EBENEZER ROAD SUBDIVISION

Transportation Impact Analysis
Ebenezer Road
Knoxville, TN

A Transportation Impact Analysis for the Ebenezer Road Subdivision

Submitted to

Knoxville-Knox County Planning

April 26, 2024 Ardurra Project No. 330.029

Submitted By:





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Executive Summary

S&E Properties, LLC is proposing a residential development. The project is located south of the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road in Knox County, Tennessee. The full buildout of the Ebenezer Road Subdivision proposes 113 single-family residential lots and a future development area by others. The current plan for the Future Development Area is a proposed apartment complex with 278 garden style apartment units. Construction is proposed to take place this year and this study assumes full build out for the development will occur in 2027.

The Ebenezer Road Subdivision has a proposed single roadway connection to Ebenezer Road and the proposed future development area has a separate proposed single roadway connection to Ebenezer Road. A roadway connection between the two developments is under consideration for the purpose of emergency access. The exact location will need to be coordinated between the property owners as well as Knox County Engineering and Public Works.

In order to maintain or provide an acceptable level-of-service for each of the intersections studied, some recommendations are presented.

Kingston Pike (SR 70) at Ebenezer Road

After the completion of the Ebenezer Road Subdivision including the future development area the traffic conditions for the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road will operate at an acceptable LOS C during the AM peak hour and a LOS D during the PM peak hour.

The northbound right turn lane (Ebenezer Road) will exceed capacity after the completion of the Ebenezer Road Subdivision and Future Development Area. There are several existing constraints including the location of guard rails and power poles and the proximity to Ten Mile Creek that would make extending the storage length of the right turn lane difficult to construct. Ardurra recommends that any future intersection improvements be reviewed, coordinated and approved by both the City of Knoxville Department of Engineering and Knox County Engineering and Public Works.

Ebenezer Road at Future Development Area

A southbound left turn lane is warranted at the intersection of Ebenezer Road at Future Development Area Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy." The southbound left turn lane has a recommended minimum storage length

of 50 feet per the AASHTO Greenbook "A Policy on Geometric Design of Highways and Streets."

After the completion of the full buildout of the Ebenezer Road Subdivision including the proposed roadway improvements the intersection of Ebenezer Road at Future Development Area Roadway will operate at an acceptable LOS B or better for each approach during both the AM and PM peak hours.

Ebenezer Road at Subdivision

Neither a southbound left turn lane nor a northbound right turn lane is warranted at the intersection of Ebenezer Road at Ebenezer Subdivision Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

After the completion of the full buildout of the Ebenezer Road Subdivision the intersection of Ebenezer Road at Subdivision Roadway will operate at an acceptable LOS B or better for each approach during both the AM and PM peak hours.

1 Introduction

1.1 Project Description

This report provides a summary of a transportation impact analysis that was performed for the Ebenezer Road Subdivision residential development. The Ebenezer Road Subdivision proposes 113 single-family residential lots and a future development area by others. The current plan for the Future Development Area is a proposed apartment complex with 278 garden style apartment units. The project is located south of the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road in Knox County, Tennessee. The location of the site is shown in Figure 1.

Construction is proposed to take place this year and this study assumes full build out for the subdivision and the future development area will occur in 2027.

The Ebenezer Road Subdivision has a proposed single roadway connection to Ebenezer Road and the proposed future development area has a separate proposed single roadway connection to Ebenezer Road. A roadway connection between the two developments is under consideration for the purpose of emergency access. The exact location will need to be coordinated between the property owners as well as Knox County Engineering and Public Works.

The proposed site layout is shown in Figure 2.

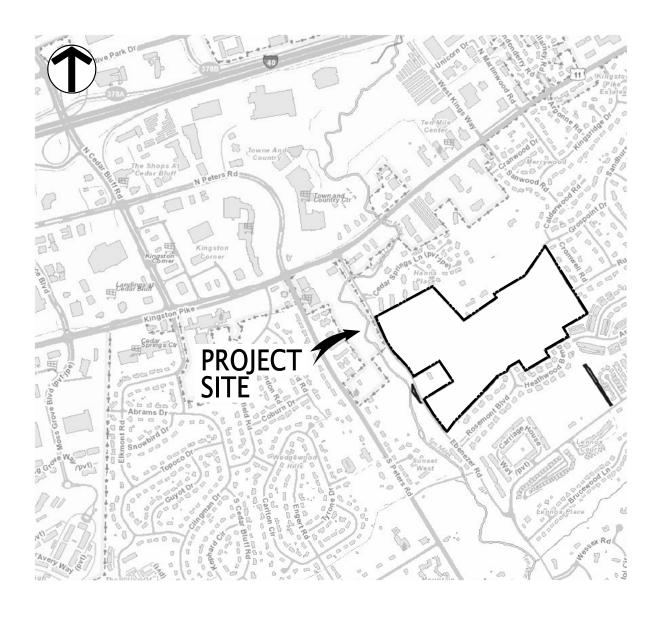


Figure 1: Location Map

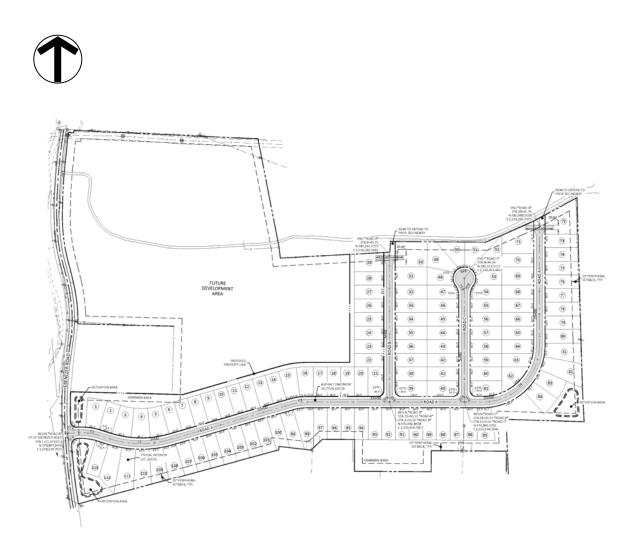


Figure 2: Site Plan

1.2 Study Area

The purpose of this study is to evaluate the impacts to the traffic conditions caused by the proposed development. Ebenezer Road is considered a north-south orientate roadway and Kingston Pike (US 11/US 70) is considered an east-west oriented roadway. The existing intersections and existing traffic control are summarized in Table 1.2-1 Study Area.

Table 1.2-1 Ebenezer Road Subdivision Study Area

| Intersection | Existing Traffic Control |
|--|--------------------------|
| Kingston Pike (US 11/US 70) at Ebenezer Road | Signalized |

1.3 Existing Site Conditions

Roadway geometry and posted speed limits were obtained by field observations. The Knoxville-Knox County Planning "2018 Major Road Plan" was used to determine road classification. This information is summarized in Table 1.3-1 Existing Site Conditions.

Table 1.3-1
Ebenezer Road Subdivision
Existing Site Conditions

| Roadway | Speed Limit | Lanes | Road Width | Major Road Plan |
|--------------------------------|----------------|-------|---------------|-----------------|
| Kingston Pike (US 11/US 70) | 45 mph | 5 | ~58 feet | Major Arterial |
| Ebenezer Road | 30 mph | 2 | ~21 feet | Minor Collector |

The intersection of Kingston Pike (US 11/US 70) at Ebenezer Road is located within the City of Knoxville limits and the signal is maintained by the City of Knoxville Department of Engineering.

At the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road the eastbound approach (Kingston Pike) has a left turn lane with an approximate storage length of 140 feet and a right turn lane with an approximate storage length of 140 feet. The westbound approach (Kingston Pike) has a left turn lane with an approximate storage length of 90 feet and a right turn lane with an approximate

storage length of 100 feet. The southbound approach (Driveway) has a separate right turn lane with an approximate storage length of 50 feet. The northbound approach (Ebenezer Road) has a separate right turn lane with an approximate storage length of 50 feet.

The measured width of Ebenezer Road south of the signalized intersection is 30 feet and tapers to 24 feet past the commercial driveway connections.

An aerial photo of the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road is included in Attachment 1.

Guardrails are located on both sides of Ebenezer Road south of Kingston Pike (US 11/US 70) at the Ten Mile Creek crossing. Pictures of the existing conditions of the guardrails are included in Attachment 1.

There are no sidewalks or bike infrastructure in the vicinity of the proposed development.

The Knoxville Area Transit (KAT) operates in the vicinity of the proposed development. Route 16 (Cedar Bluff Connector) stops include Parkwest Hospital, Cedar Bluff at Fox Lonas and Walmart Walbrook Drive. The nearest KAT stop to the development along Route 16 is currently located on Cedar Bluff Road near the Kroger Development which is approximately 1.1 miles walk to the Ebenezer Road Subdivision.

2 Existing Traffic Volumes

Ardurra conducted a peak hour turning movement count at the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road on Tuesday March 19, 2024. The AM peak hour occurred between 7:45 a.m. and 8:45 a.m. with an AM PHF of 97. The PM peak hour occurred between 5:00 p.m. and 6:00 p.m. with a PM PHF of 0.94.

The existing volumes including the AM and PM peak hour traffic volumes at the count locations are shown in Figure 3, and the count data collected is included in Attachment 2.

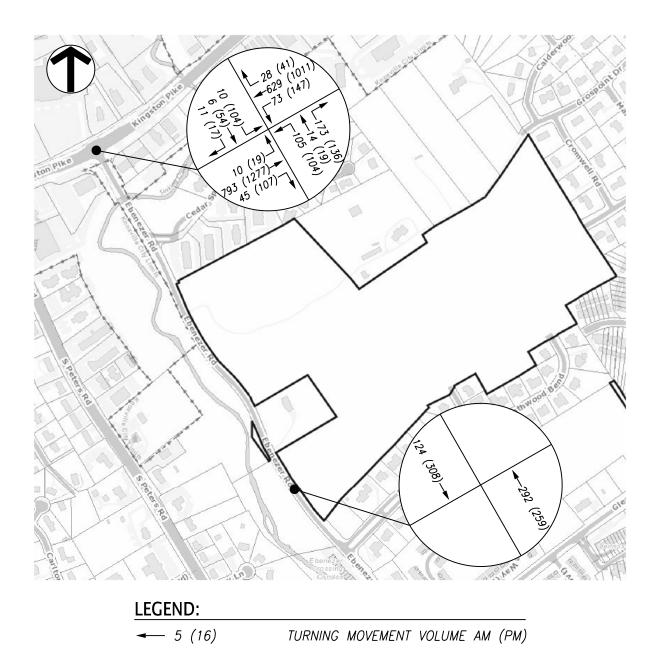


Figure 3: 2024 Existing Peak Hour Traffic

3 Background Growth

The Tennessee Department of Transportation (TDOT) maintains count stations in the vicinity of the proposed development.

TDOT count station ID 47000466 is located on Ebenezer Road between Kingston Pike (US 11/US 70) and George Williams Road in Knoxville, TN. The annual growth rate for this station over the last ten years is approximately -3.80%. The 2023 ADT was 4,581 vehicles per day.

