# EBENEZER ROAD SUBDIVISION Transportation Impact Analysis Ebenezer Road Knoxville, TN 

## A Transportation Impact Analysis for the Ebenezer Road Subdivision

Submitted to<br>Knoxville-Knox County Planning

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Ardurra Project No. 330.029

Submitted By:


ARDURRA

# Ebenezer Road Subdivision <br> Transportation Impact Analysis <br> April 26, 2024 

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## Executive Summary

S\&E Properties, LLC is proposing a residential development. The project is located south of the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road in Knox County, Tennessee. The full buildout of the Ebenezer Road Subdivision proposes 113 single-family residential lots and a future development area by others. The current plan for the Future Development Area is a proposed apartment complex with 278 garden style apartment units. Construction is proposed to take place this year and this study assumes full build out for the development will occur in 2027.

The Ebenezer Road Subdivision has a proposed single roadway connection to Ebenezer Road and the proposed future development area has a separate proposed single roadway connection to Ebenezer Road. A roadway connection between the two developments is under consideration for the purpose of emergency access. The exact location will need to be coordinated between the property owners as well as Knox County Engineering and Public Works.

In order to maintain or provide an acceptable level-of-service for each of the intersections studied, some recommendations are presented.

## Kingston Pike (SR 70) at Ebenezer Road

After the completion of the Ebenezer Road Subdivision including the future development area the traffic conditions for the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road will operate at an acceptable LOS C during the AM peak hour and a LOS D during the PM peak hour.

The northbound right turn lane (Ebenezer Road) will exceed capacity after the completion of the Ebenezer Road Subdivision and Future Development Area. There are several existing constraints including the location of guard rails and power poles and the proximity to Ten Mile Creek that would make extending the storage length of the right turn lane difficult to construct. Ardurra recommends that any future intersection improvements be reviewed, coordinated and approved by both the City of Knoxville Department of Engineering and Knox County Engineering and Public Works.

## Ebenezer Road at Future Development Area

A southbound left turn lane is warranted at the intersection of Ebenezer Road at Future Development Area Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy." The southbound left turn lane has a recommended minimum storage length

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of 50 feet per the AASHTO Greenbook "A Policy on Geometric Design of Highways and Streets."

After the completion of the full buildout of the Ebenezer Road Subdivision including the proposed roadway improvements the intersection of Ebenezer Road at Future Development Area Roadway will operate at an acceptable LOS B or better for each approach during both the AM and PM peak hours.

## Ebenezer Road at Subdivision

Neither a southbound left turn lane nor a northbound right turn lane is warranted at the intersection of Ebenezer Road at Ebenezer Subdivision Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

After the completion of the full buildout of the Ebenezer Road Subdivision the intersection of Ebenezer Road at Subdivision Roadway will operate at an acceptable LOS B or better for each approach during both the AM and PM peak hours.

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## 1 Introduction

### 1.1 Project Description

This report provides a summary of a transportation impact analysis that was performed for the Ebenezer Road Subdivision residential development. The Ebenezer Road Subdivision proposes 113 single-family residential lots and a future development area by others. The current plan for the Future Development Area is a proposed apartment complex with 278 garden style apartment units. The project is located south of the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road in Knox County, Tennessee. The location of the site is shown in Figure 1.

Construction is proposed to take place this year and this study assumes full build out for the subdivision and the future development area will occur in 2027.

The Ebenezer Road Subdivision has a proposed single roadway connection to Ebenezer Road and the proposed future development area has a separate proposed single roadway connection to Ebenezer Road. A roadway connection between the two developments is under consideration for the purpose of emergency access. The exact location will need to be coordinated between the property owners as well as Knox County Engineering and Public Works.

The proposed site layout is shown in Figure 2.


Figure 1: Location Map

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Figure 2: Site Plan

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### 1.2 Study Area

The purpose of this study is to evaluate the impacts to the traffic conditions caused by the proposed development. Ebenezer Road is considered a north-south orientate roadway and Kingston Pike (US 11/US 70) is considered an east-west oriented roadway. The existing intersections and existing traffic control are summarized in Table 1.2-1 Study Area.

Table 1.2-1
Ebenezer Road Subdivision
Study Area

| Intersection | Existing Traffic Control |
| :--- | :---: |
| Kingston Pike (US 11/US 70) at Ebenezer Road | Signalized |

### 1.3 Existing Site Conditions

Roadway geometry and posted speed limits were obtained by field observations. The Knoxville-Knox County Planning "2018 Major Road Plan" was used to determine road classification. This information is summarized in Table 1.3-1 Existing Site Conditions.

Table 1.3-1
Ebenezer Road Subdivision
Existing Site Conditions

| Roadway | Speed <br> Limit | Lanes | Road <br> Width | Major Road Plan |
| :--- | :--- | :---: | :---: | :--- |
| Kingston Pike <br> (US 11/US 70) | 45 mph | 5 | $\sim 58$ feet | Major Arterial |
| Ebenezer Road | 30 mph | 2 | $\sim 21$ feet | Minor Collector |

The intersection of Kingston Pike (US 11/US 70) at Ebenezer Road is located within the City of Knoxville limits and the signal is maintained by the City of Knoxville Department of Engineering.

At the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road the eastbound approach (Kingston Pike) has a left turn lane with an approximate storage length of 140 feet and a right turn lane with an approximate storage length of 140 feet. The westbound approach (Kingston Pike) has a left turn lane with an approximate storage length of 90 feet and a right turn lane with an approximate

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storage length of 100 feet. The southbound approach (Driveway) has a separate right turn lane with an approximate storage length of 50 feet. The northbound approach (Ebenezer Road) has a separate right turn lane with an approximate storage length of 50 feet.

The measured width of Ebenezer Road south of the signalized intersection is 30 feet and tapers to 24 feet past the commercial driveway connections.

An aerial photo of the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road is included in Attachment 1.

Guardrails are located on both sides of Ebenezer Road south of Kingston Pike (US 11/US 70) at the Ten Mile Creek crossing. Pictures of the existing conditions of the guardrails are included in Attachment 1.

There are no sidewalks or bike infrastructure in the vicinity of the proposed development.

The Knoxville Area Transit (KAT) operates in the vicinity of the proposed development. Route 16 (Cedar Bluff Connector) stops include Parkwest Hospital, Cedar Bluff at Fox Lonas and Walmart Walbrook Drive. The nearest KAT stop to the development along Route 16 is currently located on Cedar Bluff Road near the Kroger Development which is approximately 1.1 miles walk to the Ebenezer Road Subdivision.

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## 2 Existing Traffic Volumes

Ardurra conducted a peak hour turning movement count at the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road on Tuesday March 19, 2024. The AM peak hour occurred between 7:45 a.m. and 8:45 a.m. with an AM PHF of 97. The PM peak hour occurred between 5:00 p.m. and 6:00 p.m. with a PM PHF of 0.94.

The existing volumes including the AM and PM peak hour traffic volumes at the count locations are shown in Figure 3, and the count data collected is included in Attachment 2.


LEGEND:

- 5 (16) TURNING MOVEMENT VOLUME AM (PM)

Figure 3: 2024 Existing Peak Hour Traffic

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## 3 Background Growth

The Tennessee Department of Transportation (TDOT) maintains count stations in the vicinity of the proposed development.

TDOT count station ID 47000466 is located on Ebenezer Road between Kingston Pike (US 11/US 70) and George Williams Road in Knoxville, TN. The annual growth rate for this station over the last ten years is approximately $-3.80 \%$. The 2023 ADT was 4,581 vehicles per day.

TDOT count station ID 47000128 is located on Kingston Pike (US 11/US 70) west of the signalized intersection with Cedar Bluff Road. The annual growth rate for this station over the last ten years is approximately $0.59 \%$. The 2022 ADT was 27,645 vehicles per day.

For the purpose of this study, an annual growth rate of $1.0 \%$ was assumed for traffic at the studied intersections until full occupancy is reached in 2027. Attachment 3 shows the trend line growth charts for the TDOT count stations.

Figure 4 demonstrates the projected background peak hour volumes at the studied intersections after applying the background growth rate to the existing conditions.


LEGEND:
〔 5 (16) TURNING MOVEMENT VOLUME AM (PM)

Figure 4: 2027 Background Peak Hour Traffic

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### 3.1 Future Development Area

In addition to the background growth, the trips from the Future Development Area were calculated and included in the projected background peak hour traffic. The future development area is expected to be a proposed apartment complex with 275 garden style apartment units. A roadway connection between the two developments is under consideration for the purpose of emergency access.

The Knoxville-Knox County Planning Commission published a memorandum ("Local Trip Generation Rates for Multi-Family Residential Uses", August 14, 2000) for the purpose of providing locally collected data for all multi-family residential developments. The fitted curve equations from the local study were used to calculate site trips for the future development area.

The land use worksheets are included in the attachments and a trip generation summary is shown in Table 3.1.

Table 3.1-1
Future Development Area
Trip Generation Summary

| Land Use | Density | Daily | AM Peak Hour <br> Trips |  | PM Peak Hour <br> Enter |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Apartments <br> (Local Trip Gen Study) | 278 Units | 2,392 | 30 | 107 | 108 | 88 |

The total combined new trips generated by the Future Development Area were estimated to be 2,392 daily trips. The estimated trips are 137 trips during the AM peak hour and 196 trips during the PM peak hour.

The directional distribution of the traffic generated by the Ebenezer Road Subdivision was determined using the existing traffic volumes in combination with the site plan layout. The entering/exiting traffic was assumed to be 70\% Ebenezer Road northbound to/from Kingston Pike (US 11/US 70) and 30\% Ebenezer Road southbound to/from Gleason Drive/Westland Drive.

Figures 5 and 6 show the Future Development Area - apartment peak hour trip distribution and site trips.


LEGEND:
$\longleftarrow 50 \%$ (50\%) TRIP DISTRIBUTION ENTERING (EXITING)

Figure 5: Apartment Peak Hour Trip Distribution


LEGEND:

- 5 (16) TURNING MOVEMENT VOLUME AM (PM)

Figure 6: Apartment Peak Hour Site Trips

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## 4 Trip Generation and Trip Distribution

The Ebenezer Road Subdivision proposes 113 single-family residential lots. A roadway connection between the two developments is under consideration for the purpose of emergency access. Single-Family Detached Housing or Land Use 210 was used to calculate site trips for the development using the fitted curve equations from the Trip Generation, 11th Edition, published by the Institute of Transportation Engineers.

The land use worksheets are included in Attachment 4. A trip generation summary is shown in Table 4-1.

Table 4-1
Ebenezer Road Subdivision
Trip Generation Summary

| Land Use | Density | Daily <br> Trips | AM Peak Hour <br> Enter |  | Pxit Peak Hour <br> Enter Exit |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Single Family <br> Detached Housing <br> (LUC | 113 Lots | 1,129 | 21 | 62 | 71 | 41 |

The total combined new trips generated by the Ebenezer Road Subdivision were estimated to be 1,129 daily trips. The estimated trips are 83 trips during the AM peak hour and 112 trips during the PM peak hour.

