8 | .9 | • |
| Approach LOS | | , | A | | | | | | | | | | | , | A | |

APPENDIX D - TURN LANE WARRANT EVALUATIONS



TABLE 4A KNOX COUNTY LEFT-TURN LANE VOLUME THRESHOLDS FOR 2-LANE ROADWAYS WITH A PREVAILING SPEED OF 0 TO 35 MPH

Project No: 01634-0010
Project Name: EZ Stop Concord
Notes: 2nd Drive at Site Access

(If the left-turn volume exceeds the table value a left-turn lane is needed)

| OPPOSING | | THRO | OUGH VOLUME PLUS | S RIGHT-TURN VOLU | JME * | |
|-------------|-----------|-----------|------------------|-------------------|-----------|-----------|
| VOLUME | 100 - 149 | 150 - 199 | 200 - 249 | 250 - 299 | 300 - 349 | 350 - 399 |
| 100 - 149 | 300 | 235 | 185 | 145 | 120 | 100 |
| 150 - 199 | 245 | 200 | 160 | 130 | 110 | 90 |
| 200 - 249 | 205 | 170 | 140 | 115 | 100 | 80 |
| 250 - 299 | 175 | 150 | 125 | 105 | 90 | 70 |
| 300 - 349 | 155 | 135 | 110 | 95 | 80 | 65 |
| 350 - 399 | 135 | 120 | 100 | 85 | 70 | 60 |
| 400 - 449 | 120 | 105 | 90 | 75 | 65 | 55 |
| 450 - 499 | 105 | 90 | 80 | 70 | 60 | 50 |
| 500 - 549 | 95 | 80 | 70 | 65 | 55 | 50 |
| 550 - 599 | 85 | 70 | 65 | 60 | 50 | 45 |
| 600 - 649 | 75 | 65 | 60 | 55 | 45 | 40 |
| 650 - 699 | 70 | 60 | 55 | 50 | 40 | 35 |
| 700 - 749 | 65 | 55 | 50 | 45 | 35 | 30 |
| 750 or More | 60 | 50 | 45 | 40 | 35 | 30 |

| OPPOSING | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * | | | | | | | | |
|-------------|---|-----------|-----------|-----------|-----------|-----------|--|--|--|
| VOLUME | 350 - 399 | 400 - 449 | 450 - 499 | 500 - 549 | 550 - 599 | = / > 600 | | | |
| 100 - 149 | 100 | 80 | 70 | 60 | 55 | 50 | | | |
| 150 - 199 | 90 | 75 | 65 | 55 | 50 | 45 | | | |
| 200 - 249 | 80 | 72 | 60 | 55 | 50 | 45 | | | |
| 250 - 299 | 70 | 65 | 55 | 50 | 45 | 40 | | | |
| 300 - 349 | 65 | 60 | 50 | 50 | 45 | 40 | | | |
| 350 - 399 | 60 | 55 | 50 | 45 | 40 | 40 | | | |
| 400 - 449 | 55 | 50 | 45 | 45 | 40 | 35 | | | |
| 450 - 499 | 50 | 45 | 45 | 40 | 35 | 35 | | | |
| 500 - 549 | 50 | 45 | 40 | 40 | 35 | 35 | | | |
| 550 - 599 | 45 | 40 | 40 | 35 | 35 | 35 | | | |
| 600 - 649 | 40 | 35 | 35 | 35 | 35 | 30 | | | |
| 650 - 699 | 35 | 35 | 35 | 30 | 30 | 30 | | | |
| 700 - 749 | 30 | 30 | 30 | 30 | 30 | 30 | | | |
| 750 or More | 30 | 30 | 30 | 30 | 30 | 30 | | | |

^{*} Or through volume only if a right-turn lane exists

| Intersection | Time Period | Opposing Volume | Through Volume | Left-Turn Volume | Warrant Threshold | Left-Turn Lane Warranted (Yes / No) |
|----------------------|-------------|--------------------|-------------------|---------------------|----------------------|---|
| 2nd at Site Driveway | AM Peak | 4 | 4 | 219 | >300 | No |
| 2nd at Site Driveway | PM Peak | 8 | 5 | 178 | >300 | No |
| | | | | | | |
| | | | | | | |

Source: Knox County Department of Engineering and Public Works "Access Control and Driveway Design Policy"