TDOT count station ID 47000128 is located on Kingston Pike (US 11/US 70) west of the signalized intersection with Cedar Bluff Road. The annual growth rate for this station over the last ten years is approximately 0.59%. The 2022 ADT was 27,645 vehicles per day.

For the purpose of this study, an annual growth rate of 1.0% was assumed for traffic at the studied intersections until full occupancy is reached in 2027. Attachment 3 shows the trend line growth charts for the TDOT count stations.

Figure 4 demonstrates the projected background peak hour volumes at the studied intersections after applying the background growth rate to the existing conditions.

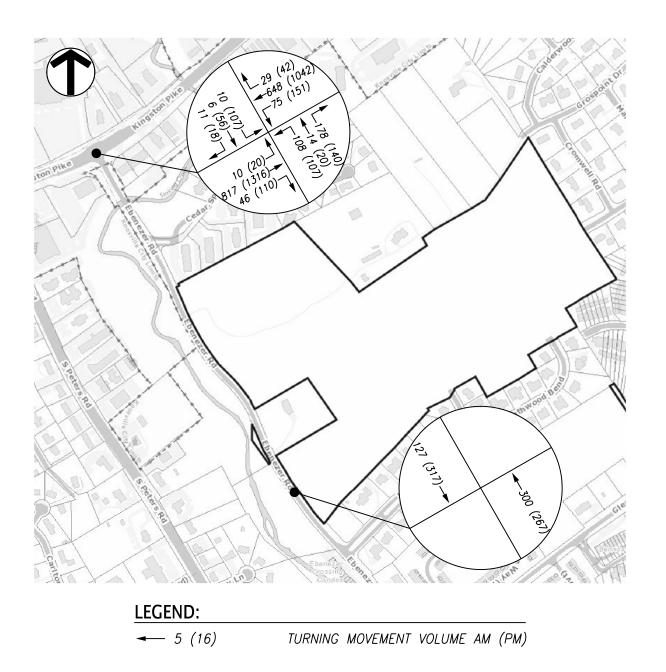


Figure 4: 2027 Background Peak Hour Traffic

3.1 Future Development Area

In addition to the background growth, the trips from the Future Development Area were calculated and included in the projected background peak hour traffic. The future development area is expected to be a proposed apartment complex with 275 garden style apartment units. A roadway connection between the two developments is under consideration for the purpose of emergency access.

The Knoxville-Knox County Planning Commission published a memorandum ("Local Trip Generation Rates for Multi-Family Residential Uses", August 14, 2000) for the purpose of providing locally collected data for all multi-family residential developments. The fitted curve equations from the local study were used to calculate site trips for the future development area.

The land use worksheets are included in the attachments and a trip generation summary is shown in Table 3.1.

Table 3.1-1
Future Development Area
Trip Generation Summary

| Land Use | Density | Daily Trips | AM Peak Hour Enter Exit | PM Peak Hour Enter Exit | | | |
|--------------------------------------|-----------|----------------|----------------------------|----------------------------|--|--|--|
| Apartments (Local Trip Gen Study) | 278 Units | 2,392 | 30 107 | 108 88 | | | |

The total combined new trips generated by the Future Development Area were estimated to be 2,392 daily trips. The estimated trips are 137 trips during the AM peak hour and 196 trips during the PM peak hour.

The directional distribution of the traffic generated by the Ebenezer Road Subdivision was determined using the existing traffic volumes in combination with the site plan layout. The entering/exiting traffic was assumed to be 70% Ebenezer Road northbound to/from Kingston Pike (US 11/US 70) and 30% Ebenezer Road southbound to/from Gleason Drive/Westland Drive.

Figures 5 and 6 show the Future Development Area – apartment peak hour trip distribution and site trips.

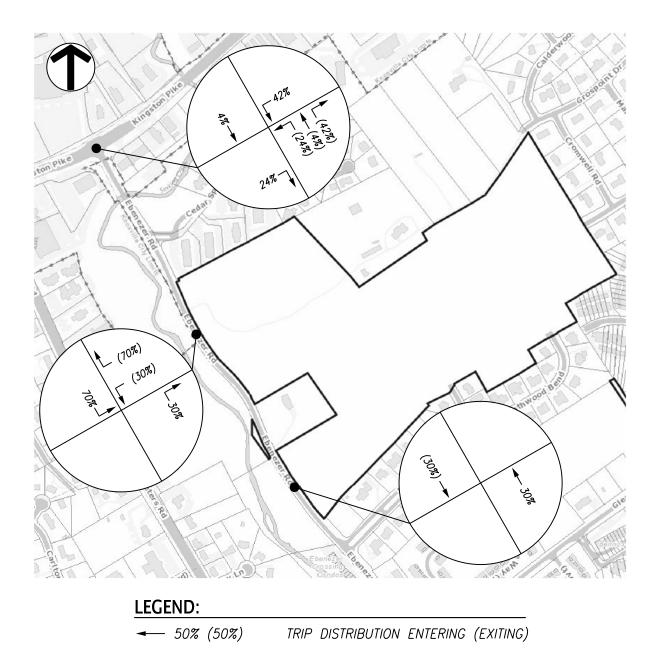


Figure 5: Apartment Peak Hour Trip Distribution

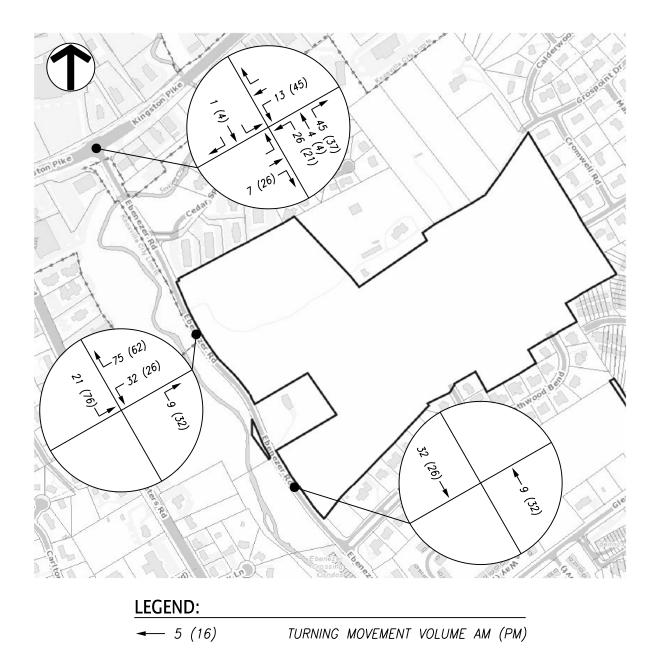


Figure 6: Apartment Peak Hour Site Trips

4 Trip Generation and Trip Distribution

The Ebenezer Road Subdivision proposes 113 single-family residential lots. A roadway connection between the two developments is under consideration for the purpose of emergency access. Single-Family Detached Housing or Land Use 210 was used to calculate site trips for the development using the fitted curve equations from the Trip Generation, 11th Edition, published by the Institute of Transportation Engineers.

The land use worksheets are included in Attachment 4. A trip generation summary is shown in Table 4-1.

Table 4-1 Ebenezer Road Subdivision Trip Generation Summary

| Land Use | Density | Daily Trips | AM Peak Hour Enter Exit | PM Peak Hour Enter Exit |
|---|----------|----------------|----------------------------|----------------------------|
| Single Family Detached Housing (LUC | 113 Lots | 1,129 | 21 62 | 71 41 |

The total combined new trips generated by the Ebenezer Road Subdivision were estimated to be 1,129 daily trips. The estimated trips are 83 trips during the AM peak hour and 112 trips during the PM peak hour.

Ebenezer Road at the intersection with Kingston Pike (US 11 / US 70) has an existing trip distribution of 70% northbound and 30% southbound during the AM peak hour and 45% northbound and 55% southbound during the PM peak hour.

The directional distribution of the traffic generated by the Ebenezer Road Subdivision was determined using the existing traffic volumes in combination with the site plan layout. The entering/exiting traffic was assumed to be 70% Ebenezer Road northbound to/from Kingston Pike (US 11 / US 70) and 30% Ebenezer Road southbound to/from Gleason Drive/Westland Drive.

Figures 7 and 8 show the subdivision peak hour trip distribution and site trips. Figure 9 shows the 2027 full buildout peak hour traffic including the background growth and the peak hour site trips from both the future development area and the Ebenezer Road Subdivision.