Ebenezer Road at the intersection with Kingston Pike (US 11 / US 70) has an existing trip distribution of $70 \%$ northbound and $30 \%$ southbound during the AM peak hour and $45 \%$ northbound and $55 \%$ southbound during the PM peak hour.

The directional distribution of the traffic generated by the Ebenezer Road Subdivision was determined using the existing traffic volumes in combination with the site plan layout. The entering/exiting traffic was assumed to be 70\% Ebenezer Road northbound to/from Kingston Pike (US 11 / US 70) and 30\% Ebenezer Road southbound to/from Gleason Drive/Westland Drive.

Figures 7 and 8 show the subdivision peak hour trip distribution and site trips. Figure 9 shows the 2027 full buildout peak hour traffic including the background growth and the peak hour site trips from both the future development area and the Ebenezer Road Subdivision.


LEGEND:
$\longleftarrow 50 \%$ (50\%) TRIP DISTRIBUTION ENTERING (EXITING)

Figure 7: Subdivision Peak Hour Trip Distribution


LEGEND:

- 5 (16) TURNING MOVEMENT VOLUME AM (PM)

Figure 8: Subdivision Peak Hour Site Trips


LEGEND:
〔 5 (16) TURNING MOVEMENT VOLUME AM (PM)

Figure 9: 2027 Full Buildout Peak Hour Traffic

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## 5 Projected Capacity and Level of Service

Intersection capacity analyses were performed using the Synchro 11 Software at signalized intersection and the Highway Capacity Software 2023 at the two-way stop-controlled intersections in order to evaluate the AM and PM peak hours for existing, background and full buildout conditions. The existing signal timing at the signalized intersection was provided by City of Knoxville Department of Engineering and is included in Attachment 5.

## Level of Service

The results from the analyses are expressed with a term "level of service" (LOS), which is based on the amount of delay experienced at the intersection. The LOS index ranges from LOS A, indicating excellent traffic conditions with minimal delay, to LOS F indicating very congested conditions with excessive delay. LOS D generally is considered the minimum acceptable condition in urban areas. Table 51 shows the LOS index range for signalized and unsignalized intersections as defined by the Highway Capacity Manual (HCM).

Table 5-1
Level of Service (LOS) Index

| Level of Service | Signalized Intersection | Unsignalized Intersection |
| :--- | :--- | :--- |
| LOS A | $\leq 10 \mathrm{sec}$ | $\leq 10 \mathrm{sec}$ |
| LOS B | $10-20 \mathrm{sec}$ | $10-15 \mathrm{sec}$ |
| LOS C | $20-35 \mathrm{sec}$ | $15-25 \mathrm{sec}$ |
| LOS D | $35-55 \mathrm{sec}$ | $25-35 \mathrm{sec}$ |
| LOS E | $55-80 \mathrm{sec}$ | $35-50 \mathrm{sec}$ |
| LOS F | $>80 \mathrm{sec}$ | $>50 \mathrm{sec}$ |

The Synchro 11 worksheets are included in Attachments 6, 7, and 8. Table 5-2 shows the results of the capacity analyses.

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Table 5-2
Level of Service (LOS) Summary

| Intersection | Time Period | Year 2024 Existing (Delay/LOS) | Year 2027 <br> Background <br> (Delay/LOS) | Year 2027 <br> Full Buildout (Delay/LOS) |
| :---: | :---: | :---: | :---: | :---: |
| Kingston Pike (US 11/US 70) @ Ebenezer Road | AM Peak Intersection PM Peak Intersection | $\begin{aligned} & 20.8 / C \\ & 29.3 / C \end{aligned}$ | $\begin{aligned} & 21.0 / C \\ & 30.7 / C \\ & \hline \end{aligned}$ | $\begin{aligned} & 22.4 / C \\ & 37.5 / D \end{aligned}$ |
| Ebenezer Road @ Apartment Driveway | AM Peak <br> WB Approach <br> SB Approach <br> PM Peak <br> WB Approach <br> SB Approach |  |  | $\begin{aligned} & 12.5 / \mathrm{B} \\ & 1.2 / \mathrm{A} \\ & \\ & 14.1 / \mathrm{B} \\ & 1.7 / \mathrm{A} \end{aligned}$ |
| Ebenezer Road @ Driveway | AM Peak <br> WB Approach <br> SB Approach <br> PM Peak <br> WB Approach <br> SB Approach |  |  | $\begin{aligned} & 11.5 / \mathrm{B} \\ & 0.8 / \mathrm{A} \\ & \\ & 12.5 / \mathrm{B} \\ & 1.4 / \mathrm{A} \end{aligned}$ |

Notes:
1.Whole intersection weighted average control delay expressed in second per vehicle for signalized intersections and all-way stop controlled intersections.

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## 6 Queue Analysis

Table 6-1 presents the Synchro traffic queueing summary for the $95^{\text {th }}$ percentile queue at the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road for both the AM and PM peak hour.

Table 6-1
Synchro Queue Summary

| Intersection | Movement | Storage <br> Capacity <br> (ft) | Existing Conditions |  | Background Conditions |  | Full Buildout Conditions |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM | PM | AM | PM | AM | PM |
| Kingston Pk (US 70/US 11) <br> @ Ebenezer Rd | EBL | 140 | 16 | 27 | 16 | 28 | 16 | 29 |
|  | EBT | 585 | 292 | \#622 | 303 | \#691 | 310 | \#731 |
|  | EBR | 140 | 0 | 22 | 0 | 24 | 0 | 54 |
|  | WBL | 90 | 46 | 128 | 48 | 139 | 59 | 215 |
|  | WBT | 1,000+ | 164 | 277 | 171 | 288 | 171 | 288 |
|  | WBR | 100 | 0 | 1 | 0 | 1 | 0 | 1 |
|  | NBT | 1,000+ | 118 | \#169 | 120 | \#180 | 163 | \#259 |
|  | NBR | 50 | 54 | 61 | 55 | 65 | 101 | 127 |
|  | SBT | 240 | 31 | \#257 | 31 | \#268 | 33 | \#281 |
|  | SBR | 50 | 0 | 0 | 0 | 0 | 0 | 0 |

Notes:
The \# footnote indicates that the volume for the $95^{\text {th }}$ percentile cycle exceeds capacity.
Bold indicates queue length exceeds available storage capacity.
Bold cells indicate that the queue lengths are more than the available storage. The $95^{\text {th }}$ percentile queue length is defined as the queue length that has only a 5-percent probability of being exceeded during the analysis time period. The $95^{\text {th }}$ percentile queue length is typically used to determine the length of turning lanes in order to minimize the risk of blockage. Synchro assumes a vehicle length of 25 feet.

The northbound right turn lane has an existing storage length of 50 feet and an additional 30 feet of taper length before the queue from the signalized intersection would block the driveway to the retail strip center. The signalized intersection capacity analysis shows the full buildout $95 \%$ queue length for the northbound right turn lane of approximately 101 feet ( 4 vehicles) during the AM peak hour and 127 feet ( 5 vehicles) during the PM peak hour and the full buildout $50 \%$ queue length for the northbound right turn lane of approximately 28 feet ( 2 vehicles) during the AM peak hour and 44 feet ( 2 vehicles) during the PM peak hour.

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Therefore; the existing northbound right turn lane storage will exceed capacity and cause spillback into the thru lane less than $50 \%$ of time after the completion of the Ebenezer Road Subdivision.

## 7 Turn Lane Warrant Analysis

The intersection of Ebenezer Road at the proposed apartment roadway connection and the proposed subdivision roadway connection was evaluated to determine if a northbound right turn lane or a southbound left turn lane are warranted. The Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy," was used to analyze the information.

At the intersection of Ebenezer Road at the proposed roadway connection to the Future Development Area a southbound left turn is warranted during the PM peak hour and a northbound right turn lane is not warranted during either the AM and or PM peak hours after the full buildout of the Ebenezer Road Subdivision and Future Development Area.

At the intersection of Ebenezer Road at the proposed roadway connection to the Ebenezer Road Subdivision neither a southbound left turn lane nor a northbound right turn lane are warranted during the AM or PM peak hours.

The turn lane warrant worksheets and analysis are included in Attachment 9.

## 8 Conclusions and Recommendations

### 8.1 Kingston Pike (US 11/US 70) at Ebenezer Road

The existing intersection of Kingston Pike (US 11/US 70) at Ebenezer Road is a signalized four-legged intersection. The southbound approach is an existing shopping center driveway connection. The existing signal timing was provided by the City of Knoxville.

Under the existing and 2027 background conditions the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road operates at an acceptable LOS C during both the AM and PM peak hours.

After the completion of the Ebenezer Road Subdivision including the future development area the traffic conditions for the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road will operate at an acceptable LOS C during the AM peak hour and a LOS D during the PM peak hour.

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The $95 \%$ queue length is defined as the queue length that has only a 5-percent probability of being exceeded during the analysis time period. The $95 \%$ queue length is typically used to determine the length of turning lanes in order to minimize the risk of blockage.

The northbound right turn lane has an existing storage length of 50 feet and an additional 30 feet of taper length before the queue from the signalized intersection would block the driveway to the retail strip center. The signalized intersection capacity analysis shows the full buildout $95 \%$ queue length for the northbound right turn lane of approximately 101 feet ( 4 vehicles) during the AM peak hour and 127 feet ( 5 vehicles) during the PM peak hour and the full buildout $50 \%$ queue length for the northbound right turn lane of approximately 28 feet ( 2 vehicles) during the AM peak hour and 44 feet ( 2 vehicles) during the PM peak hour.

The northbound right turn lane (Ebenezer Road) will exceed capacity after the completion of the Ebenezer Road Subdivision and Future Development Area. There are several existing constraints including the location of guard rails and power poles and the proximity to Ten Mile Creek that would make extending the storage length of the right turn lane difficult to construct. Ardurra recommends that any future intersection improvements be reviewed, coordinated and approved by both the City of Knoxville Department of Engineering and Knox County Engineering and Public Works.

### 8.2 Ebenezer Road at Future Development Area

The proposed full buildout conditions at the unsignalized intersection of Ebenezer Road at the Future Development Area Roadway were analyzed using the Highway Capacity Software (HCS2023).

A southbound left turn lane is warranted during the PM peak hour and a northbound right turn lane is not warranted at the intersection of Ebenezer Road at Future Development Area Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

The southbound left turn lane has a recommended minimum storage length of 50 feet per the AASHTO Greenbook "A Policy on Geometric Design of Highways and Streets."

After the completion of the full buildout of the Ebenezer Road Subdivision including the proposed roadway improvements the intersection of Ebenezer Road at Future Development Area Roadway will operate as follows. The westbound approach (Apartment Roadway) will operate at a LOS B during both the AM and PM peak

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hours and the southbound approach (Ebenezer Road) will operate at a LOS A during both the AM and PM peak hours.

Ebenezer Road is classified as Minor Collector per the Major Road Plan. The minimum intersection spacing required on a collector road is 300 feet per the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022.

The minimum required sight distance for a road with a posted speed limit of 30 mph is 300 feet in each direction in accordance with the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022.

The location of the proposed apartment roadway for the Future Development Area is still under consideration.

Ardurra recommends that the intersection sight distance be certified by a land surveyor prior to construction in order to verify that Ebenezer Road has adequate intersection sight distance at the proposed apartment roadway connection to comply with Knox County Engineering and Public Works guidelines.