TABLE 4B KNOX COUNTY RIGHT-TURN LANE VOLUME THRESHOLDS FOR 2-LANE ROADWAYS WITH A PREVAILING SPEED OF 0 TO 35 MPH

Project No: 01634-0010
Project Name: EZ Stop Concord
Notes: 2nd Drive at Site Access

| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | | | | |
|---------------|--|-----------|-----------|-----------|-----------|-----------|--|--|--|--|
| VOLUME | < 100 | 100 - 199 | 200 - 249 | 250 - 299 | 300 - 349 | 350 - 399 | | | | |
| Fewer Than 25 | | | | | | | | | | |
| 25 - 49 | | | | | | | | | | |
| 50 - 99 | | | | | | | | | | |
| 100 - 149 | | | | | | | | | | |
| 150 - 199 | | | | | | | | | | |
| 200 - 249 | | | | | | | | | | |
| 250 - 299 | | | | | | Yes | | | | |
| 300 - 349 | | | | | Yes | Yes | | | | |
| 350 - 399 | | | | Yes | Yes | Yes | | | | |
| 400 - 449 | | | Yes | Yes | Yes | Yes | | | | |
| 450 - 499 | | | Yes | Yes | Yes | Yes | | | | |
| 500 - 549 | | Yes | Yes | Yes | Yes | Yes | | | | |
| 550 - 599 | | Yes | Yes | Yes | Yes | Yes | | | | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | | | | |

| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | | | |
|---------------|--|-----------|-----------|-----------|-----------|-----------|--|--|--|
| VOLUME | 350 - 399 | 400 - 449 | 450 - 499 | 500 - 549 | 550 - 599 | = / > 600 | | | |
| Fewer Than 25 | | | | | | | | | |
| 25 - 49 | | | | | | Yes | | | |
| 50 - 99 | | | | | Yes | Yes | | | |
| 100 - 149 | | | | Yes | Yes | Yes | | | |
| 150 - 199 | | | Yes | Yes | Yes | Yes | | | |
| 200 - 249 | | Yes | Yes | Yes | Yes | Yes | | | |
| 250 - 299 | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| 300 - 349 | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| 350 - 399 | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| 400 - 449 | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| 450 - 499 | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| 500 - 549 | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| 550 - 599 | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | | | |

^{*} Or through volume only if a left-turn lane exists

| Intersection | Time Period | Through Volume | Right-Turn Volume | Right-Turn Lane Warranted (Yes / No) |
|-------------------------|-------------|-------------------|----------------------|--|
| 2nd Dr at Site Driveway | AM Peak | 4 | 0 | No |
| 2nd Dr at Site Driveway | PM Peak | 8 | 0 | No |
| | | | | |
| | | | | |

Source: Knox County Department of Engineering and Public Works "Access Control and Driveway Design Policy"

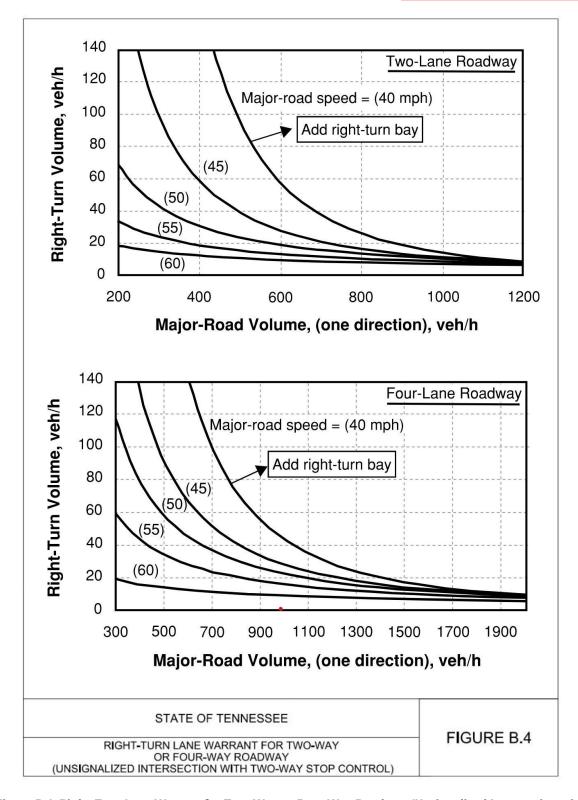


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Two-Way Stop Control)