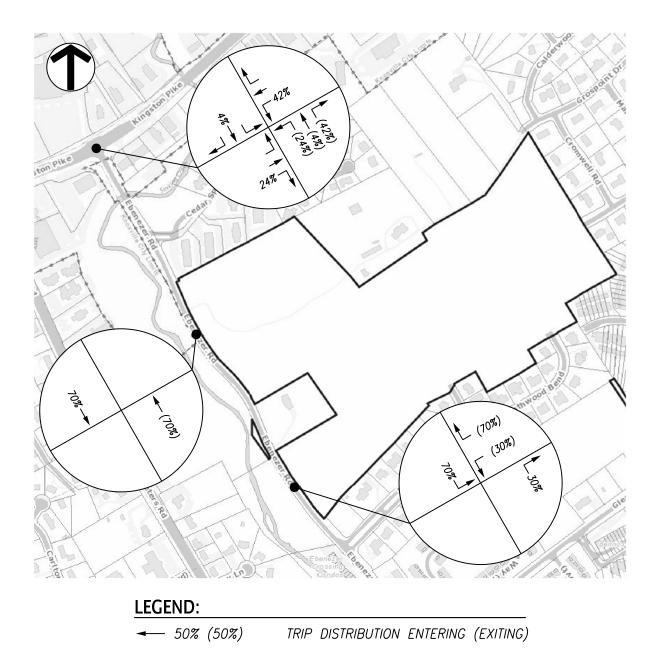


Figure 7: Subdivision Peak Hour Trip Distribution

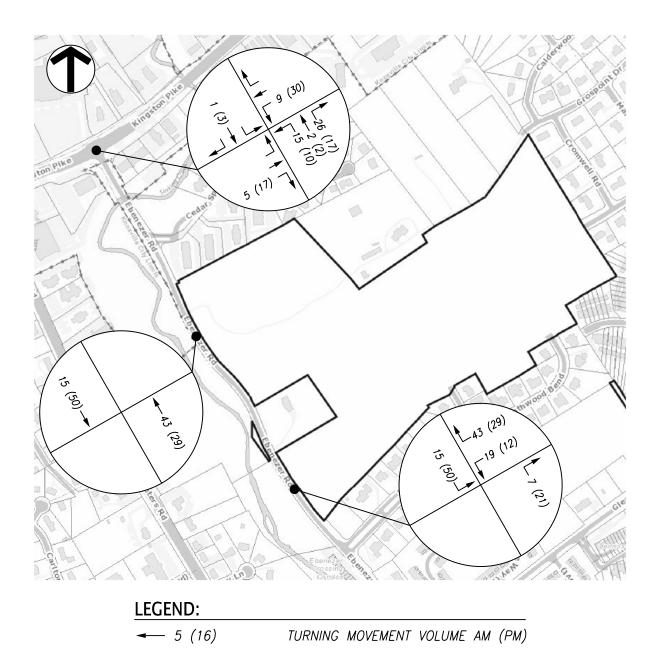


Figure 8: Subdivision Peak Hour Site Trips

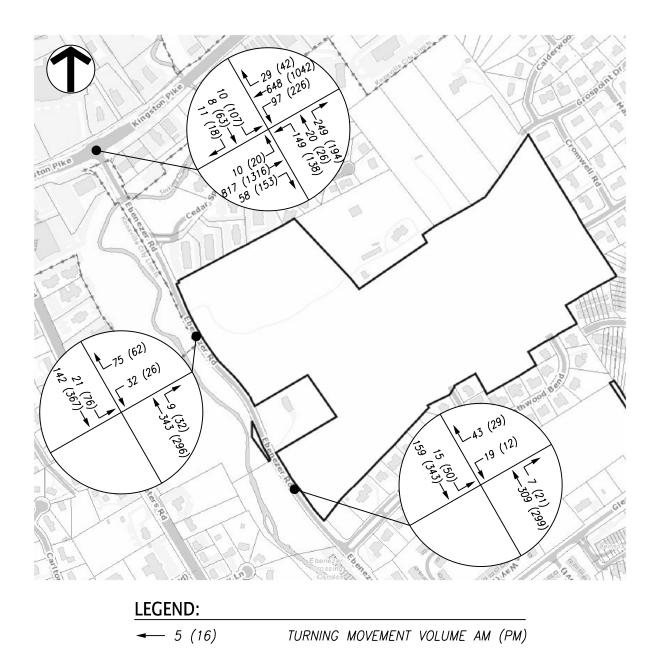


Figure 9: 2027 Full Buildout Peak Hour Traffic

5 Projected Capacity and Level of Service

Intersection capacity analyses were performed using the Synchro 11 Software at signalized intersection and the Highway Capacity Software 2023 at the two-way stop-controlled intersections in order to evaluate the AM and PM peak hours for existing, background and full buildout conditions. The existing signal timing at the signalized intersection was provided by City of Knoxville Department of Engineering and is included in Attachment 5.

Level of Service

The results from the analyses are expressed with a term "level of service" (LOS), which is based on the amount of delay experienced at the intersection. The LOS index ranges from LOS A, indicating excellent traffic conditions with minimal delay, to LOS F indicating very congested conditions with excessive delay. LOS D generally is considered the minimum acceptable condition in urban areas. Table 5-1 shows the LOS index range for signalized and unsignalized intersections as defined by the Highway Capacity Manual (HCM).

Table 5-1 Level of Service (LOS) Index

| Level of Service | Signalized Intersection | Unsignalized Intersection |
|------------------|-------------------------|---------------------------|
| LOS A | ≤ 10 sec | ≤ 10 sec |
| LOS B | 10 – 20 sec | 10 – 15 sec |
| LOS C | 20 – 35 sec | 15 – 25 sec |
| LOS D | 35 – 55 sec | 25 – 35 sec |
| LOS E | 55 – 80 sec | 35 – 50 sec |
| LOS F | > 80 sec | > 50 sec |

The Synchro 11 worksheets are included in Attachments 6, 7, and 8. Table 5-2 shows the results of the capacity analyses.

Table 5-2 Level of Service (LOS) Summary

| Intersection | Time Period | Year 2024 Existing (Delay/LOS) | Year 2027 Background (Delay/LOS) | Year 2027 Full Buildout (Delay/LOS) |
|--|---|--------------------------------------|--|--|
| Kingston Pike (US 11/US 70) @ Ebenezer Road | AM Peak Intersection PM Peak Intersection | 20.8 / C 29.3 / C | 21.0 / C 30.7 / C | 22.4 / C 37.5 / D |
| Ebenezer Road @ Apartment Driveway | AM Peak WB Approach SB Approach PM Peak WB Approach SB Approach | | | 12.5 / B 1.2 / A 14.1 / B 1.7 / A |
| Ebenezer Road @ Driveway | AM Peak WB Approach SB Approach PM Peak WB Approach SB Approach | | | 11.5 / B 0.8 / A 12.5 / B 1.4 / A |

Notes:

^{1.} Whole intersection weighted average control delay expressed in second per vehicle for signalized intersections and all-way stop controlled intersections.

6 Queue Analysis

Table 6-1 presents the Synchro traffic queueing summary for the 95^{th} percentile queue at the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road for both the AM and PM peak hour.

Table 6-1 Synchro Queue Summary

| Intersection | Movement | Storage Capacity | | · · | | ground ditions | Full Buildout Conditions | | |
|---------------|----------|---------------------|-----|------|--------------|-------------------|-----------------------------|------|--|
| | | (ft) | AM | PM | AM | PM | AM | PM | |
| | EBL | 140 | 16 | 27 | 16 | 28 | 16 | 29 | |
| | EBT | 585 | 292 | #622 | 303 | #691 | 310 | #731 | |
| Kingston Pk | EBR | 140 | 0 | 22 | 0 | 24 | 0 | 54 | |
| (US 70/US 11) | WBL | 90 | 46 | 128 | 48 | 139 | 59 | 215 | |
| @ Ebenezer Rd | WBT | 1,000+ | 164 | 277 | 1 <i>7</i> 1 | 288 | 1 <i>7</i> 1 | 288 | |
| | WBR | 100 | 0 | 1 | 0 | 1 | 0 | 1 | |
| | NBT | 1,000+ | 118 | #169 | 120 | #180 | 163 | #259 | |
| | NBR | 50 | 54 | 61 | 55 | 65 | 101 | 127 | |
| | SBT | 240 | 31 | #257 | 31 | #268 | 33 | #281 | |
| | SBR | 50 | 0 | 0 | 0 | 0 | 0 | 0 | |

Notes:

The # footnote indicates that the volume for the 95th percentile cycle exceeds capacity. Bold indicates queue length exceeds available storage capacity.

Bold cells indicate that the queue lengths are more than the available storage. The 95th percentile queue length is defined as the queue length that has only a 5-percent probability of being exceeded during the analysis time period. The 95th percentile queue length is typically used to determine the length of turning lanes in order to minimize the risk of blockage. Synchro assumes a vehicle length of 25 feet.

The northbound right turn lane has an existing storage length of 50 feet and an additional 30 feet of taper length before the queue from the signalized intersection would block the driveway to the retail strip center. The signalized intersection capacity analysis shows the full buildout 95% queue length for the northbound right turn lane of approximately 101 feet (4 vehicles) during the AM peak hour and 127 feet (5 vehicles) during the PM peak hour and the full buildout 50% queue length for the northbound right turn lane of approximately 28 feet (2 vehicles) during the AM peak hour and 44 feet (2 vehicles) during the PM peak hour.

Therefore; the existing northbound right turn lane storage will exceed capacity and cause spillback into the thru lane less than 50% of time after the completion of the Ebenezer Road Subdivision.

7 Turn Lane Warrant Analysis

The intersection of Ebenezer Road at the proposed apartment roadway connection and the proposed subdivision roadway connection was evaluated to determine if a northbound right turn lane or a southbound left turn lane are warranted. The Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy," was used to analyze the information.

At the intersection of Ebenezer Road at the proposed roadway connection to the Future Development Area a southbound left turn is warranted during the PM peak hour and a northbound right turn lane is not warranted during either the AM and or PM peak hours after the full buildout of the Ebenezer Road Subdivision and Future Development Area.

At the intersection of Ebenezer Road at the proposed roadway connection to the Ebenezer Road Subdivision neither a southbound left turn lane nor a northbound right turn lane are warranted during the AM or PM peak hours.

The turn lane warrant worksheets and analysis are included in Attachment 9.

8 Conclusions and Recommendations

8.1 Kingston Pike (US 11/US 70) at Ebenezer Road

The existing intersection of Kingston Pike (US 11/US 70) at Ebenezer Road is a signalized four-legged intersection. The southbound approach is an existing shopping center driveway connection. The existing signal timing was provided by the City of Knoxville.

Under the existing and 2027 background conditions the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road operates at an acceptable LOS C during both the AM and PM peak hours.

After the completion of the Ebenezer Road Subdivision including the future development area the traffic conditions for the signalized intersection of Kingston Pike (US 11/US 70) at Ebenezer Road will operate at an acceptable LOS C during the AM peak hour and a LOS D during the PM peak hour.

The 95% queue length is defined as the queue length that has only a 5-percent probability of being exceeded during the analysis time period. The 95% queue length is typically used to determine the length of turning lanes in order to minimize the risk of blockage.

The northbound right turn lane has an existing storage length of 50 feet and an additional 30 feet of taper length before the queue from the signalized intersection would block the driveway to the retail strip center. The signalized intersection capacity analysis shows the full buildout 95% queue length for the northbound right turn lane of approximately 101 feet (4 vehicles) during the AM peak hour and 127 feet (5 vehicles) during the PM peak hour and the full buildout 50% queue length for the northbound right turn lane of approximately 28 feet (2 vehicles) during the AM peak hour and 44 feet (2 vehicles) during the PM peak hour.

The northbound right turn lane (Ebenezer Road) will exceed capacity after the completion of the Ebenezer Road Subdivision and Future Development Area. There are several existing constraints including the location of guard rails and power poles and the proximity to Ten Mile Creek that would make extending the storage length of the right turn lane difficult to construct. Ardurra recommends that any future intersection improvements be reviewed, coordinated and approved by both the City of Knoxville Department of Engineering and Knox County Engineering and Public Works.

8.2 Ebenezer Road at Future Development Area

The proposed full buildout conditions at the unsignalized intersection of Ebenezer Road at the Future Development Area Roadway were analyzed using the Highway Capacity Software (HCS2023).

A southbound left turn lane is warranted during the PM peak hour and a northbound right turn lane is not warranted at the intersection of Ebenezer Road at Future Development Area Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

The southbound left turn lane has a recommended minimum storage length of 50 feet per the AASHTO Greenbook "A Policy on Geometric Design of Highways and Streets."

After the completion of the full buildout of the Ebenezer Road Subdivision including the proposed roadway improvements the intersection of Ebenezer Road at Future Development Area Roadway will operate as follows. The westbound approach (Apartment Roadway) will operate at a LOS B during both the AM and PM peak

hours and the southbound approach (Ebenezer Road) will operate at a LOS A during both the AM and PM peak hours.

Ebenezer Road is classified as Minor Collector per the Major Road Plan. The minimum intersection spacing required on a collector road is 300 feet per the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022.

The minimum required sight distance for a road with a posted speed limit of 30 mph is 300 feet in each direction in accordance with the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022.

The location of the proposed apartment roadway for the Future Development Area is still under consideration.

Ardurra recommends that the intersection sight distance be certified by a land surveyor prior to construction in order to verify that Ebenezer Road has adequate intersection sight distance at the proposed apartment roadway connection to comply with Knox County Engineering and Public Works guidelines.

Ardurra recommends that the signs and pavement markings be installed in accordance with the standards provided in the *Manual on Uniform Traffic Control Devices* (MUTCD).

Any future improvements to the intersection or the various traffic management infrastructure, would need to be reviewed, coordinated, and approved by Knox County Engineering and Public Works.