Ardurra recommends that the signs and pavement markings be installed in accordance with the standards provided in the Manual on Uniform Traffic Control Devices (MUTCD).

Any future improvements to the intersection or the various traffic management infrastructure, would need to be reviewed, coordinated, and approved by Knox County Engineering and Public Works.

### 8.3 Ebenezer Road at Ebenezer Subdivision

The proposed full buildout conditions at the unsignalized intersection of Ebenezer Road at the Ebenezer Subdivision Roadway were analyzed using the Highway Capacity Software (HCS2023).

Neither a southbound left turn lane nor a northbound right turn lane is warranted at the intersection of Ebenezer Road at Ebenezer Subdivision Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

After the completion of the full buildout of the Ebenezer Road Subdivision the intersection of Ebenezer Road at Subdivision Roadway will operate as follows. The westbound approach (Subdivision Roadway) will operate at a LOS B during both the

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AM and PM peak hours and the southbound approach (Ebenezer Road) will operate at a LOS A during both the AM and PM peak hours.

Ebenezer Road is classified as Minor Collector per the Major Road Plan. The minimum intersection spacing required on a collector road is 300 feet per the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022. The Ebenezer Subdivision Roadway is located approximately 535 feet north of Rosemont Boulevard; therefore, the minimum separation on a collector is met and no change is necessary.

The minimum required sight distance for a road with a posted speed limit of 30 mph is 300 feet in each direction in accordance with the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022.

At 15 feet from the edge of pavement the intersection sight distance is greater than 300 feet looking both northbound and southbound. Attachment 10 includes pictures of the intersection sight distance at the intersection of Ebenezer Road at Ebenezer Subdivision Roadway.

Ardurra recommends that the intersection sight distance be certified by a land surveyor prior to construction in order to verify that Ebenezer Road has adequate intersection sight distance at the proposed apartment roadway connection to comply with Knox County Engineering and Public Works guidelines.

Ardurra recommends that the signs and pavement markings be installed in accordance with the standards provided in the Manual on Uniform Traffic Control Devices (MUTCD).

Any future improvements to the intersection or the various traffic management infrastructure, would need to be reviewed, coordinated, and approved by Knox County Engineering and Public Works.

## Attachment 1 <br> Aerial Photos



Kingston Pike (SR 70) at Ebenezer Road - Signalized


Ebenezer Road Guardrail - Northbound


Ebenezer Road Guardrail - Southbound

Attachment 2
Traffic Counts

Project: 330.029 Ebenezer Rd Subdivision Intersection: Kingston Pike at Ebenezer Road
Date Conducted: Tuesday March 19,2024

|  | Driveway Southbound |  |  |  | Kingston Pike Westbound |  |  |  | Ebenezer Road Northbound |  |  |  | Kingston Pike Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Int. Total |
| 7:00 AM | 0 | 0 | 0 | 0 | 7 | 81 | 3 | 91 | 13 | 0 | 18 | 31 | 0 | 65 | 3 | 68 | 190 |
| 7:15 AM | 0 | 0 | 2 | 2 | 6 | 104 | 1 | 111 | 17 | 1 | 32 | 50 | 0 | 130 | 8 | 138 | 301 |
| 7:30 AM | 2 | 4 | 2 | 8 | 14 | 98 | 4 | 116 | 27 | 1 | 45 | 73 | 0 | 154 | 9 | 163 | 360 |
| 7:45 AM | 1 | 0 | 2 | 3 | 17 | 158 | 4 | 179 | 31 | 4 | 48 | 83 | 4 | 209 | 13 | 226 | 491 |
| Total | 3 | 4 | 6 | 13 | 44 | 441 | 12 | 497 | 88 | 6 | 143 | 237 | 4 | 558 | 33 | 595 | 1342 |
| 8:00 AM | 4 | 3 | 3 | 10 | 15 | 141 | 3 | 159 | 29 | 2 | 49 | 80 | 3 | 217 | 15 | 235 | 484 |
| 8:15 AM | 1 | 3 | 1 | 5 | 21 | 160 | 8 | 189 | 20 | 2 | 46 | 68 | 1 | 213 | 10 | 224 | 486 |
| 8:30 AM | 4 | 0 | 5 | 9 | 20 | 170 | 13 | 203 | 25 | 6 | 30 | 61 | 2 | 154 | 7 | 163 | 436 |
| 8:45 AM | 5 | 7 | 2 | 14 | 14 | 150 | 4 | 168 | 22 | 3 | 36 | 61 | 3 | 182 | 12 | 197 | 440 |
| Total | 14 | 13 | 11 | 38 | 70 | 621 | 28 | 719 | 96 | 13 | 161 | 270 | 9 | 766 | 44 | 819 | 1846 |
| 9:00 AM | 4 | 3 | 0 | 7 | 15 | 115 | 9 | 139 | 20 | 2 | 26 | 48 | 0 | 139 | 14 | 153 | 347 |
| 9:15 AM | 7 | 4 | 1 | 12 | 6 | 171 | 6 | 183 | 20 | 2 | 21 | 43 | 2 | 158 | 19 | 179 | 417 |
| 9:30 AM | 4 | 1 | 0 | 5 | 13 | 129 | 8 | 150 | 22 | 0 | 26 | 48 | 1 | 142 | 11 | 154 | 357 |
| 9:45 AM | 3 | 0 | 0 | 3 | 21 | 173 | 9 | 203 | 15 | 0 | 28 | 43 | 3 | 163 | 11 | 177 | 426 |
| Total | 18 | 8 | 1 | 27 | 55 | 588 | 32 | 675 | 77 | 4 | 101 | 182 | 6 | 602 | 55 | 663 | 1547 |
| 10:00 AM | 9 | 6 | 2 | 17 | 11 | 158 | 10 | 179 | 18 | 5 | 10 | 33 | 1 | 133 | 8 | 142 | 371 |
| 10:15 AM | 4 | 6 | 3 | 13 | 7 | 175 | 11 | 193 | 13 | 4 | 17 | 34 | 3 | 196 | 10 | 209 | 449 |
| 10:30 AM | 9 | 4 | 3 | 16 | 13 | 193 | 13 | 219 | 16 | 6 | 22 | 44 | 2 | 147 | 8 | 157 | 436 |
| 10:45 AM | 6 | 4 | 3 | 13 | 13 | 194 | 15 | 222 | 17 | 3 | 16 | 36 | 1 | 191 | 12 | 204 | 475 |
| Total | 28 | 20 | 11 | 59 | 44 | 720 | 49 | 813 | 64 | 18 | 65 | 147 | 7 | 667 | 38 | 712 | 1731 |
| 11:00 AM | 14 | 6 | 4 | 24 | 14 | 199 | 14 | 227 | 21 | 8 | 15 | 44 | 6 | 189 | 14 | 209 | 504 |
| 11:15 AM | 5 | 4 | 8 | 17 | 14 | 220 | 12 | 246 | 26 | 4 | 16 | 46 | 2 | 207 | 11 | 220 | 529 |
| 11:30 AM | 12 | 6 | 4 | 22 | 21 | 191 | 14 | 226 | 23 | 6 | 15 | 44 | 6 | 185 | 22 | 213 | 505 |
| 11:45 AM | 7 | 7 | 6 | 20 | 19 | 259 | 12 | 290 | 17 | 5 | 25 | 47 | 5 | 265 | 18 | 288 | 645 |
| Total | 38 | 23 | 22 | 83 | 68 | 869 | 52 | 989 | 87 | 23 | 71 | 181 | 19 | 846 | 65 | 930 | 2183 |
| 12:00 PM | 11 | 3 | 7 | 21 | 25 | 226 | 12 | 263 | 24 | 7 | 22 | 53 | 6 | 231 | 9 | 246 | 583 |
| 12:15 PM | 15 | 1 | 7 | 23 | 20 | 259 | 16 | 295 | 20 | 2 | 27 | 49 | 4 | 255 | 17 | 276 | 643 |
| 12:30 PM | 14 | 10 | 3 | 27 | 13 | 264 | 12 | 289 | 23 | 3 | 28 | 54 | 3 | 231 | 28 | 262 | 632 |
| 12:45 PM | 6 | 5 | 4 | 15 | 24 | 269 | 10 | 303 | 19 | 7 | 19 | 45 | 7 | 256 | 15 | 278 | 641 |
| Total | 46 | 19 | 21 | 86 | 82 | 1018 | 50 | 1150 | 86 | 19 | 96 | 201 | 20 | 973 | 69 | 1062 | 2499 |
| 1:00 PM | 19 | 4 | 6 | 29 | 16 | 197 | 14 | 227 | 26 | 1 | 18 | 45 | 6 | 207 | 15 | 228 | 529 |
| 1:15 PM | 12 | 3 | 5 | 20 | 15 | 268 | 18 | 301 | 24 | 5 | 18 | 47 | 2 | 262 | 25 | 289 | 657 |
| 1:30 PM | 12 | 7 | 4 | 23 | 14 | 261 | 15 | 290 | 29 | 2 | 16 | 47 | 5 | 221 | 23 | 249 | 609 |
| 1:45 PM | 8 | 2 | 4 | 14 | 19 | 307 | 19 | 345 | 29 | 4 | 17 | 50 | 5 | 246 | 18 | 269 | 678 |
| Total | 51 | 16 | 19 | 86 | 64 | 1033 | 66 | 1163 | 108 | 12 | 69 | 189 | 18 | 936 | 81 | 1035 | 2473 |
| 2:00 PM | 17 | 6 | 8 | 31 | 17 | 243 | 18 | 278 | 16 | 4 | 22 | 42 | 3 | 213 | 29 | 245 | 596 |
| 2:15 PM | 13 | 7 | 6 | 26 | 23 | 261 | 14 | 298 | 19 | 3 | 16 | 38 | 2 | 251 | 22 | 275 | 637 |
| 2:30 PM | 4 | 7 | 3 | 14 | 16 | 269 | 11 | 296 | 20 | 5 | 15 | 40 | 4 | 217 | 20 | 241 | 591 |
| 2:45 PM | 9 | 4 | 3 | 16 | 19 | 251 | 19 | 289 | 28 | 4 | 22 | 54 | 3 | 244 | 13 | 260 | 619 |
| Total | 43 | 24 | 20 | 87 | 75 | 1024 | 62 | 1161 | 83 | 16 | 75 | 174 | 12 | 925 | 84 | 1021 | 2443 |
| 3:00 PM | 9 | 8 | 6 | 23 | 22 | 231 | 12 | 265 | 32 | 2 | 23 | 57 | 3 | 237 | 22 | 262 | 607 |
| 3:15 PM | 9 | 8 | 1 | 18 | 21 | 270 | 15 | 306 | 20 | 4 | 17 | 41 | 5 | 269 | 29 | 303 | 668 |
| 3:30 PM | 11 | 7 | 4 | 22 | 26 | 257 | 15 | 298 | 33 | 8 | 30 | 71 | 1 | 221 | 20 | 242 | 633 |
| 3:45 PM | 11 | 8 | 5 | 24 | 37 | 304 | 14 | 355 | 26 | 2 | 18 | 46 | 5 | 266 | 20 | 291 | 716 |
| Total | 40 | 31 | 16 | 87 | 106 | 1062 | 56 | 1224 | 111 | 16 | 88 | 215 | 14 | 993 | 91 | 1098 | 2624 |
| 4:00 PM | 12 | 7 | 5 | 24 | 26 | 218 | 11 | 255 | 32 | 1 | 29 | 62 | 10 | 264 | 27 | 301 | 642 |
| 4:15 PM | 6 | 7 | 2 | 15 | 27 | 251 | 11 | 289 | 28 | 3 | 23 | 54 | 4 | 320 | 27 | 351 | 709 |
| 4:30 PM | 21 | 9 | 1 | 31 | 32 | 226 | 12 | 270 | 28 | 7 | 29 | 64 | 3 | 303 | 23 | 329 | 694 |
| 4:45 PM | 12 | 11 | 2 | 25 | 28 | 261 | 14 | 303 | 18 | 4 | 28 | 50 | 4 | 328 | 25 | 357 | 735 |
| Total | 51 | 34 | 10 | 95 | 113 | 956 | 48 | 1117 | 106 | 15 | 109 | 230 | 21 | 1215 | 102 | 1338 | 2780 |
| 5:00 PM | 28 | 15 | 2 | 45 | 44 | 247 | 7 | 298 | 35 | 3 | 41 | 79 | 5 | 309 | 25 | 339 | 761 |
| 5:15 PM | 30 | 13 | 4 | 47 | 38 | 253 | 8 | 299 | 29 | 6 | 40 | 75 | 6 | 313 | 28 | 347 | 768 |
| 5:30 PM | 27 | 11 | 6 | 44 | 33 | 231 | 13 | 277 | 18 | 5 | 24 | 47 | 1 | 299 | 33 | 333 | 701 |
| 5:45 PM | 19 | 15 | 5 | 39 | 32 | 280 | 13 | 325 | 22 | 5 | 31 | 58 | 7 | 356 | 21 | 384 | 806 |
| Total | 104 | 54 | 17 | 175 | 147 | 1011 | 41 | 1199 | 104 | 19 | 136 | 259 | 19 | 1277 | 107 | 1403 | 3036 |
| Grand Total | 436 | 246 | 154 | 836 | 868 | 9343 | 496 | 10707 | 1010 | 161 | 1114 | 2285 | 149 | 9758 | 769 | 10676 | 24504 |
| Approach \% | 52.2 | 29.4 | 18.4 |  | 8.1 | 87.3 | 4.6 |  | 44.2 | 7.0 | 48.8 |  | 1.4 | 91.4 | 7.2 |  |  |
| Total \% | 1.8 | 1.0 | 0.6 | 3.4 | 3.5 | 38.1 | 2.0 | 43.7 | 4.1 | 0.7 | 4.5 | 9.3 | 0.6 | 39.8 | 3.1 | 43.6 |  |