Right-Turn Volume: 1 Major Road Volume: 914

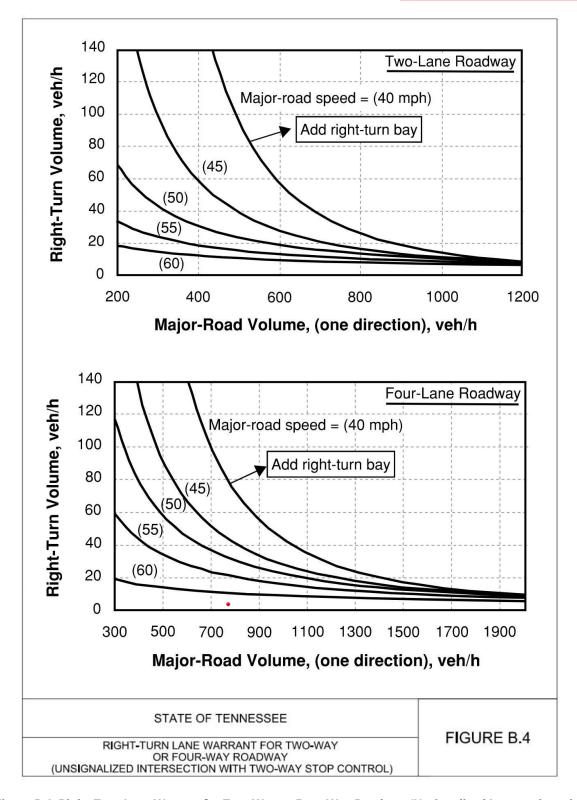


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Two-Way Stop Control)

Right-Turn Volume: 3 Major Road Volume: 755

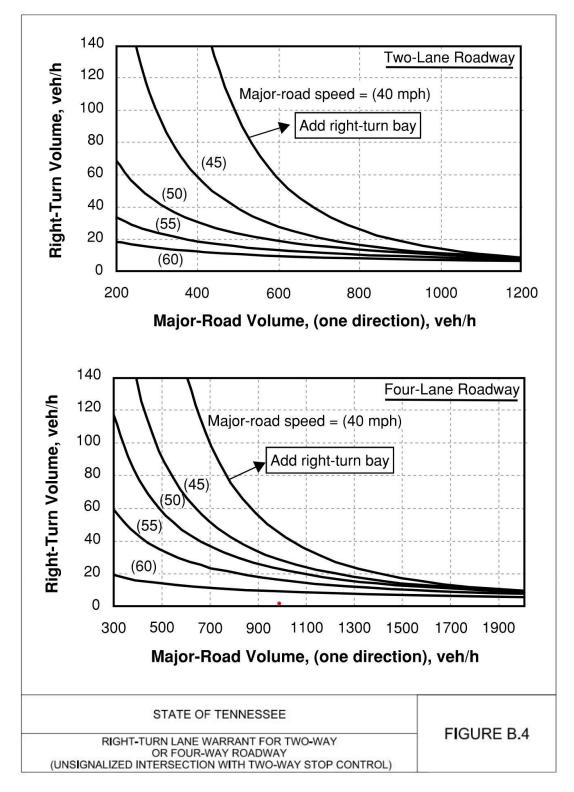


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Two-Way Stop Control)

Right-Turn Volume: 1 Major Road Volume: 979

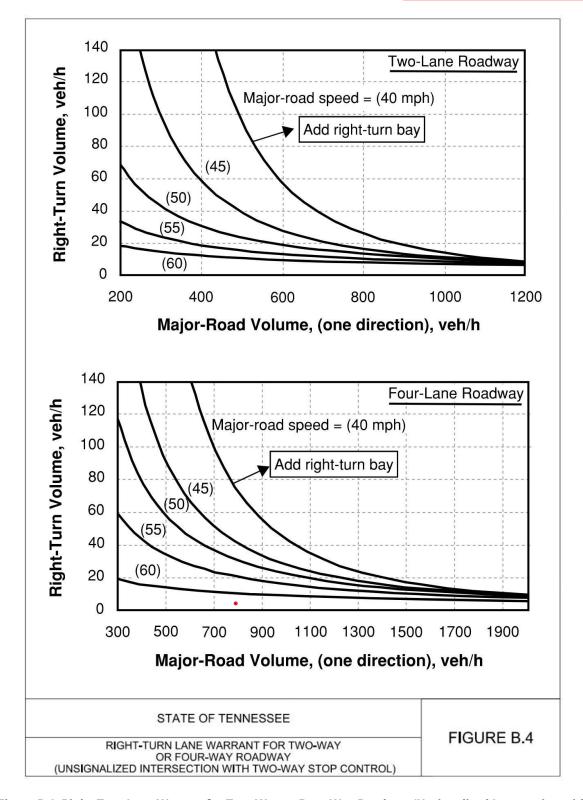


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Two-Way Stop Control)