8.3 Ebenezer Road at Ebenezer Subdivision

The proposed full buildout conditions at the unsignalized intersection of Ebenezer Road at the Ebenezer Subdivision Roadway were analyzed using the Highway Capacity Software (HCS2023).

Neither a southbound left turn lane nor a northbound right turn lane is warranted at the intersection of Ebenezer Road at Ebenezer Subdivision Roadway per the Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy."

After the completion of the full buildout of the Ebenezer Road Subdivision the intersection of Ebenezer Road at Subdivision Roadway will operate as follows. The westbound approach (Subdivision Roadway) will operate at a LOS B during both the

AM and PM peak hours and the southbound approach (Ebenezer Road) will operate at a LOS A during both the AM and PM peak hours.

Ebenezer Road is classified as Minor Collector per the Major Road Plan. The minimum intersection spacing required on a collector road is 300 feet per the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022. The Ebenezer Subdivision Roadway is located approximately 535 feet north of Rosemont Boulevard; therefore, the minimum separation on a collector is met and no change is necessary.

The minimum required sight distance for a road with a posted speed limit of 30 mph is 300 feet in each direction in accordance with the "Knoxville-Knox County Subdivision Regulations" amended through October 6, 2022.

At 15 feet from the edge of pavement the intersection sight distance is greater than 300 feet looking both northbound and southbound. Attachment 10 includes pictures of the intersection sight distance at the intersection of Ebenezer Road at Ebenezer Subdivision Roadway.

Ardurra recommends that the intersection sight distance be certified by a land surveyor prior to construction in order to verify that Ebenezer Road has adequate intersection sight distance at the proposed apartment roadway connection to comply with Knox County Engineering and Public Works guidelines.

Ardurra recommends that the signs and pavement markings be installed in accordance with the standards provided in the *Manual on Uniform Traffic Control Devices* (MUTCD).

Any future improvements to the intersection or the various traffic management infrastructure, would need to be reviewed, coordinated, and approved by Knox County Engineering and Public Works.