Project: $\mathbf{3 3 0 . 0 2 9}$ Ebenezer Rd Subdivision
Intersection: Kingston Pike at Ebenezer Road
Date Conducted: Tuesday March 19,2024

| AM Peak Hour | 7:45 AM - 8:45 AM | 1897 |
| :--- | :--- | :--- |
| PM Peak Hour | 5:00 PM - 6:00 PM | 3036 |


|  | Driveway Southbound |  |  |  | Kingston Pike Westbound |  |  |  | Ebenezer Road Northbound |  |  |  | Kingston Pike Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Int. Total |
| Peak Hour Analysis from 7:00 AM to 9:00 AM AM Peak Hour begins at 7:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:45 AM | 1 | 0 | 2 | 3 | 17 | 158 | 4 | 179 | 31 | 4 | 48 | 83 | 4 | 209 | 13 | 226 | 491 |
| 8:00 AM | 4 | 3 | 3 | 10 | 15 | 141 | 3 | 159 | 29 | 2 | 49 | 80 | 3 | 217 | 15 | 235 | 484 |
| 8:15 AM | 1 | 3 | 1 | 5 | 21 | 160 | 8 | 189 | 20 | 2 | 46 | 68 | 1 | 213 | 10 | 224 | 486 |
| 8:30 AM | 4 | 0 | 5 | 9 | 20 | 170 | 13 | 203 | 25 | 6 | 30 | 61 | 2 | 154 | 7 | 163 | 436 |
| Total Volume | 10 | 6 | 11 | 27 | 73 | 629 | 28 | 730 | 105 | 14 | 173 | 292 | 10 | 793 | 45 | 848 | 1897 |
| Future (1.0\% over 3 yrs ) | 10 | 6 | 11 |  | 75 | 648 | 29 |  | 108 | 14 | 178 |  | 10 | 817 | 46 |  | 1954 |
| PHF | 0.63 | 0.50 | 0.55 |  | 0.87 | 0.93 | 0.54 |  | 0.85 | 0.58 | 0.88 |  | 0.63 | 0.91 | 0.75 |  | 0.97 |
| Peak Hour Analysis from 3:00 PM to 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak Hour begins at 5:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM | 28 | 15 | 2 | 45 | 44 | 247 | 7 | 298 | 35 | 3 | 41 | 79 | 5 | 309 | 25 | 339 | 761 |
| 5:15 PM | 30 | 13 | 4 | 47 | 38 | 253 | 8 | 299 | 29 | 6 | 40 | 75 | 6 | 313 | 28 | 347 | 768 |
| 5:30 PM | 27 | 11 | 6 | 44 | 33 | 231 | 13 | 277 | 18 | 5 | 24 | 47 | 1 | 299 | 33 | 333 | 701 |
| 5:45 PM | 19 | 15 | 5 | 39 | 32 | 280 | 13 | 325 | 22 | 5 | 31 | 58 | 7 | 356 | 21 | 384 | 806 |
| Total Volume | 104 | 54 | 17 | 175 | 147 | 1011 | 41 | 1199 | 104 | 19 | 136 | 259 | 19 | 1277 | 107 | 1403 | 3036 |
| Future (1.0\% over 3 yrs ) | 107 | 56 | 18 |  | 151 | 1042 | 42 |  | 107 | 20 | 140 |  | 20 | 1316 | 110 |  | 3128 |
| PHF | 0.87 | 0.90 | 0.71 |  | 0.84 | 0.90 | 0.79 |  | 0.74 | 0.79 | 0.83 |  | 0.68 | 0.90 | 0.81 |  | 0.94 |

Attachment 3
ADT Trends


Most Recent Trend Line Growth

| Year | ADT |
| :--- | :--- |
| 2013 | 6321 |
| 2023 | 4581 |

Annual Percent Growth -3.80\%


| Most Recent Trend Line Growth |  |
| :---: | :---: |
| Year | ADT |
| 2012 | 26019 |
| 2022 | 27645 |

Annual Percent Growth
0.59\%

Attachment 4
Trip Generation

Project: Ebenezer Subdivision - Future Development Area
Date Conducted: 4/12/2024
Local Apartment Trip Generation Study
278 Units

Average Daily Traffic
$\mathrm{T}=15.193(\mathrm{X})^{\wedge} 0.899$
$\mathrm{T}=15.193(278)^{\wedge} 0.899$
$\mathrm{T}=2392$

Peak Hour of Adjacent Street Traffic
One Hour Between 7 and 9 a.m.
$\mathrm{T}=0.758(\mathrm{X})^{\wedge} 0.924$
$\mathrm{T}=0.758(278)^{\wedge} 0.924$
$\mathrm{T}=137$

Peak Hour of Adjacent Street Traffic
One Hour Between 4 and 6 p.m.
$\mathrm{T}=0.669(\mathrm{X})+10.069$
$\mathrm{T}=0.669(278)+10.069$
$\mathrm{T}=196$

|  |  | Percent |  | Number |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Time Period | Total Trips | Enter | Exit | Enter | Exit |
| Weekday (24 hours) | 2392 | $50 \%$ | $50 \%$ | 1196 | 1196 |
| AM Peak Hour | 137 | $22 \%$ | $78 \%$ | 30 | 107 |
| PM Peak Hour | 196 | $55 \%$ | $45 \%$ | 108 | 88 |

Project: Ebenezer Road Subdivision
Date Conducted: 4/12/2024
Single-Family Detached Housing (LUC 210)
113 Lots

Average Daily Traffic
$\operatorname{Ln}(T)=0.92 \operatorname{Ln}(X)+2.68$
$\operatorname{Ln}(T)=0.92 \operatorname{Ln}(113)+2.68$
$\mathrm{T}=1129$

Peak Hour of Adjacent Street Traffic
One Hour Between 7 and 9 a.m.
$\operatorname{Ln}(\mathrm{T})=0.91 \operatorname{Ln}(\mathrm{X})+0.12$
$\operatorname{Ln}(T)=0.91 \operatorname{Ln}(113)+0.12$
$\mathrm{T}=83$

Peak Hour of Adjacent Street Traffic One Hour Between 4 and 6 p.m.
$\operatorname{Ln}(T)=0.94 \operatorname{Ln}(X)+0.27$
$\operatorname{Ln}(T)=0.94 \operatorname{Ln}(113)+0.27$
$\mathrm{T}=112$

|  |  | Percent |  | Number |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Time Period | Total Trips | Enter | Exit | Enter | Exit |
| Weekday (24 hours) | 1129 | $50 \%$ | $50 \%$ | 565 | 565 |
| AM Peak Hour | 83 | $25 \%$ | $75 \%$ | 21 | 62 |
| PM Peak Hour | 112 | $63 \%$ | $37 \%$ | 71 | 41 |

## MEMORANDUM

To: $\quad$ Traffic Impact Study Reviewers and Preparers (see attached list)
From: Mike Conger $10{ }^{\circ}$
Date: August 14, 2000
Subject: Local Trip Generation Rates for Multi-Family Residential Uses

Attached please find a summary of the final report with data plots for the Knox County Local Apartment Trip Generation Study. As you will recall, this report was discussed when the traffic impact study group last convened this past February. A consensus was reached at that meeting that the trip generation rates developed in the local study should be used for new apartment complexes and any other "multi-family" residential uses that are being proposed.

The MPC voted at its July 2000 meeting to officially amend the Traffic Impact Study Guidelines with language which reads that "trip generation rates for proposed uses shall be calculated using the latest edition of the ITE Trip Generation Manual, or using local data when it is available". This amendment allows the full implementation of the new rates, and they should be used for future proposed multi-family developments unless it can be demonstrated otherwise.

Thanks for your assistance and cooperation in this matter, if there are any questions or comments, please let me know.