Right-Turn Volume: 3 Major Road Volume: 809

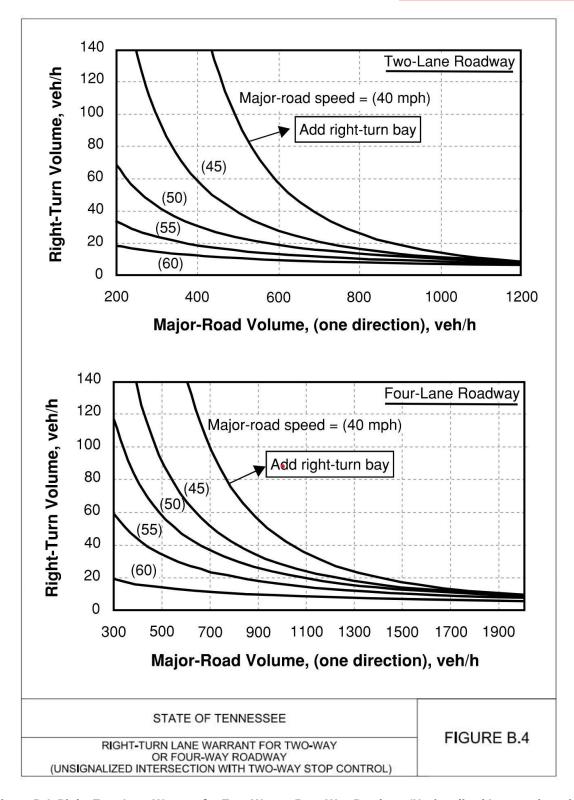


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Right-Turn Volume: 92 Major Road Volume: 1017

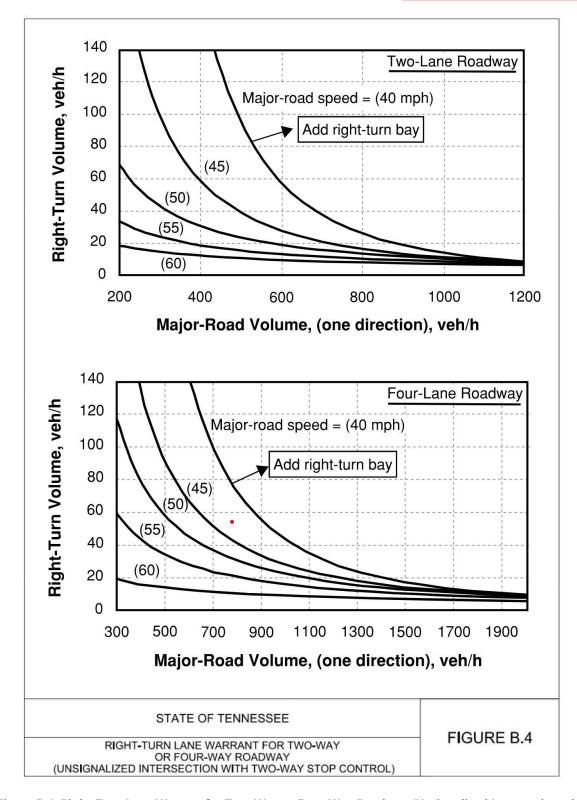


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Two-Way Stop Control)

