

# Transportation Impact Study Cardinal Place Knoxville, Tennessee



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## **EXECUTIVE SUMMARY**

#### Preface:

Cardinal Place, LLC proposes a residential development between Brooks Avenue, Delrose Drive, and Riverside Road in East Knoxville, TN. The proposed development will include constructing 570 apartments and 80 multi-family attached townhouses on two parcels containing 30.15 +/- acres. The development is named and referenced in this study as "Cardinal Place". Cardinal Place proposes three entrances – one to Riverside Road to the east and two to the south at Delrose Drive and is anticipated to be fully built and occupied by 2027.

The primary purpose of this study is to determine and evaluate the potential impacts of the development on the adjacent transportation system. The study includes a review of the primary access roads, adjacent existing intersections, and proposed entrance intersections. This report is a Level 2 study established by Knoxville/Knox County Planning. Recommendations and mitigation measures are offered if transportation operations are projected to be below recognized engineering standards.

#### Study Results:

The significant findings of this study include the following:

- The Cardinal Place development, with 570 apartments and 80 multi-family attached townhouses, is estimated to generate 5,076 vehicle trips at full build-out and occupancy on an average weekday. Of these daily trips, 295 are estimated to occur during the AM peak hour and 432 in the PM peak hour in 2027.
- All studied existing and proposed entrance intersections are projected to operate with minimal vehicle delays and queues. The existing intersections included in the study are not expected to be substantially impacted by the proposed Cardinal Place development.
- The main entrance for the proposed development, the Proposed Southeast Entrance, is estimated to meet a warrant for a separate eastbound left-turn lane on Delrose Drive in the projected 2027 PM peak hour. The Proposed Southwest Entrance is projected to almost warrant a separate eastbound left-turn lane. The other proposed entrance, the East Entrance at Riverside Road, is not projected to warrant separate entering turn lanes.



#### **Recommendations**:

The following recommendations are offered based on the study analyses to minimize the impacts of the proposed development on the adjacent transportation system while attempting to achieve an acceptable traffic flow and improved safety. The recommendations marked with an asterisk indicate an existing transportation need and are not associated with the proposed development's projected impacts. More details regarding all the recommendations are discussed at the end of the report.

#### Brooks Avenue at Dandridge Avenue and Wilder Place:

- From a transportation engineering perspective, the Cardinal Place development will have minimal impact on this intersection. No specific recommendations are provided based on these findings.
- It is recommended, however, that the City of Knoxville seriously consider eliminating the northwestbound approach of Dandridge Avenue at the 5-legged intersection by rerouting this approach further to the east at Brooks Avenue. An initial recommendation to eliminate this approach would be to reroute it east of the corner gas station/market and intersect Brooks Avenue at a t-intersection.

#### **Delrose Drive at Riverside Drive**:

- From a transportation engineering perspective, the Cardinal Place development will have minimal impact on this intersection. No specific recommendations are provided based on these findings.
- It is recommended, however, that the City of Knoxville seriously consider rerouting the southeast approach of Riverside Drive to intersect Delrose Drive further to the east and away from the Vulcan Materials Driveway.

#### Delrose Drive and Brooks Avenue at Riverside Road:

• Due to the projected increased traffic volumes on Riverside Road, it is recommended that this roadway be widened to have a minimum width of 20 feet its entire length. This road was recently repaved and slightly widened in spots but still has sections less than 18 feet wide. Details regarding the particulars of this road widening should be discussed further with the City of Knoxville Engineering Department.



#### **Riverside Road at Proposed East Entrance:**

- It is recommended that a Stop Sign (R1-1) be installed and a 24" white stop bar be applied to the Proposed East Entrance approach at Riverside Road. The stop bar should be applied a minimum of 4 feet away from the edge of Riverside Road and placed at the desired stopping point that maximizes the sight distance.
- Intersection sight distance at the Proposed East Entrance at Riverside Road must not be impacted by existing vegetation or future landscaping or signage. The existing utility pole on the west side of Riverside Road near the proposed entrance location will need to be relocated. Based on a posted speed limit of 25 mph on Riverside Road, the required intersection sight distance (ISD) is 280 feet for exiting left-turning vehicles at the Proposed East Entrance and 240 feet for exiting right-turning vehicles. The site designer must verify that these distances will be available.

#### **Delrose Drive at Proposed Southwest Entrance**:

- Due to the projected volumes nearly meeting a warrant for an eastbound leftturn lane on Delrose Drive, serious consideration should be given to providing a separate entering lane into the development at this entrance. A separate leftturn lane on Delrose Drive at this proposed entrance is nearly warranted based on the projected 2027 PM peak hour traffic volumes and Knox County thresholds. If provided, the recommended lengths for this proposed left-turn lane were based on TDOT standards and include an approach taper of 225 feet, a bay taper of 90 feet (8:1), and a vehicle storage length of 75 feet lane.
- It is recommended that a Stop Sign (R1-1) be installed and a 24" white stop bar be applied to the Proposed Southwest Entrance approach at Delrose Drive. The stop bar should be applied a minimum of 4 feet away from the edge of Delrose Drive and placed at the desired stopping point that maximizes the sight distance.
- Intersection sight distance at the Proposed Southwest Entrance at Delrose Drive must not be impacted by existing vegetation or future landscaping or signage.
  Based on a posted speed limit of 35 mph on Delrose Drive, the required ISD is 390 feet for exiting left-turning vehicles at the Proposed Southwest Entrance and 335 feet for exiting right-turning vehicles. The site designer must verify that these distances will be available.



#### **Delrose Drive at Proposed Southeast Entrance**:

- A separate left-turn lane on Delrose Drive at this proposed main entrance is warranted based on the projected 2027 PM peak hour traffic volumes and Knox County thresholds. The recommended lengths for this proposed left-turn lane were based on TDOT standards and include an approach taper of 225 feet, a bay taper of 90 feet (8:1), and a vehicle storage length of 75 feet lane.
- It is recommended that a Stop Sign (R1-1) be installed and a 24" white stop bar be applied to the Proposed Southeast Entrance approach at Delrose Drive. The stop bar should be applied a minimum of 4 feet away from the edge of Delrose Drive and placed at the desired stopping point that maximizes the sight distance.
- Intersection sight distance at the Proposed Southeast Entrance at Delrose Drive must not be impacted by existing vegetation or future landscaping or signage. Based on a posted speed limit of 35 mph on Delrose Drive, the required ISD is 390 feet for exiting left-turning vehicles at the Proposed Southeast Entrance and 335 feet for exiting right-turning vehicles. The site designer must verify that these distances will be available.

#### Cardinal Place Internal Drives/Parking Lot Aisleways:

- A 15 mph Speed Limit Sign (R2-1) is recommended to be posted near the beginning of the development entrance driveways off Riverside Road and Delrose Drive.
- As shown in the report, Stop Signs (R1-1) and 24" white stop bars are recommended on the new internal drives and parking lot aisleways.
- Sight distance at the new internal intersections must not be impacted by new signage, parked cars, or future landscaping. With a speed limit of 15 mph in the development, the internal intersection sight distance is 170 feet. The site designer should ensure that internal sight distance lengths are met.
- With long and straight parking lot aisleways proposed internally, it is recommended that speed humps or tables be considered to reduce internal traffic speeds in the development. Alternatively, parking lot islands could be extended toward the aisleways. Extending the parking lot islands a few feet would narrow the aisleway widths and reduce the available driving surface. A narrower aisleway design would reduce driver comfort and internal vehicle speeds.
- All drainage grates and covers for the residential development must be pedestrian and bicycle-safe.
- Internal sidewalks are proposed throughout the development and include an internal perimeter walking trail. Concrete sidewalks should have appropriate



ADA-compliant ramps at intersection corners with detectable surfaces, and the internal sidewalks are recommended to be 5 feet minimum in width to meet the City of Knoxville regulations. White-painted crosswalks should be applied to the internal road pavement where pedestrians are expected to cross the parking aisleways. Internal crosswalks should include Pedestrian Warning (W11-2) signs with a downward arrow plaque (W16-7p) where appropriate. The internal crosswalks should have a white transverse marking as shown in TDOT Standard Drawing T-M-4.

- The internal sidewalk system for the proposed development should connect to the existing external sidewalk system on Brooks Avenue. It is recommended that this connection be constructed where the development property has a narrow strip of land up to Brooks Avenue. It is recommended that a crosswalk and pedestrian warning signs be applied on Brooks Avenue to connect to the sidewalk on the northern side of Brooks Avenue.
- All road and intersection elements should be designed to AASHTO and the City of Knoxville specifications and guidelines to ensure proper operation.



### **DESCRIPTION OF EXISTING CONDITIONS**

#### STUDY AREA:

The proposed location of this new residential development is shown on a map in Figure 1. This development will be located between Brooks Avenue to the north, Riverside Road to the east, Delrose Drive to the south, and Williams Creek Golf Course and Mt. Zion Baptist Church to the west in East Knoxville, TN. One of the three proposed entrances will tie to the east at Riverside Road and is referenced as the East Entrance in this report. The other two entrances will tie into Delrose Drive to the south. These two entrances in this report are referred to as the Southwest Entrance and the Southeast Entrance. The proposed Southeast Entrance will be the main access point for the development.

The development will be constructed from two existing parcels that, when combined, include 30.15 +/- acres. The smaller of the two existing parcels will allow access to Riverside Road to the east. As requested, transportation impacts associated with the development were analyzed at the proposed entrances, where the development will have road access to and from external destinations. The scope of work also requested analyses of two nearby intersections, Brooks Avenue at Riverside Road and Delrose Drive at Riverside Road, and two intersections further to the west – Brooks Avenue at Dandridge Avenue and Wilder Place and Delrose Drive at Riverside Drive.

It should be noted that there are two roadways with nearly the same name in the surrounding area: Riverside Road and Riverside Drive. Riverside Road is just east of the development site and runs between Brooks Avenue and Delrose Drive in a north-south configuration. Riverside Drive is further south of the development site, traverses in an east-west configuration, and does not run next to the site.

The proposed development property is in a well-established urban area that has a mix of residential, industrial, and recreational uses. The surrounding area has no particular named residential developments or subdivisions and is generally referred to as "East Knoxville". There are several stretches of houses along Brooks Avenue, Delrose Drive, and Riverside Road in the surrounding area, but other than a smattering of condominiums, all the housing is single-family detached. Nearby industrial properties include Vulcan Materials, a quarry and producer of construction aggregates, and Meridian Waste, a private construction and demolition landfill. These industries attract and make use of heavy trucks in their transportation operations. The





Williams Creek Golf Course is adjacent to the development site to the southwest. This private golf course includes 18 holes, a clubhouse, and practice facilities on 98 acres. Mt. Zion Baptist Church is adjacent to the development site to the northwest.

In addition to these land uses, Sarah Moore Greene Magnet Academy is located nearby. It is situated just north of the development site and adjacent to the intersection of Brooks Avenue at Riverside Road. This school is named after a local civil rights leader and

educator and provides elementary school education for nearly 600 students.

The Cardinal Place development property is currently 100% forested and unoccupied. According to KGIS historical aerial imaging, the property was used for agricultural purposes around 60 years ago and had a residence on its southwest corner. However, vegetation and trees have slowly overtaken the property for the past 30 years. The topography for the development property is defined by a high point at Riverside Road on its northeastern edge, with the grade of the property falling to the southwest towards the golf course. On an adjacent small parcel to the south, a historic cemetery is on the north side of Delrose Drive. This cemetery historian, the cemetery was in use from 1890 – 1967.

Major road access to this area of Knoxville is provided by the east- and west-oriented Brooks Avenue and Delrose Drive, which transitions to Riverside Drive further to the west and provides access to James White Parkway. This parkway runs just east of downtown Knoxville and provides convenient access to nearby Interstate 40 and 275.





Figure 1 Location Map



#### • EXISTING ROADWAYS:

Table 1 lists the characteristics of the existing primary roadways near the development property and included in the study:

#### TABLE 1 STUDY CORRIDOR CHARACTERISTICS

NAME	CLASSIFICATION <sup>1</sup>	SPEED LIMIT	LANES	ROAD WIDTH <sup>2</sup>	TRANSIT <sup>3</sup>	PEDESTRIAN FACILITIES	BICYCLE FACILITIES
Brooks Avenue	Minor Arterial	30 mph	2 lanes	21 - 26 feet	KAT Route 32	5' sidewalk on north side of roadway	No bike lanes
Dandridge Avenue	Minor Arterial / Minor Collector	30 mph	2 lanes	20 - 26 feet	KAT Route 32	5' sidewalk on south side of roadway, west of Wilder Place	No bike lanes
Wilder Place	Minor Collector	25 mph	2 lanes	30 feet	No Transit	5' sidewalk on west side of roadway, north of Brooks Avenue	No bike lanes
Delrose Drive	Major Collector	35 mph	2 lanes	22 - 23 feet	No Transit	No sidewalks along roadway	No bike lanes
Riverside Road	Local Street	25 mph	2 lanes	16 - 19 feet	No Transit	No sidewalks along roadway	No bike lanes
Riverside Drive	Minor Arterial / Minor Collector	30 mph	2 lanes	25 feet	No Transit	No sidewalks along roadway	No bike lanes

<sup>1</sup> 2018 Major Road Plan by Knoxville/Knox County Planning

<sup>2</sup> From edges of pavement near project site

<sup>3</sup> According to Knoxville Area Transit System Map

**Brooks Avenue** is a 2-lane Minor Arterial that traverses southwest-northeast between Wilder Place and Dandridge Avenue to the southwest and Boyds Bridge Pike to the northeast, a total distance of 1.5 miles. The speed limit on Brooks Avenue is 30 mph, and the road has a 5-foot concrete sidewalk on its northern side for its entire length. On its southwestern end, the sidewalk on Brooks Avenue continues further west on Dandridge Avenue and to the north on Wilder Place. At its northeast end, the sidewalk on Brooks Avenue terminates at its intersection with Boyd Bridge Pike and does not continue further. The proposed development site has a small strip of land on its northern edge that borders Brooks Avenue, but the sidewalk is located on the opposite (north) side.



The pavement width of Brooks Avenue fluctuates between 26 feet on its southwestern end and narrows down to 21 feet closer to the proposed development site. A double yellow centerline is provided on the pavement its entire length with white edge lines on some sections of the road. Knoxville Area Transit (KAT) provides several bus stops along Brooks Avenue on Route 32, "Dandridge Avenue". The closest bus stop to the development property is approximately ¼ mile away. It is located on the south side of Brooks Avenue at Border Street near Sarah Moore Greene Magnet Academy.

its southwestern beginning, At Brooks Avenue comprises the east approach at an uncommon 5-legged, unsignalized This intersection is quite intersection. complex from an operations standpoint, with all five legs operating under stop control. In addition to the five street approaches, a Marathon gas station with a Stop N Go Market & Deli is located on the southeastern corner, with large expanses of pavement provided along the edges of Brooks Avenue and An entrance to the Dandridge Avenue.



Lennon Seney United Methodist Church is located just south of the intersection on Wilder Place.

All other properties along Brooks Avenue are residential besides the gas station/market, Sarah Moore Greene Magnet Academy, and Mt. Zion Baptist Church.

**Dandridge Avenue** is a 2-lane Minor Arterial and Minor Collector that traverses in a generally west-east direction between the signalized intersection of E Summit Hill Drive / Martin Luther King Jr Avenue / E Hill Avenue from the west to Riverside Drive to the east, with a total length of 1.4 miles. The road is classified as a Minor Arterial between E Summit Hill Drive / Martin Luther King Jr Avenue / E Hill Avenue and Brooks Avenue / Wilder Place on its western section. It is classified as a Minor Collector between Brooks Avenue / Wilder Place and Riverside Drive on its southeastern section. The speed limit on Dandridge Avenue is 30 mph, with a 5-foot concrete sidewalk on its southern side for its entire western section. On its western end, the sidewalk on Dandridge Avenue continues on E Summit Hill Drive / Martin Luther King Jr Avenue / E Hill Avenue. On its eastern end, the sidewalk on Dandridge Avenue continues on Wilder Place to the north and Brooks Avenue further east but does not continue on its



southeastern section.

Dandridge Avenue comprises the west and southeast approaches at the 5-legged unsignalized intersection with Brooks Avenue and Wilder Place. A white crosswalk on the west approach of Dandridge Avenue is provided at the intersection. The west approach of Dandridge Avenue is 26 feet in width, and the southeast approach has a width of 20 feet. Double yellow centerlines are provided on the pavement of Dandridge Avenue on its entire length. On its southeastern end, Dandridge Avenue intersects Riverside Drive at an acute angle and is controlled by a Stop Sign (R1-1). KAT provides several bus stops along Dandridge Avenue west of the 5-legged intersection on Route 32, "Dandridge Avenue", but none to the southeast.

**Wilder Place** is a 2-lane Minor Collector that traverses in a south-north direction between Riverside Drive from the south to Harold Avenue to the north, with a total length of 0.6 miles. The intersection of Wilder Place at Riverside Drive is an unsignalized t-intersection with Wilder Place operating under stop conditions. Wilder Place, 1,200 feet north of the 5-legged intersection, transitions to McConnell Street, eventually intersecting with Martin Luther King Jr Avenue further north. The speed limit on Wilder Place is 25 mph, and it has a 5-foot concrete sidewalk on its western side to the north of the 5-legged intersection. A short 325' section of sidewalk is on Wilder Place south of the 5-legged intersection but ends abruptly just past the Lennon Seney United Methodist Church property. An unconnected 650' section of sidewalk is also provided on the east side of Wilder Place, 800 feet further to the south.

Wilder Place comprises the south and north approaches at the 5-legged unsignalized intersection with Brooks Avenue and Dandridge Avenue. A white crosswalk on the north approach of Wilder Place is provided at the intersection. Both approaches of Wilder Place are 30 feet in width and have double yellow centerlines on the pavement. KAT does not provide bus transit on Wilder Place other than a bus stop just slightly east of the 5-legged intersection and is on Route 32, "Dandridge Avenue".

**Delrose Drive** is a 2-lane Major Collector that traverses in a southwest-northeast direction between Riverside Drive from the southwest end to Boyds Bridge Pike to the northeast, totaling 1.4 miles. The speed limit on Delrose Drive is 35 mph, and it does not have sidewalks. At its southwestern beginning, Delrose Drive transitions from the west approach of Riverside Drive at a y-intersection with Riverside Drive's southeast approach combined with a driveway entrance for Vulcan Materials to the south. The pavement width of Delrose Drive is relatively stable along its length and is between 22 and 23 feet. A double yellow centerline and white edge pavement



lines are provided on the pavement on the entire length of Delrose Drive. KAT does not provide bus service on Delrose Drive. Delrose Drive intersects Riverside Road just east of the proposed development site at an unsignalized t-intersection.

**Riverside Road** is a 2-lane Local Street that traverses in a southeast-northwest direction between Delrose Drive from the southeast to Brooks Avenue to the northwest, totaling 1,500 feet. The speed limit on Riverside Road is 25 mph, and it does not have sidewalks. On its southeastern end, Riverside Road intersects Delrose Drive at a crest vertical curve with Riverside Road controlled by a Stop Sign (R1-1). Riverside Road to the northwest intersects Brooks Avenue at an unsignalized tintersection and is controlled by a Stop Sign (R1-1).



Riverside Road has recently been repaved and slightly widened. The pavement width was measured at several points between 16 to 19 feet in width. No pavement markings are applied to the pavement on Riverside Road. KAT does not provide bus service on Riverside Road.

**Riverside Drive** is a 2-lane Minor Arterial and Minor Collector that traverses in a generally west-east direction between James White Parkway from the west and ends on a University of Tennessee (UT) property near the Tennessee River to the east, with a total length of 3.2 miles. The road is classified as a Minor Arterial between James White Parkway and Delrose Drive. Riverside Drive is classified as a Minor Collector between Delrose Drive and the UT property. The speed limit on Riverside Drive is 30 mph, and no sidewalks are provided.



Vulcan Materials Driveway

The intersection of Riverside Drive at Delrose Drive is uncommon and y-shaped, with the main



thoroughfare consisting of Riverside Drive to the west and Delrose Drive to the east-northeast. At the intersection, the roadway approach to the southeast is designated as Riverside Drive, and directly to the south a driveway entrance to Vulcan Materials ties into the intersection. Only one Stop Sign (R1-1) is provided at the intersection, with Delrose Drive and the west approach of Riverside Drive operating freely.

Figure 2 shows the existing lane configurations of the intersections examined and included in the study and the traffic count locations in the study area. The pages following Figure 2 give a further overview of the site study area with photographs.





## **PHOTO EXHIBITS**



**Proposed Development Site** 

















**Brooks Avenue at Riverside Road** 







Transportation Impact Study Cardinal Place



A]A



Delrose Drive at Riverside Drive







#### • EXISTING TRANSPORTATION VOLUMES PER MODE:

Two annual vehicular traffic count locations are in the study area, and the Tennessee Department of Transportation (TDOT) conducts both these counts. The count location data is the following and can be viewed with further details in Appendix A:

- Existing vehicular roadway traffic:
  - TDOT reported an Average Daily Traffic (ADT) on Brooks Avenue, east of Wilder Place and southwest of the development site, at 2,437 vehicles per day in 2023. From 2013 to 2023, this count station has indicated a 0.6% average annual traffic growth rate.
  - TDOT reported an ADT on Delrose Drive, east of Riverside Drive and southwest of the development site, at 3,711 vehicles per day in 2023. From 2013 to 2023, this count station has indicated a 3.1% average annual traffic growth rate.
- Existing bicycle and pedestrian volumes:

The average daily pedestrian and bicycle traffic along the roads in the study area is unknown. However, with the limited number of sidewalk locations and lack of bike lanes near the proposed development site, the adjacent roadway sections to the site were assumed to have minimal pedestrian and bicyclist activity.

During the traffic counts for this project, only a handful of bicyclists were observed, with all of them (except for one on Riverside Drive) observed at the 5-legged intersection. Most of the studied intersections saw zero to minimal amounts of pedestrians. Unsurprisingly, the most active intersection regarding pedestrian activity was the 5legged intersection. Most of this pedestrian activity was associated with the adjacent gas station/market, with a few associated with the adjacent KAT bus stop. During the 6-hour traffic count for this study, 26 pedestrians at the 5-legged intersection were observed using the crosswalks on the north approach of Wilder Place and the west approach of Dandridge Avenue. An additional 29 pedestrians were observed at the intersection outside of the crosswalks, primarily on the south and southeast approaches of Wilder Place and Dandridge Avenue, and were patrons of the adjacent gas station/market.

At the other three studied intersections, minimal pedestrian activity was observed. The intersection of Brooks Avenue at Riverside Road had two pedestrian trips on Riverside



Road to and from the adjacent bus stops on Brooks Avenue; the other pedestrians were adults and several schoolchildren from Sarah Moore Greene Magnet Academy. These pedestrians were observed on the sidewalk on the north side of Brooks Avenue at Riverside Road. At Delrose Drive at Riverside Road, one pedestrian was observed crossing Delrose Drive from Marble Hill Boulevard onto Riverside Road and walking the entire length to access the KAT bus system on Brooks Avenue. No pedestrians were observed at the intersection of Delrose Drive at Riverside Drive and the Vulcan Materials Driveway.

An online website, strava.com, provides "heat" maps detailing routes taken by pedestrians, joggers, and bicyclists. The provided heat maps show the last two years of data, are updated monthly, and are gathered from individuals allowing their smart devices to track and compile their routes (millions of users). The activities in the maps are shown on the roads with color intensities with darker colors signifying higher activity. The Strava heat maps show some pedestrian and bicycle activity in the surrounding Overall, higher bicyclist travel area. pedestrian travel is shown than occurring on the nearby streets. Surprisingly, a reasonably high amount of bicyclist activity is shown along Riverside Drive. With limited sidewalk facilities and no bike lanes in the adjacent area, the map data shows that pedestrian and bicyclist activity is occurring regardless of the lack of facilities.









#### PEDESTRIAN AND BICYCLE FACILITIES:



The only sidewalk near the development site is on Brooks Avenue. This sidewalk is 5 feet wide and runs the entire road length on its north side. Sidewalks are not provided on the south side. The City of Knoxville produced a report in June 2020 titled Sidewalk Study. In this study, the report identified the existing sidewalk system in the City of Knoxville, areas of need for sidewalks, and а framework for future sidewalk infrastructure. This study provided maps broken down into City Council District areas showing the existing and the proposed recommended

sidewalks. The proposed development site is in City Council District 6, and a map of this area from this study is included in the adjacent image. Brooks Avenue is shown with an existing sidewalk on the north side and a recommended sidewalk on the south side between the 5-legged intersection and Boyds Bridge Pike. In the study, however, this proposed recommended sidewalk is listed fairly low in their rankings. It was reported in the study with an estimated cost of nearly \$7 million for 7,748 feet of new sidewalk on the south side of Brooks Avenue.