## TRAFFIC IMPACT STUDY REVIEWER \& PREPARER GROUP

| Name | Organization | Phone Number |
| :--- | :--- | :--- |
| Daniel Armstrong | Wilbur Smith | $584-8584$ |
| Rusty Baksa | Land Dev. Solutions | $671-2281$ |
| Kim Henry Begg | SITE, inc. | $693-5010$ |
| Mark Best | TDOT | $594-9170$ |
| Alan Childers | Cannon \& Cannon | $988-4818$ |
| Steve Drummer | Barge Waggoner | $637-2810$ |
| Mark Geldmeier | City of Knoxville | $215-6100$ |
| John Gould | Wilbur Smith | $584-8584$ |
| Barbara Hatcher | SITE, inc. | $693-5010$ |
| John Heid | AR/TEC | $681-8848$ |
| Bill Kervin | Allen Hoshall | $694-1834$ |
| Hollis Loveday | Wilbur Smith | $584-8584$ |
| David McGinley | City of Knoxville | $215-2148$ |
| David Moore | TDOT | $594-9170$ |
| Linda Mosch | Consultant | $777-2025$ |
| Amanda Rule | TDOT | $594-9170$ |
| Cindy Pionke | Knox County | $215-5800$ |
| Pam Porter | TDOT | $594-9170$ |
| John Sexton | Allen Hoshall | $694-1834$ |
| Jim Snowden | Knox County | $215-5800$ |
| Darcy Sullivan | SITE, inc. | $693-5010$ |
| Jeff Welch | MPC | $215-2500$ |

## KNOX COUNTY <br> LOCAL APARTMENT TRIP GENERATION STUDY

## PURPOSE

A Traffic Impact Study (TIS) is currently required in Knox County when a proposed development is projected to generate in excess of 750 trips per day. The determinations of when the threshold is met as well as all subsequent analyses in the TIS are performed using the rates and equations given in the Institute of Transportation Engineers (ITE) Trip Generation Manual. Local governmental agencies rely heavily on the accuracy of these trip generation rates in order to correctly predict the impacts of a proposed development on the transportation system. Therefore, in certain instances, it is logical to verify whether the "national" rates and equations given in the ITE Trip Generation Manual are appropriate for use in a specific local area or region.

The decision was made to study the local trip-making characteristics of apartments because of the discrepancy between the trip generation rates for apartments and single family residential land uses as given in the ITE Trip Generation Manual. While these two land uses are similar in nature, the Trip Generation Manual predicts about three less trips per dwelling unit generated by apartments for the average weekday. Additionally the Trip Generation Manual points out that due to the age of their database, which dates back to the 1960 's, "the rates for apartments probably had changed over time". It is also assumed that some of the ITE data had come from larger metropolitan areas with denser development and greater transit use than Knox County, which would contribute to lower trip generation rates. Therefore, this study will be used to either verify the rates given in the Trip Generation Manual or generate new ones that can be applied to locally proposed apartment developments.

## PROCEDURE

The procedures recommended by ITE in conducting local trip generation studies were generally followed for this study, along with some important assumptions that have made. ITE has published a proposed recommended practice entitled "Trip Generation Handbook" which specifically outlines procedures for conducting local trip generation studies and establishing new rates and equations.

The first step in the study was to define the number and location of the sites to be studied, as well as the counting methodology. Initially 14 sites were selected, although one apartment complex - the College Park Apartments - was later omitted due to uncharacteristically high traffic generation numbers. The number of sites used in this study far exceeds the recommended minimum amount suggested by ITE, which is five sites. Traffic counts were taken for week-long periods at 15 -minute intervals between July 22, 1996 and August 9, 1996 at the access points to the apartment complexes. A Technical Appendix to this report contains the traffic count data collected at each apartment complex.

## RESULTS

The traffic count data was analyzed using spreadsheets in order to determine the weighted average rates and regression equations. In order to be considered valid, the local rates and equations for each time period of analysis that were generated must meet certain statistical criteria. First, the standard deviation of the independent variable (dwelling units) should be no more than 110 percent of the weighted average rate; and secondly, the regression equations require a computed coefficient of determination ( $\mathrm{R}^{2}$ ) value of at least 0.75 before good data fit is indicated. This statistical criteria is met by the local data results, and in fact it often exceeds the level of data fit given by their counterparts in the ITE Trip Generation Manual. Finally, in order to simplify the use of the local data, plots were generated that appear identical to the actual ones in the ITE Trip Generation Manual.

The resulting rates and equations calculated from the local data indicate that the average weekday trip generation of apartments in this area is well above the national rates reported in the ITE manual. For example, the locally computed average rate for number of trips generated during a weekday is $35 \%$ higher than the rate given by ITE (increase from 6.63 trips per dwelling unit to 9.03 trips per dwelling unit). The trip generation rates do not increase as much for the AM and PM peak hours however. The local rate is roughly $8 \%$ higher for the AM peak, and $16 \%$ higher for the PM peak. The plots from the ITE Trip Generation Manual are included in the Technical Appendix for comparison purposes.

## ASSUMPTIONS MADE

Some important assumptions have been made which may affect the results of the local data that was collected:
$>$ It is important to note that the local trip generation rates were computed for the total number of dwelling units in the apartment complex, and not necessarily for the number of occupied dwelling units. There are several reasons why this was done, chiefly because of the need for comparability with the rates given in ITE Trip Generation Manual, as it does not specify whether the dwelling units are occupied. According to ITE procedures the selected sites must only be of "reasonably full occupancy (i.e. at least 85\%)". The Apartment Association of Greater Knoxville (AAGK) publishes quarterly reports on occupancy levels of apartment complexes, and the report covering the period of the data collection was reviewed to determine occupancy levels. According to the AAGK report from July 1, 1996 - September 30, 1996 all of the apartment complexes surveyed in this study met the minimum $85 \%$ occupancy level, with an average occupancy rate for all sites studied of $94 \%$.
$>$ The count data that was collected at each apartment complex was used "raw" meaning that it was not factored for possible daily or seasonal variations. Once again, according to an ITE representative it is not known whether the data used in the Trip Generation Manual was factored or not, so therefore in order to be able to compare
local rates to those in the manual you must assume that count data should not be factored. Additionally, it was felt that apartment complexes would generally not be as susceptible to major seasonal fluctuations as other land uses might be. The local rates were also developed using count data that was collected and averaged over an entire week, which should limit some of the daily variations. Finally, reliable local daily and seasonal variation factors do not truly exist.

## CONCLUSION

The local apartment study methodology and results were distributed for comment to a group of local transportation professionals who are directly responsible for either preparing or reviewing traffic impact studies. A meeting was held between this group on February 16, 2000 in order to gather comments and discuss the study in greater detail. The following conclusions are based on the discussion and consensus reached at this meeting:

1. The trip generation rates and equations meet statistical requirements and resulted from a study that followed accepted procedures; therefore they should be adopted for future use. Furthermore, the rates and equations are recommended for use in reviewing the traffic impact of any development termed as "multi-family", such as townhouse and condominium developments due to their similarity to apartment complexes.
2. The Traffic Access and Impact Study Guidelines and Procedures adopted by MPC should be amended with the language that local data should be used when available, which will allow the implementation of these new multi-family trip generation rates.
3. The following suggestions were made for future consideration:

- This study should be updated with data collected from local townhouse and condominium developments in order to further justify the use of the new trip generation rates.
- A statistical comparison should be made between any newly developed rates and the ITE single family trip generation rates to determine if there is a significant difference. If there is no difference then perhaps ITE single-family rates could be used for any residential development proposed in Knox County.


# Local Apartment Trip Generation Study 

Average Vehicle Trip Ends vs: Dwelling Units On a: Weekday

Number of Studies: 13<br>Average Number of Dwelling Units: 193<br>Directional Distribution: $50 \%$ entering, $50 \%$ exiting

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 9.03 | $6.59-17.41$ | 2.47 |

Data Plot and Equation


# Local Apartment Trip Generation Study 

Average Vehlcle Trip Ends vs: Dwelling Units<br>On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.<br>Number of Studies: 13<br>Average Number of Dwelling Units: 193<br>Directional Distribution: $22 \%$ entering, $78 \%$ exiting

Trip Generation Per Dwelling Unlt

| Average Rate | Ranges of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.55 | $0.14-0.78$ | 0.18 |

Data Plot and Equation


# Local Apartment Trip Generation Study 

| Average Vehicle Trip Ends vs: |  |
| ---: | :--- |
| On a: | Dwelling Units <br> Weekday, <br> Peak Hour of Adjacent Street Traffic, <br> One Hour Between 4 and 6 p.m. |
|  |  |
| Number of Studies: | 13 |
| Average Number of Dwelling Units: | 193 |
| Directional Distribution: | $55 \%$ entering, $45 \%$ exiting |

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.72 | $0.32-1.66$ | 0.25 |

Data Plot and Equation


# Single-Family Detached Housing (210) 

Vehicle Trip Ends vs: Dwelling Units
On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 174
Avg. Num. of Dwelling Units: 246
Directional Distribution: 50\% entering, 50\% exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 9.43 | $4.45-22.61$ | 2.13 |

Data Plot and Equation


## Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units
On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

## Setting/Location: General Urban/Suburban

Number of Studies: 192
Avg. Num. of Dwelling Units: 226
Directional Distribution: $26 \%$ entering, $74 \%$ exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.70 | $0.27-2.27$ | 0.24 |

Data Plot and Equation


## Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units
On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

## Setting/Location: General Urban/Suburban

Number of Studies: 208
Avg. Num. of Dwelling Units: 248
Directional Distribution: 63\% entering, 37\% exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.94 | $0.35-2.98$ | 0.31 |

Data Plot and Equation


## Attachment 5 <br> Signal Timing

Intersection Name : Kingston Pike and Ebenezer Rd

| Basic Timing (seconds) | Phase 1 | Phase 2 | Phase 3 | Phase 4 | Phase 5 | Phase 6 | Phase 7 | Phase 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Min Green | $\mathbf{6}$ | $\mathbf{1 8}$ | $\mathbf{8}$ | $\mathbf{8}$ |  | 18 |  |  |
| Gap / Extension | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{3}$ | $\mathbf{2}$ |  | 3 |  |  |
| Max 1 | 20 | 50 | 30 | 15 |  | 50 |  |  |
| Max 2 | 25 | 55 | 25 | 30 |  | 55 |  |  |
| Yellow Clearance | 4 | 4.5 | 4 | 4 |  | 4.5 |  |  |
| Red Clearance | 1.5 | 1.5 | 2 | 3 |  | 1.5 |  |  |
| Walk | N/A | N/A | N/A | N/A |  | N/A |  |  |
| Pedestrian Clearance | N/A | N/A | N/A | N/A |  | N/A |  |  |
| Max Recall |  | X |  |  |  | X |  |  |
| Active (Enable) Phases | X | X | X | X |  | X |  |  |
| Flashing Yellow Arrow |  |  |  |  |  |  |  |  |
| Overlaps (1-4) |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |


| Coordination Timing/(seconds) |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Split \# | Coord. Phase | Phase 1 | Phase 2 | Phase 3 | Phase 4 | Phase 5 | Phase 6 | Phase 7 | Phase 8 |  |
| Split 1 | 2 | 17 | 36 | 21 | 21 |  | 53 |  |  |  |
| Split 2 | 2 | 16 | 38 | 28 | 18 |  | 54 |  |  |  |
| Split 3 | 2 | 18 | 60 | 21 | 21 |  | 78 |  |  |  |
| Split 4 | 2 | 26 | 54 | 20 | 20 |  | 80 |  |  |  |
| Split 5 | 2 | 18 | 63 | 19 | 25 |  | 81 |  |  |  |
| Split 6 | 2 | 28 | 63 | 22 | 22 |  | 91 |  |  |  |


| Pattern Table |  |  |  |  | Lead / Lag |  | Fixed / Floating | Fixed |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pattern\# | Cycle | Offset | Split | Seq. \# | Phase \# |  | Beginning of <br> (Green/Yellow) | Yellow |
| 1 | 95 | 22 | 1 | 1 | 1 |  | Intersection ID\# | 252 |
| 2 | 100 | 76 | 2 | 1 | 1 |  | I/P Address | N/A |
| 3 | 120 | 18 | 3 | 1 | 1 |  | Hub Address | N/A |
| 4 | 120 | 24 | 4 | 1 | 1 |  | Radio Address |  |
| 5 | 125 | 24 | 5 | 1 | 1 |  | Comm. Type | N/A |
| 6 | 135 | 13 | 6 | 1 | 1 |  | Detection | Inductive Loops |


| Day Plan | HH:MM | Pattern | Day Plan | HH:MM | Pattern |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 00:00 | 54 | 2 | 00:00 | 54 |
| 1 | 6:00 | 2 | 2 | 7:00 | 1 |
| 1 | 9:30 | 3 | 2 | 8:00 | 5 |
| 1 | 14:00 | 4 | 2 | 21:00 | 1 |
| 1 | 18:30 | 1 | 2 | 23:00 | 54 |
| 1 | 23:00 | 54 |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Year Plan Scheduler |  |  |  |  |  |
| Plan | Month of Year: 01-12 |  | Day of Month: 01-31 |  | Plan |
| M - F | 1-12 |  |  |  | 1 |
| SAT | 1-12 |  |  |  | 2 |
| SUN | 1-12 |  |  |  | 2 |