Attachment 1 Aerial Photos



Kingston Pike (SR 70) at Ebenezer Road - Signalized



Ebenezer Road Guardrail - Northbound



Ebenezer Road Guardrail - Southbound

Attachment 2 Traffic Counts

| South Sout | [| | Drive | , | | | - | on Pike | | I | Ebeneze | | I | | - | on Pike | | |
|--|-------------|-------|----------------|-----|-------|------|------|---------|-------|------|---------|------|----------------|-----|------|---------|-------|-----------|
| 7.00 AM | Chart | 1.6.1 | | | Titil | 1.6 | | | Tirel | 1.6 | | | Tital | 1.6 | | _ | Tirel | 1.6 T.6.1 |
| 7:30 AM 0 0 0 2 2 2 8 14 98 4 110 17 17 1 122 90 0 130 8 138 301 7:30 AM 1 0 0 2 3 17 158 4 179 31 4 48 7 33 0 154 9 132 26 491 7 7 601 3 4 6 0 13 44 44 11 24 497 8 8 6 142 227 4 5 5 8 3 3 9 26 491 1342 8 18 18 18 18 18 18 18 18 18 18 18 18 1 | | | | | | | | | | | | | | | | | | |
| Total 1 | | | | | | | | | | | | | | | | | | |
| Total 18 | | | | | | | | | | | | | | | | | | |
| 8:00 AM | | | | | | | | | | | 4 | | | | | | | |
| 8.39 AM | Total | 3 | 4 | 6 | 13 | 44 | 441 | 12 | 497 | 88 | 6 | 143 | 237 | 4 | 558 | 33 | 595 | 1342 |
| 8.39 AM 1 3 3 1 5 5 21 160 8 1890 20 2 4 66 68 1 2133 10 224 486 8.39 AM 4 0 5 7 103 436 8.39 AM 5 5 7 2 14 14 150 4 168 22 3 3 6 61 32 154 7 103 436 8.34 AM 5 7 7 2 14 14 150 4 168 22 3 3 6 61 32 162 17 17 163 436 8.34 AM 1 1 12 13 87 70 621 28 7 19 96 13 161 270 9 766 44 819 1846 99.00 AM 4 3 3 0 7 1 15 115 9 130 20 2 2 26 48 0 139 14 153 347 9.39 AM 7 4 4 1 12 6 171 6 183 20 2 2 21 43 2 158 19 179 417 9.39 AM 7 4 4 1 12 6 171 6 183 20 2 2 21 43 2 158 19 179 417 9.39 AM 7 4 4 1 12 6 171 172 6 183 20 2 2 21 43 2 158 19 179 417 9.39 AM 1 3 0 0 1 10 10 10 10 10 10 10 10 10 10 10 | , | | | | | | | | | | | | | | | | | ı |
| 8-35 MM | | | | | | | | | | | | | | | | | | |
| Best SAM 5 7 2 14 14 150 4 168 22 3 3 36 61 3 182 12 197 440 | | | | | | | | | | | | | | | | | | |
| Total 14 13 11 38 70 621 28 719 96 13 161 270 9 766 44 819 1846 | | | | | | | | | | | | | | | | | | |
| 9-00 AM | | | | | | | | | | | | | | | | | | |
| 9-15 AM | | | | | | | | | | | | | - 1 | | | | | |
| 9-945 AM | 9:00 AM | 4 | 3 | 0 | | 15 | 115 | 9 | 139 | 20 | | 26 | 48 | | 139 | 14 | 153 | 347 |
| Part | | | | | | | | | | | | | | | | | | |
| Total 18 | | | | | | | | | | | | | | | | | | |
| 10:00 AM | | | | | | | | | | | | | | | | | | |
| 10:15 AM | rotar J | 10 | 0 | ' | 2/ | 33 | 300 | 32 | 6/3 | // | 4 | 101 | 102 | 6 | 602 | 33 | 663 | 1547 |
| 10:15 AM | 10:00 AM I | 9 | 6 | 2 | 17 | 11 | 158 | 10 | 179 | 18 | 5 | 10 | 33 | 1 | 133 | 8 | 142 | 371 |
| 10.43 AM | | | | | | | | | | | | | | | | | | |
| Total 28 20 | | | | | | | | | | | | | | | | | | |
| 11:00 AM | | | | | | | | | | | | | | | | | | |
| 11:15 AM | Total | 28 | 20 | 11 | 59 | 44 | 720 | 49 | 813 | 64 | 18 | 65 | 147 | 7 | 667 | 38 | 712 | 1731 |
| 11:15 AM | 11.00 III I | 4.4 | , | | ابہ | | 100 | | 22-1 | 0.4 | ^ | 4 = | امد | | 100 | | 200 | F0.4 |
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| 12:15 PM | | | | | | | | | | | | | | | | | | |
| 12:15 PM | | | | | | | | | | | | | · | • | | | | |
| 12:30 PM | | | | | | | | | | | | | | | | | | |
| Total 12:45 PM | | | | | | | | | | | | | | | | | | |
| Total 46 19 21 86 82 1018 50 1150 86 19 96 201 20 973 69 1062 2499 | | | | | | | | | | | | | - | | | | | |
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| 1:15 PM 12 3 5 20 15 268 18 301 24 5 18 47 2 262 25 289 657 130 PM 12 7 4 23 14 261 15 290 29 29 1 16 47 5 221 23 249 669 178 145 PM 8 2 4 14 19 307 19 345 29 4 17 50 5 246 18 269 678 170 18 18 18 18 18 18 18 18 18 18 18 18 18 | rotarj | 40 | | - 1 | 001 | 02 | 1010 | 30 | 1150 | 00 | 13 | 30 | 201 | 20 | 373 | 03 | 1002 | 2433 |
| 1:30 PM | 1:00 PM | 19 | 4 | 6 | 29 | 16 | 197 | 14 | 227 | 26 | 1 | 18 | 45 | 6 | 207 | 15 | 228 | 529 |
| Time | 1:15 PM | 12 | | 5 | 20 | 15 | 268 | 18 | 301 | 24 | 5 | 18 | 47 | 2 | 262 | 25 | 289 | 657 |
| Total 51 16 19 86 64 1033 66 1163 108 12 69 189 18 936 81 1035 2473 2:00 PM 17 6 8 31 17 243 18 278 16 4 22 42 3 213 29 245 596 2:15 PM 13 7 6 26 26 23 261 14 298 19 3 16 38 2 2 251 22 275 637 2:30 PM 4 7 3 14 16 269 11 296 20 5 15 40 4 217 20 241 591 Total 43 24 20 87 75 1024 62 1161 83 16 75 174 12 925 84 1021 2443 3:00 PM 9 8 6 23 22 231 12 265 32 2 2 23 57 3 237 22 262 607 3:15 PM 9 8 1 18 21 270 15 306 20 4 17 41 5 269 29 303 668 3:30 PM 11 7 4 22 26 257 15 298 33 8 30 71 1 221 20 242 633 3:45 PM 11 1 8 5 24 37 304 14 355 26 2 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:00 PM 12 7 5 24 26 218 11 255 32 1 29 62 10 264 27 301 642 4:15 PM 6 7 2 15 27 251 11 289 28 7 29 64 3 303 23 329 694 4:445 PM 12 1 2 2 2 2 28 26 1 2 30 1 2 2 2 2 2 3 5 7 3 303 23 329 664 4:00 PM 12 7 5 24 26 218 11 255 32 1 29 62 10 264 27 301 642 4:15 PM 6 7 2 15 27 251 11 289 28 7 29 64 3 303 23 329 694 4:445 PM 12 1 2 2 2 2 28 261 14 303 18 4 28 50 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 2 2 2 28 261 14 303 18 4 28 50 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 2 5 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 | | | | | | | | | | | | | | | | | | |
| 2:00 PM | | | | | | | | | | | | | | | | | | |
| 2:15 PM 13 7 6 26 23 261 14 298 19 3 16 38 2 251 22 275 637 230 PM 4 7 3 14 16 269 11 296 20 5 15 40 4 217 20 241 591 Total 43 24 20 87 75 1024 62 1161 83 16 75 174 12 925 84 1021 2443 3:00 PM 9 8 6 23 22 231 12 265 32 2 2 3 57 3 237 22 262 607 3:15 PM 9 8 1 18 21 270 15 306 20 4 17 41 5 269 29 303 668 3:30 PM 11 7 4 22 26 25 25 26 257 15 298 33 8 30 71 1 221 20 242 633 3:45 PM 11 8 5 24 37 304 14 355 26 2 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:00 PM 12 7 5 5 24 26 218 11 259 28 3 22 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:15 PM 6 7 2 15 25 28 261 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:45 PM 19 15 5 39 32 280 13 327 7 1 1 2285 14 99.55 15 100 1338 2780 5:45 PM 19 15 5 39 32 280 13 327 7 1 1 1 2285 14 97.58 759 10676 24504 Approach 6 52.2 29.4 18.4 8 86 868 9343 496 10707 1010 161 1114 2285 149 9758 769 10676 24504 Approach 6 52.2 29.4 18.4 8 86 88 343 46.5 44.2 7.0 48.8 1.4 91.4 7.2 | I otal | 51 | 16 | 19 | 86] | 64 | 1033 | 66 | 1163 | 108 | 12 | 69 | 189 | 18 | 936 | 81 | 1035 | 2473 |
| 2:15 PM 13 7 6 26 23 261 14 298 19 3 16 38 2 251 22 275 637 230 PM 4 7 3 14 16 269 11 296 20 5 15 40 4 217 20 241 591 Total 43 24 20 87 75 1024 62 1161 83 16 75 174 12 925 84 1021 2443 3:00 PM 9 8 6 23 22 231 12 265 32 2 2 3 57 3 237 22 262 607 3:15 PM 9 8 1 18 21 270 15 306 20 4 17 41 5 269 29 303 668 3:30 PM 11 7 4 22 26 25 25 26 257 15 298 33 8 30 71 1 221 20 242 633 3:45 PM 11 8 5 24 37 304 14 355 26 2 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:00 PM 12 7 5 5 24 26 218 11 259 28 3 22 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:15 PM 6 7 2 15 25 28 261 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:45 PM 19 15 5 39 32 280 13 327 7 1 1 2285 14 99.55 15 100 1338 2780 5:45 PM 19 15 5 39 32 280 13 327 7 1 1 1 2285 14 97.58 759 10676 24504 Approach 6 52.2 29.4 18.4 8 86 868 9343 496 10707 1010 161 1114 2285 149 9758 769 10676 24504 Approach 6 52.2 29.4 18.4 8 86 88 343 46.5 44.2 7.0 48.8 1.4 91.4 7.2 | 2:00 PM | 17 | 6 | 8 | 31 | 17 | 243 | 18 | 278 | 16 | 4 | 22 | 42 | l 3 | 213 | 29 | 245 | 596 |
| 2:30 PM 4 7 3 14 16 269 11 296 20 5 15 40 4 217 20 241 591 2:45 PM 9 4 3 16 19 251 19 289 28 4 22 54 3 244 13 260 619 Total 43 24 20 87 75 1024 62 1161 83 16 75 174 12 925 84 1021 2443 3:00 PM 9 8 6 23 22 231 12 265 32 2 23 57 3 237 22 262 607 3:15 PM 9 8 1 18 21 270 15 306 20 4 17 41 5 262 29 303 668 3:345 PM 11 8 5 24 | | | | | | | | | | | | | | | | | | |
| Total 43 | 2:30 PM | 4 | 7 | 3 | 14 | 16 | 269 | 11 | 296 | 20 | 5 | 15 | | 4 | | 20 | | 591 |
| 3:00 PM 9 8 6 23 22 231 12 265 32 2 23 57 3 237 22 262 607 3:15 PM 9 8 1 18 21 270 15 306 20 4 17 41 5 269 29 303 668 3:30 PM 11 7 4 22 26 257 15 298 33 8 30 71 1 221 20 242 633 3:45 PM 11 8 5 24 37 304 14 355 26 2 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:00 PM 12 7 5 24 26 218 11 255 32 1 29 62 10 264 27 301 642 4:15 PM 6 7 2 15 27 251 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 | | 9 | | | | | | 19 | | | 4 | | | 3 | | 13 | | |
| 3:15 PM 9 8 1 18 21 270 15 306 20 4 17 41 5 269 29 303 668 3:30 PM 11 7 4 22 26 257 15 298 33 8 30 71 1 221 20 242 633 3:45 PM 11 8 5 24 37 304 14 355 26 2 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:00 PM 12 7 5 24 26 218 11 255 32 1 29 62 10 264 27 301 642 4:15 PM 6 7 2 15 27 251 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 | Total | 43 | 24 | 20 | 87 | 75 | 1024 | 62 | 1161 | 83 | 16 | 75 | 174 | 12 | 925 | 84 | 1021 | 2443 |
| 3:15 PM 9 8 1 18 21 270 15 306 20 4 17 41 5 269 29 303 668 3:30 PM 11 7 4 22 26 257 15 298 33 8 30 71 1 221 20 242 633 3:45 PM 11 8 5 24 37 304 14 355 26 2 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:00 PM 12 7 5 24 26 218 11 255 32 1 29 62 10 264 27 301 642 4:15 PM 6 7 2 15 27 251 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 | 2.00 BM I | 0 | o | | 221 | 22 | 224 | 10 | 26.51 | 2.2 | 2 | 22 | ₋ - | ر ا | 227 | 22 | 262 | 607 |
| 3:30 PM | | | | | | | | | | | | | | | | | | |
| 3:45 PM 11 8 5 24 37 304 14 355 26 2 18 46 5 266 20 291 716 Total 40 31 16 87 106 1062 56 1224 111 16 88 215 14 993 91 1098 2624 4:00 PM 12 7 5 24 26 218 11 255 32 1 29 62 10 264 27 301 642 4:15 PM 6 7 2 15 27 251 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 <td></td> | | | | | | | | | | | | | | | | | | |
| 4:00 PM 12 7 5 24 26 218 11 255 32 1 29 62 10 264 27 301 642 4:15 PM 6 7 2 15 27 251 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 | | | | | | | | | | | | | | | | | | |
| 4:15 PM 6 7 2 15 27 251 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313< | Total | 40 | 31 | 16 | 87 | 106 | 1062 | 56 | 1224 | 111 | 16 | 88 | 215 | 14 | 993 | 91 | 1098 | 2624 |
| 4:15 PM 6 7 2 15 27 251 11 289 28 3 23 54 4 320 27 351 709 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313< | | | _ | _ | ا. ہ | | | | 1 | | | | | | ~ - | | a ! | |
| 4:30 PM 21 9 1 31 32 226 12 270 28 7 29 64 3 303 23 329 694 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 29 | | | | | | | | | | | | | | | | | | |
| 4:45 PM 12 11 2 25 28 261 14 303 18 4 28 50 4 328 25 357 735 Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 3 | | | | | | | | | | | | | | | | | | |
| Total 51 34 10 95 113 956 48 1117 106 15 109 230 21 1215 102 1338 2780 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 1 | | | | | | | | | | | | | | | | | | |
| 5:00 PM 28 15 2 45 44 247 7 298 35 3 41 79 5 309 25 339 761 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 Grand Total 436 246 154 836 868 9343 496 10707 1010 1010 1011 1011 1014 1114 2285 149 9758 769 10676 24504 24 | | | | | | | | | | | | | | | | | | |
| 5:15 PM 30 13 4 47 38 253 8 299 29 6 40 75 6 313 28 347 768 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 Grand Total Approach % 52.2 29.4 18.4 8.1 8.7 8.7 8.7 8.7 8.7 8.7 8.7 | | | | | ' | | | | • | | | | | | | | | |
| 5:30 PM 27 11 6 44 33 231 13 277 18 5 24 47 1 299 33 333 701 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 Grand Total 436 246 154 836 868 9343 496 10707 1010 161 1114 2285 149 9758 769 10676 24504 Approach % 52.2 29.4 18.4 81. 87.3 4.6 44.2 7.0 48.8 1.4 91.4 7.2 | | | | | | | | | | | | | | | | | | |
| 5:45 PM 19 15 5 39 32 280 13 325 22 5 31 58 7 356 21 384 806 Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 Grand Total 436 246 154 836 868 9343 496 10707 1010 161 1114 2285 149 9758 769 10676 24504 Approach % 52.2 29.4 18.4 81. 87.3 4.6 44.2 7.0 48.8 1.4 91.4 7.2 24504 | | | | | | | | | | | | | | | | | | |
| Total 104 54 17 175 147 1011 41 1199 104 19 136 259 19 1277 107 1403 3036 Grand Total A36 246 154 836 868 9343 496 10707 1010 161 1114 2285 149 9758 769 10676 24504 Approach 52.2 29.4 18.4 81 87.3 4.6 44.2 7.0 48.8 1.4 91.4 7.2 | | | | | | | | | | | | | | | | | | |
| Grand Total 436 246 154 836 868 9343 496 10707 1010 161 1114 2285 149 9758 769 10676 24504 Approach % 52.2 29.4 18.4 8.1 87.3 4.6 44.2 7.0 48.8 1.4 91.4 7.2 | | | | | | | | | | | | | | | | | | |
| Approach % 52.2 29.4 18.4 8.1 87.3 4.6 44.2 7.0 48.8 1.4 91.4 7.2 | TOTAL | 104 | J 4 | 17 | 1/3 | 1-1/ | 1011 | 71 | 1177 | 104 | 19 | 130 | 233 | 13 | 14// | 107 | 1703 | 5050 |
| Approach % 52.2 29.4 18.4 8.1 87.3 4.6 44.2 7.0 48.8 1.4 91.4 7.2 | Grand Total | 436 | 246 | 154 | 836 | 868 | 9343 | 496 | 10707 | 1010 | 161 | 1114 | 2285 | 149 | 9758 | 769 | 10676 | 24504 |
| Total % 1.8 1.0 0.6 3.4 3.5 38.1 2.0 43.7 4.1 0.7 4.5 9.3 0.6 39.8 3.1 43.6 | Approach % | | | | | | 87.3 | 4.6 | | | 7.0 | 48.8 | | 1.4 | | 7.2 | | |
| · | Total % | 1.8 | 1.0 | 0.6 | 3.4 | 3.5 | 38.1 | 2.0 | 43.7 | 4.1 | 0.7 | 4.5 | 9.3 | 0.6 | 39.8 | 3.1 | 43.6 | |

Project: 330.029 Ebenezer Rd Subdivision Intersection: Kingston Pike at Ebenezer Road Date Conducted: Tuesday March 19,2024

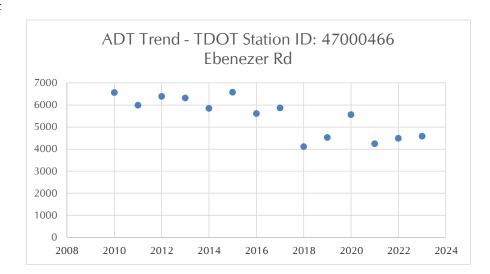
| AM Peak Hour | 7:45 AM - 8:45 AM | 1897 |
|--------------|-------------------|------|
| PM Peak Hour | 5:00 PM - 6:00 PM | 3036 |