Delrose Drive and Brooks Avenue are shown Knoxville Transportation Planning on Organization (TPO) mapping for bicycle travel as a "Comfortable Route" south and north of the proposed development site. These roads do not have painted white bicycle pavement markings but do have signage warning motorists of potential bicycle activity. A "Comfortable Route" is defined as a route "based on low to medium traffic speeds and volumes along with other criteria. Warning signage is posted on these roads and states, "Share the Road".





#### WALK SCORE:

A private company offers a website at <u>walkscore.com</u> that grades and gives scores to locations within the United States based on "walkability", "bikeability", and transit availability based on a patented system. According to the website, the numerical values assigned for the Walk Score and the Bike Score are based on the distance to the closest amenity in various relevant categories (businesses, schools, parks, etc.) and are graded from 0 to 100.

The project site location is graded with a Walk Score of 1 at the development property address. This Walk



Score indicates that almost all errands currently require a vehicle for travel to and from the development property. The Walk Score is graded very low due to the lack of sidewalks adjacent to the site and the lack of nearby amenities. The site is given a Bike Score of 11, meaning there is minimal bike infrastructure. The site is given a Transit Score of 26 since a few public transportation options are available.

#### TRANSIT SERVICES:

The City of Knoxville has a network of public transit opportunities offered by Knoxville Area Transit (KAT). Bus service is available near the development site. The closest bus stop to the development site is approximately <sup>1</sup>/<sub>4</sub> mile to the north. It is on Route 32, "Dandridge Avenue", near the intersection of Brooks Avenue at Border Street close to Sarah Moore Greene Magnet Academy. KAT made several changes and



improvements to their routes that began on August 26<sup>th</sup>, 2024. This recent change removed some bus stops on Brooks Avenue and its travel along Brooks Avenue, where the development property has a narrow access point on its northern edge. Before this change, this route traveled on Brooks Avenue between Biddle Street and Border Street, but now, it skips this section and travels this east-west section a bit further to the north on Boyds Bridge Pike. This route has established bus service every 60 minutes. It operates on weekdays and weekends; the route map



is also included in Appendix B. Other transit services in the area include the East Tennessee Human Resource Agency (ETHRA) and the Community Action Committee (CAC), which provides transportation services when requested.

Overall, due to the proximity of this public transportation, this study assumed that 5% of trips would use this alternative travel means and subsequently would reduce vehicle trips by 5% to and from the proposed development. This small percentage would also account for a minor amount of potential travel by future residents via walking or biking.

#### • <u>CRASH DATA</u>:

For this project, TDOT (and the City of Knoxville) provided access to the AASHTOWare Safety online platform. This AASHTO (American Association of State Highway and Transportation Officials) platform is a component of several offerings that include the compilation of crash data for local state DOTs to use in safety analyses. TDOT provides vehicle crash data to this system and is an extension of its existing E-TRIMS (Enhanced Tennessee Roadway Information Management System) database. The crash data in the E-TRIMS system is from the statewide TITAN (Tennessee Integrated Traffic Analysis Network) database. The TITAN database includes all reportable vehicle crash data from Tennessee law enforcement agencies.

In this project's study area, 30 crashes occurred between January 1<sup>st</sup>, 2021, and September 30<sup>th</sup>, 2024. At the studied intersections, ten occurred in and around the intersection of Brooks Avenue at Dandridge Avenue and Wilder Place, zero at the intersection of Brooks Avenue at Riverside Road, two at the intersection of Delrose Drive at Riverside Road, and four at the intersection of Delrose Drive at Riverside Roat at Riverside Road, The other 14 occurred at



AASHTOWare Safety Platform

other road locations in the study area. A summary of the dates, manner of collision, light conditions, weather conditions, and type of crash are shown in Figure 3. The most common manner of collision was "No Collision with Vehicle", which means that the crash involved a single vehicle colliding with other objects, that included utility poles, mailboxes, ditches, and a wall. Most of the 30 crashes occurred during daylight and with clear weather conditions.







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FIGURE 3

Cardinal Place

Vehicle Crash Data in Study Area

NORTH

Most crashes involved "Property Damage Only" and did not include injuries. No fatalities were recorded, but several resulted in suspected minor injuries or possible injuries. The breakdown of the crashes at the studied intersections is the following:

	MANNER OF		TYPE OF	
INTERSECTION	FIRST COLLISION	#	CRASH	#
	Angle	4	Property Damage Only	6
Brooks Avenue at Dandridge	No Collision with Vehicle	2	Suspected Minor Injury	3
Avenue and Wilder Place	Rear End	2	Possible Injury	1
	Head On	1		
	Sideswipe - Same Direction	1		
Brooks Avenue at	None	-	None	-
Riverside Road				
Delrose Drive at	Angle	1	Property Damage Only	1
<b>Riverside Road</b>	No Collision with Vehicle	1	Possible Injury	1
Delrose Drive at	No Collision with Vehicle	3	Property Damage Only	2
<b>Riverside Drive</b>	Angle	1	Suspected Minor Injury	1
		-	Possible Injury	1

# TABLE 2CRASH DATA FOR STUDIED INTERSECTIONS

From AASHTOWare Safety online platform

A review of the narratives for the 30 crashes indicated that the intersection of Brooks Avenue at Dandridge Avenue and Wilder Place experienced several crashes that could be attributed to the incorrect or dual assumption of the right of way when motorists proceeded into the intersection. These crashes could be an aspect of the complicated and unusual configuration of the intersection having five approaches. The objects struck at this intersection included utility poles, and the rearend crashes involved stopped vehicles being struck from behind.

The other intersections also experienced crashes where motorists struck utility poles, a vehicle that ran off the road due to excessive speed, and one motorist who overcorrected after avoiding an oncoming vehicle that crossed into their lane.



## **PROJECT DESCRIPTION**

#### LOCATION AND SITE PLAN:

The proposed plan layout with 570 apartments and 80 multi-family attached townhouses on 30.15 +/- acres is designed by Heyoh Design + Development and is shown in Figure 4. The proposed property is jigsaw-shaped and has access to Brooks Avenue, Riverside Road, and Delrose Drive.

As shown in the figure, three entrances will be constructed for the development, with one at Riverside Road to the east and two to the south at Delrose Drive. The main entrance will be the Proposed Southeast Entrance at Delrose Drive. The Proposed Southwest Entrance will be constructed 715 feet west of this main entrance. The Proposed Southeast (main) Entrance will be built with a 23-foot wide landscaped median in the center separating the entering and exiting traffic. The Proposed Southwest Entrance will be constructed with an entering and exiting lane and no median. The Proposed East Entrance will tie into Riverside Road just north of the existing house at 1521 Riverside Road with a single exiting and entering lane. The Proposed East Entrance will intersect Riverside Road approximately 575 feet to the south of the intersection with Brooks Avenue.

As shown in the site layout, an existing property to the south with a single-family detached house at 2819 Delrose Drive will remain and is owned by a private owner. At the southwest corner of this private property, a small separate parcel contains the Historic Williams-Masterson Cemetery. The current plan in Figure 4 shows six buildings, each four stories in height, containing 570 apartment units. Four buildings will contain 75 apartment units, and two will have 135 units. The townhouses will be grouped into 10 clusters, each containing between 6 and 13 units, for a total of 80 townhouses.

In addition to the housing units, several on-site amenities are proposed for the future residents, including a community building and swimming pool, shaded outdoor area, sand volleyball court, playground, dog park, natural park, pickleball courts, public art, community gardens, and a 1mile perimeter walking path. The development will also include signage about the historic adjacent cemetery. None of the townhouses will have separate driveways or garages.

A total of 981 parking spaces will be provided in several internal parking lots and will include the appropriate number of ADA-accessible parking spaces. This number will provide each townhouse with a minimum of 2.25 parking spots and 1.45 spaces for each apartment. Concrete



sidewalks are proposed internally for this development along the buildings and parking areas. The site plan also shows a sidewalk between the main campus and Brooks Avenue to the north. Two hundred bicycle parking spaces will also be provided throughout the development. Stormwater detention is proposed along Delrose Drive between the roadway and the proposed housing units and will provide additional separation and buffer.

The schedule for the completion of this new residential development depends on economic factors and construction timelines. This project is also contingent on permitting, design, and other regulatory approvals. Overall, the local real estate market for new housing remains quite competitive. This study assumed that the total construction build-out of the development and full occupancy would occur within the next three years (2027) to provide a conservative outlook.







#### PROPOSED USES AND ZONING REQUIREMENTS:

The two parcels comprising the Cardinal Place development property are in the City of Knoxville, and the largest, main parcel, was requested to be rezoned. The Knoxville/Knox County Planning Commission approved the rezoning, and the Knoxville City Council gave final approval on March 19<sup>th</sup>, 2024. This parcel's previous zoning was Single-Family Residential Neighborhood (RN-1) and was approved for a General Residential Neighborhood (RN-4) zoning. According to the City of Knoxville's Zoning Code, the "RN-4 General Residential Neighborhood Zoning District is intended to accommodate mixed medium density residential development within the City of Knoxville. Single-family, two-family, and townhouse dwellings are permitted with low-rise multi-family dwellings and new development forms such as pocket neighborhoods allowed by review and in some cases with special use approval." The other, smaller, flag-shaped parcel between the main parcel and Riverside Road is zoned as Single-Family Residential Neighborhood (RN-1) and was not and is not requested to be changed.

Additionally, a small portion of the development property to the southeast is overlaid with a Hillside Protection (HP) area. The most recently published online KGIS zoning map is provided in Appendix C. The existing adjacent surrounding zoning and land uses are the following:

- To the north, the development property is bound by Brooks Avenue and single-family detached houses along Brooks Avenue zoned as Single-Family Residential Neighborhood (RN-1). A handful of the parcels to the north are undeveloped and unoccupied. These properties to the north have road access to Brooks Avenue and Colby Way, a private drive south and off Brooks Avenue.
- To the east, the development property is bound by Riverside Road and single-family detached houses along Riverside Road that are zoned as Single-Family Residential Neighborhood (RN-1). These houses have road access to Riverside Road. One property to the southeast and adjacent to the development property is zoned as Neighborhood Commercial (C-N). This property has two commercial buildings with road access to the south to Delrose Drive. According to Google Maps, an auto repair business occupies one of these buildings.
- The development property is bound by Delrose Drive to the south and abuts two parcels on the same side of Delrose Drive. The largest abutting property has a single-family detached house and is zoned Single-Family Residential Neighborhood (RN-1). This house will remain and will be surrounded by the proposed development. The smaller abutting property is adjacent, right next to Delrose Drive, and is zoned Parks and Open



Space (OS). The Historic Williams-Masterson Cemetery is located on this parcel and was used from 1890 – 1967. Across the street on the south side, all the properties are zoned as Single-Family Residential Neighborhood (RN-1) and are occupied by single-family detached houses and a small church.

• Williams Creek Golf Course is zoned as Parks and Open Space (OS) and to the southwest of the development site. The primary road access to this golf course is provided further to the west off Dandridge Avenue. To the northwest, the property is zoned as Single-Family Residential Neighborhood (RN-1) and is owned and occupied by Mt. Zion Baptist Church. The sanctuary and main parking lot are located just south of Brooks Avenue, and the church also has auxiliary parking across Brooks Avenue to the north.





#### On-Site Circulation:

The driveway and internal parking lot aisleways will be approximately 6,055 feet (1.15 miles) in length. They will be designed and constructed according to the specifications of the City of Knoxville, TN. The internal drives and aisleways will be asphalt-paved and include concrete curbs. The lane widths will be 13 feet each for a 26-foot pavement driveway and parking lot aisle width, except the roadway for the Proposed Southwest Entrance, which will be 20 feet wide. A few parking lot aisleways will be 30 feet in width. Concrete sidewalks are being proposed internally along the parking lot aisleways and adjacent to the buildings. The driveway entrance and internal aisleways will be private and maintained by the development owner in the future.


#### • <u>SERVICE AND DELIVERY VEHICLE ACCESS AND CIRCULATION:</u>

Besides residential passenger vehicles, the development's entrances will also provide access to service, delivery, maintenance, and fire protection/rescue vehicles. None of these other vehicle types will impact roadway operations other than when they occasionally enter and exit the development. Trash collection areas will be designed on-site for the residents, and City trash collection trucks are expected to enter and exit this development. The new entrances and parking lot aisleways will be designed and constructed to the City of Knoxville specifications and are expected to be adequate for fire protection and rescue vehicles. The development's internal drives are anticipated to accommodate the larger vehicle types and residents' standard passenger vehicles.



## ANALYSIS OF EXISTING AND PROJECTED CONDITIONS

#### EXISTING TRAFFIC CONDITIONS:

This study conducted 6-hour traffic counts on Thursday, October  $3^{rd}$ , 2024, at four unsignalized intersections as requested in the scope of work. Manual traffic counts were conducted to identify and tabulate the morning and afternoon peak period volumes and the travel directions near and around the proposed development site. All the intersections had an AM and PM peak hour at 7:15 – 8:15 a.m. and 5:00 – 6:00 p.m., except for the intersection of Delrose Drive at Riverside Drive, which had a slightly earlier PM peak hour of 4:45 – 5:45 p.m. The manual tabulated traffic counts can be reviewed in Figures 5a and 5b and Appendix D. Some observations at the intersections include the following:

Brooks Avenue at Dandridge Avenue and Wilder Place:

- As described earlier, due to the adjacent neighborhood gas station/market, many pedestrians and a handful of bicyclists were observed at this intersection. In addition to the market, the adjacent KAT bus stop in the northeast corner of the intersection attracted a couple of pedestrians.
- Vehicles observed at this intersection, in addition to passenger cars, included school buses, KAT buses, dump trucks, and trash collection trucks. In the afternoon, a public school bus stopped in the northwest corner of the intersection and let out several schoolage children who used the crosswalks on Dandridge Avenue and Wilder Place.
- Several motorists were observed using the generously provided gas station/market parking lot area to travel between Brooks Avenue and the southeast approach of Dandridge Avenue. For motorists wanting to turn left from westbound Brooks Avenue to the southeast approach of Dandridge Avenue (and vice versa), cutting through the parking area is much more manageable than turning sharply to navigate the acute angle of these intersecting streets. Likewise, several turns occurred to and from the gas station/market and directly in and from the intersection because of the openness of the parking area. Note: these turning volumes are not included in the figures.
- With the unusual nature of the 5-legged intersection, many motorists were observed hesitating to proceed due to confusion about which motorist had the right-of-way. Also, due to the unusual layout, several vehicles were observed traveling near each other in the center of the intersection.
- The acute angles of some of the approaches at the intersection presented challenges for several motorists attempting to turn left or right to and from these approaches.



Brooks Avenue at Riverside Road:

- The heaviest traffic flows near the intersection occurred during the student arrival and departure times of the adjacent Sarah Moore Greene Magnet Academy. During these periods, several vehicles were observed using Riverside Road when entering and leaving the school. The observed school traffic peaks occurred from 7:15 8:15 a.m. and 2:15 3:15 p.m. In the afternoon, parents were observed queueing on the school property beginning at 2:00 p.m. For the most part, all school vehicle queues were contained on the school property and off Brooks Avenue.
- A few school-age children and several adults were observed walking on the sidewalk on the north side of Brooks Avenue. One individual was observed walking via Riverside Road to and from the KAT bus stops on Brooks Avenue.

Delrose Drive at Riverside Road:

- The vehicles observed at this intersection included passenger cars, school buses, and many dump trucks, assumed to be associated with the nearby construction debris landfill off Delrose Drive further to the east. The largest vehicle observed on Riverside Road was a public school bus.
- Only one individual was observed at this intersection. This person walked across Delrose Drive from Marble Hill Boulevard, continued along Riverside Road to Brooks Avenue, and caught a KAT bus. This same individual returned from the KAT bus stop on Brooks Avenue later in the day.

Delrose Drive at Riverside Drive:

- Many dump trucks were observed entering and leaving Vulcan Materials via the private driveway that ties into the intersection of Delrose Drive and Riverside Drive. Nearly all these dump trucks were observed leaving and returning from the west on Riverside Drive.
- Only one bicyclist was observed at this intersection, and no pedestrians were observed.
  The bicyclist traveled eastbound on Riverside Drive and continued on Riverside Drive at the intersection with Delrose Drive.
- The acute angle at which Riverside Drive from the southeast intersects at Delrose Drive, combined with the available view when approaching the intersection, allowed some determined motorists to continue driving west on Riverside Drive without stopping during times of lower volumes.







Capacity analyses were undertaken to determine the Level of Service (LOS) for the existing 2024 intersection traffic volumes shown in Figures 5a and 5b. The capacity analyses were calculated following the Highway Capacity Manual (HCM) methods and utilizing Synchro Traffic Software (Version 12).

### <u>Methodology</u>:

LOS is a qualitative measurement developed by the transportation profession to express how well an intersection or roadway performs based on a driver's perception. LOS designations include LOS A through LOS F. The designation of LOS A signifies a roadway or intersection operating at best, while LOS F signifies road operations at worst. This grading system provides a reliable, straightforward means to communicate road operations to the public. The HCM lists the level of service criteria for unsignalized intersections and signalized intersections.



LOS is defined by delay per vehicle (seconds), and roadway facilities are also characterized by the volume-to-capacity ratio (v/c). LOS designations, which are based on delay, are reported differently for unsignalized and signalized intersections. For example, a delay of 20 seconds at an unsignalized intersection would indicate LOS C, representing the additional delay a motorist would experience traveling through the intersection. Also, for example, a v/c ratio of 0.75 for an approach at an unsignalized intersection would indicate that it is operating at 75% of its available capacity. This difference is primarily due to motorists' different expectations between the two road facilities. Generally, for most instances, the LOS D / LOS E boundary is considered the upper limit of acceptable delay during peak periods in urban and suburban areas.

For unsignalized intersections, LOS is measured in terms of delay (in seconds). This measure attempts to quantify delay, including travel time, driver discomfort, and fuel consumption. For unsignalized intersections, the analysis assumes that the mainline thru and right-turn traffic does not stop and is not affected by the traffic on the minor side streets. Thus, the LOS for a two-way stop (or yield) controlled intersection is defined by



STOP

the delay for each minor approach and major street left-turn movements. Table 3 lists the level of service criteria for unsignalized intersections. The analysis results of unsignalized intersections using the HCM methodologies are conservative due to the more significant vehicle gap parameters used. More often, in normal road conditions, drivers are more willing to accept smaller gaps in traffic than what is modeled using the HCM methodology. The unsignalized intersection methodology also does not account for more significant gaps sometimes produced by nearby upstream and downstream signalized intersections. For unsignalized intersections, in most instances, the upper limit of acceptable delay during peak hours is the LOS D/E boundary at 35 seconds.

#### TABLE 3

LEVEL OF SERVICE AND DELAY FOR UNSIGNALIZED INTERSECTIONS V

LEVEL OF SERVICE	DESCRIPTION	CONTROL DELAY (seconds/vehicle)
А	Little or no delay	0 - 10
В	Short Traffic Delays	>10 -15
с	Average Traffic Delays	>15 - 25
D	Long Traffic Delays	>25 - 35
E	Very Long Traffic Delays	>35 - 50
F	Extreme Traffic Delays	>50

Source: Highway Capacity Manual, 6th Edition





Unfortunately, the 5-legged intersection of Brooks Avenue at Dandridge Avenue and Wilder Place cannot be analyzed using standard unsignalized HCM methods or in the Synchro 12 software, which is limited to a maximum of 4 intersection approaches. Due to this limitation, a companion software, SimTraffic 12, was utilized. SimTraffic performs micro-simulation and animation of vehicular traffic, and based on the simulation, it can calculate performance measures such as delay, vehicle queues, fuel efficiency, vehicle speeds, and other factors. According to the software, the "total delay is total travel time minus the travel time for the vehicle with no other vehicles or traffic control devices." Thus, the delay per vehicle is calculated by dividing the total delay by the number of vehicles in the simulation, and this measure was selected as the most appropriate means to overcome the HCM's limitation and provide intersection performance measures. The vehicle delay results presented in this study for this 5-legged intersection were based on ten simulations.

Intersection capacity results from the existing 2024 peak hour traffic are shown in Tables 4a and 4b. The 5-legged intersection approach results are shown in Table 4a, which shows the total delay per vehicle (in seconds) from the simulation. The other intersections are shown in Table 4b with a LOS designation, delay (in seconds), and v/c ratio (volume/capacity) for the AM and PM peak hours. Appendix E includes the worksheets for the existing 2024 peak hour capacity analyses.

The approaches of the 5-legged intersection in Table 4a are shown in the existing peak hour conditions with reasonable delay outcomes. As shown in Table 4b, all the other studied intersections are calculated to operate with excellent LOS and short vehicle delays in the existing peak hour 2024 conditions.

#### TABLE 4a 2024 INTERSECTION CAPACITY ANALYSIS RESULTS -EXISTING TRAFFIC CONDITIONS

	TRAFFIC	APPROACH/	AM PEAK	PM PEAK
INTERSECTION	CONTROL	MOVEMENT	TOTAL DELAY	TOTAL DELAY
			PER VEHICLE	PER VEHICLE
			(seconds)	(seconds)
Brooks Avenue (WB) at Dandridge Avenue (EB) and		Eastbound	6.6	8.0
Dandridge Avenue (NW) and Wilder Place (SB & NB)	zed	Westbound	7.7	7.6
	STOP	Northbound	4.8	5.7
		Southbound	4.9	6.3
	'n	Northwestbound	5.0	5.4
		All Lanes	6.4	7.0

Note: Results were obtained from SimTraffic 12 Performance Analyses from Simulation



#### TABLE 4b 2024 INTERSECTION CAPACITY ANALYSIS RESULTS -EXISTING TRAFFIC CONDITIONS

	TRAFFIC	APPROACH/	AM PEAK			PM PEAK		
INTERSECTION	CONTROL	MOVEMENT	LOS	DELAY	V/C	LOS	DELAY	V/C
				(seconds)			(seconds)	
Delrose Drive (WB) / Riverside Drive (EB) at	zed	Northwestbound Left/Right	В	12.0	0.085	В	13.0	0.131
Riverside Drive & Vulcans Materials	STOP Heug	Westbound Left	А	8.6	0.004	А	0.0	-
Driveway (NWB)	Unsign							
Delrose Drive (WB & EB) at	zed	Eastbound Left/Thru	А	8.0	0.013	А	7.7	0.024
Riverside Road (SB)	STOP ITE	Southbound Left/Right	В	10.1	0.059	А	9.9	0.047
	Unsign							
Brooks Avenue (WB & EB) at	bəz	Northbound Left/Right	А	9.8	0.031	А	9.4	0.042
Riverside Road (NB)	STOP STOP	Westbound Left/Thru	А	7.4	0.024	А	7.5	0.016
	Unsign							

Note: All analyses were calculated in Synchro 12 software and reported using 7th Edition intersection methodology

 $^{\rm a}$  Level of Service ,  $^{\rm b}$  Average Delay (sec/vehicle) ,  $^{\rm c}$  Volume-to-Capacity Ratio



#### PROJECTED TRAFFIC CONDITIONS WITHOUT THE PROJECT:

Horizon year traffic conditions represent the projected traffic volumes in the study area without the proposed project being developed (no-build option). This proposed development's build-out and full occupancy are assumed to occur by 2027.

According to the nearby TDOT count stations, vehicular traffic the on surrounding roads has shown low and moderate growth on Brooks Avenue and Delrose Drive, respectively, over the past Specifically, the TDOT data few years. provided in Appendix A shows that Brooks Avenue has experienced annual growth of +0.6%, and Delrose Drive has experienced +3.1% over the past ten years. The traffic count stations both showed a drop in vehicular volumes in 2018 but have experienced stable to slight growth since.



This study used an annual growth rate of +2% to calculate future growth on Brooks Avenue, Dandridge Avenue, Wilder Place, and Riverside Road. An annual growth rate of 3% was assumed for Delrose Drive and Riverside Drive. These annual growth rates were applied to the existing 2024 intersection volumes to estimate the future volumes in the horizon year of 2027 without the potential additional development traffic. Figures 6a and 6b show the projected 2027 horizon year traffic volumes at the studied intersections without the project during the AM and PM peak hours.







Capacity analyses were undertaken to determine the total delay per vehicle and projected LOS in 2027 without the project at the studied intersections. The results are shown in Tables 5a and 5b, and Appendix E includes the capacity analysis worksheets from the software.