## Notes :

Ring and Barrier Diagram:
Sequence 1:


Attachment 6
Intersection Worksheets - Existing AM/PM Peaks

c Critical Lane Group

Queues
1: Ebenezer Road/Driveway \& Kingston Pike

|  | 4 | $\rightarrow$ | $\geqslant$ | 7 | $\leftarrow$ | 4 | $\dagger$ | 7 | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR |
| Lane Group Flow (vph) | 10 | 818 | 46 | 75 | 648 | 29 | 122 | 178 | 16 | 11 |
| v/c Ratio | 0.03 | 0.50 | 0.06 | 0.22 | 0.32 | 0.03 | 0.31 | 0.37 | 0.11 | 0.04 |
| Control Delay | 21.0 | 22.8 | 0.1 | 13.1 | 13.0 | 0.1 | 35.3 | 7.4 | 44.7 | 0.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 21.0 | 22.8 | 0.1 | 13.1 | 13.0 | 0.1 | 35.3 | 7.4 | 44.7 | 0.3 |
| Queue Length 50th ( ft ) | 4 | 217 | 0 | 23 | 124 | 0 | 66 | 0 | 10 | 0 |
| Queue Length 95th (ft) | 16 | 292 | 0 | 46 | 164 | 0 | 118 | 54 | 31 | 0 |
| Internal Link Dist (ft) |  | 551 |  |  | 715 |  | 608 |  | 380 |  |
| Turn Bay Length (ft) |  |  | 140 |  |  | 100 |  | 50 |  | 50 |
| Base Capacity (vph) | 348 | 1634 | 821 | 375 | 2016 | 948 | 392 | 487 | 198 | 314 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.03 | 0.50 | 0.06 | 0.20 | 0.32 | 0.03 | 0.31 | 0.37 | 0.08 | 0.04 |

[^0]

C Critical Lane Group

Queues
1: Ebenezer Road/Driveway \& Kingston Pike

|  | $\stackrel{ }{*}$ | $\rightarrow$ | 7 | $\checkmark$ | - | 4 | $\dagger$ | $p$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR |
| Lane Group Flow (vph) | 20 | 1359 | 114 | 156 | 1076 | 44 | 131 | 145 | 168 | 18 |
| v/c Ratio | 0.09 | 0.81 | 0.14 | 0.66 | 0.49 | 0.04 | 0.63 | 0.46 | 0.88 | 0.06 |
| Control Delay | 20.5 | 32.4 | 2.2 | 33.7 | 13.6 | 0.1 | 64.9 | 13.1 | 91.9 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 20.5 | 32.4 | 2.2 | 33.7 | 13.6 | 0.1 | 64.9 | 13.1 | 91.9 | 0.4 |
| Queue Length 50th (ft) | 8 | 455 | 0 | 59 | 225 | 0 | 98 | 0 | 130 | 0 |
| Queue Length 95th (ft) | 27 | \#622 | 22 | 128 | 277 | 1 | \#169 | 61 | \#257 | 0 |
| Internal Link Dist (ft) |  | 551 |  |  | 715 |  | 608 |  | 380 |  |
| Turn Bay Length (tt) |  |  | 140 |  |  | 100 |  | 50 |  | 50 |
| Base Capacity (vph) | 234 | 1677 | 824 | 361 | 2187 | 1013 | 208 | 312 | 195 | 292 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.81 | 0.14 | 0.43 | 0.49 | 0.04 | 0.63 | 0.46 | 0.86 | 0.06 |

Intersection Summary
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Attachment 7
Intersection Worksheets - Background AM/PM Peaks

|  | 4 | $\rightarrow$ |  | $\dagger$ |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个个 | \％ | ＊ | ¢4 | 「 |  | $\uparrow$ | 「 |  | 4 | F |
| Traffic Volume（vph） | 10 | 817 | 46 | 75 | 648 | 29 | 108 | 14 | 178 | 10 | 6 | 11 |
| Future Volume（vph） | 10 | 817 | 46 | 75 | 648 | 29 | 108 | 14 | 178 | 10 | 6 | 11 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 7.0 | 7.0 |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |  | 1.00 | 0.85 |  | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |  | 0.96 | 1.00 |  | 0.97 | 1.00 |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 |  | 1784 | 1583 |  | 1806 | 1583 |
| Flt Permitted | 0.40 | 1.00 | 1.00 | 0.21 | 1.00 | 1.00 |  | 0.96 | 1.00 |  | 0.97 | 1.00 |
| Satd．Flow（perm） | 741 | 3539 | 1583 | 384 | 3539 | 1583 |  | 1784 | 1583 |  | 1806 | 1583 |
| Peak－hour factor，PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj．Flow（vph） | 10 | 842 | 47 | 77 | 668 | 30 | 111 | 14 | 184 | 10 | 6 | 11 |
| RTOR Reduction（vph） | 0 | 0 | 27 | 0 | 0 | 14 | 0 | 0 | 144 | 0 | 0 | 10 |
| Lane Group Flow（vph） | 10 | 842 | 20 | 77 | 668 | 16 | 0 | 125 | 40 | 0 | 16 | 1 |
| Turn Type | Perm | NA | Perm | pm＋pt | NA | Perm | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 |  |  | 3 |  |  | 4 |
| Actuated Green，G（s） | 42.2 | 42.2 | 42.2 | 54.2 | 54.2 | 54.2 |  | 22.0 | 22.0 |  | 4.8 | 4.8 |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 42.2 | 42.2 | 42.2 | 54.2 | 54.2 | 54.2 |  | 22.0 | 22.0 |  | 4.8 | 4.8 |
| Actuated g／C Ratio | 0.42 | 0.42 | 0.42 | 0.54 | 0.54 | 0.54 |  | 0.22 | 0.22 |  | 0.05 | 0.05 |
| Clearance Time（s） | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 7.0 | 7.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 312 | 1493 | 668 | 298 | 1918 | 857 |  | 392 | 348 |  | 86 | 75 |
| v／s Ratio Prot |  | c0．24 |  | 0.02 | c0．19 |  |  | c0．07 |  |  | c0．01 |  |
| v／s Ratio Perm | 0.01 |  | 0.01 | 0.12 |  | 0.01 |  |  | 0.03 |  |  | 0.00 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.03 | 0.56 | 0.03 | 0.26 | 0.35 | 0.02 |  | 0.32 | 0.12 |  | 0.19 | 0.01 |
| Uniform Delay，d1 | 16.9 | 21.9 | 16.9 | 12.9 | 12.9 | 10.6 |  | 32.7 | 31.2 |  | 45.7 | 45.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Incremental Delay，d2 | 0.2 | 1.5 | 0.1 | 0.5 | 0.1 | 0.0 |  | 2.1 | 0.7 |  | 1.0 | 0.0 |
| Delay（s） | 17.1 | 23.5 | 17.0 | 13.4 | 13.0 | 10.6 |  | 34.8 | 31.9 |  | 46.8 | 45.4 |
| Level of Service | B | C | B | B | B | B |  | C | C |  | D | D |
| Approach Delay（s） |  | 23.1 |  |  | 13.0 |  |  | 33.1 |  |  | 46.2 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 21.0 |  | HCM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.46 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 100.0 |  | Sum of los | time（s） |  |  | 24.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 56．1\％ |  | CU Level | f Service |  |  | B |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

C Critical Lane Group

Queues
1: Ebenezer Road/Driveway \& Kingston Pike

|  | 4 | $\rightarrow$ | 7 | 7 | $\leftarrow$ | 4 | $\uparrow$ | 7 | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR |
| Lane Group Flow (vph) | 10 | 842 | 47 | 77 | 668 | 30 | 125 | 184 | 16 | 11 |
| v/c Ratio | 0.03 | 0.52 | 0.06 | 0.24 | 0.33 | 0.03 | 0.32 | 0.37 | 0.11 | 0.04 |
| Control Delay | 21.0 | 23.1 | 0.1 | 13.2 | 13.1 | 0.1 | 35.4 | 7.4 | 44.7 | 0.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 21.0 | 23.1 | 0.1 | 13.2 | 13.1 | 0.1 | 35.4 | 7.4 | 44.7 | 0.3 |
| Queue Length 50th (ft) | 4 | 226 | 0 | 24 | 129 | 0 | 67 | 0 | 10 | 0 |
| Queue Length 95th (ft) | 16 | 303 | 0 | 48 | 171 | 0 | 120 | 55 | 31 | 0 |
| Internal Link Dist (tt) |  | 551 |  |  | 715 |  | 608 |  | 380 |  |
| Turn Bay Length (ft) |  |  | 140 |  |  | 100 |  | 50 |  | 50 |
| Base Capacity (vph) | 342 | 1632 | 821 | 366 | 2016 | 948 | 392 | 491 | 198 | 314 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.03 | 0.52 | 0.06 | 0.21 | 0.33 | 0.03 | 0.32 | 0.37 | 0.08 | 0.04 |