| | | Driveway | | | Kingston Pike | | | Ebenezer Road | | | | Kingston Pike | | | | | |
|--------------------------|---------|-----------|-------|-------|---------------|-------|-------|---------------|------------|------|-------|---------------|-----------|------|-------|-------|------------|
| | | Southb | ound | | | Westb | ound | | Northbound | | | | Eastbound | | | | |
| Start | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Left | Thru | Right | Total | Int. Total |
| Peak Hour Analysis from | 7:00 AN | 1 to 9:00 |) AM | | | - | | | | | | | | | | | |
| AM Peak Hour begins at | 7:45 AM | | | | | | | | | | | | | | | | |
| 7:45 AM | 1 | 0 | 2 | 3 | 17 | 158 | 4 | 179 | 31 | 4 | 48 | 83 | 4 | 209 | 13 | 226 | 491 |
| 8:00 AM | 4 | 3 | 3 | 10 | 15 | 141 | 3 | 159 | 29 | 2 | 49 | 80 | 3 | 217 | 15 | 235 | 484 |
| 8:15 AM | 1 | 3 | 1 | 5 | 21 | 160 | 8 | 189 | 20 | 2 | 46 | 68 | 1 | 213 | 10 | 224 | 486 |
| 8:30 AM | 4 | 0 | 5 | 9 | 20 | 170 | 13 | 203 | 25 | 6 | 30 | 61 | 2 | 154 | 7 | 163 | 436 |
| Total Volume | 10 | 6 | 11 | 27 | 73 | 629 | 28 | 730 | 105 | 14 | 173 | 292 | 10 | 793 | 45 | 848 | 1897 |
| Future (1.0% over 3 yrs) | 10 | 6 | 11 | | 75 | 648 | 29 | | 108 | 14 | 178 | | 10 | 817 | 46 | | 1954 |
| PHF | 0.63 | 0.50 | 0.55 | | 0.87 | 0.93 | 0.54 | | 0.85 | 0.58 | 0.88 | | 0.63 | 0.91 | 0.75 | | 0.97 |
| Peak Hour Analysis from | 3:00 PM | to 6:00 | PM | | | | | | | | | | | | | | |
| PM Peak Hour begins at | 5:00 PM | | | | | | | | | | | | | | | | |
| 5:00 PM | 28 | 15 | 2 | 45 | 44 | 247 | 7 | 298 | 35 | 3 | 41 | 79 | 5 | 309 | 25 | 339 | 761 |
| 5:15 PM | 30 | 13 | 4 | 47 | 38 | 253 | 8 | 299 | 29 | 6 | 40 | 75 | 6 | 313 | 28 | 347 | 768 |
| 5:30 PM | 27 | 11 | 6 | 44 | 33 | 231 | 13 | 277 | 18 | 5 | 24 | 47 | 1 | 299 | 33 | 333 | 701 |
| 5:45 PM | 19 | 15 | 5 | 39 | 32 | 280 | 13 | 325 | 22 | 5 | 31 | 58 | 7 | 356 | 21 | 384 | 806 |
| Total Volume | 104 | 54 | 17 | 175 | 147 | 1011 | 41 | 1199 | 104 | 19 | 136 | 259 | 19 | 1277 | 107 | 1403 | 3036 |
| Future (1.0% over 3 yrs) | 107 | 56 | 18 | | 151 | 1042 | 42 | | 107 | 20 | 140 | | 20 | 1316 | 110 | | 3128 |
| PHF | 0.87 | 0.90 | 0.71 | | 0.84 | 0.90 | 0.79 | | 0.74 | 0.79 | 0.83 | | 0.68 | 0.90 | 0.81 | | 0.94 |

Attachment 3 ADT Trends

Adjusted Average Daily Traffic

| | Year | Daily Traffi |
|----|------|--------------|
| 10 | 2010 | 6563 |
| 11 | 2011 | 5988 |
| 12 | 2012 | 6391 |
| 13 | 2013 | 6321 |
| 14 | 2014 | 5845 |
| 15 | 2015 | 6576 |
| 16 | 2016 | 5609 |
| 17 | 2017 | 5866 |
| 18 | 2018 | 4111 |
| 19 | 2019 | 4526 |
| 20 | 2020 | 5562 |
| 21 | 2021 | 4240 |
| 22 | 2022 | 4491 |
| 23 | 2023 | 4581 |
| | | |



Most Recent Trend Line Growth

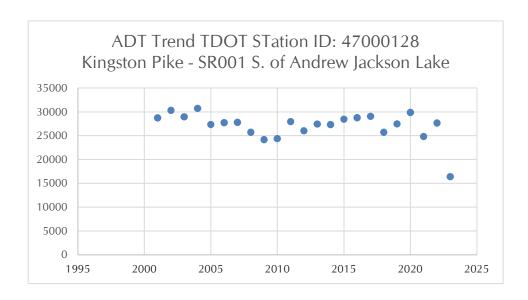
Year ADT 2013 6321 2023 4581

Annual Percent Growth

-3.80%

Adjusted Average

| Year | Daily Traffic |
|------|---------------|
| 2001 | 28732 |
| 2002 | 30319 |
| 2003 | 28953 |
| 2004 | 30734 |
| 2005 | 27340 |
| 2006 | 27738 |
| 2007 | 27777 |
| 2008 | 25714 |
| 2009 | 24173 |
| 2010 | 24388 |
| 2011 | 27957 |
| 2012 | 26019 |
| 2013 | 27441 |
| 2014 | 27306 |
| 2015 | 28450 |
| 2016 | 28758 |
| 2017 | 29058 |
| 2018 | 25708 |
| 2019 | 27477 |
| 2020 | 29865 |
| 2021 | 24832 |
| 2022 | 27645 |
| 2023 | 16397 |



Most Recent Trend Line Growth

Year ADT 2012 26019 2022 27645

Annual Percent Growth

0.59%

Attachment 4 Trip Generation

Project: Ebenezer Subdivision - Future Development Area

Date Conducted: 4/12/2024

Local Apartment Trip Generation Study 278 Units

Average Daily Traffic

 $T = 15.193(X)^{\circ}0.899$

 $T = 15.193(278)^{\circ}0.899$

T = 2392

Peak Hour of Adjacent Street Traffic One Hour Between 7 and 9 a.m.

 $T = 0.758(X)^{0.924}$

 $T = 0.758(278)^{\circ}0.924$

T = 137

Peak Hour of Adjacent Street Traffic One Hour Between 4 and 6 p.m.

T = 0.669(X) + 10.069

T = 0.669(278) + 10.069

T = 196

| | | Per | cent | Number | | |
|--------------------|-------------|-------|------|--------|------|--|
| Time Period | Total Trips | Enter | Exit | Enter | Exit | |
| Weekday (24 hours) | 2392 | 50% | 50% | 1196 | 1196 | |
| AM Peak Hour | 137 | 22% | 78% | 30 | 107 | |
| PM Peak Hour | 196 | 55% | 45% | 108 | 88 | |

Project: Ebenezer Road Subdivision

Date Conducted: 4/12/2024

Single-Family Detached Housing (LUC 210) 113 Lots

Average Daily Traffic

$$Ln(T) = 0.92 Ln(X) + 2.68$$

 $Ln(T) = 0.92 Ln(113) + 2.68$
 $T = 1129$

Peak Hour of Adjacent Street Traffic One Hour Between 7 and 9 a.m.

$$Ln(T) = 0.91 Ln(X) + 0.12$$

$$Ln(T) = 0.91 Ln(113) + 0.12$$

$$T = 83$$

Peak Hour of Adjacent Street Traffic One Hour Between 4 and 6 p.m.

$$Ln(T) = 0.94 Ln(X) + 0.27$$

 $Ln(T) = 0.94 Ln(113) + 0.27$
 $T = 112$

| | | Per | cent | Nun | nber |
|--------------------|-------------|-------|------|-------|------|
| Time Period | Total Trips | Enter | Exit | Enter | Exit |
| Weekday (24 hours) | 1129 | 50% | 50% | 565 | 565 |
| AM Peak Hour | 83 | 25% | 75% | 21 | 62 |
| PM Peak Hour | 112 | 63% | 37% | 71 | 41 |



MEMORANDUM

To: Traffic Impact Study Reviewers and Preparers (see attached list)

From: Mike Conger

Date: August 14, 2000

Subject: Local Trip Generation Rates for Multi-Family Residential Uses

Attached please find a summary of the final report with data plots for the Knox County Local Apartment Trip Generation Study. As you will recall, this report was discussed when the traffic impact study group last convened this past February. A consensus was reached at that meeting that the trip generation rates developed in the local study should be used for new apartment complexes and any other "multi-family" residential uses that are being proposed.

The MPC voted at its July 2000 meeting to officially amend the Traffic Impact Study Guidelines with language which reads that "trip generation rates for proposed uses shall be calculated using the latest edition of the ITE Trip Generation Manual, or using local data when it is available". This amendment allows the full implementation of the new rates, and they should be used for future proposed multi-family developments unless it can be demonstrated otherwise.

Thanks for your assistance and cooperation in this matter, if there are any questions or comments, please let me know.

TRAFFIC IMPACT STUDY REVIEWER & PREPARER GROUP

| Organization | Phone Number |
|---------------------|--|
| Wilbur Smith | 584-8584 |
| Land Dev. Solutions | 671-2281 |
| SITE, inc. | 693-5010 |
| TDOT | 594-9170 |
| Cannon & Cannon | 988-4818 |
| Barge Waggoner | 637-2810 |
| City of Knoxville | 215-6100 |
| Wilbur Smith | 584-8584 |
| SITE, inc. | 693-5010 |
| AR/TEC | 681-8848 |
| Allen Hoshall | 694-1834 |
| Wilbur Smith | 584-8584 |
| City of Knoxville | 215-2148 |
| TDOT | 594-9170 |
| Consultant | 777-2025 |
| TDOT | 594-9170 |
| Knox County | 215-5800 |
| TDOT | 594-9170 |
| Allen Hoshall | 694-1834 |
| Knox County | 215-5800 |
| SITE, inc. | 693-5010 |
| MPC | 215-2500 |
| | Wilbur Smith Land Dev. Solutions SITE, inc. TDOT Cannon & Cannon Barge Waggoner City of Knoxville Wilbur Smith SITE, inc. AR/TEC Allen Hoshall Wilbur Smith City of Knoxville TDOT Consultant TDOT Knox County TDOT Allen Hoshall Knox County SITE, inc. |

KNOX COUNTY LOCAL APARTMENT TRIP GENERATION STUDY

PURPOSE

A Traffic Impact Study (TIS) is currently required in Knox County when a proposed development is projected to generate in excess of 750 trips per day. The determinations of when the threshold is met as well as all subsequent analyses in the TIS are performed using the rates and equations given in the Institute of Transportation Engineers (ITE) Trip Generation Manual. Local governmental agencies rely heavily on the accuracy of these trip generation rates in order to correctly predict the impacts of a proposed development on the transportation system. Therefore, in certain instances, it is logical to verify whether the "national" rates and equations given in the ITE Trip Generation Manual are appropriate for use in a specific local area or region.

The decision was made to study the local trip-making characteristics of apartments because of the discrepancy between the trip generation rates for apartments and single family residential land uses as given in the ITE Trip Generation Manual. While these two land uses are similar in nature, the Trip Generation Manual predicts about three less trips per dwelling unit generated by apartments for the average weekday. Additionally the Trip Generation Manual points out that due to the age of their database, which dates back to the 1960's, "the rates for apartments probably had changed over time". It is also assumed that some of the ITE data had come from larger metropolitan areas with denser development and greater transit use than Knox County, which would contribute to lower trip generation rates. Therefore, this study will be used to either verify the rates given in the Trip Generation Manual or generate new ones that can be applied to locally proposed apartment developments.

PROCEDURE

The procedures recommended by ITE in conducting local trip generation studies were generally followed for this study, along with some important assumptions that have made. ITE has published a proposed recommended practice entitled "Trip Generation Handbook" which specifically outlines procedures for conducting local trip generation studies and establishing new rates and equations.