As expected, Tables 5a and 5b show slightly worse vehicle delays at the intersections in the 2027 projected conditions versus the existing 2024 conditions. This result is due to the slight increase in traffic volumes due to the assumed general growth unrelated to the proposed development.

# TABLE 5a2027 INTERSECTION CAPACITY ANALYSIS RESULTS -PROJECTED TRAFFIC CONDITIONS WITHOUT THE PROJECT

	TRAFFIC	APPROACH/	AM PEAK	PM PEAK
INTERSECTION	CONTROL	MOVEMENT	TOTAL DELAY	TOTAL DELAY
			PER VEHICLE	PER VEHICLE
			(seconds)	(seconds)
Brooks Avenue (WB) at Dandridge Avenue (EB) and		Eastbound	6.7	8.5
Dandridge Avenue (NW) and Wilder Place (SB & NB)	zed	Westbound	8.0	7.9
	STOP	Northbound	5.0	5.8
		Southbound	5.1	6.2
	L L	Northwestbound	5.0	5.4
		All Lanes	6.6	7.3

Note: Results were obtained from SimTraffic 12 Performance Analyses from Simulation

## TABLE 5b2027 INTERSECTION CAPACITY ANALYSIS RESULTS -PROJECTED TRAFFIC CONDITIONS WITHOUT THE PROJECT

	TRAFFIC	APPROACH/	AM PEAK			PM PEAK		
INTERSECTION	CONTROL	MOVEMENT	LOS	DELAY	V/C	LOS	DELAY	V/C
				(seconds)			(seconds)	
Delrose Drive (WB) / Riverside Drive (EB) at	zed	Northwestbound Left/Right	В	12.5	0.097	В	13.7	0.151
Riverside Drive & Vulcans Materials	STOP international	Westbound Left	А	8.6	0.004	Α	0.0	-
Driveway (NWB)	Unsign							
Delrose Drive (WB & EB) at	zed	Eastbound Left/Thru	A	8.1	0.015	A	7.8	0.026
Riverside Road (SB)	STOP STIB	Southbound Left/Right	В	10.3	0.064	В	10.1	0.050
	Unsign							
Brooks Avenue (WB & EB) at	zed	Northbound Left/Right	А	10.0	0.034	Α	<b>9</b> .5	0.045
Riverside Road (NB)	STOP Ignali	Westbound Left/Thru	А	7.4	0.025	Α	7.6	0.018
	Unsign							

Note: All analyses were calculated in Synchro 12 software and reported using 7th Edition intersection methodology

<sup>a</sup> Level of Service , <sup>b</sup> Average Delay (sec/vehicle) , <sup>c</sup> Volume-to-Capacity Ratio



#### • <u>Trip Generation</u>:

A generated trip is a single or one-direction vehicle movement entering or exiting the study site. The estimated traffic the 570 apartments and 80 townhouses in the Cardinal Place development will generate was based on the equations provided by Knoxville/Knox County Planning. These equations from Knoxville/Knox County Planning were developed from an extensive local study to estimate townhouse (and apartment) trip generation in the surrounding area. For Knox County, this is the preferred rate to use for townhouses and apartments. This local rate calculates slightly higher trip rates than the similar land use in the often-used ITE (Institute of Transportation Engineers) Trip Generation Manual.

As previously mentioned, this study assumed a 5% reduction in vehicle trips due to the proximity of the KAT bus transit system on Brooks Avenue. This reduction was approved beforehand by Knoxville/Knox County Planning and the City of Knoxville Engineering Department.

The data and calculations from the local trip generation study for the proposed land uses are shown in Appendix F. A summary of this information is presented in Table 6:

ITE LAND USE CODE	LAND USE DESCRIPTION	# OF UNITS	GENERATED DAILY TRAFFIC	GENERATED TRAFFIC AM PEAK HOUR			GENERATED TRAFFIC I PEAK HOUR						
				ENTER	EXIT	TOTAL	ENTER	EXIT	TOTAL				
Local Trip		570		22%	78%		55%	45%					
Rate	Apartments		4,562	59	208	267	215	176	391				
Local Trip	Multi-Family Attached	80		22%	78%		55%	45%					
Rate	Townhouses 80		80	80	80	80	- 80	781	9	34	43	35	29
New Volume Site Trips		5,343	68	242	310	250	205	455					
Vehicle Trip Reduction due to Transit Activity (5%)		-267	-3	-12		-13	-10						
Total New Volume Site Trips		5,076	65	230	295	237	195	432					
			•						•				

#### TABLE 6 TRIP GENERATION FOR CARDINAL PLACE 570 Apartments and 80 Townhouses

Local Trip Rates calculated by using Fitted Curve Equations

For the proposed Cardinal Place development, it is estimated that 65 vehicles will enter and 230 will exit, for a total of 295 generated trips during the AM peak hour in the year 2027. Similarly, it is estimated that 237 vehicles will enter and 195 will exit, for a total of 432 generated trips during



the PM peak hour in the year 2027. The calculated trips generated for an average weekday are estimated to be 5,076 vehicles for the proposed development. The table shows the assumed 5% trip reduction applied to account for transit activity and overall vehicle trip reductions.

#### • <u>TRIP DISTRIBUTION AND ASSIGNMENT</u>:

The projected trip distribution and assignment for the Cardinal Place development are based on several sources and engineering judgment. The first source is based on the existing traffic count volumes and the observed travel directions collected at the studied intersections and adjacent roadways. Overall, during the traffic counts, motorists in the area showed a distinct inclination for westbound travel towards Knoxville in the morning and the opposite in the afternoon peak period.



The second source for determining the projected trip distribution is based on work-related trips in the local area. Work-based trips will be a significant impetus for trips generated by the development, and these trips are more likely to travel to and from the west and southwest. This assertion is based on data from the United States Bureau website for Census Tract 21, where the development property is located. Based on 2021 (latest available) census data and as presented in Appendix G, most work-based trips in the surrounding area correspond to Oak Ridge, TN, downtown Knoxville, the University of

Tennessee, and areas of West Knoxville. However, the largest area of work-related trips is shown just to the east. This area is assumed to be associated with the Forks of the River Industrial Park and the other businesses along E Governor John Sevier Highway.

In addition to employment centers, some generated traffic will travel to and from public and private schools. Schools will be another impetus for external trip-making. The development property is currently zoned for Sarah Moore Greene Magnet Academy (elementary), Vine Middle, and Austin-East (high school). This development property's zoned elementary and high school are all located to the north. The middle school, Vine, is slightly to the west. Sarah Moore Greene Magnet Academy is approximately 1,500 feet to the north, and Austin-East is 1.5 miles to the north. Vine Middle School is 2.1 miles away to the west. The shortest travel to the elementary and high school will be via Riverside Road, Brooks Avenue, and Boyds Bridge Pike to and from the north. The shortest and quickest routes from the proposed development to and from Vine Middle on Martin Luther King Jr Avenue will be made by traveling to and from the west via



Brooks Avenue, Delrose Drive, Dandridge Avenue, and Wilder Place.

The Knox County Schools Transportation Department has developed Parental Responsibility Zones (PRZ) to determine whether students are offered transportation services to and from school. The PRZ is defined as being 1.5 miles for grades 6 - 12and 1.0 miles for grades K - 5 from where the students' parcel is accessed to the point where the buses unload at the school. Except for elementary students at Sarah Moore Greene Magnet Academy, this development will be outside the PRZ for all the middle and high schools, and all school-age children attending



these schools in the development will be able to utilize the school bus service if desired.

For shopping, grocery, and similar retail and business services, the closet opportunities will be provided along Magnolia Avenue to the north, with the quickest route provided via Brooks Avenue and Boyds Bridge Pike to and from the north.

Based on these factors, Figures 7a and 7b show the projected distribution of traffic entering and exiting the proposed residential development at the proposed entrances and the studied intersections. The percentages shown in the figure only pertain to the trips generated by the proposed dwellings in the development calculated from the local trip rates. Ultimately, the projected trip distribution was heavily based on the observed traffic at the intersections, the traffic flows adjacent to the site, and the expected work, school-related, and shopping-related travel. Overall, 10% was assumed to and from the north, 20% east, and 70% west (and south via west travel).

Figures 8a and 8b show the traffic assignment of the computed trips generated by the Cardinal Place development. These assignments are based on the assumed distribution of trips shown in Figures 7a and 7b.











#### PROJECTED TRAFFIC CONDITIONS WITH THE PROJECT:

Several additive steps were taken to estimate the <u>total</u> projected traffic volumes at the proposed entrances and other studied intersections when the Cardinal Place development is constructed and fully occupied in 2027. The steps are illustrated below for clarity and review:



The calculated peak hour traffic generated by the Cardinal Place development was added to the 2027 horizon year traffic by following the predicted trip distributions and assignments. This procedure was completed to obtain the <u>total</u> projected traffic volumes at the studied intersections and proposed entrances when the Cardinal Place development is fully built and occupied in 2027. Figures 9a and 9b show the projected 2027 AM and PM peak hour volumes with the Cardinal Place development trips.







Capacity analyses were conducted to determine the total delay per vehicle and projected LOS at the studied intersections and proposed entrances with the development traffic in 2027, shown in Figures 9a and 9b. Intersection capacity results from the projected 2027 peak hour traffic are shown in Tables 7a and 7b. Appendix E includes the worksheets for the projected 2027 peak hour capacity analyses.

As shown in Table 7a, the approaches at the 5-legged intersection of Brooks Avenue at Dandridge Avenue and Wilder Place are projected to operate with slightly increased total delays per vehicle compared to the existing conditions. The largest impacted approach, eastbound Dandridge Avenue, will only be increased by 2.1 seconds per vehicle in the PM peak hour compared to the existing result, from 8 seconds to 10.2 seconds. All the other approaches at the 5-legged intersection will experience increased delays of 1.2 seconds per vehicle or less in the AM or PM peak hours compared to the existing conditions, all of which are acceptable.

# TABLE 7a2027 INTERSECTION CAPACITY ANALYSIS RESULTS -PROJECTED TRAFFIC CONDITIONS WITH THE PROJECT

	TRAFFIC	APPROACH/	AM PEAK	PM PEAK
INTERSECTION	CONTROL	MOVEMENT	TOTAL DELAY	TOTAL DELAY
			PER VEHICLE	PER VEHICLE
			(seconds)	(seconds)
Brooks Avenue (WB) at Dandridge Avenue (EB) and		Eastbound	7.2	10.1
Dandridge Avenue (NW) and Wilder Place (SB & NB)	zed	Westbound	8.9	8.8
	STOP Here	Northbound	5.3	6.3
	is is	Southbound	5.4	7.3
	L L	Northwestbound	5.7	6.6
		All Lanes	7.3	8.4

Note: Results were obtained from SimTraffic 12 Performance Analyses from Simulation

All the other studied intersections and proposed entrance intersections are calculated to operate with very good to average LOS and vehicle delays in the projected 2027 AM and PM peak hours. All movements are projected to operate at LOS A or B, except for the northwestbound approach of Riverside Drive/Vulcan Materials Driveway at Delrose Drive, calculated at LOS C. This increased delay on this approach is directly related to the increased thru movements on Riverside Drive and Delrose Drive due to the trips generated by the Cardinal Place development, but is still quite reasonable.



## TABLE 7b2027 INTERSECTION CAPACITY ANALYSIS RESULTS -PROJECTED TRAFFIC CONDITIONS WITH THE PROJECT

	TRAFFIC	APPROACH/		AM PEAK		PM PEAK		
INTERSECTION	CONTROL	MOVEMENT	LOS	DELAY (seconds)	V/C	LOS	DELAY (seconds)	V/C
Delrose Drive (WB) / Riverside Drive (EB) at	zed	Northwestbound Left/Right	С	15.1	0.128	С	19.1	0.224
Riverside Drive & Vulcans Materials	STOP	Westbound Left	Α	8.8	0.004	Α	0.0	-
Driveway (NWB)	Unsignalized							
Delrose Drive (WB & EB) at	zed	Eastbound Left/Thru	Α	8.2	0.022	Α	8.0	0.032
Riverside Road (SB)	STOP	Southbound Left/Right	В	11.1	0.094	В	12.5	0.121
	Unsignalized							
Brooks Avenue (WB & EB) at	zed	Northbound Left/Right	В	10.1	0.096	Α	10.0	0.106
Riverside Road (NB)	Unsignalized	Westbound Left/Thru	А	7.4	0.031	Α	7.7	0.044
Riverside Road (SB & NB) at	zed	Northbound Left	А	7.3	0.001	А	7.3	0.005
Proposed East Entrance (EB)	STOP	Eastbound Left/Right	Α	9.0	0.046	Α	9.0	0.038
	Unsignalized							
Delrose Drive (WB & EB) at	zed	Eastbound Left	Α	8.3	0.015	Α	8.2	0.050
Proposed Southwest Entrance (SB)	Unsignalized	Southbound Left/Right	В	12.1	0.118	В	11.9	0.096
Delrose Drive (WB & EB) at	zed	Eastbound Left	А	8.1	0.025	А	8.2	0.087
Proposed Southeast Entrance (SB)	STOP	Southbound Left/Right	В	12.8	0.249	В	14.5	0.249
	Unsignalized							

Note: All analyses were calculated in Synchro 12 software and reported using 7th Edition intersection methodology

<sup>a</sup> Level of Service , <sup>b</sup> Average Delay (sec/vehicle) , <sup>c</sup> Volume-to-Capacity Ratio



#### <u>POTENTIAL TRANSPORTATION SAFETY ISSUES:</u>

The study area was investigated for potential existing and future safety issues when the development is constructed. These transportation features are discussed in the following pages.

#### • EVALUATION OF SIGHT DISTANCE

For intersections, sight distance evaluations have two categories: Stopping Sight Distance (SSD) and Intersection Sight Distance (ISD).

#### Methodology:

SSD is the distance required for a motorist on a major street to perceive, react, and the vehicle to come to a complete stop before colliding with an object on the road. For evaluating intersections, this object would be another vehicle entering the intersection from a minor street. SSD can be considered the <u>minimum</u> visibility distance standard for evaluating the safety of an intersection.

ISD is the <u>required</u> visibility distance standard for evaluating the safety of an intersection. ISD is based on the time required to perceive, react, and complete the desired traffic maneuver once a motorist on a minor street decides to perform a traffic maneuver. Three traffic maneuvers are available for vehicles stopped on a minor street



at a 4-way intersection: (1) left-turn, (2) right-turn, (3) or a crossing maneuver across the major street. For turns from the minor street, ISD is needed to allow a stopped motorist to turn onto a major street without being overtaken by an approaching vehicle. The most critical ISD is for left turns from the minor street. The ISD for this maneuver includes the time to turn left and clear half of the intersection without conflicting with the oncoming traffic from the left and accelerating to the road's operating speed without causing the approaching vehicles from the right to reduce their speed substantially.

With a posted speed limit of 35 mph on Delrose Drive, the ISD is 390 feet for left turns exiting the development site at the Proposed Southeast and Southwest Entrances. This value is calculated



based on AASHTO's guidance. This distance is required for a motorist to safely exit to the left (eastbound) onto Delrose Drive from the proposed entrances. The ISD for a right-turn movement (westbound) from the proposed entrance is 335 feet.

At the Proposed East Entrance on Riverside Road, with a posted speed limit of 25 mph, the ISD for left turns is 280 feet and 240 feet for right turns.

Visual observations of the sight distances at the proposed entrance locations were undertaken. Using a Nikon Laser Rangefinder at the proposed entrance locations, the available sight distances were measured and are expected to be adequate for motorists exiting the development at all three entrances. These measurements assumed that vegetation along Delrose Drive would be removed along the road frontage and maintained in future conditions. The same was assumed for Riverside Road, which includes an existing utility pole adjacent to the Proposed East Entrance location, which will require relocation.

Images of the existing sight distances at the proposed entrance locations are labeled below with the required ISD and rangefinder-measured sight distances.





View of Sight Distance on Delrose Drive

at the Proposed Southeast Entrance Location

(Looking East)

View of Sight Distance on Delrose Drive

at the Proposed Southeast Entrance Location

(Looking West)



#### • EVALUATION OF TURN LANE THRESHOLDS

The need for separate left and right-turn lanes was evaluated in the projected 2027 conditions for the proposed entrances at Delrose Drive. It was not evaluated for the Proposed East Entrance due to the projected low volumes on Riverside Road.

The criteria used for these turn lane evaluations were based on Knox County's "Access Control and Driveway Design Policy". This design policy relates vehicle volume thresholds based on prevailing speeds for two-lane and four-lane roadways. The Proposed Southeast and Southwest Entrance locations on Delrose Drive are within a 35 mph speed zone; thus, these entrances were evaluated based on this posted speed. The worksheets for these evaluations are provided in Appendix H.

Based on the projected 2027 traffic volumes at the intersections, none of the proposed entrances warrant separate entering right-turn lanes on Delrose Drive. The Proposed Southwest Entrance does not meet a warrant for a separate entering left-turn lane on Delrose Drive, but a warrant for a left-turn lane is met at the Proposed Southeast (main) Entrance during the PM peak hour. Additionally, a warrant for a left-turn lane at the Proposed Southwest Entrance is nearly met during the PM peak hour.

#### • **PROJECTED VEHICLE QUEUES**

The SimTraffic software also calculates the 95<sup>th</sup> percentile vehicle queues at intersections. The 95<sup>th</sup> percentile vehicle queue is the recognized measurement in the transportation engineering profession as the design standard used when considering vehicle queue lengths. A 95<sup>th</sup> percentile vehicle queue length means 95% certainty that the vehicle queue will not extend beyond that point. The calculated vehicle queue results were based on averaging the outcome obtained during ten traffic simulations in the software. The 95<sup>th</sup> percentile vehicle queue lengths at the intersections are shown in Table 8 for the projected 2027 conditions. The vehicle queue worksheet results from the SimTraffic software are in Appendix I.

Table 8 shows minimal vehicle queue lengths on all the studied intersection approaches in the 2027 AM and PM peak hours. Based on these results, the longest vehicle queue calculated for the studied intersections will occur on the Dandridge Avenue eastbound approach at the 5-legged intersection in the PM peak hour. This approach was calculated to have a vehicle queue length of 103 feet and will be just over four passenger vehicles, assuming a length of 25 feet per vehicle.



# TABLE 8VEHICLE QUEUE SUMMARY -2027 PROJECTED TRAFFIC CONDITIONS WITH THE PROJECT

	TRAFFIC	APPROACH/	SIMTRAFFIC 95 <sup>th</sup> PERCENTILE QUEUE LENGTH (ft)		
INTERSECTION	CONTROL	MOVEMENT	AM PEAK HOUR	PM PEAK HOUR	
Brooks Avenue (WB) at Dandridge Avenue (EB) and	g.	Eastbound	63	103	
Dandridge Avenue (NW) and Wilder Place (SB & NB)	Unsignalized	Westbound	92	71	
Driveway (NWB)	STOP E	Northbound	47	58	
	Insi	Southbound	58	66	
		Northwestbound	40	43	
Delrose Drive (WB) / Riverside Drive (EB) at	zed	Westbound Left/Thru	9	0	
Riverside Drive & Vulcans Materials	STOP	Northwestbound Left/Right	60	47	
Driveway (NWB)	Unsignalized				
Delrose Drive (WB & EB) at	zed	Eastbound Left/Thru	20	29	
Riverside Road (SB)	STOP	Southbound Left/Right	43	41	
	Unsignalized				
Brooks Avenue (WB & EB) at	zed	Northbound Left/Right	57	24	
Riverside Road (NB)	STOP	Westbound Left/Thru	17	46	
	Unsignalized	and the second second			
Riverside Road (SB & NB) at	zed	Northbound Left	3	4	
Proposed East Entrance (EB)	STOP	Eastbound Left/Right	45	44	
	Unsignalized				
Delrose Drive (WB & EB) at	zed	Eastbound Left	26	53	
Proposed Southwest Entrance (SB)	STOP I	Southbound Left/Right	46	46	
	Unsignalized				
Delrose Drive (WB & EB) at	zed	Eastbound Left	32	63	
Proposed Southeast Entrance (SB)	STOP	Southbound Left/Right	66	66	
	Unsignalized				

Vehicle Queues calculated in SimTraffic 12 Software



### **CONCLUSIONS & RECOMMENDATIONS**

The following is an overview of recommendations to minimize the transportation impacts of the Cardinal Place development on the adjacent transportation system while attempting to achieve an acceptable traffic flow and safety level.



**Brooks Avenue at Dandridge Avenue and Wilder Place**: This intersection is projected to operate with reasonable total vehicle delays per vehicle and minimal vehicle queues for all approaches. From a transportation engineering perspective, the Cardinal Place development will have minimal impact on this intersection. No specific recommendations are provided based on these findings. However, based on the observations during the traffic counts and the crash history reviewed at the intersection, it is apparent that this unusual 5-legged intersection is difficult for motorists to navigate. This intersection, having five approaches, with one at an acute angle, presents a challenge to motorists in determining which has the right-of-way when proceeding into the intersection. Motorist hesitation and confusion, near misses, and sharp turning movements were observed during the traffic counts, and the crash data lends credence to these observations.

It is recommended that the City of seriously Knoxville consider eliminating the northwestbound approach of Dandridge Avenue at the 5-legged intersection. This approach intersects at an acute angle and provides nearly unlimited turning movement locations to and from the adjacent gas station/market parking area, which is less than desirable. An initial recommendation to eliminate this approach would be to reroute it further east of the corner gas



station/market and intersect Brooks Avenue at a t-intersection, as presented in the adjacent image. This alternative routing would traverse private property and a portion of the existing gas station/market parking lot. This alternative route would require



property acquisition and accommodation of a few private driveways on the southern side of Dandridge Avenue. However, eliminating this approach would solve many detrimental issues currently occurring at the 5-legged intersection. As shown in the image, the closed portion of the "old" route of Dandridge Avenue could be swapped with the gas station/market property owner to lower acquisition costs since the "new" route would cross their property. Once the Dandridge Avenue northwestbound leg could be removed, alternative traffic control at the intersection with Brooks Avenue and Wilder Place, such as a roundabout, could be considered instead of its current all-way stop conditions.

Delrose Drive at Riverside Drive: This intersection is projected to operate with reasonable vehicle delays per vehicle and minimal vehicle queues for all movements. From a transportation engineering perspective, the Cardinal Place development will have minimal impact on this intersection. No specific recommendations are provided based on these findings. The thru movements on Delrose Drive and Riverside Drive will be increased once the development comes to fruition. Still, this will only slightly increase the vehicle delay for vehicles attempting to turn westbound onto Riverside Drive or eastbound onto Delrose Drive.

This intersection's current layout is less than desirable due to the acute angle at which the southeast approach of Riverside Drive intersects Delrose Drive and combines with the Vulcans Material Driveway. The crash data from the past three years did not indicate any specific patterns or occurrences that would lend indicators to needed improvements.

However, once again, similar to the 5-legged intersection, the City of Knoxville should consider rerouting the southeast approach of Riverside Drive to intersect Delrose Drive further to the east and away from the Vulcan Materials Driveway. Shifting and separating this approach further to the east would allow greater separation of heavy trucks and passenger cars, increase safety, and eliminate the less-than-desirable combined approach of Riverside Drive and the Vulcan Materials Driveway. The corner property that would allow for this relocation is currently unoccupied, and the City should consider correcting this before this property becomes developed or occupied.



- **Delrose Drive and Brooks Avenue at Riverside Road**: These intersections are projected to operate with reasonable vehicle delays per vehicle and minimal vehicle queues for all movements. From a transportation engineering perspective, the Cardinal Place development will have minimal impact on these intersections. No specific recommendations are provided based on these findings. However, due to the projected increased traffic volumes on Riverside Road, it is recommended that this roadway be widened to have a minimum width of 20 feet its entire length. This road was recently repaved and slightly widened in spots but still has sections less than 18 feet wide. Details regarding the particulars of this road widening should be discussed further with the City of Knoxville Engineering Department.
- A Riverside Road at Proposed East Entrance: The 2027 projected level of service calculations for this proposed intersection resulted in very short vehicle delays and good LOS.
  - 4a) The construction of separate turn lanes on Riverside Road for entering traffic at the Proposed East Entrance will not be needed due to the projected low volumes in the 2027 conditions.
  - 4b) It is recommended that a Stop Sign (R1-1) be installed and a 24" white stop bar be applied to the Proposed East Entrance approach at Riverside Road. The stop bar should be applied a minimum of 4 feet away from the edge of Riverside Road and placed at the desired stopping point that maximizes the sight distance.
  - 4c) A single exiting lane for the Proposed East Entrance at Riverside Road will be sufficient. The 95<sup>th</sup> percentile vehicle queue lengths were calculated at this intersection for the 2027 projected conditions with the project, and the calculated vehicle queues are reasonable. The longest exiting queue in the projected 2027 conditions is calculated to be 45 feet in the AM peak hour and 45 feet in the PM peak hour. These queue lengths translate to just under two passenger cars, assuming a length of 25 feet per vehicle.
  - 4d) Intersection sight distance at the Proposed East Entrance at Riverside Road must not be impacted by existing vegetation or future landscaping or signage. The existing utility pole on the west side of Riverside Road near the proposed entrance



location will need to be relocated. Based on a posted speed limit of 25 mph on Riverside Road, the required ISD is 280 feet for exiting left-turning vehicles at the Proposed East Entrance and 240 feet for exiting right-turning vehicles. The site designer must verify that these distances will be available.