[^1]|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

C Critical Lane Group

Queues
1: Ebenezer Road/Driveway \& Kingston Pike

|  | $\rangle$ | $\rightarrow$ | $\stackrel{7}{ }$ | 1 | $\leftarrow$ | 4 | $\dagger$ | $p$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR |
| Lane Group Flow (vph) | 21 | 1400 | 117 | 161 | 1109 | 45 | 135 | 149 | 174 | 19 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.09 | 0.84 | 0.14 | 0.69 | 0.51 | 0.04 | 0.65 | 0.48 | 0.89 | 0.07 |
| Control Delay | 20.9 | 34.4 | 2.4 | 38.5 | 13.9 | 0.1 | 66.0 | 14.0 | 94.7 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 20.9 | 34.4 | 2.4 | 38.5 | 13.9 | 0.1 | 66.0 | 14.0 | 94.7 | 0.4 |
| Queue Length 50th (ft) | 9 | 481 | 0 | 69 | 236 | 0 | 101 | 3 | 135 | 0 |
| Queue Length 95th (ft) | 28 | \#691 | 24 | 139 | 288 | 1 | \#180 | 65 | \#268 | 0 |
| Internal Link Dist (ft) |  | 551 |  |  | 715 |  | 608 |  | 380 |  |
| Turn Bay Length (t) |  |  | 140 |  |  | 100 |  | 50 |  | 50 |
| Base Capacity (vph) | 224 | 1663 | 818 | 355 | 2182 | 1011 | 208 | 312 | 195 | 292 |
| Starvation Cap Reductn | , | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.84 | 0.14 | 0.45 | 0.51 | 0.04 | 0.65 | 0.48 | 0.89 | 0.07 |

Intersection Summary
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Attachment 8

c Critical Lane Group

Queues
1: Ebenezer Road/Driveway \& Kingston Pike

|  | 4 | $\rightarrow$ | $\rangle$ | 7 | $\leftarrow$ | 4 | $\dagger$ | 7 | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR |
| Lane Group Flow (vph) | 10 | 842 | 60 | 100 | 668 | 30 | 175 | 257 | 18 | 11 |
| v/c Ratio | 0.03 | 0.52 | 0.07 | 0.30 | 0.33 | 0.03 | 0.45 | 0.51 | 0.12 | 0.04 |
| Control Delay | 21.8 | 23.8 | 0.2 | 13.9 | 13.1 | 0.1 | 38.0 | 12.5 | 44.9 | 0.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 21.8 | 23.8 | 0.2 | 13.9 | 13.1 | 0.1 | 38.0 | 12.5 | 44.9 | 0.3 |
| Queue Length 50th (ft) |  | 230 | 0 | 31 | 129 | 0 | 97 | 28 | 11 | 0 |
| Queue Length 95th (ft) | 16 | 310 | 0 | 59 | 171 | 0 | 163 | 101 | 33 | 0 |
| Internal Link Dist (tt) |  | 551 |  |  | 715 |  | 608 |  | 380 |  |
| Turn Bay Length (ft) |  |  | 140 |  |  | 100 |  | 50 |  | 50 |
| Base Capacity (vph) | 336 | 1609 | 812 | 364 | 2015 | 948 | 392 | 506 | 199 | 314 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.03 | 0.52 | 0.07 | 0.27 | 0.33 | 0.03 | 0.45 | 0.51 | 0.09 | 0.04 |

[^2]
## General Information

| Analyst | Addie Kirkham |
| :--- | :--- |
| Agency/Co. | Ardurra |
| Date Performed | $4 / 13 / 2024$ |
| Analysis Year | 2027 |
| Time Analyzed | Full Buildout AM Peak |
| Intersection Orientation | North-South |
| Project Description | 330.029 - Ebenezer Subdivision |

Site Information

| Intersection | Ebenezer Road at Apartment Driveway |
| :--- | :--- |
| Jurisdiction | Knox County |
| East/West Street | Apartment Driveway |
| North/South Street | Ebenezer Road |
| Peak Hour Factor | 0.92 |
| Analysis Time Period (hrs) | 0.25 |

Lanes


Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority |  | 10 | 11 | 12 |  | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |
| Number of Lanes |  | 0 | 0 | 0 |  | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 |
| Configuration |  |  |  |  |  |  | LR |  |  |  |  | TR |  | L | T |  |
| Volume (veh/h) |  |  |  |  |  | 32 |  | 75 |  |  | 343 | 9 |  | 21 | 142 |  |
| Percent Heavy Vehicles (\%) |  |  |  |  |  | 2 |  | 2 |  |  |  |  |  | 2 |  |  |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |  |  |  |  |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Critical and Follow-up Headways |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Critical Headway (sec) |  |  |  |  |  | 7.1 |  | 6.2 |  |  |  |  |  | 4.1 |  |  |
| Critical Headway (sec) |  |  |  |  |  | 6.42 |  | 6.22 |  |  |  |  |  | 4.12 |  |  |
| Base Follow-Up Headway (sec) |  |  |  |  |  | 3.5 |  | 3.3 |  |  |  |  |  | 2.2 |  |  |
| Follow-Up Headway (sec) |  |  |  |  |  | 3.52 |  | 3.32 |  |  |  |  |  | 2.22 |  |  |

Delay, Queue Length, and Level of Service


HCS Two-Way Stop-Control Report

## General Information

| Analyst | Addie Kirkham |
| :--- | :--- |
| Agency/Co. | Ardurra |
| Date Performed | $4 / 13 / 2024$ |
| Analysis Year | 2027 |
| Time Analyzed | Full Buildout AM Peak |
| Intersection Orientation | North-South |
| Project Description | 330.029 - Ebenezer Subdivision |


| Intersection | Ebenezer Road at Driveway |
| :--- | :--- |
| Jurisdiction | Knox County |
| East/West Street | Subdivision Driveway |
| North/South Street | Ebenezer Road |
| Peak Hour Factor | 0.92 |
| Analysis Time Period (hrs) | 0.25 |

Lanes


Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority |  | 10 | 11 | 12 |  | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |
| Number of Lanes |  | 0 | 0 | 0 |  | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration |  |  |  |  |  |  | LR |  |  |  |  | TR |  | LT |  |  |
| Volume (veh/h) |  |  |  |  |  | 19 |  | 43 |  |  | 309 | 7 |  | 15 | 159 |  |
| Percent Heavy Vehicles (\%) |  |  |  |  |  | 2 |  | 2 |  |  |  |  |  | 2 |  |  |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |  |  |  |  |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Critical and Follow-up Headways |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Critical Headway (sec) |  |  |  |  |  | 7.1 |  | 6.2 |  |  |  |  |  | 4.1 |  |  |
| Critical Headway (sec) |  |  |  |  |  | 6.42 |  | 6.22 |  |  |  |  |  | 4.12 |  |  |
| Base Follow-Up Headway (sec) |  |  |  |  |  | 3.5 |  | 3.3 |  |  |  |  |  | 2.2 |  |  |
| Follow-Up Headway (sec) |  |  |  |  |  | 3.52 |  | 3.32 |  |  |  |  |  | 2.22 |  |  |

Delay, Queue Length, and Level of Service


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

C Critical Lane Group

Queues
1: Ebenezer Road/Driveway \& Kingston Pike

|  | $\stackrel{ }{*}$ | $\rightarrow$ | 7 | $\checkmark$ | - | 4 | $\dagger$ | $p$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR |
| Lane Group Flow (vph) | 21 | 1400 | 163 | 240 | 1109 | 45 | 175 | 206 | 181 | 19 |
| v/c Ratio | 0.10 | 0.91 | 0.21 | 0.81 | 0.51 | 0.04 | 0.84 | 0.66 | 0.93 | 0.07 |
| Control Delay | 23.9 | 42.5 | 6.1 | 49.3 | 13.9 | 0.1 | 84.3 | 27.6 | 101.5 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 23.9 | 42.5 | 6.1 | 49.3 | 13.9 | 0.1 | 84.3 | 27.6 | 101.5 | 0.4 |
| Queue Length 50th (ft) | 10 | 530 | 10 | 128 | 236 | 0 | 135 | 44 | 141 | 0 |
| Queue Length 95th (ft) | 29 | \#731 | 54 | 215 | 288 | 1 | \#259 | 127 | \#281 | 0 |
| Internal Link Dist (ft) |  | 551 |  |  | 715 |  | 608 |  | 380 |  |
| Turn Bay Length (tt) |  |  | 140 |  |  | 100 |  | 50 |  | 50 |
| Base Capacity (vph) | 208 | 1537 | 767 | 360 | 2182 | 1011 | 208 | 312 | 195 | 292 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.10 | 0.91 | 0.21 | 0.67 | 0.51 | 0.04 | 0.84 | 0.66 | 0.93 | 0.07 |

Intersection Summary
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

HCS Two-Way Stop-Control Report

## General Information

| Analyst | Addie Kirkham |
| :--- | :--- |
| Agency/Co. | Ardurra |
| Date Performed | $4 / 13 / 2024$ |
| Analysis Year | 2027 |
| Time Analyzed | Full Buildout PM Peak |
| Intersection Orientation | North-South |
| Project Description | 330.029 - Ebenezer Subdivision |


| Intersection | Ebenezer Road at Apartment Driveway |
| :--- | :--- |
| Jurisdiction | Knox County |
| East/West Street | Apartment Driveway |
| North/South Street | Ebenezer Road |
| Peak Hour Factor | 0.92 |
| Analysis Time Period (hrs) | 0.25 |

Lanes


Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority |  | 10 | 11 | 12 |  | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |
| Number of Lanes |  | 0 | 0 | 0 |  | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 |
| Configuration |  |  |  |  |  |  | LR |  |  |  |  | TR |  | L | T |  |
| Volume (veh/h) |  |  |  |  |  | 26 |  | 62 |  |  | 296 | 32 |  | 76 | 367 |  |
| Percent Heavy Vehicles (\%) |  |  |  |  |  | 2 |  | 2 |  |  |  |  |  | 2 |  |  |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |  |  |  |  |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Critical and Follow-up Headways |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Critical Headway (sec) |  |  |  |  |  | 7.1 |  | 6.2 |  |  |  |  |  | 4.1 |  |  |
| Critical Headway (sec) |  |  |  |  |  | 6.42 |  | 6.22 |  |  |  |  |  | 4.12 |  |  |
| Base Follow-Up Headway (sec) |  |  |  |  |  | 3.5 |  | 3.3 |  |  |  |  |  | 2.2 |  |  |
| Follow-Up Headway (sec) |  |  |  |  |  | 3.52 |  | 3.32 |  |  |  |  |  | 2.22 |  |  |

## Delay, Queue Length, and Level of Service



HCS Two-Way Stop-Control Report

## General Information

| Analyst | Addie Kirkham |
| :--- | :--- |
| Agency/Co. | Ardurra |
| Date Performed | $4 / 13 / 2024$ |
| Analysis Year | 2027 |
| Time Analyzed | Full Buildout PM Peak |
| Intersection Orientation | North-South |
| Project Description | 330.029 - Ebenezer Subdivision |


| Intersection | Ebenezer Road at Driveway |
| :--- | :--- |
| Jurisdiction | Knox County |
| East/West Street | Subdivision Driveway |
| North/South Street | Ebenezer Road |
| Peak Hour Factor | 0.92 |
| Analysis Time Period (hrs) | 0.25 |