The first step in the study was to define the number and location of the sites to be studied, as well as the counting methodology. Initially 14 sites were selected, although one apartment complex – the College Park Apartments – was later omitted due to uncharacteristically high traffic generation numbers. The number of sites used in this study far exceeds the recommended minimum amount suggested by ITE, which is five sites. Traffic counts were taken for week-long periods at 15-minute intervals between July 22, 1996 and August 9, 1996 at the access points to the apartment complexes. A Technical Appendix to this report contains the traffic count data collected at each apartment complex.

RESULTS

The traffic count data was analyzed using spreadsheets in order to determine the weighted average rates and regression equations. In order to be considered valid, the local rates and equations for each time period of analysis that were generated must meet certain statistical criteria. First, the standard deviation of the independent variable (dwelling units) should be no more than 110 percent of the weighted average rate; and secondly, the regression equations require a computed coefficient of determination (R²) value of at least 0.75 before good data fit is indicated. This statistical criteria is met by the local data results, and in fact it often exceeds the level of data fit given by their counterparts in the ITE Trip Generation Manual. Finally, in order to simplify the use of the local data, plots were generated that appear identical to the actual ones in the ITE Trip Generation Manual.

The resulting rates and equations calculated from the local data indicate that the average weekday trip generation of apartments in this area is well above the national rates reported in the ITE manual. For example, the locally computed average rate for number of trips generated during a weekday is 35% higher than the rate given by ITE (increase from 6.63 trips per dwelling unit to 9.03 trips per dwelling unit). The trip generation rates do not increase as much for the AM and PM peak hours however. The local rate is roughly 8% higher for the AM peak, and 16% higher for the PM peak. The plots from the ITE Trip Generation Manual are included in the Technical Appendix for comparison purposes.

ASSUMPTIONS MADE

Some important assumptions have been made which may affect the results of the local data that was collected:

- It is important to note that the local trip generation rates were computed for the *total* number of dwelling units in the apartment complex, and <u>not</u> necessarily for the number of *occupied* dwelling units. There are several reasons why this was done, chiefly because of the need for comparability with the rates given in ITE Trip Generation Manual, as it does not specify whether the dwelling units are occupied. According to ITE procedures the selected sites must only be of "reasonably full occupancy (i.e. at least 85%)". The Apartment Association of Greater Knoxville (AAGK) publishes quarterly reports on occupancy levels of apartment complexes, and the report covering the period of the data collection was reviewed to determine occupancy levels. According to the AAGK report from July 1, 1996 September 30, 1996 all of the apartment complexes surveyed in this study met the minimum 85% occupancy level, with an average occupancy rate for all sites studied of 94%.
- The count data that was collected at each apartment complex was used "raw" meaning that it was not factored for possible daily or seasonal variations. Once again, according to an ITE representative it is not known whether the data used in the Trip Generation Manual was factored or not, so therefore in order to be able to compare

local rates to those in the manual you must assume that count data should not be factored. Additionally, it was felt that apartment complexes would generally not be as susceptible to major seasonal fluctuations as other land uses might be. The local rates were also developed using count data that was collected and averaged over an entire week, which should limit some of the daily variations. Finally, reliable local daily and seasonal variation factors do not truly exist.

CONCLUSION

The local apartment study methodology and results were distributed for comment to a group of local transportation professionals who are directly responsible for either preparing or reviewing traffic impact studies. A meeting was held between this group on February 16, 2000 in order to gather comments and discuss the study in greater detail. The following conclusions are based on the discussion and consensus reached at this meeting:

- The trip generation rates and equations meet statistical requirements and resulted from a study that followed accepted procedures; therefore they should be adopted for future use. Furthermore, the rates and equations are recommended for use in reviewing the traffic impact of any development termed as "multi-family", such as townhouse and condominium developments due to their similarity to apartment complexes.
- 2. The Traffic Access and Impact Study Guidelines and Procedures adopted by MPC should be amended with the language that local data should be used when available, which will allow the implementation of these new multi-family trip generation rates.
- 3. The following suggestions were made for future consideration:
 - This study should be updated with data collected from local townhouse and condominium developments in order to further justify the use of the new trip generation rates.
 - A statistical comparison should be made between any newly developed rates and the ITE single family trip generation rates to determine if there is a significant difference. If there is no difference then perhaps ITE single-family rates could be used for any residential development proposed in Knox County.

Local Apartment Trip Generation Study

Average Vehicle Trip Ends vs:

Dwelling Units

On a:

Weekday

Number of Studies:

13

Average Number of Dwelling Units:

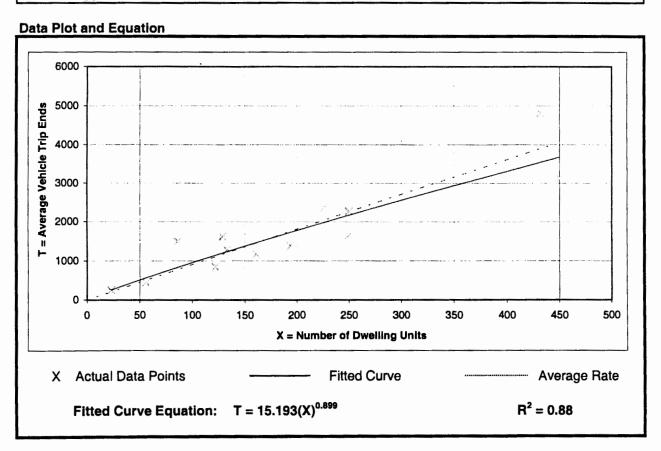
193

Directional Distribution:

50% entering, 50% exiting

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 9.03 | 6.59 - 17.41 | 2.47 |



Local Apartment Trip Generation Study

Average Vehicle Trip Ends vs:

Dwelling Units

On a:

Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Number of Studies:

13

Average Number of Dwelling Units:

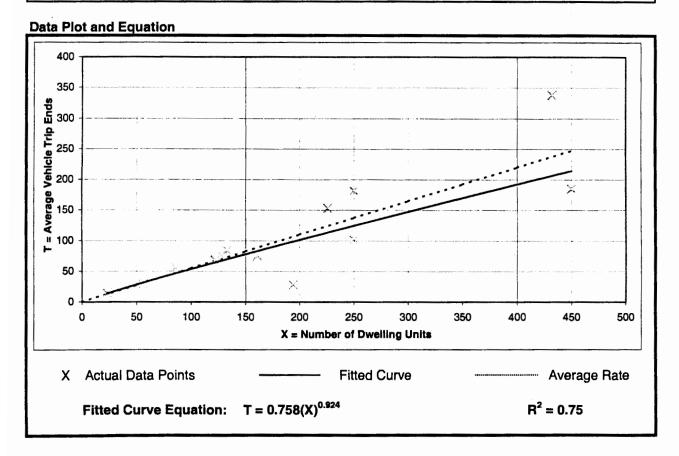
193

Directional Distribution:

22% entering, 78% exiting

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 0.55 | 0.14 - 0.78 | 0.18 |



Knoxville/Knox Co. MPC December 1999

Local Apartment Trip Generation Study

Average Vehicle Trip Ends vs:

Dwelling Units

On a:

Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Number of Studies:

13 193

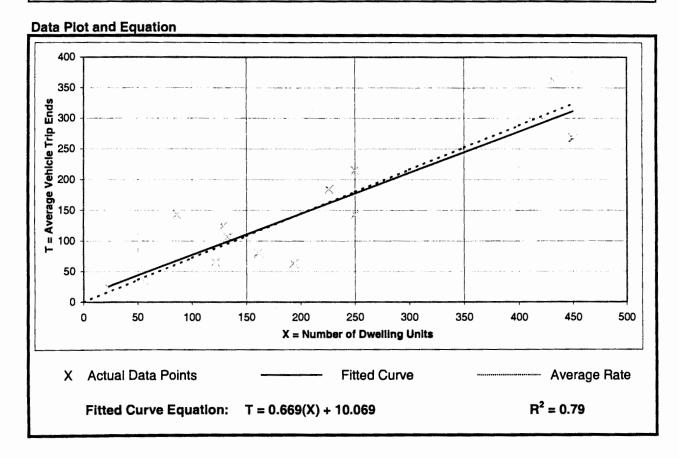
Average Number of Dwelling Units:

Directional Distribution:

55% entering, 45% exiting

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 0.72 | 0.32 - 1.66 | 0.25 |



Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units On a: Weekday

Setting/Location: General Urban/Suburban

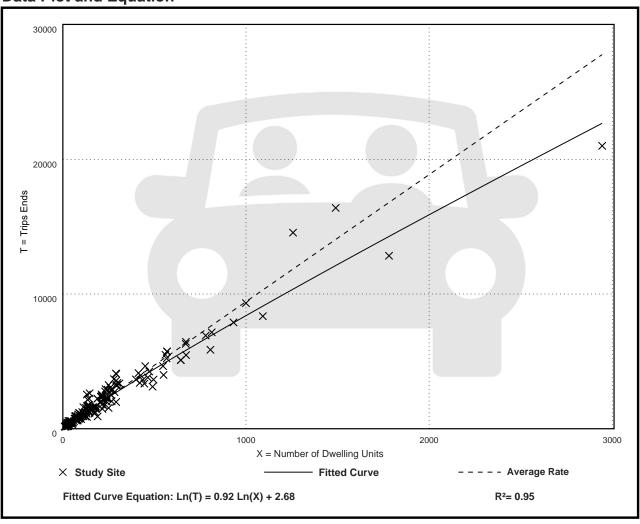
Number of Studies: 174 Avg. Num. of Dwelling Units: 246

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 9.43 | 4.45 - 22.61 | 2.13 |

Data Plot and Equation





Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

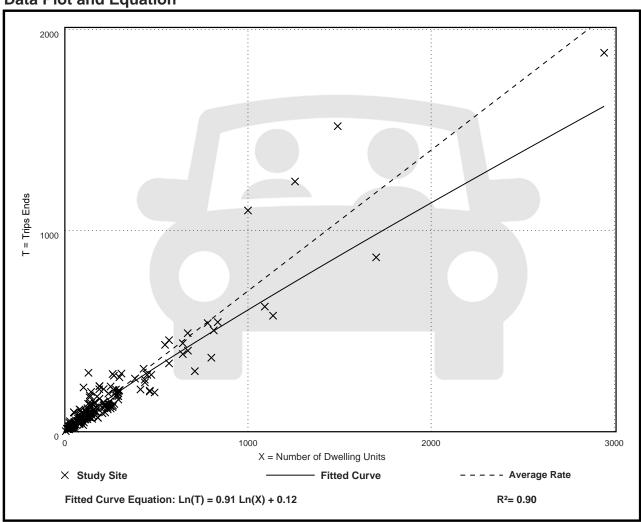
Number of Studies: 192 Avg. Num. of Dwelling Units: 226

Directional Distribution: 26% entering, 74% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.70 | 0.27 - 2.27 | 0.24 |