**Delrose Drive at Proposed Southwest Entrance**: The 2027 projected level of service calculations for this proposed intersection resulted in very short vehicle delays and good LOS.

5a) The construction of separate turn lanes on Delrose Drive for entering traffic at the Proposed Southwest Entrance is not expected to meet warrants based on the projected 2027 traffic volumes. However, a warrant for a left-turn lane at the Proposed Southwest Entrance is nearly met during the PM peak hour. This result is a "borderline" situation. It should be understood that the analysis and this nearly satisfied warrant result are based on several assumptions in the study. Thus, the actual, realized traffic conditions could vary from the projections.

Serious consideration should be given to providing a separate left-turn lane on Delrose Drive at the Proposed Southwest Entrance. If provided, the recommended lengths for this proposed eastbound left-turn lane were based on TDOT standards and include an approach taper of 225 feet, a bay taper of 90 feet (8:1), and a vehicle storage length of 75 feet lane. Seventy-five feet of storage will allow a vehicle queue of up to three passenger cars. A storage length of 75 feet will be appropriate since the longest vehicle queue for this left turning movement without a turn lane at the Proposed Southwest Entrance was calculated to be 26 feet in the AM peak hour and 53 feet in the PM peak hour. (This queue length would be reduced with a provided turn lane.) An approach taper will be required to allow for a transition to create space to add an eastbound left-turn lane on Delrose Drive.

The recommended lengths are shown in the following TDOT diagram from their <u>Highway System Access Manual</u> (Figure 3-21):




To provide this lane with these lengths on Delrose Drive at the Proposed Southwest Entrance, further engineering review and design will be required to determine the most appropriate means of modifying the roadway to incorporate this additional lane within the ROW constraints and the presence of a utility entrance driveway to Williams Creek Golf Course further to the southwest.

- 5b) It is recommended that a Stop Sign (R1-1) be installed and a 24" white stop bar be applied to the Proposed Southwest Entrance approach at Delrose Drive. The stop bar should be applied a minimum of 4 feet away from the edge of Delrose Drive and placed at the desired stopping point that maximizes the sight distance.
- 5c) A single exiting lane for the Proposed Southwest Entrance at Delrose Drive will be sufficient. The 95<sup>th</sup> percentile vehicle queue lengths were calculated at this intersection for the 2027 projected conditions with the project, and the calculated vehicle queues are reasonable. The longest exiting queue in the projected 2027 conditions is calculated to be 46 feet in the AM peak hour and PM peak hour. These queue lengths translate to just under two passenger cars, assuming a length of 25 feet per vehicle.
- 5d) Intersection sight distance at the Proposed Southwest Entrance at Delrose Drive must not be impacted by existing vegetation or future landscaping or signage. Based on a posted speed limit of 35 mph on Delrose Drive, the required ISD is 390 feet for exiting left-turning vehicles at the Proposed Southwest Entrance and 335 feet for exiting right-turning vehicles. The site designer must verify that these distances will be available.





6a) The construction of a separate right-turn lane on Delrose Drive for entering traffic at the Proposed Southeast Entrance is not warranted based on the projected 2027 PM peak hour traffic volumes. However, a separate left-turn lane on Delrose Drive at this proposed main entrance is warranted based on the projected 2027 traffic volumes and Knox County thresholds. The recommended lengths for this proposed eastbound left-turn lane were based on TDOT standards and include an approach taper of 225 feet, a bay taper of 90 feet (8:1), and a vehicle storage length of 75 feet lane. Seventy-five feet of storage will allow a vehicle queue of up to three passenger cars. A storage length of 75 feet will be appropriate since the longest vehicle queue for this left turning movement without a turn lane at the Proposed Southeast Entrance was calculated to be 32 feet in the AM peak hour and 63 feet in the PM peak hour. (This queue length would be reduced with a turn lane.) An approach taper will be required to allow for a transition to create space to add an eastbound left-turn lane on Delrose Drive.

The recommended lengths are shown in the following TDOT diagram from their <u>Highway System Access Manual</u> (Figure 3-21):



To provide this lane with these lengths on Delrose Drive at the Proposed Southeast Entrance, further engineering review and design will be required to determine the most appropriate means of modifying the roadway to incorporate this additional



lane within the ROW constraints and complicated by the presence of the nearby historic cemetery.

- 6b) It is recommended that a Stop Sign (R1-1) be installed and a 24" white stop bar be applied to the Proposed Southeast Entrance approach at Delrose Drive. The stop bar should be applied a minimum of 4 feet away from the edge of Delrose Drive and placed at the desired stopping point that maximizes the sight distance.
- 6c) A single exiting lane for the Proposed Southeast Entrance at Delrose Drive will be sufficient. The 95<sup>th</sup> percentile vehicle queue lengths were calculated at this intersection for the 2027 projected conditions with the project, and the calculated vehicle queues are reasonable. The longest exiting queue in the projected 2027 conditions is calculated to be 66 feet in the AM peak hour and PM peak hour. These queue lengths translate to just under three passenger cars, assuming a length of 25 feet per vehicle.
- 6d) Intersection sight distance at the Proposed Southeast Entrance at Delrose Drive must not be impacted by existing vegetation or future landscaping or signage. Based on a posted speed limit of 35 mph on Delrose Drive, the required ISD is 390 feet for exiting left-turning vehicles at the Proposed Southeast Entrance and 335 feet for exiting right-turning vehicles. The site designer must verify that these distances will be available.





- 7a) A 15 mph Speed Limit Sign (R2-1) is recommended to be posted near the beginning of the development entrance driveways off Riverside Road and Delrose Drive.
   Since this will be a private development, a posted speed limit of less than 25 mph (minimum posted speed in the City of Knoxville) is allowable.
- 7b) Stop Signs (R1-1) and 24" white stop bars are recommended on the new internal drives and parking lot aisleways, as shown in the image below.





- 7c) Sight distance at the new internal intersections must not be impacted by new signage, parked cars, or future landscaping. With a speed limit of 15 mph in the development, the internal intersection sight distance is 170 feet. The site designer should ensure that internal sight distance lengths are met.
- 7d) With long and straight parking lot aisleways proposed internally, it is recommended that speed humps or tables be considered to reduce internal traffic speeds in the development. Alternatively, parking lot islands could be extended toward the aisleways. Extending the parking lot islands a few feet would narrow the aisleway widths and reduce the available driving surface. A narrower aisleway design would reduce driver comfort and internal vehicle speeds.
- 7e) All drainage grates and covers for the residential development must be pedestrian and bicycle-safe.
- 7f) Internal sidewalks are proposed throughout the development and will include an internal perimeter walking trail. Concrete sidewalks should have appropriate ADA-compliant ramps at intersection corners with detectable surfaces, and the internal sidewalks are recommended to be 5 feet minimum in width to meet the City of Knoxville regulations. White-painted crosswalks should be applied to the internal road pavement internally where pedestrians are expected to cross the parking aisleways. Internal crosswalks should include Pedestrian Warning (W11-2) signs with a downward arrow plaque (W16-7p) where appropriate. The internal crosswalks should have a white transverse marking as shown in TDOT Standard Drawing T-M-4.
- 7g) The internal sidewalk system for the proposed development should connect to the existing external sidewalk system on Brooks Avenue. It is recommended that this connection be constructed where the development property has a narrow strip of land up to Brooks Avenue. It is recommended that a crosswalk and pedestrian warning signs be applied on Brooks Avenue to connect to the sidewalk on the northern side of Brooks Avenue.

A Rectangular Rapid Flashing Beacon (RRFP) system could be a potential candidate for inclusion at this mid-block pedestrian crossing on Brooks Avenue. Further engineering regarding this crossing should be investigated, and sight



distance requirements should be included since the proposed crossing location will be at the bottom of a sag vertical curve on Brooks Avenue, with vegetation on the south side of Brooks Avenue potentially restricting sight distance.

The details regarding the mid-block pedestrian crossing must be coordinated with the City of Knoxville. It is recommended that the mid-block pedestrian crossing on Brooks Avenue include the following features:

- i. The existing roadway lighting on Brooks Avenue must be supplemented at the crossing location for night-time and low-light visibility. An additional roadway light may need to be installed on the south side of Brooks Avenue, where the development's sidewalk intersects the road corridor.
- The marked crosswalk on Brooks Avenue must be a white high-visibility patterned crosswalk. A continental or ladder design would be an appropriate high-visibility pattern on the pavement.
- iii. Pedestrian warning signage should be placed at the appropriate distances on each approach of Brooks Avenue.
- 7h) All internal and external road and intersection elements should be designed to AASHTO and the City of Knoxville specifications and guidelines to ensure proper operation.



APPENDIX A

HISTORICAL TRAFFIC COUNT DATA

# **Historical Traffic Counts**

Organization: TDOT

Station ID #: 47000484

Location: Brooks Avenue, east of Wilder Place



2013 - 2023 Growth Rate = 6.5% Average Annual Growth Rate = 0.6%

	TTOT Traffic Count	(TCDS)	
Home	All DIRs	Auto-Locate:	Google - 10.538 (23) 2 3 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		and the second se	3,884 (01)
Location ID		MPO ID	ANT FIVE PUINTS of Directory OWAY
Туре	SPOT	HPMS ID	• Olive St • Count: 2437 (2023)
On NHS	1705000001	On HPMS	View Detail in a New Search
	4705662001 Lower FC (2024)	LRS Loc Pt. 1.349 Route Type	The second in Current Search So und ut Ne une Are Be perfective Detrose The second in Current Search Detrose The second in Curren
	Region 1 Urban Major Collector (2024)	Route	
	Knox (2024)		3,709 (23) 2 + <sup>60</sup>
		Active Yes	
Class Dist Grp	Region 1 Urban Major Collector (2024)	Category CC	Harden he E Brooks he Brooks he
Seas Clss			Boond Are of Gaton Are a Brown
Grp			Been we a contrant we a
WIM Group			- A specific ad
QC Group			pandridge Ave Danne Se
Located On	Major Collector	Milepost	25 3 100 days 5 3 744 (22)
	BROOKS AVE.		
	KNOXVILLE		Hand A A A A A A A A A A A A A A A A A A A
ore Detail 🕨	I WIGHT Hadde		MORNINGSIDE Knox
TATION DAT	A		MORNINGSIDE Knox
			Hazen St Halon 3
rections:	Z-WAY 🧐		
AADT 🕐	and the second se		MONUTI Shoals
Year	AADT DHV-30 K% D%	PA BC Src	Priverside Dr
2023	3 2,437 211 9 65 2,3	85 (98%) 52 (2%)	River.
2022		255 (98%) 56 (2%)	James White Other Riverside Dr
2021		84 (97%) 67 (3%)	James White Otan Lames White Otan
2020		17 (96%) 85 (4%)	Knoxville
2019			Downtown
<< <	> >>  1-5 of 14		21.755 (23) Island

# **Historical Traffic Counts**

Organization: TDOT

Station ID #: 47000300

Location: Delrose Drive, east of Riverside Drive





Traffic Count (TCDS)	
Home Locate Locate All Email This Auto-Locate:	
	10,538 (23) <sup>4</sup>
List View All DIRs	
Record H 💜 372 🕨 🗰 of 662 Goto Record 🛛 go	
	3,884 (01)
Location ID         47000300         MPO ID           Type         SPOT         HPMS ID	under Ave FIVE POINTS and the Broads a grade a
On NHS On HPMS ID	Solive St Solive
LRS ID 4701124001 LRS Loc Pt. 1	
SF Group Lower FC (2024) Route Type	a where the second seco
AF Group Region 1 Urban Minor Collector (2024) Route	
GF Group Knox (2024) Active Y	Location ID: 47000300
Class Dist Grp Region 1 Urban Minor Collector (2024) Category C	Located On: DI124 DELROSE DR-NORTH OF DICKINSON ISLAND
Seas Clss	weight Ave
Grp	entry of the second sec
VIM Group	Go to Record in Current Search
QC Group Default Default Milepost Milepost	
nct'l Class Minor Collector Milepost ocated On 01124	Dandridge Ave Dandridge Ave Sit (K3)
c On Alias DELROSE DR.	A A A A A A A A A A A A A A A A A A A
DELROSE DR.NORTH OF DICKINSON ISLAND	
Detail	MORNINGSIDE 5 Knox
ATION DATA	whee he
ections: 2-WAY (7)	Li Hozen St Nam
	Multitristical
adt 🕐	
Year         AADT         DHV-30         K%         D%         PA         B0           2023         3,711         377         10         65         3,592 (97%)         119 (	Src 2 Prietsde Dr Prietsde Dr
2023 3,711 377 10 05 3,592 (97%) 119 ( 2022 3,682 318 9 65 3,590 (98%) 92 (2	75) verside Dr
2021 4,110 346 8 65 4,053 (99%) 57 (1	
2020 4,047 516 13 65 3,910 (97%) 137 (	
2019 3,891 12 65	NO VIIIE DOWNTOWN
< < > >>  1-5 of 39	21,755 (23) Diver

**APPENDIX B** 

# KNOXVILLE AREA TRANSIT MAP AND INFORMATION

# **Rider Tools and Tips**

#### **Fare Information**

Fare Type	Regular Fare	<b>Discounted Fare</b>
1-Ride pass	\$1.00	\$.50
1-Day pass	\$2.00	\$1.00
20-Ride pass	\$15.00	\$7.50
30-Day Pass	\$30.00	\$15.00

Discounted fare for seniors 65+. Medicare cardholders, and persons with disabilities. KAT ID or Medicare card required.

#### Children 4 and under ride free.

Knox County School Students also ride free with the Youth Freedom Pass.

To learn more about our fares, the Youth Freedom Pass and how to buy tickets, visit katbus.com.

#### **Riding Tips**

- · Plan your trip using this map, the free Transit app, or our homepage trip planner on katbus.com.
- Always arrive at your bus stop 5 minutes early.
- When you see your bus coming, wave to the operator so they know you want to board.
- Have your fare ready when the bus arrives.
- · When nearing your destination, pull the cord next to the windows to alert the operator that you want to get off at the next stop.
- View our Passenger Ride Guide at katbus.com.

#### **KAT Holidays**

KAT Services do not operate on the following holidays: New Year's Day, Independence Day, Thanksgiving & Christmas.

KAT buses run on a Sunday schedule on the following holidays: Martin Luther King, Jr. Day, Memorial Day, Juneteenth, Labor Day, day after Thanksgiving, day before Christmas.

KAT's administrative offices are closed on all of the holidays listed above.

#### Go paperless!

PLAN your trip, PAY your fare, and SCAN your ticket, all in our FREE official app:



Scan QR code to download Transit

# Google Play

# Herramientas y consejos para los pasajeros

#### Información sobre tarifas

Tipo de tarifa	Tarifa regular	Tarifa con descuento
Pase de 1 viaje	\$1.00	\$.50
Pase de 1 día	\$2.00	\$1.00
Pase de 20 viajes	\$15.00	\$7.50
Pase de 30 días	\$30.00	\$15.00

Tarifa descontada para mayores de 65 años, personas con tarjeta de Medicare y personas con discapacidades. Se necesita el ID de KAT o tarieta de Medicare

Los niños menores de 4 años viajan gratis.

Los estudiantes de las escuelas públicas del Condado de Knox también viajan gratis con el pase Youth Freedom Pass.

Visite katbus.com para averiguar más sobre nuestras tarifas, el pase para jóvenes y para comprar boletos.

#### Consejos para viajar

- Planifique su travecto con este mapa, la aplicación gratuita Transit o el planificador en katbus.com.
- Siempre llegue a la parada del autobús 5 minutos antes. · Cuando vea que llega el autobús, haga una seña al
- operador para que sepa que quiere subir. Tenga su pago listo cuando llega el autobús.
- · Cuando se acerque a su destino, jale del cordón cercano a la ventana para alertar al operador de que quiere bajarse en la siguiente parada.
- Repase nuestra Guia del Pasajero en katbus.com.

Los servicios de KAT no funcionan en los siguientes días feriados: Año Nuevo, Día de la Independencia, Acción de Gracias y Navidad.

Los autobuses de KAT siguen los horarios de los domingos en los siguientes feriados: día de Martin Luther King Jr., Dia de los Caídos (Memorial Day), Juneteenth, Dia del Trabajador, día después del Día de Acción de Gracias, día antes de Navidad.

Las oficinas de KAT estarán cerradas en todos esos días feriados.

#### ¡Haga todo sin papel!

PLANIFIQUE su viaje, PAGUE la tarifa y ESCANEE su boleto, todo en Transit, ¡nuestra aplicación oficial gratuita! La aplicación se configura en el mismo idioma de su teléfono. Escanee el código QR para descargar Transit.

#### Accesibilidad

Todos los autobuses de KAT van equipados con un elevador. También existe servicio de paratransito para quienes cualifiquen. Para más información, visite katbus.com o llame a KAT al 865-637-3000.

Internación en espand en el Inte

- 1100 Studio Apartments
- Alex Haley Heritage Square Statue
- Beck Cultural Exchange Center
- Brooks Rd
- Golden Age Retirement Village
- Green Magnet Academy
- **Knoxville Botanical Garden**
- Knowville Station/ Downlewn
- Mabry-Hazen House
- Sarah Moore Greene Magnet School

# **KAT Reimagined**

**Effective Date:** August 26, 2024

Dand

Avenue





# Route 32: Dandridge Avenue

		SAT	URDAY		
Going away fron	n downtown		Going loward do	wntown	
Knoxville Station Bay I	Boyds Bridge Pike EB and Border St	Golden Age Retirement Village	Kirkwood St Superstop WB Arrival	Border St NB and Boyds Bridge Pike	Knoxville Station Bay I
_	1		Transfer to Rts. 31 & 34	-	
1	2	3	4	5	6
			6:43 AM	6:55 AM	7:10 AM
7:15 AM	7:23 AM	7:32 AM	7:43 AM	7:55 AM	8:10 AM
8:15 AM	8:23 AM	8:32 AM	8:43 AM	8:55 AM	9:10 AM
9:15 AM	9:23 AM	9:32 AM	9:43 AM	9:55 AM	10:10 AM
10:15 AM	10:23 AM	10:32 AM	10:43 AM	10:55 AM	11:10 AM
11:15 AM	11:23 AM	11:32 AM	11:43 AM	11:55 AM	12:10 PM
12:15 PM	12:23 PM	12:32 PM	12:43 PM	12:55 PM	1:10 PM
1:15 PM	1:23 PM	1:32 PM	1:43 PM	1:55 PM	2:10 PM
2:15 PM	2:23 PM	2:32 PM	2:43 PM	2:55 PM	3:10 PM
3:15 PM	3:23 PM	3:32 PM	3:43 PM	3:55 PM	4:10 PM
4:15 PM	4:23 PM	4:32 PM	4:43 PM	4:55 PM	5:10 PM
5:15 PM	5:23 PM	5:32 PM	5:43 PM	5:55 PM	6:10 PM
6:15 PM	6:23 PM	6:32 PM	6:43 PM	6:55 PM	7:10 PM
7:15 PM	7:23 PM	7:32 PM	7:43 PM	7:55 PM	8:10 PM
8:15 PM	8:23 PM	8:32 PM	8:38 PM		

		SUN	DAY		
8:15 AM	8:23 AM	8:32 AM	8:43 AM	8:55 AM	9:10 AM
9:15 AM	9:23 AM	9:32 AM	9:43 AM	9:55 AM	10:10 AM
10:15 AM	10:23 AM	10:32 AM	10:43 AM	10:55 AM	11:10 AM
11:15 AM	11:23 AM	11:32 AM	11:43 AM	11:55 AM	12:10 PM
12:15 PM	12:23 PM	12:32 PM	12:43 PM	12:55 PM	1:10 PM
1:15 PM	1:23 PM	1:32 PM	1:43 PM	1:55 PM	2:10 PM
2:15 PM	2:23 PM	2:32 PM	2:43 PM	2:55 PM	3:10 PM
3:15 PM	3:23 PM	3:32 PM	3:43 PM	3:55 PM	4:10 PM
4:15 PM	4:23 PM	4:32 PM	4:43 PM	4:55 PM	5:10 PM
5:15 PM	5:23 PM	5:32 PM	5:43 PM	5:55 PM	6:10 PM
6:15 PM	6:23 PM	6:32 PM	6:43 PM	6:55 PM	7:10 PM
7:15 PM	7:23 PM	7:32 PM	7:43 PM	7:55 PM	8:10 PM
8:15 PM	8:23 PM	8:32 PM	8:38 PM		

#### To determine when the bus serves a location, match the numbers on the timetable to the numbers on the map these locations are called "timepoints ø 0 APP IN G WEEKDAY SCHEDULE DUC fit 76 0 00 0 AM 1090 1115 1122 1 1125 1145 11:52 E 00 1159 12:15 13:22 0 TI MEW DR West 0 P.M. 12:29 12:45 12:52 HS 12:59 1:15 1:22

How to Read this Schedule

To determine when the bus serves a stop in between timepoints, look at when it is due at the timepoint before your stop and the timepoint after your stop, and you can estimate when it will arrive. Always be at your stop 5 minutes early!

These symbols indicate transfer points or Superstops, which are specific stops where you can transfer to a different route. Routes serving a transfer point or Superstop are indicated at the top of the times schedule, just above the name of the stop.

#### Cómo leer este horario

Conecte el número dentro del círculo en el mapa con la columna del horano con el morno número para ver cuándo el bus para en ese lugar (esos lugares se llaman "timepoiros").

Para determinar cuándo un bus atiende una parada entre timepoints, mire a que hora debería llegar al timepoint antes de su parada y el timepoint después de su parada, y podra estimar la hora de llegada, jSiempre llegue a su parada con 5 minutos de antelacioni.

Estos simbolos indican puntos de trasbordo Superstops que son paradas específicas donde puedes trasbordar a una ruta diferente. Las rutas que atlenden un punto de trasbordo o Superstop están indicadas en la parte superior del horario, justo encima del nombre de la paradá.

#### ACCESSIBILITY

All KAT buses are lift-equipped. Paratransit service is also available to those who qualify. For more information, visit katbus.com or call 865-637-3000.