Right-Turn Volume: 55 Major Road Volume: 830

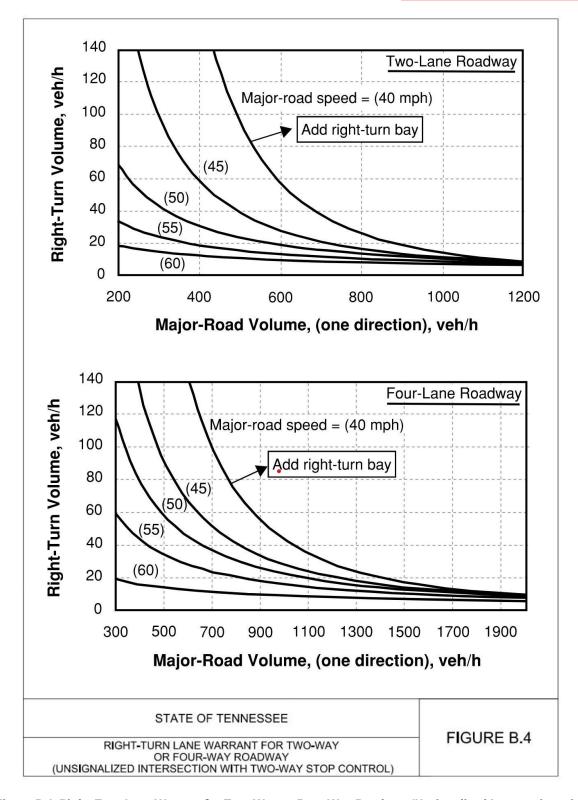


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Right-Turn Volume: 85 Major Road Volume: 980

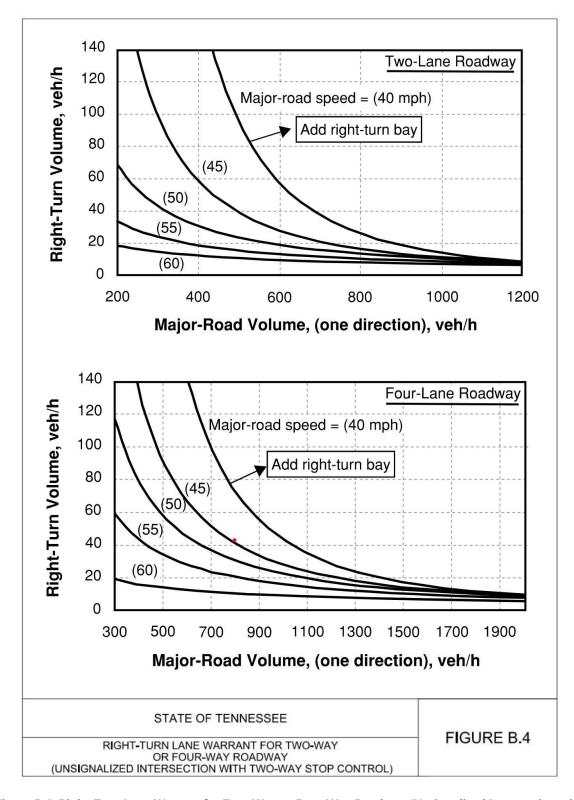


Figure B.4: Right-Turn Lane Warrant for Two-Way or Four-Way Roadway (Unsignalized Intersection with

Two-Way Stop Control)

Right-Turn Volume: 41 Major Road Volume: 803 APPENDIX E - SIGNAL WARRANT EVALUATIONS



TRAFFIC SIGNAL WARRANT ANALYSIS - VOLUME WARRANTS

| Intersection City or Count State | ty: Knox County Date of Count: | 2024 Existing | | to be adjusted for speeds or buty of week and month of year of Major Street 2 | | 1.00 | | | |
|--|---|----------------|--|--|---|---|--|--|--|
| Time Beginning 6:00 am 7:00 8:00 9:00 am 10:00 11:00 12:00 noon 1:00 2:00 3:00 pm 4:00 5:00 6:00 pm 7:00 8:00 | Major Street | | Warrant #1B (8 Hr Interruption) Percent of Warrant | Combination (Warrants 1A & 1B) Percent of Warrant Major Minor 0 0 211 8 234 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Warrant #2 (Four Hour Vols.) Warrant Percent of Volume Warrant | Warrant #3 (Peak Hour Vols.) Warrant Percent of Volume Warrant | | | |
| – V . N | - Where more than one minor approach exists use the higher approach volume Number of hours shown is the minimum meeting the MUTCD requirements. Additional hours outside of the count period may meet the MUTCD specified volume levels. Total Hours Meeting Warrant = 0. Warrant Met No Warrant Met No Total Hours Meeting Warrant = 0. Warrant Met No Warrant Met No Total Hours Meeting Warrant = 0. Warrant Met No Warrant Met No ***** Major Street volume is so low that no Minor Street warrant exists | | | | | | | | |
| Analysis Pre | pared by: CANNON AND CANNON, INC. William Ring, E.I. | Date: Time: | 04/25/24 14:29 | | cy Sullivan, P.E. ssee Transportation Assista | VC/R1 nce Program (TTAP) | | | |