Lanes


Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority |  | 10 | 11 | 12 |  | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |
| Number of Lanes |  | 0 | 0 | 0 |  | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration |  |  |  |  |  |  | LR |  |  |  |  | TR |  | LT |  |  |
| Volume (veh/h) |  |  |  |  |  | 12 |  | 29 |  |  | 299 | 21 |  | 50 | 343 |  |
| Percent Heavy Vehicles (\%) |  |  |  |  |  | 2 |  | 2 |  |  |  |  |  | 2 |  |  |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |  |  |  |  |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Critical and Follow-up Headways |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Critical Headway (sec) |  |  |  |  |  | 7.1 |  | 6.2 |  |  |  |  |  | 4.1 |  |  |
| Critical Headway (sec) |  |  |  |  |  | 6.42 |  | 6.22 |  |  |  |  |  | 4.12 |  |  |
| Base Follow-Up Headway (sec) |  |  |  |  |  | 3.5 |  | 3.3 |  |  |  |  |  | 2.2 |  |  |
| Follow-Up Headway (sec) |  |  |  |  |  | 3.52 |  | 3.32 |  |  |  |  |  | 2.22 |  |  |

## Delay, Queue Length, and Level of Service



## Attachment 9

Turn Lane Warrants

## Project: Ebenezer Road Subdivision

Ebenezer Road at Apartment Roadway
Ebenezer Road
at Apartment Roadway LEFT TURN

AM
PM
VOLUMES

AM

| Opposing | Thru | LT | LT MAX | Warrant Met |
| :---: | :---: | :---: | :---: | :---: |
| 352 | 142 | 21 | 135 | NO |
| 328 | 367 | 76 | 65 | YES |

Ebenezer Road
at Apartment Roadway RIGHT TURN

AM
PM
VOLUMES

| Thru | RT | RT MAX | Warrant Met |
| :---: | :---: | :---: | :---: |
| 343 | 9 | 299 | NO |
| 296 | 32 | 349 | NO |

Ebenezer Road at Subdivision Roadway
Ebenezer Road
at Subdivision Roadway
LEFT TURN
AM
PM
VOLUMES

| Opposing | Thru | LT | LT MAX | Warrant Met |
| :---: | :---: | :---: | :---: | :---: |
| 316 | 159 | 15 | 135 | NO |
| 320 | 343 | 50 | 80 | NO |

Ebenezer Road
at Subdivision Roadway RIGHT TURN

AM
PM

VOLUMES

| Thru | RT | RT MAX | Warrant Met |
| :---: | :---: | :---: | :---: |
| 309 | 7 | 299 | NO |
| 299 | 21 | 349 | NO |

TABLE 4A
LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAMING SPEED OF 35 MPH OR LESS
(If the left-turn volume exceeds the table value a left -turn lane is needed)

| OPPOSING <br> VOLUME | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100-149 | 150-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ | $\begin{aligned} & 300 \\ & 245 \end{aligned}$ | $\begin{aligned} & 235 \\ & 200 \end{aligned}$ | $\begin{aligned} & 185 \\ & 160 \end{aligned}$ | $\begin{aligned} & 145 \\ & 130 \end{aligned}$ | $\begin{aligned} & 120 \\ & 110 \end{aligned}$ | $\begin{gathered} 100 \\ 90 \end{gathered}$ |
| $\begin{aligned} & 200-241 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 205 \\ & 175 \end{aligned}$ | $\begin{aligned} & 170 \\ & 150 \end{aligned}$ | $\begin{aligned} & 140 \\ & 125 \end{aligned}$ | $\begin{aligned} & 115 \\ & 105 \end{aligned}$ | $\begin{aligned} & 100 \\ & 90 \end{aligned}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350 \cdot 399 \end{aligned}$ |  | $\begin{array}{l\|l} 135 \\ \mathrm{~K} & \left.\begin{array}{l} 120 \end{array}\right) \end{array}$ | $\begin{aligned} & 110 \\ & 100 \end{aligned}$ | 95  <br> $85 \cdot$ PM Peak <br> 76 LT  |  | 65 |
| $\begin{aligned} & 4001-419 \\ & 450-499 \end{aligned}$ | 120 <br> 105 | $\begin{gathered} 105 \\ 90 \\ \hline \end{gathered}$ | $\begin{aligned} & 90 \\ & 80 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ |
| $\begin{aligned} & 5(K)-549 \\ & 550-549 \end{aligned}$ | $\begin{aligned} & 95 \\ & 85 \end{aligned}$ | $\begin{aligned} & 8 i 1 \\ & 70 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ |
| $\begin{aligned} & 6(0)-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ |
| $\begin{gathered} 700-749 \\ 750 \text { or Mort } \end{gathered}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | 30 30 |


| $\begin{gathered} \text { OPPOSING } \\ \text { VOLCMIE } \end{gathered}$ | TEIROUGH VOLUME PLUS RYGFIT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $350 \cdot 399$ | 460-49 | $450-49$ | 500-549 | 550.599 | $=1>600$ |
| $\begin{aligned} & 1(60-149 \\ & 150-199 \end{aligned}$ | $\begin{gathered} 100 \\ 90 \end{gathered}$ | $\begin{aligned} & 80 \\ & 75 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ | $\begin{aligned} & 72 \\ & 65 \end{aligned}$ | $\begin{gathered} 460 \\ 55 \end{gathered}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-304 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ |
| $\begin{aligned} & 600-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |
| $\begin{gathered} 700-7 d y \\ 750 \text { or Mure } \end{gathered}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |

* Or through volume only if a right-turn lane exists.

TABLE 4B
RIGHT-TURN LANE VOLUME THRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

| RIGHT-TURN VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | <100 | 100-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & \text { Fewer Than } 25 \\ & 25-49 \\ & 50-99 \end{aligned}$ |  |  | $\begin{aligned} & \text { PM Peak } \\ & 32 \text { RT } \end{aligned}$ |  | AM Peak9 RT |  |
| 100-149 |  |  |  |  |  |  |
| 150-199 |  |  |  |  |  |  |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ |  |  |  |  |  | Yes |
| $\begin{aligned} & 300-349 \\ & 350-34 \end{aligned}$ |  |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 4(0)-449 \\ & 450-499 \end{aligned}$ |  |  | $\begin{aligned} & \text { I'cs } \\ & \text { I'es } \end{aligned}$ | Y'es <br> Y'es | $\begin{aligned} & \text { Yus } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ |  | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Y'es } \\ & \text { Yes } \end{aligned}$ | Y'es <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Y'es | Yes | Yes | Yes | Yes | Yes |


| RIGEIT-TURN VOLUME | THROUGH VOLUME PLUS LEET-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $350 \cdot 399$ | $400 \cdot 449$ | 450-499 | $500-549$ | 550-600 | $+1>600$ |
| $\begin{aligned} & \text { Fewer Than } 25 \\ & 25-49 \\ & 50-99 \end{aligned}$ |  |  |  |  | Yes | $\begin{aligned} & \text { Ycs } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  |  | Yes | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Y'es } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-591 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Y'es } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |

* Or through volume only if a left-turn lane exists.

TABLE 4A
LEFT-TURN LANE VOLUME THRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVALING SPEED OF 35 MPH OR LESS
(If the left-turn volume exceeds the table value a left -turn lane is needed)

| OPPOSING <br> VOLUME | THROUGH VOLUME PLUS RIGHT-TURN VOLUMD** |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100-149 | 150-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ | $\begin{aligned} & 300 \\ & 245 \end{aligned}$ | $\begin{aligned} & 235 \\ & 200 \end{aligned}$ | $\begin{aligned} & 185 \\ & 160 \end{aligned}$ | $\begin{aligned} & 145 \\ & 130 \end{aligned}$ | $\begin{aligned} & 120 \\ & 110 \end{aligned}$ | $\begin{gathered} 100 \\ 90 \end{gathered}$ |
| $\begin{aligned} & 200-241 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 205 \\ & 175 \end{aligned}$ | $\begin{aligned} & 170 \\ & 150 \end{aligned}$ | $\begin{aligned} & 140 \\ & 125 \end{aligned}$ | $\begin{aligned} & 115 \\ & 105 \end{aligned}$ | $\begin{gathered} 100 \\ 90 \end{gathered}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ |
| $\begin{aligned} & 300-319 \\ & 350 \cdot 399 \end{aligned}$ | $\begin{aligned} & 155 \\ & 135 \end{aligned}$ |  | $\begin{array}{r} 110 \\ 100 \end{array}$ | $\begin{aligned} & 95 \\ & 85 . \end{aligned}$ |  | $\begin{aligned} & \frac{65}{\mathrm{M} \text { Peak }} \\ & 0 \mathrm{LT} \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 4001-49 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & 120 \\ & 105 \end{aligned}$ | $\begin{gathered} 105 \\ 90 \end{gathered}$ | $\begin{aligned} & 90 \\ & 80 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | 50 |
| $\begin{aligned} & 5(k)-5 \cdot 49 \\ & 550-5(4) \end{aligned}$ | $\begin{aligned} & 95 \\ & 85 \end{aligned}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ |
| $\begin{aligned} & 606-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | 40 35 |
| $\begin{gathered} 700-749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |


| $\begin{gathered} \text { OPPOSING } \\ \text { VOLCMIE } \end{gathered}$ | TEIROUGH VOIUME PLUS RIGFI-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | 400-49 | 450-429 | $5(0)-549$ | 530-599 | $=1>600$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ | $\begin{gathered} 100 \\ 90 \end{gathered}$ | $\begin{aligned} & 80 \\ & 75 \end{aligned}$ | $\begin{aligned} & 710 \\ & 65 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ | $\begin{aligned} & 72 \\ & 65 \end{aligned}$ | $\begin{gathered} 460 \\ 55 \end{gathered}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ |
| $\begin{aligned} & 300-345 \\ & 350-305 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ |
| $\begin{array}{r} 400-449 \\ 450-499 \end{array}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ |
| $\begin{aligned} & 600-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |
| $\begin{gathered} 700-74 y \\ 750 \text { or Mare } \end{gathered}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |

* Or through volume only if a right-turn lane exists.

TABLE 4B
RIGHT-TURN LANE VOLUME THRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

| RIGET-TURN VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $<100$ | 100-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & \text { Fewer Than } 25 \\ & 25-49 \\ & 50-99 \end{aligned}$ |  |  | PM Peak 21 RT |  | AM Peak 7 LT |  |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  |  |  |  |  |  |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ |  |  |  |  |  | Yes |
| $\begin{aligned} & 300-349 \\ & 350-349 \end{aligned}$ |  |  |  | Yes | Yes <br> Yes | $\begin{aligned} & \text { Y'cs } \\ & \text { Y's } \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ |  |  | $\begin{aligned} & \text { l'es } \\ & \text { J'es } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Jess } \\ & \text { Yes } \end{aligned}$ | Yes Yes |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ |  | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Y'es | Y'es | Yes | Yes | Yes | Yes |


| RIGIIT-TURN VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUMDE * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $350 \cdot 399$ | $400 \cdot 444$ | 450-499 | $500-549$ | 550-600 | $+1>600$ |
| $\begin{aligned} & \text { Fewer Than } 25 \\ & 25-49 \\ & 50-99 \end{aligned}$ |  |  |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Y'es } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-349 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-494 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-591 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Y'es } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Y'es } \\ & \text { Y'es } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |

* Or through volume only if a left-turn lane exists.


## Attachment 10

## Sight Distance



Ebenezer Road at Subdivision Roadway - Looking Left (Southbound)


Ebenezer Road at Subdivision Roadway - Looking Right (Northbound)


[^0]:    Intersection Summary

[^1]:    Intersection Summary

[^2]:    Intersection Summary