Bike racks are available on all KAT buses. Bikes ride free.



katbus.com • Customer Service: 865-637-3000

#### WEEKDAY Going away from downtown Going toward downtown **Boyds Bridge** Golden Age Kirkwood St Border St NB Knoxville Knoxville Pike EB and Retirement Superstop WB and Boyds Station Bay I Station Bay I Border St **Bridge Pike** Village Arrival Transfer to Rts. 31 & 34 1 2 3 4 5 6 5:43 AM 5:55 AM 6:10 AM 6:32 AM 6:15 AM 6:23 AM 6:43 AM 6:55 AM 7:10 AM 7:15 AM 7:23 AM 7:32 AM 7:43 AM 7:55 AM 8:10 AM 8:15 AM 8:23 AM 8:32 AM 8:43 AM 8:55 AM 9:10 AM 9:15 AM 9:23 AM 9:32 AM 9:43 AM 9:55 AM 10:10 AM 10:15 AM 10:23 AM 10:32 AM 10:43 AM 10:55 AM 11:10 AM 11:15 AM 11:23 AM 11:32 AM 11:43 AM 11:55 AM 12:10 PM 12:23 PM 12:15 PM 12:32 PM 12:43 PM 12:55 PM 1:10 PM 1:15 PM 1:23 PM 1:32 PM 1:43 PM 1:55 PM 2:10 PM 2:15 PM 2:23 PM 2:32 PM 2:43 PM 2:55 PM 3:10 PM 3:15 PM 3:23 PM 3:32 PM 3:43 PM 3:55 PM 4:10 PM 4:15 PM 4:23 PM 4:32 PM 4:43 PM 4:55 PM 5:10 PM 5:15 PM 5:23 PM 5:32 PM 5:43 PM 5:55 PM 6:10 PM 6:15 PM 6:23 PM 6:32 PM 6:43 PM 6:55 PM 7:10 PM 7:15 PM 7:23 PM 7:32 PM 7:43 PM 8:10 PM 7:55 PM 8:15 PM 8:23 PM 8:32 PM 8:38 PM

Route 32: Dandridge Avenue



APPENDIX C

ZONING MAP



APPENDIX D

MANUAL TRAFFIC COUNT DATA

#### TRAFFIC COUNT DATA

Major Street: Brooks Avenue (WB) and Dandridge Avenue (EB) Minor Street: Wilder Place (SB and NB) and Dandridge Avenue (NWB) Traffic Control: All-Way Stop Control

		Wilder	Place			Brooks	Avenue			Wilde	r Place			Dandrid	ge Avenue			Dandridg	ge Avenue		1	
TIME		SOUTHB	OUND			WESTE	BOUND			NORTH	IBOUND			EASTI	BOUND			NORTHW	ESTBOUND		VEHICLE	PEAK
BEGIN	LT	LT-THRU	THRU	RT	LT-LT	LT	THRU	RT	LT	THRU	RT	RT-RT	LT	THRU	THRU-RT	RT	LT	THRU	THRU-RT	RT	TOTAL	HOUR
7:00 AM	2	0	6	6	0	8	16	2	1	5	3	2	5	35	4	1	1	3	1	0	101	
7:15 AM	6	0	2	12	0	12	50	4	3	5	6	1	5	33	1	0	2	8	1	0	151	7:15 AM - 8:15 AM
7:30 AM	2	1	11	14	0	18	47	2	5	12	11	0	2	35	5	3	3	18	1	0	190	
7:45 AM	4	0	6	6	0	11	51	3	0	9	2	0	3	27	5	4	2	6	0	0	139	
8:00 AM	5	3	10	5	0	9	44	1	5	8	8	2	6	17	7	2	1	10	3	0	146	
8:15 AM	4	1	7	2	0	7	48	0	2	5	4	0	11	17	8	1	2	8	0	0	127	
8:30 AM	3	1	8	12	0	5	29	2	1	2	3	2	4	16	3	2	4	7	0	0	104	
8:45 AM	1	0	3	5	0	10	28	2	0	6	1	1	2	18	2	1	1	5	1	0	87	
TOTAL	27	6	53	62	0	80	313	16	17	52	38	8	38	198	35	14	16	65	7	0	1045	
2:00 PM	5	1	11	9	0	8	20	4	6	8	9	5	4	23	6	5	0	10	1	0	135	
2:15 PM	6	1	17	6	0	20	19	9	4	13	6	4	4	31	7	1	3	9	4	0	164	
2:30 PM	3	3	13	3	0	9	30	1	4	10	12	4	5	26	4	6	5	3	1	0	142	
2:45 PM	9	3	12	2	0	10	24	8	1	11	15	4	5	30	9	4	2	7	2	0	158	
3:00 PM	1	0	12	11	0	10	41	5	4	11	13	2	10	30	10	6	2	4	1	0	173	
3:15 PM	6	1	8	2	0	13	27	4	3	10	14	4	5	29	5	4	4	7	1	0	147	
3:30 PM	4	0	12	6	0	11	25	4	5	12	7	1	7	34	5	8	0	6	2	0	149	
3:45 PM	12	0	19	9	0	14	26	6	2	11	17	4	9	25	8	7	3	3	2	0	177	
4:00 PM	2	3	20	12	0	15	24	1	1	15	4	2	12	34	10	1	2	3	4	0	165	
4:15 PM	5	2	8	10	1	15	48	10	2	14	10	3	7	50	7	2	3	5	3	1	206	
4:30 PM	4	1	15	6	0	10	35	4	2	9	8	3	1	42	14	3	2	5	5	0	169	
4:45 PM	4	3	14	6	0	4	31	4	2	6	6	3	9	38	9	5	3	2	1	0	150	
5:00 PM	5	0	23	9	0	13	34	3	4	15	10	2	8	33	6	9	0	10	3	1	188	5:00 PM - 6:00 PM
5:15 PM	2	3	14	3	0	17	29	6	1	10	15	10	6	57	10	3	3	4	1	0	194	
5:30 PM	8	1	14	5	0	13	30	6	4	14	15	5	8	46	9	2	3	12	3	1	199	
5:45 PM	7	3	14	7	0	18	34	3	3	12	14	2	5	31	8	5	2	3	3	0	174	
TOTAL	83	25	226	106	1	200	477	78	48	181	175	58	105	559	127	71	37	93	37	3	2690	

#### 2024 AM Peak Hour

7:15 AM - 8:15 AM

	Wilder Place Brooks Avenue						Wilde	r Place			Dandridg	ge Avenue		Dandridge Avenue						
TIME		SOUTHB	OUND			WESTE	BOUND			NORTH	BOUND			EASTE	BOUND			NORTHW	ESTBOUND	
BEGIN	LT	LT-THRU	THRU	RT	LT-LT	LT	THRU	RT	LT	THRU	RT	RT-RT	LT	THRU	THRU-RT	RT	LT	THRU	THRU-RT	RT
7:15 AM	6	0	2	12	0	12	50	4	3	5	6	1	5	33	1	0	2	8	1	0
7:30 AM	2	1	11	14	0	18	47	2	5	12	11	0	2	35	5	3	3	18	1	0
7:45 AM	4	0	6	6	0	11	51	3	0	9	2	0	3	27	5	4	2	6	0	0
8:00 AM	5	3	10	5	0	9	44	1	5	8	8	2	6	17	7	2	1	10	3	0
TOTAL	17	4	29	37	0	50	192	10	13	34	27	3	16	112	18	9	8	42	5	0
TRUCK %	5.9%	0.0%	0.0%	2.7%	0.0%	0.0%	0.5%	0.0%	0.0%	2.9%	0.0%	0.0%	0.0%	2.7%	5.5%	0.0%	0.0%	0.0%	4.8%	0.0%
PHF mvmt	0.71	0.33	0.66	0.66	-	0.69	0.94	0.63	0.65	0.71	0.61	0.38	0.67	0.80	0.64	0.56	0.67	0.58	0.42	-
PHF app	0.78 0.94						0.69				0.86				0.63					
PHF int		0.82																		

#### 2024 PM Peak Hour

5:00 PM - 6:00 PM

	Wilder Place Brooks Avenue							Wilde	r Place			Dandridg	ge Avenue		Dandridge Avenue					
TIME		SOUTHB	OUND			WESTE	BOUND			NORTH	BOUND			EASTE	BOUND			NORTHW	ESTBOUND	
BEGIN	LT	LT-THRU	THRU	RT	LT-LT	LT	THRU	RT	LT	THRU	RT	RT-RT	LT	THRU	THRU-RT	RT	LT	THRU	THRU-RT	RT
5:00 PM	5	0	23	9	0	13	34	3	4	15	10	2	8	33	6	9	0	10	3	1
5:15 PM	2	3	14	3	0	17	29	6	1	10	15	10	6	57	10	3	3	4	1	0
5:30 PM	8	1	14	5	0	13	30	6	4	14	15	5	8	46	9	2	3	12	3	1
5:45 PM	7	3	14	7	0	18	34	3	3	12	14	2	5	31	8	5	2	3	3	0
TOTAL	22	7	65	24	0	61	127	18	12	51	54	19	27	167	33	19	8	29	10	2
TRUCK %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.8%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.6%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
PHF mvmt	0.69	0.58	0.71	0.67	-	0.85	0.93	0.75	0.75	0.85	0.90	0.48	0.84	0.73	0.83	0.53	0.67	0.60	0.83	0.50
PHF app	0.80 0.94				_	0.89			0.81				0.64							
PHF int		0.95																		



Major Street: Brooks Avenue (EB and WB) Minor Street: Riverside Road (NB) Traffic Control: Stop Sign on Minor Street 10/3/2024 (Thursday) Morning: Fog / Afternoon: Mostly Sunny Conducted by: Ajax Engineering

	Brooks	Avenue	Riversio	de Road	Brooks	Avenue		
TIME	WESTE	BOUND	NORTH	BOUND	EASTE	OUND	VEHICLE	PEAK
BEGIN	LT	THRU	LT	RT	THRU	RT	TOTAL	HOUR
7:00 AM	3	19	1	0	9	0	32	
7:15 AM	6	42	2	1	14	3	68	7:15 AM - 8:15 AM
7:30 AM	8	38	3	2	16	3	70	
7:45 AM	3	26	4	2	15	1	51	
8:00 AM	9	23	0	2	14	0	48	
8:15 AM	2	28	2	5	10	1	48	
8:30 AM	4	17	0	1	12	0	34	
8:45 AM	3	20	0	1	16	1	41	
TOTAL	38	213	12	14	106	9	392	
2:00 PM	0	12	0	1	8	0	21	
2:15 PM	3	16	0	3	20	1	43	
2:30 PM	4	11	2	3	14	2	36	
2:45 PM	2	15	3	1	11	2	34	
3:00 PM	1	28	1	3	15	6	54	
3:15 PM	3	11	2	5	15	4	40	
3:30 PM	4	14	1	2	18	1	40	
3:45 PM	2	15	2	5	10	2	36	
4:00 PM	1	20	2	5	15	1	44	
4:15 PM	3	15	0	6	27	3	54	
4:30 PM	2	15	4	1	31	2	55	
4:45 PM	5	13	2	3	18	4	45	
5:00 PM	4	13	2	2	19	2	42	5:00 PM - 6:00 PM
5:15 PM	1	23	3	6	33	3	69	
5:30 PM	6	12	1	0	21	4	44	
5:45 PM	4	20	2	6	25	3	60	
TOTAL	45	253	27	52	300	40	717	

2024 AM Peak Hour

# 7:15 AM - 8:15 AM

	Brooks	Avenue	Riversi	de Road	Brooks Avenue			
TIME	WESTE	BOUND	NORTH	IBOUND	EASTBOUND			
BEGIN	LT	THRU	LT	RT	THRU	RT		
7:15 AM	6	42	2	1	14	3		
7:30 AM	8	38	3	2	16	3		
7:45 AM	3	26	4	2	15	1		
8:00 AM	9	23	0	2	14	0		
TOTAL	26	129	9	7	59	7		
PHF	0.72	0.77	0.56	0.88	0.92	0.58		
Truck %	0.0% 0.8%		0.0%	14.3%	6.8%	0.0%		

2024 PM Peak Hour

5:00 PM - 6:00 PM

	Brooks	Avenue	Riversi	de Road	Brooks Avenue			
TIME	WESTE	BOUND	NORTH	IBOUND	EASTBOUND			
BEGIN	LT	THRU	LT	RT	THRU	RT		
5:00 PM	4	13	2	2	19	2		
5:15 PM	1	23	3	6	33	3		
5:30 PM	6	12	1	0	21	4		
5:45 PM	4	20	2	6	25	3		
TOTAL	15	68	8	14	98	12		
PHF	0.63	0.74	0.67	0.58	0.74	0.75		
Truck %	0.0%	1.5%	0.0%	0.0%	1.0%	0.0%		



# PEAK HOUR DATA

Major Street: Brooks Avenue (EB and WB) Minor Street: Riverside Road (NB) Traffic Control: Stop Sign on Minor Street 10/3/2024 (Thursday) Morning: Fog / Afternoon: Mostly Sunny Conducted by: Ajax Engineering





# TRAFFIC COUNT DATA

Major Street: Delrose Drive (WB and EB) Minor Street: Riverside Road (SB) Traffic Control: Stop Conditions on Minor Street 10/3/2024 (Thursday) Morning: Fog / Afternoon: Mostly Sunny Conducted by: Ajax Engineering

	Riversic	le Road	Delros	e Drive	Delros	e Drive		
TIME	SOUTH	BOUND	WESTE	OUND	EASTB	OUND	VEHICLE	PEAK
BEGIN	LT	RT	THRU	RT	LT	THRU	TOTAL	HOUR
7:00 AM	0	4	53	0	0	24	81	
7:15 AM	0	10	67	0	2	22	101	7:15 AM - 8:15 AM
7:30 AM	1	10	62	3	3	25	104	
7:45 AM	1	3	73	1	4	27	109	
8:00 AM	0	8	56	1	0	28	93	
8:15 AM	0	3	41	1	6	24	75	
8:30 AM	0	5	44	0	1	14	64	
8:45 AM	0	4	32	0	1	20	57	
TOTAL	2	47	428	6	17	184	684	
2:00 PM	0	0	35	0	0	24	59	
2:15 PM	0	4	28	2	1	26	61	
2:30 PM	1	4	37	0	4	36	82	
2:45 PM	1	3	45	0	3	29	81	
3:00 PM	1	3	34	1	3	36	78	
3:15 PM	1	5	29	1	4	48	88	
3:30 PM	1	4	38	1	2	38	84	
3:45 PM	0	4	22	0	8	57	91	
4:00 PM	1	2	33	0	6	58	100	
4:15 PM	0	5	39	0	6	48	98	
4:30 PM	1	4	48	1	4	47	105	
4:45 PM	1	8	32	1	5	56	103	
5:00 PM	0	6	42	0	4	82	134	5:00 PM - 6:00 PM
5:15 PM	1	1	57	1	5	74	139	
5:30 PM	0	8	46	0	1	64	119	
5:45 PM	0	6	43	0	8	48	105	
TOTAL	9	67	608	8	64	771	1527	

# 2024 AM Peak Hour

# 7:15 AM - 8:15 AM

	Riversio	de Road	Delros	e Drive	Delros	e Drive
TIME	SOUTH	BOUND	WESTE	BOUND	EASTB	OUND
BEGIN	LT	RT	THRU	RT	LT	THRU
7:15 AM	0	10	67	0	2	22
7:30 AM	1	10	62	3	3	25
7:45 AM	1	3	73	1	4	27
8:00 AM	0	8	56	1	0	28
TOTAL	2	31	258	5	9	102
PHF	0.50	0.78	0.88	0.42	0.56	0.91
TRUCK %	0.0%	0.0%	5.4%	0.0%	11.1%	2.9%

# 2024 PM Peak Hour

# 5:00 PM - 6:00 PM

	Riversie	de Road	Delros	e Drive	Delros	e Drive
TIME	SOUTH	BOUND	WESTE	BOUND	EASTB	OUND
BEGIN	LT	RT	THRU	RT	LT	THRU
5:00 PM	0	6	42	0	4	82
5:15 PM	1	1	57	1	5	74
5:30 PM	0	8	46	0	1	64
5:45 PM	0	6	43	0	8	48
TOTAL	1	21	188	1	18	268
PHF	0.25	0.66	0.82	0.25	0.56	0.82
TRUCK %	0.0%	0.0%	0.5%	0.0%	0.0%	0.4%



# PEAK HOUR DATA

Major Street: Delrose Drive (WB and EB) Minor Street: Riverside Road (SB) Traffic Control: Stop Conditions on Minor Street 10/3/2024 (Thursday) Morning: Fog / Afternoon: Mostly Sunny Conducted by: Ajax Engineering





# TRAFFIC COUNT DATA

Major Street: Delrose Drive (WB) and Riverside Drive (EB) Minor Street: Riverside Drive & Vulcan Materials Driveway (NWB) Traffic Control: Stop Sign on Minor Street 10/3/2024 (Thursday) Morning: Fog / Afternoon: Mostly Sunny Conducted by: Ajax Engineering

	Delros	e Drive	Riverside Drive & Vulo	an Materials Driveway	Riversi	de Drive		
TIME	WESTE	BOUND	NORTHWI	ESTBOUND	EASTE	OUND	VEHICLE	PEAK
BEGIN	LT	THRU	LT	RT	THRU	RT	TOTAL	HOUR
7:00 AM	0	49	6	0	23	7	85	
7:15 AM	0	79	5	0	25	2	111	7:15 AM - 8:15 AM
7:30 AM	0	69	9	0	29	6	113	
7:45 AM	1	82	9	0	29	3	124	
8:00 AM	0	64	12	0	29	5	110	
8:15 AM	0	50	6	1	25	4	86	
8:30 AM	0	55	5	0	15	5	80	
8:45 AM	0	35	5	0	21	3	64	
TOTAL	1	483	57	1	196	35	773	
					-			
2:00 PM	0	34	7	0	28	9	78	
2:15 PM	1	35	7	0	26	5	74	
2:30 PM	0	35	7	0	43	4	89	
2:45 PM	0	47	9	1	36	4	97	
3:00 PM	0	45	6	1	34	8	94	
3:15 PM	1	29	6	1	48	8	93	
3:30 PM	0	38	7	1	48	2	96	
3:45 PM	1	26	7	0	57	4	95	
4:00 PM	0	36	6	0	65	11	118	
4:15 PM	1	44	4	3	50	6	108	
4:30 PM	0	46	6	0	52	3	107	
4:45 PM	0	45	14	1	66	13	139	4:45 PM - 5:45 PM
5:00 PM	0	45	5	0	85	1	136	
5:15 PM	0	61	7	0	72	4	144	
5:30 PM	0	52	6	3	63	5	129	
5:45 PM	0	47	6	1	55	5	114	
TOTAL	4	665	110	12	828	92	1711	

# 2024 AM Peak Hour

# 7:15 AM - 8:15 AM

	Delros	e Drive	Riverside Drive & Vulo	can Materials Driveway	Riversic	le Drive
TIME	WESTE	OUND	NORTHWE	ESTBOUND	EASTB	OUND
BEGIN	LT	THRU	LT	RT	THRU	RT
7:15 AM	0	79	5	0	25	2
7:30 AM	0	69	9	0	29	6
7:45 AM	1	82	9	0	29	3
8:00 AM	0	64	12	0	29	5
TOTAL	1	294	35	0	112	16
PHF	0.25	0.90	0.73	-	0.97	0.67
Truck %	100.0%	5.4%	14.3%	0.0%	3.6%	18.8%

# 2024 PM Peak Hour

# 4:45 PM - 5:45 PM

	Delros	e Drive	Riverside Drive & Vulo	an Materials Driveway	Riversic	le Drive
TIME	WESTE	OUND	NORTHWI	ESTBOUND	EASTB	OUND
BEGIN	LT	THRU	LT	RT	THRU	RT
4:45 PM	0	45	14	1	66	13
5:00 PM	0	45	5	0	85	1
5:15 PM	0	61	7	0	72	4
5:30 PM	0	52	6	3	63	5
TOTAL	0	203	32	4	286	23
PHF	-	0.83	0.57	0.33	0.84	0.44
Truck %	0.0%	1.0%	0.0%	0.0%	0.7%	0.0%



# PEAK HOUR DATA

Major Street: Delrose Drive (WB) and Riverside Drive (EB) Minor Street: Riverside Drive & Vulcan Materials Driveway (NWB) Traffic Control: Stop Sign on Minor Street 10/3/2024 (Thursday) Morning: Fog / Afternoon: Mostly Sunny Conducted by: Ajax Engineering





**APPENDIX E** 

CAPACITY ANALYSES – HCM WORKSHEETS (SYNCHRO AND SIMTRAFFIC 12)

**EXISTING CONDITIONS** 

2: Wilder Place & Dandridge Avenue & Brooks Avenue Performanc	e bv lane
2. Milder Flace & Ballanage / Herlae & Breenae / Herlae Ferenae	o by lanc

Lane	EB	WB	NB	SB	NW	All
Movements Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr< td=""><td></td></lr<></td></ltr<>	<lr< td=""><td></td></lr<>	
Denied Del/Veh (s)						0.2
Total Del/Veh (s)	6.6	7.7	4.8	4.9	5.0	6.4

# Intersection

Int Delay, s/veh	1.2						
Movement	EBT	EBR	WBL	WBT	NWL	NWR	ł
Lane Configurations	et 👘			÷.	۰¥		
Traffic Vol, veh/h	112	16	1	294	35	0	)
Future Vol, veh/h	112	16	1	294	35	0	)
Conflicting Peds, #/hr	0	0	0	0	0	0	)
Sign Control	Free	Free	Free	Free	Stop	Stop	)
RT Channelized	-	None	-	None	-	None	÷
Storage Length	-	-	-	-	0	-	-
Veh in Median Storage	,# 0	-	-	0	0	-	-
Grade, %	0	-	-	-2	-2	-	-
Peak Hour Factor	97	67	25	90	73	90	)
Heavy Vehicles, %	4	19	100	5	14	0	)
Mvmt Flow	115	24	4	327	48	0	)

Majar/Minar	laiar1	N	Acier?		Vinor1	
	lajor1		/lajor2		Minor1	105
Conflicting Flow All	0	0	139	0	462	127
Stage 1	-	-	-	-	127	-
Stage 2	-	-	-	-	335	-
Critical Hdwy	-	-	5.1	-	6.14	6
Critical Hdwy Stg 1	-	-	-	-	5.14	-
Critical Hdwy Stg 2	-	-	-	-	5.14	-
Follow-up Hdwy	-	-	3.1	-	3.626	3.3
Pot Cap-1 Maneuver	-	-	1012	-	565	935
Stage 1	-	-	-	-	882	-
Stage 2	-	-	-	-	725	-
Platoon blocked, %	-	-		-	-	
Mov Cap-1 Maneuver	-	-	1012	-	562	935
Mov Cap-2 Maneuver	-	-	-	-	562	-
Stage 1	_	-	-	-	882	-
Stage 2	_	-	-	-	722	-
otago 2						
Approach	EB		WB		NW	
HCM Control Delay, s/v	0		0.1		12	
HCM LOS					В	
NA' I /NA - ' NA 1	•		EDT			
Minor Lane/Major Mvmt		IWLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		562	-	-	22	-
HCM Lane V/C Ratio		0.085	-	-	0.004	-
HCM Control Delay (s/v	reh)	12	-	-	8.6	0
HCM Lane LOS		В	-	-	Α	Α

0

-

-

0.3

-

HCM 95th %tile Q(veh)

# Intersection

Int Delay, s/veh	1.2					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		÷.	4Î		Y	
Traffic Vol, veh/h	9	102	258	5	2	31
Future Vol, veh/h	9	102	258	5	2	31
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	3	3	-	-3	-
Peak Hour Factor	56	91	88	42	50	78
Heavy Vehicles, %	11	3	5	0	0	0
Mvmt Flow	16	112	293	12	4	40

Major/Minor	Major1	Ν	/lajor2	1	Minor2	
Conflicting Flow All	305	0	-	0	443	299
Stage 1	-	-	-	-	299	-
Stage 2	-	-	-	-	144	-
Critical Hdwy	4.21	-	-	-	5.8	5.9
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	2.299	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1206	-	-	-		764
Stage 1	-	-	-	-	796	-
Stage 2	-	-	-	-	910	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	611	764
Mov Cap-2 Maneuver	r –	-	-	-	611	-
Stage 1	-	-	-	-	784	-
Stage 2	-	-	-	-	910	-
Approach	EB		WB		SB	
HCM Control Delay, s	s/v 1.01		0		10.12	
HCM LOS					В	
Minor Lane/Major Mv	mt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		226		_	-	747
HCM Lane V/C Ratio		0.013	-	-		0.059
HCM Control Delay (s			0	-	-	10.1
HCM Control Delay (s HCM Lane LOS		8 A	0 A	-	-	10.1 B

# Intersection

Int Delay, s/veh	1.7						
Movement	EBT	EBR	WBL	WBT	NBL	NBR	(
Lane Configurations	el 🗧			÷.	۰¥		
Traffic Vol, veh/h	59	7	26	129	9	7	,
Future Vol, veh/h	59	7	26	129	9	7	,
Conflicting Peds, #/hr	0	0	0	0	0	0	1
Sign Control	Free	Free	Free	Free	Stop	Stop	,
RT Channelized	-	None	-	None	-	None	÷
Storage Length	-	-	-	-	0	-	
Veh in Median Storage	,# 0	-	-	0	0	-	
Grade, %	1	-	-	-1	-3	-	
Peak Hour Factor	92	58	72	77	56	88	5
Heavy Vehicles, %	7	0	0	1	0	14	ł
Mvmt Flow	64	12	36	168	16	8	5