TRAFFIC SIGNAL WARRANT ANALYSIS - VOLUME WARRANTS

| Intersection City or Cour State | | [| Date of Count: Day of Week of Count: | 2026 Background Average Weekday | | s to be adjusted for speeds or bu ay of week and month of year of Major Street 2 | | <u></u> <u>1.00</u> |
|---|--|--|---|--|--|--|---|---|
| Time Beginning 6:00 am 7:00 8:00 9:00 am 10:00 11:00 12:00 noon 1:00 2:00 3:00 pm 4:00 5:00 6:00 pm 7:00 8:00 | Actual Volume App #1 App #2 Total 0 0 0 0 828 311 1139 800 463 1263 0 | Adjusted Total Volum, 0 1139 1263 0 0 0 0 0 0 1598 1832 | Minor Street | Warrant #1A (8 Hr Min. Vol.) Percent of Warrant Major Minor 0 0 271 7 301 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Warrant #1B (8 Hr Interruption) Percent of Warrant Major Minor 0 0 181 13 200 8 0 254 11 291 17 0 0 0 0 0 0 | Combination (Warrants 1A & 1B) Percent of Warrant | Warrant #2 (Four Hour Vols.) Warrant Percent of Volume Warrant | Warrant #3 (Peak Hour Vols.) Warrant Percent of Warrant 0 ***** 90 8 8 80 5 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 1 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** 0 ***** |
| Note: , | No adjus ment made Where more than one mino approach volume Number of hours shown is t requirements. Additional h meet the MUTCD specified (include any information | r approach ex the minimum nours outside d volume leve | xists use the higher meeting the MUTCD of the count period mails. | Warranting Volumes 420 105 Total Hours Meeting Warrant = 0. Warrant Met No | Warranting Volumes 630 53 Total Hours Meeting Warrant = 0 Warrant Met No | Warranting Volumes 504 84 Total Hours Meeting | Warranting Volumes From MUTCD Fig. 4-8 Total Hours Meeting Warrant = 0 . Warrant Mel No ****** Major Street volumnor Street w | Warranting Volumes From MUTCD Fig. 4-6 Total Hours Meeting Warrant = 0 Warrant Met No |
| Analysis Pre | epared by: CANNON AND William Ring, E | | NC. | Date Time | | , , | rcy Sullivan, P.E. essee Transportation Assista | VC/R1 ance Program (TTAP) |

TRAFFIC SIGNAL WARRANT ANALYSIS - VOLUME WARRANTS

| Intersection : Concord Road at 2nd Drive City or County : Knox County State : Tennessee | Date of Count: 2026 Con Day of Week of Count: Average | | | o be adjusted for speeds or bu of week and month of year of Major Street 2 | | <u>.</u> <u>1.00</u> | | |
|--|---|---|---|--|---|---|--|--|
| Major Street | Minor Street Actual Adjusted Volume Total Volum, 0 0 0 150 150 | Warrant #1A (8 Hr Min. Vol.) Percent of Warrant Major Minor 0 0 363 143 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Warrant #1B (8 Hr Interruption) Percent of Warrant Major Minor 0 0 242 283 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Combination (Warrants 1A & 1B) Percent of Warrant Major Minor 0 0 0 302 179 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Warrant #2 (Four Hour Vols.) Warrant Percent of Volume Warrant | Warrant #3 (Peak Hour Vols.) Warrant Percent of Volume Warrant | | |
| Note: , No adjus ment made - Where more than one minor approach exists use the higher approach volume sequencements. Additional hours outside of the count period may meet the MUTCD specified volume levels. Warranting Volumes 420 105 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No Warranting Volumes 504 84 Total Hours Meeting Warrant = 2. Warrant Met No *********************************** | | | | | | | | |
| Analysis Prepared by: CANNON AND CANNON, INC. William Ring, E.I. Date: 05/20/24 Time: 16:17 Developed by: T. Darcy Sullivan, P.E. VC/R1 Distributed by: Tennessee Transportation Assistance Program (TTAP) | | | | | | | | |