Major/Minor M	ajor1	Ν	/lajor2		Minor1	
Conflicting Flow All	0	0	76	0	310	70
Stage 1	-	-	-	-	70	-
Stage 2	-	-	-	-	240	-
Critical Hdwy	-	-	4.1	-	5.8	6.04
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	-	-	2.2	-	3.5	3.426
Pot Cap-1 Maneuver	-	-	1536	-	723	966
Stage 1	-	-	-	-	969	-
Stage 2	-	-	-	-	838	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1536	-	704	966
Mov Cap-2 Maneuver	-	-	-	-	704	-
Stage 1	-	-	-	-	969	-
Stage 2	-	-	-	-	816	-
Approach	EB		WB		NB	
HCM Control Delay, s/v	0		1.31		9.8	
HCM LOS	-				A	
Miner Lene (Meier Munet			ГОТ			
Minor Lane/Major Mvmt		NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		774	-	-	319	-
HCM Lane V/C Ratio	. 1. \	0.031	-		0.024	-
HCM Control Delay (s/ve	en)	9.8	-	-	7.4	0
HCM Lane LOS		A 0.1	-	-	A	A
HCM 95th %tile Q(veh)		0.1	-	-	0.1	-
Lane	EB	WB	NB	SB	NW	All
--------------------	------	-----	------	------------------------------------------------	-----------	-----
Movements Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr></lr></td><td></td></ltr<>	<lr></lr>	
Denied Del/Veh (s)						0.2
Total Del/Veh (s)	8.0	7.6	5.7	6.3	5.4	7.0

Int Delay, s/veh	1.3					
Movement	EBT	EBR	WBL	WBT	NWL	NWR
Lane Configurations	et -			÷.	۰¥	
Traffic Vol, veh/h	286	23	0	203	32	4
Future Vol, veh/h	286	23	0	203	32	4
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	-2	-2	-
Peak Hour Factor	84	44	90	83	57	33
Heavy Vehicles, %	1	0	0	1	0	0
Mvmt Flow	340	52	0	245	56	12

Major/Minor N	/lajor1	Ν	/lajor2	1	Minor1	
Conflicting Flow All	0	0	393	0	611	367
Stage 1	-	-	-	-	367	-
Stage 2	-	-	-	-	245	-
Critical Hdwy	-	-	4.1	-	6	6
Critical Hdwy Stg 1	-	-	-	-	5	-
Critical Hdwy Stg 2	-	-	-	-	5	-
Follow-up Hdwy	-	-	2.2	-	3.5	3.3
Pot Cap-1 Maneuver	-	-	1177	-	493	697
Stage 1	-	-	-	-	735	-
Stage 2	-	-	-	-	823	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1177	-	493	697
Mov Cap-2 Maneuver	-	-	-	-	493	-
Stage 1	-	-	-	-	735	-
Stage 2	-	-	-	-	823	-
Approach	EB		WB		NW	
HCM Control Delay, s/v			0		12.97	
HCM LOS	Ū		U		B	
					5	
Minor Lane/Major Mvm	t N	IWLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		520	-	-	1177	-
HCM Lane V/C Ratio		0.131	-	-	-	-
HCM Control Delay (s/v	/eh)	13	-	-	0	-
HCM Lane LOS		В	-	-	A	-
HCM 95th %tile Q(veh)		0.5	-	-	0	-

1

### Intersection

-						
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		÷.	4Î		Y	
Traffic Vol, veh/h	18	268	188	1	1	21
Future Vol, veh/h	18	268	188	1	1	21
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	, # -	0	0	-	0	-
Grade, %	-	3	3	-	-3	-
Peak Hour Factor	56	82	82	25	25	66
Heavy Vehicles, %	0	0	1	0	0	0
Mvmt Flow	32	327	229	4	4	32

Major/Minor	Major1	Ν	/lajor2	I	Minor2	
Conflicting Flow All	233	0	-	0	622	231
Stage 1	-	-	-	-	231	-
Stage 2	-	-	-	-	391	-
Critical Hdwy	4.1	-	-	-	5.8	5.9
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1346	-	-	-	503	829
Stage 1	-	-	-	-	844	-
Stage 2	-	-	-	-	734	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	488	829
Mov Cap-2 Maneuver	-	-	-	-	488	-
Stage 1	-	-	-	-	819	-
Stage 2	-	-	-	-	734	-
Approach	EB		WB		SB	
HCM Control Delay, s	/v 0.69		0		9.91	
HCM LOS					А	
Minor Lane/Major Mvr	nt	EBL	EBT	WBT	WBR S	BLn1
Capacity (veh/h)		161	-	-	-	769
HCM Lane V/C Ratio		0.024	-	-	-	0.047
HCM Control Delay (s	/veh)	7.7	0	-	-	9.9
HCM Lane LOS	,	А	А	-	-	А
HCM 95th %tile Q(veh	า)	0.1	-	-	-	0.1

Int Delay, s/veh	1.7					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	4Î -			÷.	Y	
Traffic Vol, veh/h	98	12	15	68	8	14
Future Vol, veh/h	98	12	15	68	8	14
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	1	-	-	-1	-3	-
Peak Hour Factor	74	75	63	74	67	58
Heavy Vehicles, %	1	0	0	2	0	0
Mvmt Flow	132	16	24	92	12	24

Major/Minor	Major	1 _	Major2		Minor1	
Conflicting Flow All		0 0	148	0	280	140
Stage 1			-	-	140	-
Stage 2			-	-	140	-
Critical Hdwy			4.1	-		5.9
Critical Hdwy Stg 1			-	-	4.8	-
Critical Hdwy Stg 2			-	-	4.8	-
Follow-up Hdwy			2.2	-	3.5	3.3
Pot Cap-1 Maneuver			1445	-	748	924
Stage 1			-	-	912	-
Stage 2			-	-	913	-
Platoon blocked, %				-		
Mov Cap-1 Maneuver			1445	-	735	924
Mov Cap-2 Maneuver			-	-	735	-
Stage 1			-	-	912	-
Stage 2			-	-	897	-
Approach	E	3	WB		NB	
HCM Control Delay, s		0	1.55		9.41	
HCM LOS		•	1.00		A	
					71	
			EDT	500		WDT
Minor Lane/Major Mvn	nt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		851	-	-	370	-
HCM Lane V/C Ratio		0.042	-		0.016	-
HCM Control Delay (s	/veh)	9.4	-	-	1.0	0
HCM Lane LOS	`	A	-	-	A	A
HCM 95th %tile Q(veh	1)	0.1	-	-	0.1	-

**PROJECTED CONDITIONS WITHOUT THE PROJECT** 

6.7

8.0

Denied Del/Veh (s) Total Del/Veh (s)

2: Wilder Place & [	Dandridg	e Ave	nue &	Brooks	s Avenu	ie Perfo	ormance by l	ane	
Lane	EB	WB	NB	SB	NW	All			
Movements Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr< td=""><td></td><td></td><td></td><td></td></lr<></td></ltr<>	<lr< td=""><td></td><td></td><td></td><td></td></lr<>				

5.1

5.0

0.2

6.6

5.0

Int Delay, s/veh	1.2						
Movement	EBT	EBR	WBL	WBT	NWL	NWR	(
Lane Configurations	et -			÷.	۰¥		
Traffic Vol, veh/h	122	17	1	320	38	0	)
Future Vol, veh/h	122	17	1	320	38	0	1
Conflicting Peds, #/hr	0	0	0	0	0	0	1
Sign Control	Free	Free	Free	Free	Stop	Stop	,
RT Channelized	-	None	-	None	-	None	÷
Storage Length	-	-	-	-	0	-	
Veh in Median Storage	,# 0	-	-	0	0	-	
Grade, %	0	-	-	-2	-2	-	
Peak Hour Factor	97	67	25	90	73	90	)
Heavy Vehicles, %	4	19	100	5	14	0	)
Mvmt Flow	126	25	4	356	52	0	1

Major/Minor N	lajor1	Ν	/lajor2		Minor1	
Conflicting Flow All	0	0	151	0	502	138
Stage 1	-	-	-	-	138	-
Stage 2	-	-	-	-	364	-
Critical Hdwy	-	-	5.1	-		6
Critical Hdwy Stg 1	-	-	-	-	5.14	-
Critical Hdwy Stg 2	-	-	-	-		-
Follow-up Hdwy	-	-	3.1	-	3.626	3.3
Pot Cap-1 Maneuver	-	-	1000	-	537	922
Stage 1	-	-	-	-	873	-
Stage 2	-	-	-	-	706	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1000	-	535	922
Mov Cap-2 Maneuver	-	-	-	-	535	-
Stage 1	-	-	-	-	873	-
Stage 2	-	-	-	-	702	-
Approach	EB		WB		NW	
HCM Control Delay, s/v			0.1		12.46	
HCM LOS	v		0.1		B	
					_	
			FDT			WDT
Minor Lane/Major Mvmt	N	IWLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		535	-	-	20	-
HCM Lane V/C Ratio		0.097	-		0.004	-
HCM Control Delay (s/v	eh)	12.5	-	-	•.•	0
HCM Lane LOS		В	-	-	A	А
HCM 95th %tile Q(veh)		0.3	-	-	0	-

Int Delay, s/veh	1.2					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		÷.	4Î		Y	
Traffic Vol, veh/h	10	111	281	5	2	33
Future Vol, veh/h	10	111	281	5	2	33
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	3	3	-	-3	-
Peak Hour Factor	56	91	88	42	50	78
Heavy Vehicles, %	11	3	5	0	0	0
Mvmt Flow	18	122	319	12	4	42

Major/Minor	Major1	Ν	/lajor2	1	Minor2	
Conflicting Flow All	331	0	· -	0	483	325
Stage 1	-	-	-	-	325	-
Stage 2	-	-	-	-	158	-
Critical Hdwy	4.21	-	-	-	5.8	5.9
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	2.299	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1179	-	-	-	592	740
Stage 1	-	-	-	-	778	-
Stage 2	-	-	-	-	899	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	582	740
Mov Cap-2 Maneuver	· -	-	-	-	582	-
Stage 1	-	-	-	-	765	-
Stage 2	-	-	-	-	899	-
Approach	EB		WB		SB	
HCM Control Delay, s	s/v 1.03		0		10.32	
HCM LOS					В	
Minor Lane/Major Mvi	mt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		230	-	-	-	723
HCM Lane V/C Ratio		0.015	-	-	-	0.064
HCM Control Delay (s	s/veh)	8.1	0	-	-	10.3
HCM Lane LOS		А	А	-	-	В
HCM 95th %tile Q(vel	h)	0	-	-	-	0.2

Int Delay, s/veh	1.7						
Movement	EBT	EBR	WBL	WBT	NBL	NBR	(
Lane Configurations	et -			÷.	۰¥		
Traffic Vol, veh/h	63	7	28	137	10	7	,
Future Vol, veh/h	63	7	28	137	10	7	,
Conflicting Peds, #/hr	0	0	0	0	0	0	1
Sign Control	Free	Free	Free	Free	Stop	Stop	1
RT Channelized	-	None	-	None	-	None	÷
Storage Length	-	-	-	-	0	-	•
Veh in Median Storage	,# 0	-	-	0	0	-	
Grade, %	1	-	-	-1	-3	-	
Peak Hour Factor	92	58	72	77	56	88	5
Heavy Vehicles, %	7	0	0	1	0	14	ł
Mvmt Flow	68	12	39	178	18	8	;

Major/Minor Ma	ajor1	Ν	/lajor2	1	Minor1	
Conflicting Flow All	0	0	81	0	330	75
Stage 1	-	-	-	-	75	-
Stage 2	-	-	-	-	256	-
Critical Hdwy	-	-	4.1	-	5.8	6.04
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	-	-	2.2	-	3.5	3.426
Pot Cap-1 Maneuver	-	-	1530	-	706	961
Stage 1	-	-	-	-	965	-
Stage 2	-	-	-	-	826	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1530	-	686	961
Mov Cap-2 Maneuver	-	-	-	-	686	-
Stage 1	-	-	-	-	965	-
Stage 2	-	-	-	-	803	-
Approach	EB		WB		NB	
HCM Control Delay, s/v	0		1.33		9.95	
HCM LOS	-				A	
Minor Long/Major Murat			ГРТ			
Minor Lane/Major Mvmt		NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		753	-	-	323	-
HCM Lane V/C Ratio	L- )	0.034	-		0.025	-
HCM Control Delay (s/ve HCM Lane LOS	en)	10	-	-	7.4	0
		A 0.1	-	-	A 0.1	А
HCM 95th %tile Q(veh)		0.1	-	-	0.1	-

Lane	EB	WB	NB	SB	NW	All
Movements Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr></lr></td><td></td></ltr<>	<lr></lr>	
Denied Del/Veh (s)						0.2
Total Del/Veh (s)	8.5	7.9	5.8	6.2	5.4	7.3

Int Delay, s/veh	1.3						
Movement	EBT	EBR	WBL	WBT	NWL	NWR	ł
Lane Configurations	et 👘			÷.	۰¥		
Traffic Vol, veh/h	312	25	0	221	35	4	ł
Future Vol, veh/h	312	25	0	221	35	4	ŀ
Conflicting Peds, #/hr	0	0	0	0	0	0	)
Sign Control	Free	Free	Free	Free	Stop	Stop	)
RT Channelized	-	None	-	None	-	None	÷
Storage Length	-	-	-	-	0	-	-
Veh in Median Storage	,# 0	-	-	0	0	-	-
Grade, %	0	-	-	-2	-2	-	-
Peak Hour Factor	84	44	90	83	57	33	5
Heavy Vehicles, %	1	0	0	1	0	0	)
Mvmt Flow	371	57	0	266	61	12	2

Major/Minor M	/lajor1	Ν	/lajor2	Ν	Ainor1	
Conflicting Flow All	0		428	0	666	400
Stage 1	-	· -	-	-	400	-
Stage 2	-		-	-	266	-
Critical Hdwy	-		4.1	-	6	6
Critical Hdwy Stg 1	-		-	-	5	-
Critical Hdwy Stg 2	-		-	-	5	-
Follow-up Hdwy	-		2.2	-	3.5	3.3
Pot Cap-1 Maneuver	-		1142	-	460	669
Stage 1	-		-	-	712	-
Stage 2	-		-	-	807	-
Platoon blocked, %	-			-		
Mov Cap-1 Maneuver	-		1142	-	460	669
Mov Cap-2 Maneuver	-		-	-	460	-
Stage 1	-		-	-	712	-
Stage 2	-		-	-	807	-
Approach	EB	}	WB		NW	
HCM Control Delay, s/v	<i>/</i> 0	)	0		13.74	
HCM LOS					В	
Minor Lane/Major Mvmt	ł	NWLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	ι <u></u>	485	-	-	1142	-
HCM Lane V/C Ratio		0.151	-	-	-	-
HCM Control Delay (s/v	(ph)	13.7	_	-	0	-
HCM Lane LOS	/611)	13.7 B	_	-	A	-
HCM 95th %tile Q(veh)		0.5	_	-	0	-

Int Delay, s/veh	0.9					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		÷.	4Î		Y	
Traffic Vol, veh/h	19	292	205	1	1	22
Future Vol, veh/h	19	292	205	1	1	22
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	,# -	0	0	-	0	-
Grade, %	-	3	3	-	-3	-
Peak Hour Factor	56	82	82	25	25	66
Heavy Vehicles, %	0	0	1	0	0	0
Mvmt Flow	34	356	250	4	4	33

Major/Minor	Major1	Ν	lajor2	Ν	Minor2	
Conflicting Flow All	254	0	-	0	676	252
Stage 1	-	-	-	-	252	-
Stage 2	-	-	-	-	424	-
Critical Hdwy	4.1	-	-	-	5.8	5.9
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1323	-	-	-	472	808
Stage 1	-	-	-	-	829	-
Stage 2	-	-	-	-	713	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	457	808
Mov Cap-2 Maneuver	• -	-	-	-	457	-
Stage 1	-	-	-	-	802	-
Stage 2	-	-	-	-	713	-
Approach	EB		WB		SB	
HCM Control Delay, s	s/v 0.68		0		10.07	
HCM LOS					В	
Minor Lane/Major Mvi	mt	EBL	EBT	WBT	WBR S	BLn1
Capacity (veh/h)		157	-	-	-	747
HCM Lane V/C Ratio		0.026	-	-	-	0.05
HCM Control Delay (s	s/veh)	7.8	0	-	-	10.1
HCM Lane LOS		А	А	-	-	В
HCM 95th %tile Q(vel	h)	0.1	-	-	-	0.2

Int Delay, s/veh	1.7					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	et			ŧ	Y	
Traffic Vol, veh/h	104	13	16	72	8	15
Future Vol, veh/h	104	13	16	72	8	15
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	1	-	-	-1	-3	-
Peak Hour Factor	74	75	63	74	67	58
Heavy Vehicles, %	1	0	0	2	0	0
Mvmt Flow	141	17	25	97	12	26

Major/Minor M	Major1		Major2		Minor1	
Conflicting Flow All	(		158	0	297	149
Stage 1			-	-	149	-
Stage 2			-	-	148	-
Critical Hdwy			4.1	-	5.8	5.9
Critical Hdwy Stg 1			-	-	4.8	-
Critical Hdwy Stg 2			-	-	4.8	-
Follow-up Hdwy			2.2	-	3.5	3.3
Pot Cap-1 Maneuver			1434	-	734	914
Stage 1			-	-	906	-
Stage 2			-	-	907	-
Platoon blocked, %				-		
Mov Cap-1 Maneuver			1434	-	720	914
Mov Cap-2 Maneuver			-	-	720	-
Stage 1			-	-	906	-
Stage 2			-	-	890	-
Approach	EE	}	WB		NB	
HCM Control Delay, s/\	/ (	)	1.56		9.47	
HCM LOS					A	
			ГРТ			
Minor Lane/Major Mvm	It	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		842	-	-	373	-
HCM Lane V/C Ratio	. 1. \	0.045	-		0.018	-
HCM Control Delay (s/	ven)	9.5	-	-	7.6	0
HCM Lane LOS		A	-	-	A	A
HCM 95th %tile Q(veh)		0.1	-	-	0.1	-

**PROJECTED CONDITIONS WITH THE PROJECT** 

2: Wilder Place & Dan	dridge	e Avenu	ie & Bi	rooks	Avenue	Performance	by lane
•				~ -			

Lane	EB	WB	NB	SB	NW	All	
Movements Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr< td=""><td></td><td></td></lr<></td></ltr<>	<lr< td=""><td></td><td></td></lr<>		
Denied Del/Veh (s)						0.2	
Total Del/Veh (s)	7.2	8.9	5.3	5.4	5.7	7.3	

Int Delay, s/veh	1.1					
Movement	EBT	EBR	WBL	WBT	NWL	NWR
Lane Configurations	ef –			÷.	۰¥	
Traffic Vol, veh/h	164	17	1	474	38	0
Future Vol, veh/h	164	17	1	474	38	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	-2	-2	-
Peak Hour Factor	97	67	25	90	73	90
Heavy Vehicles, %	4	19	100	5	14	0
Mvmt Flow	169	25	4	527	52	0

Major/Minor M	Major1	Ν	/lajor2	1	Minor1	
Conflicting Flow All	0	0	194	0	716	182
Stage 1	-	-	-	-	182	-
Stage 2	-	-	-	-	535	-
Critical Hdwy	-	-	5.1	-		6
Critical Hdwy Stg 1	-	-	-	-	5.14	-
Critical Hdwy Stg 2	-	-	-	-	5.14	-
Follow-up Hdwy	-	-	3.1	-	3.626	3.3
Pot Cap-1 Maneuver	-	-	958	-		875
Stage 1	-	-	-	-	838	-
Stage 2	-	-	-	-	598	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	958	-	408	875
Mov Cap-2 Maneuver	-	-	-	-	408	-
Stage 1	-	-	-	-	838	-
Stage 2	-	-	-	-	595	-
Approach	EB		WB		NW	
HCM Ctrl Dly, s/v	0		0.07		15.1	
HCM LOS	U		0.07		C	
					0	
Minor Lane/Major Mvm	t N\	NLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		408	-	-	14	-
HCM Lane V/C Ratio	(	0.128	-	-	0.004	-
HCM Ctrl Dly (s/v)		15.1	-	-	8.8	0
HCM Lane LOS		С	-	-	A	А
HCM 95th %tile Q(veh)		0.4	-	-	0	-

Int Delay, s/veh	1.5					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		÷.	4Î		Y	
Traffic Vol, veh/h	14	151	293	7	9	34
Future Vol, veh/h	14	151	293	7	9	34
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	3	3	-	-3	-
Peak Hour Factor	56	91	88	42	50	78
Heavy Vehicles, %	11	3	5	0	0	0
Mvmt Flow	25	166	333	17	18	44

Major/Minor	Major1	Ν	/lajor2		Minor2	
Conflicting Flow All	350	0	-	0	557	341
Stage 1	-	-	-	-	341	-
Stage 2	-	-	-	-	216	-
Critical Hdwy	4.21	-	-	-	5.8	5.9
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	2.299	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1161	-	-	-	543	726
Stage 1	-	-	-	-	767	-
Stage 2	-	-	-	-	855	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	530	726
Mov Cap-2 Maneuver	-	-	-	-	530	-
Stage 1	-	-	-	-	749	-
Stage 2	-	-	-	-	855	-
Approach	EB		WB		SB	
HCM Ctrl Dly, s/v	1.07		0		11.06	
HCM LOS					В	
Minor Lane/Major Mvn	nt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)		236	-	-	-	655
HCM Lane V/C Ratio		0.022	-	-	-	0.094
HCM Ctrl Dly (s/v)		8.2	0	-	-	11.1
HCM Lane LOS		А	А	-	-	В
HCM 95th %tile Q(veh	ר)	0.1	-	-	-	0.3

Int Delay, s/veh 2.9 EBT EBR WBL WBT NBL NBR Movement Y Lane Configurations Þ đ 63 22 Traffic Vol, veh/h 10 34 137 31 Future Vol, veh/h 63 10 34 137 22 31 0 Conflicting Peds, #/hr 0 0 0 0 0 Sign Control Free Free Free Free Stop Stop RT Channelized -None -None -None Storage Length 0 --\_ --Veh in Median Storage, # 0 --0 0 -Grade, % -1 1 -3 --\_ Peak Hour Factor 77 92 58 72 56 88 Heavy Vehicles, % 7 0 0 0 14 1 Mvmt Flow 68 17 47 178 39 35

Major/Minor M	1ajor1	Ν	/lajor2	1	Minor1	
Conflicting Flow All	0	0	86	0	349	77
Stage 1	-	-	-	-	77	-
Stage 2	-	-	-	-	272	-
Critical Hdwy	-	-	4.1	-	5.8	6.04
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	-	-	2.2	-		3.426
Pot Cap-1 Maneuver	-	-	1523	-	691	958
Stage 1	-	-	-	-	963	-
Stage 2	-	-	-	-	814	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1523	-	667	958
Mov Cap-2 Maneuver	-	-	-	-	667	-
Stage 1	-	-	-	-	963	-
Stage 2	-	-	-	-	786	-
Approach	EB		WB		NB	
Approach						
HCM Ctrl Dly, s/v	0		1.56		10.11	
HCM LOS					В	
Minor Lane/Major Mvmt	. N	IBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		779	-	-	378	-
HCM Lane V/C Ratio		0.096	-	-	0.031	-
HCM Ctrl Dly (s/v)		10.1	-	-	7.4	0
HCM Lane LOS		В	-	-	А	А
HCM 95th %tile Q(veh)		0.3	-	-	0.1	-

Int Delay, s/veh	3.4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	۰Y			ŧ	4Î	
Traffic Vol, veh/h	32	7	2	23	36	8
Future Vol, veh/h	32	7	2	23	36	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e, # 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	36	8	2	26	40	9

Major/Minor	Minor2	I	Major1	Maj	jor2	
Conflicting Flow All	74	44	49	0	-	0
Stage 1	44	-	-	-	-	-
Stage 2	30	-	-	-	-	-
Critical Hdwy	6.4	6.2	4.1	-	-	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	2.2	-	-	-
Pot Cap-1 Maneuver	934	1031	1571	-	-	-
Stage 1	983	-	-	-	-	-
Stage 2	998	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuve	r 933	1031	1571	-	-	-
Mov Cap-2 Maneuve	r 933	-	-	-	-	-
Stage 1	982	-	-	-	-	-
Stage 2	998	-	-	-	-	-

Approach	EB	NB	SB
HCM Ctrl Dly, s/v	8.97	0.58	0
HCM LOS	А		

Minor Lane/Major Mvmt	NBL	NBT E	EBLn1	SBT	SBR
Capacity (veh/h)	144	-	949	-	-
HCM Lane V/C Ratio	0.001	-	0.046	-	-
HCM Ctrl Dly (s/v)	7.3	0	9	-	-
HCM Lane LOS	А	А	А	-	-
HCM 95th %tile Q(veh)	0	-	0.1	-	-

Int Delay, s/veh	1.3					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		ŧ	4Î		Y	
Traffic Vol, veh/h	15	148	413	2	6	55
Future Vol, veh/h	15	148	413	2	6	55
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	91	88	90	90	90
Heavy Vehicles, %	0	3	5	0	0	0
Mvmt Flow	17	163	469	2	7	61

Major/Minor	Major1	Ν	lajor2		Minor2	
Conflicting Flow All	472	0	-	0	666	470
Stage 1	-	-	-	-	470	-
Stage 2	-	-	-	-	196	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1101	-	-	-		597
Stage 1	-	-	-	-	633	-
Stage 2	-	-	-	-	842	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	420	597
Mov Cap-2 Maneuver	r -	-	-	-	420	-
Stage 1	-	-	-	-	622	-
Stage 2	-	-	-	-	842	-
Approach	EB		WB		SB	
HCM Ctrl Dly, s/v	0.77		0		12.12	
HCM LOS					В	
Minor Lane/Major Mvi	mt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		167	-	-	-	574
HCM Lane V/C Ratio		0.015	-	-	-	0.118
HCM Ctrl Dly (s/v)		8.3	0	-	-	12.1
HCM Lane LOS		А	А	-	-	В
HCM 95th %tile Q(vel	h)	0	-	-	-	0.4

Intersection						
Int Delay, s/veh	3.2					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
	EDL	EDI	VVDI	WDR		JDR
Lane Configurations		- सी	- î÷		- Y	
Traffic Vol, veh/h	27	127	316	11	38	99
Future Vol, veh/h	27	127	316	11	38	99
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	91	88	90	90	90
Heavy Vehicles, %	0	3	5	0	0	0
Mvmt Flow	30	140	359	12	42	110

Major/Minor	Major1	Ν	/lajor2	1	Vinor2	
Conflicting Flow All	371	0	· -	0	565	365
Stage 1	-	-	-	-	365	-
Stage 2	-	-	-	-	200	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1198	-	-	-	490	684
Stage 1	-	-	-	-	707	-
Stage 2	-	-	-	-	839	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1198	-	-	-	476	684
Mov Cap-2 Maneuver	• -	-	-	-	476	-
Stage 1	-	-	-	-	687	-
Stage 2	-	-	-	-	839	-
Approach	EB		WB		SB	
HCM Ctrl Dly, s/v	1.43		0		12.84	
HCM LOS			Ū		B	
					_	
Miner Lene (Meier Ma	t		гот			1
Minor Lane/Major Mv	mt	EBL	EBT	WBT	WBR	
Capacity (veh/h)		318	-	-	-	610
HCM Lane V/C Ratio		0.025	-	-		0.249
HCM Ctrl Dly (s/v)		8.1	0	-	-	12.8
HCM Lane LOS		A	A	-	-	В
HCM 95th %tile Q(vel	n)	0.1	-	-	-	1

Lane	EB	WB	NB	SB	NW	All
Movements Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr></lr></td><td></td></ltr<>	<lr></lr>	
Denied Del/Veh (s)						0.2
Total Del/Veh (s)	10.1	8.8	6.3	7.3	6.6	8.4

Int Delay, s/veh	1.3					
Movement	EBT	EBR	WBL	WBT	NWL	NWR
Lane Configurations	et -			÷.	۰¥	
Traffic Vol, veh/h	462	25	0	348	35	4
Future Vol, veh/h	462	25	0	348	35	4
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	-2	-2	-
Peak Hour Factor	84	44	90	83	57	33
Heavy Vehicles, %	1	0	0	1	0	0
Mvmt Flow	550	57	0	419	61	12

Major/Minor	Major	1 .	Major2	1	Minor1	
Conflicting Flow All		) 0	607	0	998	578
Stage 1			-	-	578	-
Stage 2			-	-	419	-
Critical Hdwy			4.1	-	6	6
Critical Hdwy Stg 1			-	-	5	-
Critical Hdwy Stg 2			-	-	5	-
Follow-up Hdwy			2.2	-	3.5	3.3
Pot Cap-1 Maneuver			981	-	305	536
Stage 1			-	-	602	-
Stage 2			-	-	700	-
Platoon blocked, %				-		
Mov Cap-1 Maneuver			981	-	305	536
Mov Cap-2 Maneuver			-	-	305	-
Stage 1			-	-	602	-
Stage 2			-	-	700	-
Approach	EE	3	WB		NW	
HCM Ctrl Dly, s/v	(	)	0		19.12	
HCM LOS			-		С	
Miner Long /Maier Mur			ГРТ			
Minor Lane/Major Mvr	nt	NWLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		328	-	-	981	-
HCM Lane V/C Ratio		0.224	-	-	-	-
HCM Ctrl Dly (s/v)		19.1	-	-	0	-
HCM Lane LOS	•	C 0.8	-	-	A 0	-
HCM 95th %tile Q(veh	1)	0.0	-	-	0	-

Int Delay, s/veh	1.4					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		÷.	4Î		Y	
Traffic Vol, veh/h	22	325	244	8	7	25
Future Vol, veh/h	22	325	244	8	7	25
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	3	3	-	-3	-
Peak Hour Factor	56	82	82	25	25	66
Heavy Vehicles, %	0	0	1	0	0	0
Mvmt Flow	39	396	298	32	28	38

Major/Minor	Major1	Ν	/lajor2		Minor2	
Conflicting Flow All	330	0	-	0	788	314
Stage 1	-	-	-	-	314	-
Stage 2	-	-	-	-	475	-
Critical Hdwy	4.1	-	-	-	5.8	5.9
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1241	-	-	-	413	751
Stage 1	-	-	-	-	786	-
Stage 2	-	-	-	-	682	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	397	751
Mov Cap-2 Maneuver	· –	-	-	-	397	-
Stage 1	-	-	-	-	754	-
Stage 2	-	-	-	-	682	-
Approach	EB		WB		SB	
HCM Ctrl Dly, s/v	0.72		0		12.52	
HCM LOS					В	
Minor Lane/Major Mvr	mt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)		162	-	-	-	544
HCM Lane V/C Ratio		0.032	-	-	-	0.121
HCM Ctrl Dly (s/v)		8	0	-	-	12.5
						_
HCM Lane LOS		Α	А	-	-	В

Int Delay, s/veh 3.2 EBT EBR WBL WBT NBL NBR Movement **Y** 17 Lane Configurations Þ đ Traffic Vol, veh/h 104 72 24 39 35 Future Vol, veh/h 104 24 39 72 17 35 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Free Free Free Free Stop Stop RT Channelized -None -None -None Storage Length 0 --\_ --Veh in Median Storage, # 0 --0 0 -Grade, % 1 -1 -3 ---Peak Hour Factor 74 74 75 63 67 58 Heavy Vehicles, % 1 0 0 2 0 0 Mvmt Flow 141 32 62 97 25 60

Major/Minor M	1ajor1	Ν	/lajor2	1	Minor1	
Conflicting Flow All	0	0	173	0	378	157
Stage 1	-	-	-	-	157	-
Stage 2	-	-	-	-	221	-
Critical Hdwy	-	-	4.1	-	5.8	5.9
Critical Hdwy Stg 1	-	-	-	-	4.8	-
Critical Hdwy Stg 2	-	-	-	-	4.8	-
Follow-up Hdwy	-	-	2.2	-	3.5	3.3
Pot Cap-1 Maneuver	-	-	1417	-	669	906
Stage 1	-	-	-	-	900	-
Stage 2	-	-	-	-	851	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1417	-	638	906
Mov Cap-2 Maneuver	-	-	-	-	638	-
Stage 1	-	-	-	-	900	-
Stage 2	-	-	-	-	812	-
Approach	EB		WB		NB	
HCM Ctrl Dly, s/v	0		2.98		10	
HCM LOS	U		2.90		A	
					A	
Minor Lane/Major Mvmt	: N	VBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		806	-	-	700	-
HCM Lane V/C Ratio		0.106	-	-	0.044	-
HCM Ctrl Dly (s/v)		10	-	-	7.7	0
HCM Lane LOS		А	-	-	А	А
HCM 95th %tile Q(veh)		0.4	-	-	0.1	-

#### Intersection Int Delay, s/veh 2.9 EBL EBR NBL NBT SBT SBR Movement Y Lane Configurations đ Þ 26 27 Traffic Vol, veh/h 6 19 31 7 Future Vol, veh/h 26 6 7 19 27 31 0 0 Conflicting Peds, #/hr 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized None -None -None -Storage Length 0 -\_ ---Veh in Median Storage, # 0 -0 0 -\_ Grade, % 0 0 0 --\_ Peak Hour Factor 90 90 90 90 90 90 Heavy Vehicles, % 0 0 0 0 0 0 Mvmt Flow 29 7 8 21 30 34

Major/Minor	Minor2	Ν	Major1	Ma	ajor2	
Conflicting Flow All	84	47	64	0	· -	0
Stage 1	47	-	-	-	-	-
Stage 2	37	-	-	-	-	-
Critical Hdwy	6.4	6.2	4.1	-	-	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	2.2	-	-	-
Pot Cap-1 Maneuver	923	1028	1551	-	-	-
Stage 1	980	-	-	-	-	-
Stage 2	991	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuve		1028	1551	-	-	-
Mov Cap-2 Maneuve	r 918	-	-	-	-	-
Stage 1	975	-	-	-	-	-
Stage 2	991	-	-	-	-	-
Approach	EB		NB		SB	
HCM Ctrl Dly, s/v	8.99		1.97		0	

HCM Ctrl Dly, s/v	8.99	1.97
HCM LOS	А	

Minor Lane/Major Mvmt	NBL	NBT E	EBLn1	SBT	SBR
Capacity (veh/h)	485	-	937	-	-
HCM Lane V/C Ratio	0.005	-	0.038	-	-
HCM Ctrl Dly (s/v)	7.3	0	9	-	-
HCM Lane LOS	А	А	А	-	-
HCM 95th %tile Q(veh)	0	-	0.1	-	-

Int Delay, s/veh	1.1					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		÷.	4Î		Y	
Traffic Vol, veh/h	53	408	309	6	5	45
Future Vol, veh/h	53	408	309	6	5	45
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	82	82	90	90	90
Heavy Vehicles, %	0	0	1	0	0	0
Mvmt Flow	59	498	377	7	6	50

Conflicting Flow All 383 0 - 0 996 380   Stage 1 - - - 380 - 380 -   Stage 2 - - - 615 - - 615 -   Critical Hdwy 4.1 - - 6.4 6.2 - - 5.4 -   Critical Hdwy Stg 1 - - - 5.4 - - 5.4 -   Critical Hdwy Stg 2 - - - 5.4 - - 5.4 -   Follow-up Hdwy 2.2 - - 3.5 3.3 Pot Cap-1 Maneuver 1186 - - 274 671   Stage 1 - - - 543 - - 1400 0 - 110 - 255 671   Mov Cap-1 Maneuver 1186 - - 255 671 - 255 - - 543 - - 543 - - 543 - - 543	Major/Minor	Major1	Ν	/lajor2	1	Minor2	
Stage 1 - - - 380 -   Stage 2 - - - 615 -   Critical Hdwy Stg 1 - - 5.4 -   Critical Hdwy Stg 2 - - 3.5 3.3   Pot Cap-1 Maneuver 1186 - - 274 671   Stage 1 - - 696 -   Stage 2 - - 543 -   Platoon blocked, % - - 255 671   Mov Cap-1 Maneuver 1186 - - 255 -   Mov Cap-2 Maneuver - - 255 - - 543 -   Mov Cap-2 Maneuver - - - 648 - - 543 -   Mov Cap-2 Maneuver - - - 543 - - -	Conflicting Flow All						380
Critical Hdwy 4.1 - - 6.4 6.2   Critical Hdwy Stg 1 - - 5.4 -   Critical Hdwy Stg 2 - - 5.4 -   Follow-up Hdwy 2.2 - - 3.5 3.3   Pot Cap-1 Maneuver 1186 - - 274 671   Stage 1 - - - 696 -   Stage 2 - - - 543 -   Platoon blocked, % - - - 255 671   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver - - 255 - 543 -   Stage 1 - - - 648 - - 543 -   Approach EB WB SB - - 543 -   Minor Lane/Major Mvmt EBL EBT WBT WBR SBLn1 - -		-	-	-	-	380	-
Critical Hdwy Stg 1 - - 5.4 -   Critical Hdwy Stg 2 - - 5.4 -   Follow-up Hdwy 2.2 - - 3.5 3.3   Pot Cap-1 Maneuver 1186 - - 274 671   Stage 1 - - - 696 -   Stage 2 - - - 543 -   Platoon blocked, % - - - 255 671   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-1 Maneuver 1186 - - 255 -   Mov Cap-2 Maneuver - - 255 - -   Stage 1 - - - 648 -   Stage 2 - - - 543 -   Minor Lane/Major Mvmt EBL EBT WBT WBR SBLn1   Capacity (veh/h) 190 - - 577   HCM Lane V/C Ratio 0.05 - - 0.096   HCM Lan	Stage 2	-	-	-	-	615	-
Critical Hdwy Stg 2 - - 5.4 -   Follow-up Hdwy 2.2 - - 3.5 3.3   Pot Cap-1 Maneuver 1186 - - 274 671   Stage 1 - - - 696 -   Stage 2 - - - 543 -   Platoon blocked, % - - - 543 -   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver - - 255 - 543 -   Mov Cap-2 Maneuver - - - 648 - 543 -   Stage 2 - - - 543 - - 543 -   Approach EB WB SB - - 543 -   Minor Lane/Major Mvmt EBL EBT WBT WBR SBLn1 - - 577   HCM LoS B - - - 577 - - 0.096   HCM	Critical Hdwy	4.1	-	-	-	6.4	6.2
Follow-up Hdwy 2.2 - - 3.5 3.3   Pot Cap-1 Maneuver 1186 - - 274 671   Stage 1 - - - 696 -   Stage 2 - - - 543 -   Platoon blocked, % - - - 543 -   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver 1186 - - 255 -   Stage 1 - - - 648 -   Stage 2 - - - 543 -   Approach EB WB SB -   HCM Ctrl Dly, s/v 0.87 0 11.9   HCM LOS B - - 577   HCM Lane V/C Ratio 0.05 - - 0.096   HCM Ctrl Dly (s/v) 8.2 0 - 11.9   HCM Lane LOS A A - B	Critical Hdwy Stg 1	-	-	-	-	5.4	-
Pot Cap-1 Maneuver 1186 - - 274 671   Stage 1 - - - 696 -   Stage 2 - - - 543 -   Platoon blocked, % - - - 543 -   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver - - 255 - Stage 1 - - 648 -   Stage 2 - - - 543 - - 543 -   Approach EB WB SB - - 543 -   HCM Ctrl Dly, s/v 0.87 0 11.9 - - 577   HCM LOS B - - 577 - - 577   HCM Lane V/C Ratio 0.05 - - 0.096 - - 11.9   HCM Lane LOS A A - B -	Critical Hdwy Stg 2		-	-	-		
Stage 1 - - - 696 -   Stage 2 - - - 543 -   Platoon blocked, % - - - 543 -   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver - - 255 - 543 -   Mov Cap-2 Maneuver - - - 648 - - 543 -   Stage 1 - - - 648 - - 543 -   Approach EB WB SB - - 543 -   HCM Ctrl Dly, s/v 0.87 0 11.9 - - 577   HCM LOS B - - 577 - - 577   HCM Lane V/C Ratio 0.05 - - 0.096   HCM Ctrl Dly (s/v) 8.2 0 - 11.9   HCM Lane LOS A A - B	Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Stage 2 - - - 543 -   Platoon blocked, % - - - - -   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver - - 255 - Stage 1 - - 255 -   Stage 1 - - - 648 - - 543 -   Approach EB WB SB - - 543 -   Approach EB WB SB - - 543 -   Minor Lane/Major Mvmt EBL EBT WBT WBR SBLn1 - - 577   Capacity (veh/h) 190 - - 577 - 0.096   HCM Lane V/C Ratio 0.05 - - 0.096 - 11.9   HCM Lane LOS A A - - B		1186	-	-	-		671
Platoon blocked, % - - -   Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver - - - 255 -   Stage 1 - - - 648 -   Stage 2 - - - 543 -   Approach EB WB SB   HCM Ctrl Dly, s/v 0.87 0 11.9   HCM LOS B B B   Minor Lane/Major Mvmt EBL EBT WBT WBR SBLn1   Capacity (veh/h) 190 - - 577   HCM Lane V/C Ratio 0.05 - - 0.096   HCM Ctrl Dly (s/v) 8.2 0 - 11.9   HCM Lane LOS A A - B		-	-	-	-		-
Mov Cap-1 Maneuver 1186 - - 255 671   Mov Cap-2 Maneuver - - - 255 -   Stage 1 - - - 648 -   Stage 2 - - - 543 -   Approach EB WB SB -   HCM Ctrl Dly, s/v 0.87 0 11.9   HCM LOS B - - 577   Minor Lane/Major Mvmt EBL EBT WBT WBR SBLn1   Capacity (veh/h) 190 - - 577   HCM Lane V/C Ratio 0.05 - - 0.096   HCM Ctrl Dly (s/v) 8.2 0 - 11.9   HCM Lane LOS A A - B		-	-	-	-	543	-
Mov Cap-2 Maneuver   -   -   -   255   -     Stage 1   -   -   -   648   -     Stage 2   -   -   -   543   -     Approach   EB   WB   SB     HCM Ctrl Dly, s/v   0.87   0   11.9     HCM LOS   B   -   -   577     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B			-	-	-		
Stage 1   -   -   -   648   -     Stage 2   -   -   -   543   -     Approach   EB   WB   SB     HCM Ctrl Dly, s/v   0.87   0   11.9     HCM LOS   B   B     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B			-	-	-		671
Stage 2   -   -   -   543   -     Approach   EB   WB   SB     HCM Ctrl Dly, s/v   0.87   0   11.9     HCM LOS   B   B     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B		-	-	-	-		-
Approach   EB   WB   SB     HCM Ctrl Dly, s/v   0.87   0   11.9     HCM LOS   B   B     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B		-	-	-	-		-
HCM Ctrl Dly, s/v   0.87   0   11.9     HCM LOS   B   B   B     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B	Stage 2	-	-	-	-	543	-
HCM Ctrl Dly, s/v   0.87   0   11.9     HCM LOS   B   B   B     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B							
HCM Ctrl Dly, s/v   0.87   0   11.9     HCM LOS   B   B     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B	Approach	EB		WB		SB	
HCM LOS   B     Minor Lane/Major Mvmt   EBL   EBT   WBT   WBR SBLn1     Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B		0.87		0		11.9	
Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B	HCM LOS						
Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B							
Capacity (veh/h)   190   -   -   577     HCM Lane V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B	Minor Lane/Maior Myr	nt	EBL	EBT	WBT	WBR S	SBLn1
HCM Lane   V/C Ratio   0.05   -   -   0.096     HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   B							
HCM Ctrl Dly (s/v)   8.2   0   -   11.9     HCM Lane LOS   A   A   -   -   B					-		
HCM Lane LOS A A B							
					-	-	
	HCM 95th %tile Q(veh	1)	0.2	-	-	-	0.3

Intersection						
Int Delay, s/veh	2.9					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		र्भ	eî 👘		۰Y	
Traffic Vol, veh/h	97	316	234	36	31	82
Future Vol, veh/h	97	316	234	36	31	82
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	82	82	90	90	90
Heavy Vehicles, %	0	0	1	0	0	0
Mvmt Flow	108	385	285	40	34	91

Major/Minor	Major1	Ν	/lajor2		Minor2	
Conflicting Flow All	325	0	-	0	906	305
Stage 1	-	-	-	-	305	-
Stage 2	-	-	-	-	601	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1246	-	-	-	309	739
Stage 1	-	-	-	-	752	-
Stage 2	-	-	-	-	551	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1246	-	-	-	275	739
Mov Cap-2 Maneuver	-	-	-	-	275	-
Stage 1	-	-	-	-	669	-
Stage 2	-	-	-	-	551	-
Approach	EB		WB		SB	
HCM Ctrl Dly, s/v	1.78		0		14.47	
HCM LOS					В	
Minor Lane/Major Mvr	nt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		393	-	-	-	505
HCM Lane V/C Ratio		0.087	-	-	-	0.249
HCM Ctrl Dly (s/v)		8.2	0	-	-	14.5
HCM Lane LOS		А	А	-	-	В
HCM 95th %tile Q(veh	ר)	0.3	-	-	-	1

### **APPENDIX F**

TRIP GENERATION DATA

## Local Apartment Trip Generation Study

Average Vehicle Trip Ends vs: Dwelling Units On a: Weekday

Number of Studies:	13
Average Number of Dwelling Units:	193
Directional Distribution:	50% entering, 50% exiting

### **Trip Generation Per Dwelling Unit**

Average Rate	Ranges of Rates	Standard Deviation
9.03	6.59 - 17.41	2.47

### Data Plot and Equation



- 124

## Local Apartment Trip Generation Study

Average Vehicle Trip Ends vs: On a:	Dwelling Units Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.
Number of Studies:	13
Average Number of Dwelling Units:	193
Directional Distribution:	22% entering, 78% exiting

### **Trip Generation Per Dwelling Unit**

Average Rate	Ranges of Rates	Standard Deviation
0.55	0.14 - 0.78	0.18

#### **Data Plot and Equation**



Inter Leve

### Local Apartment Trip Generation Study

Average Vehicle Trip Ends vs: On a:	Dwelling Units Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.
Number of Studies:	13
Average Number of Dwelling Units:	193
Directional Distribution:	55% entering, 45% exiting

### **Trip Generation Per Dwelling Unit**

Average Rate	Ranges of Rates	Standard Deviation
0.72	0.32 - 1.66	0.25

### Data Plot and Equation



-

### TRIP GENERATION FOR CARDINAL PLACE

570 Apartments and 80 Townhouses

ITE LAND USE CODE			GENERATED DAILY TRAFFIC	GENERATED TRAFFIC AM PEAK HOUR			GENERATED TRAFFIC PM PEAK HOUR		
				ENTER	EXIT	TOTAL	ENTER	EXIT	TOTAL
Local Trip			4,562	22%	78%		55%	45%	
Rate	Apartments	570		59	208	267	215	176	391
Local Trip	Multi-Family Attached	80	781	22%	78%		55%	45%	
Rate	Townhouses			9	34	43	35	29	64
	New Volume Site Trips	5,343	68	242	310	250	205	455	
Vehicle Tri	p Reduction due to Transit A	-267	-3	-12		-13	-10		
]	Гotal New Volume Site Trip	5,076	65	230	295	237	195	432	
									-

Local Trip Rates calculated by using Fitted Curve Equations

# TRIP GENERATION FOR CARDINAL PLACE 570 Apartments

570 Units = X

### Weekday:

				_	
	T =	4,562	trips	_	
	T =	15	*	300.28	
Fitted Curve Equation:	T = 15.	$T = 15.193(X)^{0.899}$			

### Peak Hour of Adjacent Traffic between 7 and 9 am:

T =	267	trips		
T =	0.758	*	352	
Fitted Curve Equation: $T = 0.75$	$T = 0.758(X)^{0.924}$			

### Peak Hour of Adjacent Traffic between 4 and 6 pm:

Fitted Curve Equation:	T = 0.66	59(X)+10	).069			
	T =	0.669	*	570	+ (	10.07
	T =	391	trips			

# TRIP GENERATION FOR CARDINAL PLACE 80 Townhouses

80 Units = X

### <u>Weekday:</u>

Fitted Curve Equation:	$T = 15.193(X)^{0.899}$			
	T =	15 * 51.39		
	T =	781 trips		

### Peak Hour of Adjacent Traffic between 7 and 9 am:

T = 43 trips				
T = 0.758 *	57			
Fitted Curve Equation: $T = 0.758(X)^{0.924}$	$T = 0.758(X)^{0.924}$			

### Peak Hour of Adjacent Traffic between 4 and 6 pm:

Fitted Curve Equation:	T = 0.6	69(X)+10.069		
	T =	0.669 *	80	+ 10.07
	T =	64 trips		

### APPENDIX G

2021 CENSUS BUREAU DATA
# Census OnTheMap

### **Destination Analysis**

Workers: Living in 21 (Knox, TN) Showing: Employment locations grouped by Census Tracts

Created by the U.S. Census Bureau's OnTheMap https://onthemap.ces.census.gov on 10/10/2024

### Counts of All Jobs from Home Selection Area to Work Census Tracts in 2021

All Workers



### Map Legend

Job Count	Selection Areas	Job Count
<b>55 - 62</b>	Home Area	<b>5</b> 5 - 62
<b>48 - 54</b>		<b>4</b> 8 - 54
<b>41 - 47</b>		41 - 47
<b>33 -</b> 40		$\sqrt[3]{33-40}$
<b>26 - 32</b>		$\sqrt[2]{26}$ - 32
<b>19 - 25</b>		$\sqrt{20-32}$
11 - 18		4 10 10
		🖾 11 - 18







All Workers

All Jobs from Home Selection Area to Work Census Tracts in 2021

All Workers

	20	21
Census Tracts as Work Destination Area	Count	Share
All Census Tracts	1,160	100.0%
1 (Knox, TN)	62	5.3%
54.01 (Knox, TN)	43	3.7%
57.06 (Knox, TN)	28	2.4%
48 (Knox, TN)	25	2.2%
46.10 (Knox, TN)	24	2.1%
66 (Knox, TN)	24	2.1%
38.01 (Knox, TN)	21	1.8%
57.04 (Knox, TN)	21	1.8%
69.01 (Knox, TN)	21	1.8%



	20	21
Census Tracts as Work Destination Area	Count	Share
35.02 (Knox, TN)	20	1.7%
38.02 (Knox, TN)	20	1.7%
68 (Knox, TN)	20	1.7%
46.15 (Knox, TN)	19	1.6%
59.11 (Knox, TN)	19	1.6%
59.08 (Knox, TN)	18	1.6%
70 (Knox, TN)	18	1.6%
9.02 (Knox, TN)	16	1.4%
58.03 (Knox, TN)	14	1.2%
112.01 (Blount, TN)	13	1.1%
44.03 (Knox, TN)	13	1.1%
44.04 (Knox, TN)	13	1.1%
46.11 (Knox, TN)	13	1.1%
19 (Knox, TN)	12	1.0%
58.07 (Knox, TN)	12	1.0%
9801 (Anderson, TN)	11	0.9%
All Other Locations	640	55.2%



### **Analysis Settings**

Analysis Type	Destination
Destination Type	Census Tracts
Selection area as	Home
Year(s)	2021
Job Type	All Jobs
Selection Area	21 (Knox, TN) from Census Tracts
Selected Census Blocks	58
Analysis Generation Date	10/10/2024 17:02 - On The Map 6.24.1
Code Revision	bc 639735180 b6 b7 a de 65403 c2 b ed fe 53 b70 b1 e56
LODES Data Vintage	$20231016\_1512$

### Data Sources

Source: U.S. Census Bureau, OnTheMap Application and LEHD Origin-Destination Employment Statistics (Beginning of Quarter Employment, 2nd Quarter of 2002-2021).

#### Notes

1. Race, Ethnicity, Educational Attainment, and Sex statistics are beta release results and are not available before 2009.

2. Educational Attainment is only produced for workers aged 30 and over.

3. Firm Age and Firm Size statistics are beta release results for All Private jobs and are not available before 2011.



**APPENDIX H** 

KNOX COUNTY TURN LANE VOLUME THRESHOLD WORKSHEETS

### TABLE 4A

### LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

	OPPOSING	127 THROU	GH VOLUME	PLUS RIGH	T-TURN	VOLUME	<u>;</u> *
	VOLUME	100 - 149	150 - 199	200 - 249	250 - 299	300 - 349	350 - 399
	100 - 149 150 - 199	31)0 245	235 200	185 160	145 130	120 110	100 90
11 + 316 = 327	200 - 249 250 - 299	205 175	Delrose Dr Proposed SE I	ive at 🔰	115 105	100 90	80 70
	300 - 349 350 - 399	155 135	2027 Projecto	1	95 85	80 70	65 60
	400 - 449 450 - 499	120 105	EB Left Turr	3	75 70	65 60	55 50
	500 - 549 550 - 599	95 85	Warrant	ed	65 60	55 50	50 45
	600 - 649 650 - 699	75 70	65 60	60 55	55 50	45 40	40 35
	700 - 749 750 or More	65 60	55 50	50 45	45 40	35 35	30 30

(If the left-turn volume exceeds the table value a left -turn lane is needed)

OPPOSING	THROUGH VOLUME PLUS RIGHT-TURN VOLUME *						
VOLUME	350 - 399	400 - 449	450 - 499	51)0 - 549	550 - 599	= / > 600	
100 - 149	100	80	70	60	55	50	
150 - 199	90	75	65	55	50	45	
200 - 249	80	72	- 460	55	50	45	
250 - 299	70	65	55	50	45	40	
300 - 349	65	60	50	50	45	40	
350 - 399	60	55	50	45	40	40	
400 - 449	55	50	45	45	40	35	
450 - 499	50	45	45	40	35	35	
500 - 549	50	45	40	40	35	35	
550 - 599	45	40	40	35	35	35	
600 - 649	40	35	35	35	35	30	
650 - 699	35	35	35	30	30	30	
700 - 749	30	30	30	30	30 `	30	
750 or Morc	30	30	30	30	30	30	

\* Or through volume only if a right-turn lane exists.

A-4

### TABLE 4B

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### RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

•	RIGHT-TURN	THROUGH VOLUME PLUS LEFT-TURN VOLUME *					
	VOLUME	<100	100 - 199	200 - 249	250 - 299	300 - 349	350 - 399
11	Fewer Than 25 25 - 49 50 - 99						
	100 - 149 150 - 199		Delrose D Proposed SE				
	200 - 249 250 - 299		2027 Projec WB Right Tu			Yes	
	300 - 349 350 - 399		Right Turn Lane NOT		Yes	Yes Yes	Yes Yes
	400 - 449 450 - 499			Yes Yes	Yes Yes	Yes Yes	Yes Yes
	500 - 549 550 - 599		Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
	600 or More	Yes	Yes	Yes	Yes	Yes	Yes

RIGHT-TURN	THROUGH VOLUME PLUS LEFT-TURN VOLUME *							
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 600	+ / > 600		
Fewer Than 25 25 - 49 50 - 99					Yes	Yes Yes		
100 - 149 150 - 199			Yes	Yes Yes	Yes Yes	Yes Yes		
200 - 249 250 - 299	Yes	Yes Y <del>e</del> s	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
300 - 349 350 - 399	Yes Yes	Yes <b>Yes</b>	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
400 - 449 450 - 499	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
500 - 549 550 - 599	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
600 or More	Yes	Yes	Yes	Yes	Yes	Yes		

\* Or through volume only if a left-turn lane exists.

### TABLE 4A

### LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF <mark>35 MPH OR LESS</mark>

·	OPPOSING	THROUGH VOLUME PLUS RIGHT-TURN VOLUME *					
	VOLUME	100 - 149	150 - 199	200 - 249	250 - 299	300 - 349	350 - 399
	100 - 149 150 - 199	300 245	235 200	185 160	145 130	120 110	100 90
4	200 - 249 250 - 299	205 175	170 150	140 125	115 105	1\0 90	80 70
	300 - 349 350 - 399	155 135	135 120	110 100	95 85	80 70	65 60
	400 - 449 450 - 499	120 105	Delrose Drive at Proposed SE Entrance 2027 Projected PM EB Left Turns = 97 Left Turn Lane		75 70	65 60	55 50
	500 - 549 550 - 599	95 85			65 60	55 50	50 45
	600 - 649 650 - 699	75 70			55 50	45 40	40 35
	700 - 749 750 or More	65 60	ξ Wa		45 40	35 35	30 30

(If the left-turn volume exceeds the table value a left -turn lane is needed)

OPPOSING	THROUGH VOLUME PLUS RIGHT-TURN VOLUME *						
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 599	= / > 600	
100 - 149	100	80	70	60	55	50	
150 - 199	90	75	65	55	50	45	
200 - 249	80	72	- 460	55	50	45	
250 - 299	70	65	55	50	45	40	
300 - 349	65	60	50	50	45	40	
350 - 399	60	55	50	45	40	40	
400 - 449	55	50	45	45	40	35	
450 - 499	50	45	45	40	35	35	
500 - 549	50	45	40	40	35	35	
550 - 599	45	40	40	35	35	35	
600 - 649	40	35	35	35	35	30	
650 - 699	35	35	35	30	30	30	
700 - 749	30	30	30	30	30	30	
750 ог Могс	30	30	30	30	30	30	

\* Or through volume only if a right-turn lane exists.

### TABLE 4B

### RIGHT-TURN LANE VOLUME THRESHOLDS

### FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

<b>RIGHT-TURN</b>	THROUGH VOLUME PLUS LEFT-TURN VOLUME *							
VOLUME	<100	100 - 199	200 - 249	250 - 299	300 - 349	350 - 399		
Fewer Than 25 25 - 49 50 - 99								
100 - 149 150 - 199		Delrose Driv Proposed SE Er	eat 🔰					
200 - 249 250 - 299		2027 Projected	3			Yes		
300 - 349 350 - 399		WB Right Turn	3	Yes	Yes Yes	Yes Yes		
400 - 449 450 - 499		Warrantee	1 }	Yes Yes	Yes Yes	Yes Yes		
500 - 549 550 - 599		Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
600 or More	Yes	Yes	Yes	Yes	Yes	Yes		

RIGHT-TURN	THROUGH VOLUME PLUS LEFT-TURN VOLUME *							
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 600	+ / > 600		
Fewer Than 25 25 - 49 50 - 99					Yes	Yes Yes		
100 - 149 150 - 199			Yes	Yes Yes	Yes Yes	Yes Yes		
200 - 249 250 - 299	Yes	Yes Y <del>e</del> s	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
300 - 349 350 - 399	Yes Yes	Yes <b>Yes</b>	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
400 - 449 450 - 499	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
500 - 549 550 - 599	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes		
600 or More	Yes	Yes	Yes	Yes	Yes	Yes		

\* Or through volume only if a left-turn lane exists.

### TABLE 4A

### LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

,		148					
	OPPOSING		GH VOLUME	PLUS RIGH	T-TURN	VOLUMI	<u>c</u> *
	VOLUME	100 - 149	150 - 199	200 - 249	250 - 299	300 - 349	350 - 399
	100 - 149	300	235	185	145	120	100
	150 - 199	245	200	160	130	110	90
	200 - 249	205	170	140	115	100	80
	250 - 299	175	150	125	105	90	70
	300 - 349	155	135	110	95	\$0	65
	350 - 399	115	120	100	85	70	60
413	<b>400 - 449</b>	120	105	90	75	65	55
15	450 - 499	105	Delrose Dr	ive at	70	60	50
	500 - 549 550 - 599	95 85	Proposed SW	2	65 60	55 50	50 45
	600 - 649 650 - 699	75 70	2027 Project EB Left Turn		55 50	45 40	40 35
	700 - 749 750 or More	65 60	Left Turn Lar Warrant	<b>1</b>	45 40	35 35	30 30
1			Turn	Juni			
	OPPOSING	THROU	GH VOLUME	PLUS RIGH	T-TURN	VOLUM	£ *
	VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 599	= / > 600
	100 - 149	100	80	70	60	55	50
	150 - 199	90	75	65	55	50	45
	200 - 249	80	72	- 460	55	50	45
	250 - 299	70	65	55	50	45	40
	300 - 349	65	60	50	50	45	40
	350 - 399	60	55	50	45	40	40
	400 - 449	55	50	45	45	40	35
	450 - 499	50	45	45	40	35	35
	500 - 549	50	45	40	40	35	35
	550 - 599	45	40	40	35	35	35

(If the left-turn volume exceeds the table value a left -turn lane is needed)

\* Or through volume only if a right-turn lane exists.

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2 + 413 = 415

600 - 649

650 - 699

700 - 749

750 or More

### TABLE 4B

### RIGHT-TURN LANE VOLUME THRESHOLDS

:

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### FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

RIGHT-TURN	THRO	UGH VOLUM	E PLUS LEI	T-TURN	VOLUMI	<b>*</b> -
VOLUME	<100	100 - 199	200 - 249	250 - 299	300 - 349	350 - 399
Fewer Than 25 25 - 49 50 - 99						
100 - 149						
150 - 199						
200 - 249 250 - 299						Yes
300 - 349 350 - 399				Yes	Yes Yes	Yes Yes
400 - 449 450 - 499			Yes Yes	Yes Yes	Yes Yes	Yes Yes
500 - 549 550 - 599		Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
600 or More	Yes	Yes	Yes	Yes	Yes	Yes

413	
-----	--

	RIGHT-TURN	THRO	UGH VOLUMI	E PLUS LEF	T-TURN	VOLUMI	<u>;</u> *
	VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 600	+ / > 600
2	Fewer Than 25 25 - 49 50 - 99					Yes	Yes Yes
	100 - 149 150 - 199		Delrose	Drive at W Entrance	Yes Yes	Yes Yes	Yes Yes
	200 - 249 250 - 299	Yes	2027 Proj	ected AM	Yes Yes	Yes Yes	Yes Yes
	300 - 349 350 - 399	Yes Yes		Turns = 2 Lane NOT	Yes Yes	Yes Yes	Yes Yes
	400 - 449 450 - 499	Yes Yes	Warr	anted }	Yes Yes	Yes Yes	Yes Yes
	500 - 549 550 - 599	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
	600 or More	Yes	Yes	Yes	Yes	Yes	Yes

\* Or through volume only if a left-turn lane exists.

### TABLE 4A

### LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

OPPOSING	THROUG	GH VOLUME	PLUS RIGH	T-TURN V	VOLUMI	C *
VOLUME	100 - 149	150 - 199	200 - 249	250 - 299	300 - 349	350 - 399
100 - 149	300	235	185	145	120	100
150 - 199	245	200	160	130	110	90
200 - 249	205	170	140	115	100	80
250 - 299	175	150	125	105	90	70
300 - 349	155	135	110	95	80	65
350 - 399	135	120	100	85	70	60
400 - 449	120	105	90	75	65	55
450 - 499	105	90	80	70	60	50
500 - 549	95	80	70	65	55	50
550 - 599	85	70	65	60	50	45
600 - 649	75	65	60	55	45	40
650 - 699	70	60	55	50	40	35
700 - 749	65	55	50	45	35	30
750 or More	60	50	45	40	35	30

(If the left-turn volume exceeds the table value a left -turn lane is needed)

		408				
OPPOSING	THROU	GH VOLUME	PLUS RIGE	IT-TURN	VOLUM	£ *
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 599	= / > 600
100 - 149 150 - 199	100 90	80 75	70 65	60 55	55 50	50 45
130 - 133	<del>70</del>	/p	05		50	45
200 - 249	80	72	- 460	55	50	45
250 - 299	70	42	55	50	45	40
300 - 349	65	60	50	50	45	40
350 - 399	60	55	50	45	40	40
400 - 449	55	50	Delrose Drive a	L	40	35
450 - 499	50	45 C Pr	oposed SW Entra	ance 🎾	35	35
500 - 549	50	45	-	20	35	35
550 - 599	45		2027 Projected P		35	35
600 - 649	40	35	EB Left Turns =	53 5	35	30
650 - 699	35	35 E	eft Turn Lane N	от 🦻	30	30
700 - 749	30	30	Warranted	}	30 `	30
750 or More	30	30 (	juusu	jus	30	30

\* Or through volume only if a right-turn lane exists.

6 + 309 = 315

### TABLE 4B

### RIGHT-TURN LANE VOLUME THRESHOLDS

:

### FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

	RIGHT-TURN	THR	OUGH VOLUM	E PLUS LEF	T-TURN	VOLUME	*-
	VOLUME	<100	100 - 199	200 - 249	250 - 299	300 - 349	350 - 399
6	Fewer Than 25 25 - 49 50 - 99						
	100 - 149 150 - 199		Delrose 1 Proposed SW	<b>~</b>			
	200 - 249 250 - 299		2027 Proje	cted PM			Yes
	300 - 349 350 - 399		WB Right 7	3	Yes	Yes Yes	Yes Yes
	400 - 449 450 - 499	_	Warra	nted	Yes Yes	Yes Yes	Yes Yes
	500 - 549 550 - 599		Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
	600 or More	Yes	Yes	Yes	Yes	Yes	Yes

RIGHT-TURN	THRO	UGH VOLUM	E PLUS LEI	T-TURN	VOLUMI	<u>}</u> *
VOLUME	350 - 399	400 - 449	450 - 499	500 - 549	550 - 600	+ / > 600
Fewer Than 25 25 - 49 50 - 99					Yes	Yes Yes
100 - 149 150 - 199			Yes	Yes Yes	Yes Yes	Yes Yes
200 - 249 250 - 299	Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
300 - 349 350 - 399	Yes Yes	Yes <b>Yes</b>	Yes Yes	Yes Yes	Yes Yes	Yes Yes
400 - 449 450 - 499	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
500 - 549 550 - 599	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes	Yes Yes
600 or More	Yes	Yes	Yes	Yes	Yes	Yes

\* Or through volume only if a left-turn lane exists.

**APPENDIX I** 

SIMTRAFFIC 12 VEHICLE QUEUE WORKSHEETS

### Intersection: 2: Wilder Place & Dandridge Avenue & Brooks Avenue

Movement	EB	WB	NB	SB	NW
Directions Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr< td=""></lr<></td></ltr<>	<lr< td=""></lr<>
Maximum Queue (ft)	75	122	57	68	52
Average Queue (ft)	34	55	25	33	19
95th Queue (ft)	63	92	47	58	40
Link Distance (ft)	379	505	355	555	446
Upstream Blk Time (%)					
Queuing Penalty (veh)					
Storage Bay Dist (ft)					
Storage Blk Time (%)					
Queuing Penalty (veh)					

### Intersection: 10: Riverside Drive & Delrose Drive

Movement	WB	NW
Directions Served	LT	LR
Maximum Queue (ft)	12	72
Average Queue (ft)	0	26
95th Queue (ft)	9	60
Link Distance (ft)	236	232
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 14: Delrose Drive & Riverside Road

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	38	44
Average Queue (ft)	3	21
95th Queue (ft)	20	43
Link Distance (ft)	234	342
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 18: Riverside Road & Brooks Avenue

Movement	WB	NB
Directions Served	LT	LR
Maximum Queue (ft)	32	68
Average Queue (ft)	2	29
95th Queue (ft)	17	57
Link Distance (ft)	273	220
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 22: Riverside Road & Proposed East Entrance

Movement	EB	NB
Directions Served	LR	LT
Maximum Queue (ft)	42	3
Average Queue (ft)	23	0
95th Queue (ft)	45	3
Link Distance (ft)	157	215
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 25: Delrose Drive & Proposed SW Entrance

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	35	50
Average Queue (ft)	6	26
95th Queue (ft)	26	46
Link Distance (ft)	264	380
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 27: Delrose Drive & Proposed SE Entrance

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	39	78
Average Queue (ft)	9	41
95th Queue (ft)	32	66
Link Distance (ft)	662	312
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Network Summary

Network wide Queuing Penalty: 0

### Intersection: 2: Wilder Place & Dandridge Avenue & Brooks Avenue

Movement	EB	WB	NB	SB	NW
Directions Served	LTR>	LTR	LTR>	<ltr< td=""><td><lr></lr></td></ltr<>	<lr></lr>
Maximum Queue (ft)	126	86	74	78	56
Average Queue (ft)	56	41	34	40	22
95th Queue (ft)	103	71	58	66	43
Link Distance (ft)	379	493	355	555	450
Upstream Blk Time (%)					
Queuing Penalty (veh)					
Storage Bay Dist (ft)					
Storage Blk Time (%)					
Queuing Penalty (veh)					

### Intersection: 10: Riverside Drive & Delrose Drive

Movement	NW
Directions Served	LR
Maximum Queue (ft)	51
Average Queue (ft)	24
95th Queue (ft)	47
Link Distance (ft)	232
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

### Intersection: 14: Delrose Drive & Riverside Road

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	45	42
Average Queue (ft)	6	19
95th Queue (ft)	29	41
Link Distance (ft)	234	342
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 18: Riverside Road & Brooks Avenue

Movement	WB	NB
Directions Served	LT	LR
Maximum Queue (ft)	40	47
Average Queue (ft)	5	27
95th Queue (ft)	24	46
Link Distance (ft)	273	380
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 20: Riverside Road & Proposed East Entrance

Movement	EB	NB
Directions Served	LR	LT
Maximum Queue (ft)	38	6
Average Queue (ft)	19	0
95th Queue (ft)	44	4
Link Distance (ft)	156	205
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 23: Delrose Drive & Proposed SW Entrance

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	78	46
Average Queue (ft)	15	23
95th Queue (ft)	53	46
Link Distance (ft)	261	347
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

### Intersection: 26: Delrose Drive & Proposed SE Entrance

Movement	EB	WB	SB
Directions Served	LT	TR	LR
Maximum Queue (ft)	85	2	83
Average Queue (ft)	24	0	40
95th Queue (ft)	63	2	66
Link Distance (ft)	651	268	329
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

### Network Summary

Network wide Queuing Penalty: 0

APPENDIX J

LETTER RESPONSE TO ADDRESS COMMENTS



11812 Black Road Knoxville, Tennessee 37932 Phone (865) 556-0042 ajaxengineering@gmail.com

November 20, 2024

### PROJECT NAME: Cardinal Place (12-A-24-PD) TO: Knoxville-Knox County Planning SUBJECT: Response Document for the Cardinal Place TIS Review Comments

Knoxville-Knox County Planning and City of Knoxville Department of Engineering Staff:

The following response document addresses the comments in an email from Mike Conger, PE, dated November 15, 2024. This letter is added to the end of the revised report in Appendix J.

1) On Page 2 (Executive Summary, Recommendations Section) - the second intersection listed is titled "Delrose Drive at Riverside Road." Please correct this to say "Delrose Drive at Riverside Drive" instead since that is the location that this section is discussing.

<u>Response</u>: On Page 2 – the second intersection listed has been changed as requested to "Delrose Drive at Riverside Drive".

- 2) On Page 61 (Evaluation of Turn Lane Thresholds) and Page 66 (Recommendations for Delrose Drive at SW Entrance) The turn lane analysis for this location should note that the threshold is very nearly met for an eastbound left-turn lane based on the high through volumes and left turning vehicles in the PM peak period. The recommendations made for this location needs to note that there should be consideration of a left-turn lane since this is a borderline situation and the analysis relies on several assumptions about trip distribution percentages and other variables which could vary from the actual conditions once the development is complete. Please also include the minimum required storage and taper lengths for a potential left-turn lane at this location.
  - <u>Response</u>: An additional sentence has been added to the end of the Evaluation of Turn Lane Thresholds section on Page 62 (formerly Page 61) regarding the near warrant of a left-turn lane at the Proposed Southwest Entrance. An additional discussion regarding the consideration of a separate left-turn lane on Delrose Drive at the Proposed Southwest Entrance was added to the report on Pages 67-68 (formerly Pages 66-67). Finally, this recommendation has been added at the beginning of the report on Page 3.

## 3) On Page 70 (Section 7, subsection 7f) – Please specify longitudinal crosswalk type for the recommended internal crosswalks.

<u>Response</u>: On Page 72, Section 7, Subsection 7f (formerly page 70), the longitudinal crosswalk type has been included. This addition was also made on Pages 4-5.

In addition to the revisions listed above, other changes in the report include the following:

- Updated Title Page
- Updated Table of Contents
- Updated Page Footers and Page Numbers
- Minor grammatical changes
- Added Appendix J to include this response letter

If you have any questions or further comments, don't hesitate to contact me. We look forward to your approval.

Sincerely,

Ajax Engineering, LLC Robert W. Jacks, P.E.





11812 Black Road Knoxville, Tennessee 37932 Phone (865) 556-0042 ajaxengineering@gmail.com

February 28, 2025

### PROJECT NAME: Cardinal Place (12-A-24-PD) TO: Knoxville-Knox County Planning SUBJECT: Response Document for the Cardinal Place TIS Review Comments

Knoxville-Knox County Planning and City of Knoxville Department of Engineering Staff:

The following response document addresses the comments in an email from Jessie Hillman, AICP, dated February 27, 2025. This letter is added to the end of the revised report in Appendix J.

- 1) The final plan package we have for the Cardinal Place development stipulates a total of 650 units (570 apartments + 80 townhouses), rather than the 627 units in the TIS. Can you revise the study to account for this increase, or provide an addendum about this with any recommendation changes?
  - <u>Response</u>: The increase in housing units has been reflected and changed throughout the updated TIS report. Overall, this small increase in housing units only slightly impacted the results and did not change any of the original recommendations provided in the report other than the road widening width listed in the following.
- 2) Also, City Engineering has shared that they would require Riverside Road to be widened by 20 ft, not 18 ft. Can you reflect that requirement in the study as well?

<u>Response</u>: This requested change has been made in the recommendations on Pages 2 and 66.

In addition to the revisions listed above, other changes in the report include the following:

- Updated Title Page
- Updated Page Footer Date
- A few Minor grammatical changes

If you have any questions or further comments, please get in touch with me. We look forward to your approval.

Sincerely,

Ajax Engineering, LLC Robert W. Jacks, P.E.





Ajax Engineering, LLC 11812 Black Road Knoxville, TN 37932 ajaxengineering@gmail.com © 2025 Ajax Engineering, LLC