Data Plot and Equation





Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

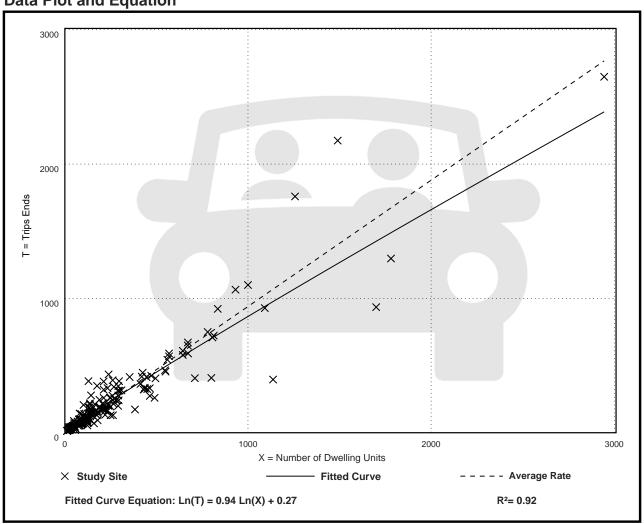
Number of Studies: 208 Avg. Num. of Dwelling Units: 248

Directional Distribution: 63% entering, 37% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.94 | 0.35 - 2.98 | 0.31 |

Data Plot and Equation



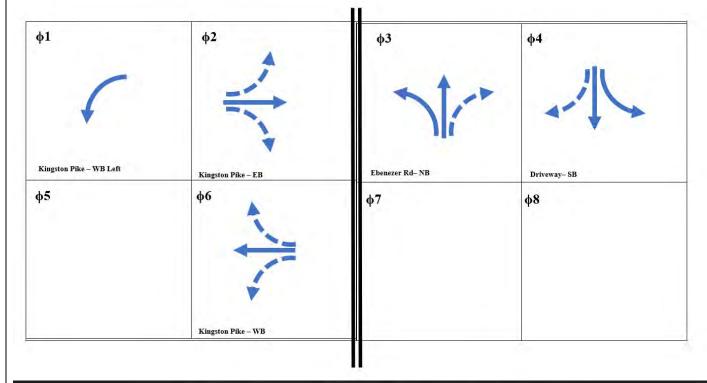


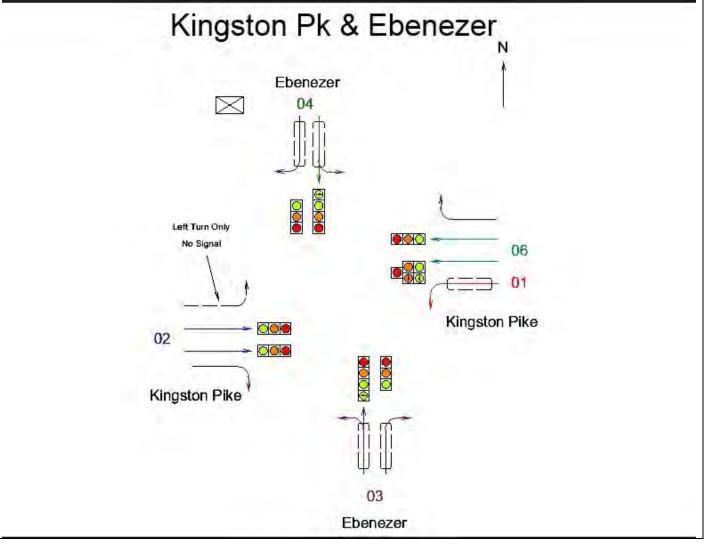
Attachment 5 Signal Timing

| Basic Tim | ing (secor | nds) | Phase 1 | Phase 2 | Phase 3 | Phase 4 | Phase 5 | Phase 6 | Phase 7 | Phase | | | | | | |
|------------|--------------------------------|----------|----------|------------|---------------|---------|-----------------------|---------|--------------|---------|------------------|--|---------------------|--|-------|--|
| | Green | iusj | 6 | 18 | 8 | 8 | 1 11050 0 | 18 | 1 11650 / | 1 11450 | | | | | | |
| | Extension | | 2 | 3 | 3 | 2 | | 3 | | | | | | | | |
| | Iax 1 | | 20 | 50 | 30 | 15 | | 50 | | | | | | | | |
| | lax 1 | | 25 | 55 | 25 | 30 | | 55 | | | | | | | | |
| | Clearanc | | 4 | 4.5 | 4 | 4 | | 4.5 | | | | | | | | |
| | Clearance | <u> </u> | 1.5 | 1.5 | 2 | 3 | | 1.5 | | | | | | | | |
| | Valk | | N/A | N/A | N/A | N/A | | N/A | | | | | | | | |
| | n Clearar | 1CE | N/A | N/A | N/A | N/A | | N/A | | | | | | | | |
| | Recall | 100 | 1071 | X | 1,111 | 1 1/11 | | X | | | | | | | | |
| Active (E) | | ases | X | X | X | X | | X | | | | | | | | |
| Flashing Y | | | | | | | | | | | | | | | | |
| | aps (1-4) | | | I | | | | | | | | | | | | |
| | <u> </u> | | Coord | dination [| Fiming/(s | seconds |) | | | | | | | | | |
| Split # | Coord. | Phase | Phase 1 | Phase 2 | Phase 3 | Phase 4 | | Phase 6 | Phase 7 | Phase | | | | | | |
| Split 1 | 2 | | 17 | 36 | 21 | 21 | | 53 | | | | | | | | |
| Split 2 | 2 | | 16 | 38 | 28 | 18 | | 54 | | | | | | | | |
| Split 3 | 2 | | 18 | 60 | 21 | 21 | | 78 | | | | | | | | |
| Split 4 | 2 | | 26 | 54 | 20 | 20 | | 80 | | | | | | | | |
| Split 5 | 2 | | 18 | 63 | 19 | 25 | | 81 | | | | | | | | |
| Split 6 | 2 | | 28 | 63 | 22 | 22 | | 91 | | | | | | | | |
| | Patter | n Table | <u>'</u> | · | Lead / Lag | | Lead / Lag | | Lead / Lag F | | Fixed / Floating | | ag Fixed / Floating | | Fixed | |
| Pattern# | Cycle | Offset | Split | Seq. # | Phas | e # | Beginnin (Green/Ye | | Yellow | | | | | | | |
| 1 | 95 | 22 | 1 | 1 | 1 | | Intersection ID# | | 25 | 2 | | | | | | |
| 2 | 100 | 76 | 2 | 1 | 1 | | I/P Add | | N/A | | | | | | | |
| 3 | 120 | 18 | 3 | 1 | 1 | | Hub Address | | N/A | 4 | | | | | | |
| 4 | 120 | 24 | 4 | 1 | 1 | _ | Radio Address | | | | | | | | | |
| 5 | 125 | 24 | 5 | 1 | 1 | | Comm. | | N/A | | | | | | | |
| 6 | 135 | 13 | 6 | 1 | 1 | | Detecti | on | Inductive | e Loop | | | | | | |
| | | | T | | an Events | | | | | | | | | | | |
| Day Plan | HH: | | | tern | - · | Plan | HH: | | Patt | | | | | | | |
| 1 | 00: | | | 34 | | 2 | | 00:00 | | 4 | | | | | | |
| 1 | 6:0 | | | 2 | | 2 | | 7:00 | | 1 | | | | | | |
| 1 | 9:3 | - | | 3 | | 2 | 8:00 | | 5 | | | | | | | |
| 1 | 14: | | | 4 | | 2 | 21: | | 1 | | | | | | | |
| 1 | 18: | | | 1 | 4 | 2 | 23: | 00 | 54 | 4 | | | | | | |
| 1 | 23: | UU | 3 | 54 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | , | Year Plai | n Schedu | ler | | | | | | | | | | |
| Plan | Mor | th of Ye | | | | | Month: 01 | - 31 | | Plan | | | | | | |
| M - F | Month of Year: 01 - 12 1-12 | | | | | _uj 01 | 01-31 | | | 1 | | | | | | |
| SAT | | 1-1 | | | | | 01-31 | | | 2 | | | | | | |
| SUN | | 1-1 | | | | | 01-31 | | | 2 | | | | | | |
| otes : | | | | | t | | | | | | | | | | | |

Ring and Barrier Diagram:

Sequence 1:





Attachment 6 Intersection Worksheets – Existing AM/PM Peaks

| | • | - | • | • | • | • | 1 | † | 1 | - | Ţ | 4 |
|--|------|----------|-------|-------|-------------|------------|---------|----------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ^ | 7 | | ર્ન | 7 | | ર્ન | 7 |
| Traffic Volume (vph) | 10 | 793 | 45 | 73 | 629 | 28 | 105 | 14 | 173 | 10 | 6 | 11 |
| Future Volume (vph) | 10 | 793 | 45 | 73 | 629 | 28 | 105 | 14 | 173 | 10 | 6 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | | 1784 | 1583 | | 1806 | 1583 |
| Flt Permitted | 0.41 | 1.00 | 1.00 | 0.22 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (perm) | 756 | 3539 | 1583 | 403 | 3539 | 1583 | | 1784 | 1583 | | 1806 | 1583 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 10 | 818 | 46 | 75 | 648 | 29 | 108 | 14 | 178 | 10 | 6 | 11 |
| RTOR Reduction (vph) | 0 | 0 | 27 | 0 | 0 | 13 | 0 | 0 | 139 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 10 | 818 | 19 | 75 | 648 | 16 | 0 | 122 | 39 | 0 | 16 | 1 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 3 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | | | 3 | | | 4 |
| Actuated Green, G (s) | 42.3 | 42.3 | 42.3 | 54.2 | 54.2 | 54.2 | | 22.0 | 22.0 | | 4.8 | 4.8 |
| Effective Green, g (s) | 42.3 | 42.3 | 42.3 | 54.2 | 54.2 | 54.2 | | 22.0 | 22.0 | | 4.8 | 4.8 |
| Actuated g/C Ratio | 0.42 | 0.42 | 0.42 | 0.54 | 0.54 | 0.54 | | 0.22 | 0.22 | | 0.05 | 0.05 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 319 | 1496 | 669 | 305 | 1918 | 857 | | 392 | 348 | | 86 | 75 |
| v/s Ratio Prot | | c0.23 | | 0.02 | c0.18 | | | c0.07 | | | c0.01 | |
| v/s Ratio Perm | 0.01 | | 0.01 | 0.12 | | 0.01 | | | 0.02 | | | 0.00 |
| v/c Ratio | 0.03 | 0.55 | 0.03 | 0.25 | 0.34 | 0.02 | | 0.31 | 0.11 | | 0.19 | 0.01 |
| Uniform Delay, d1 | 16.9 | 21.7 | 16.9 | 12.7 | 12.8 | 10.6 | | 32.7 | 31.2 | | 45.7 | 45.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.2 | 1.4 | 0.1 | 0.4 | 0.1 | 0.0 | | 2.1 | 0.7 | | 1.0 | 0.0 |
| Delay (s) | 17.1 | 23.1 | 16.9 | 13.1 | 12.9 | 10.6 | | 34.7 | 31.8 | | 46.8 | 45.4 |
| Level of Service | В | С | В | В | В | В | | С | С | | D | D |
| Approach Delay (s) | | 22.7 | | | 12.9 | | | 33.0 | | | 46.2 | |
| Approach LOS | | С | | | В | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay 20.8 | | | | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capacity ratio 0.45 | | | | | | | | | | | | |
| Actuated Cycle Length (s) 100.0 | | | | | um of lost | ` ' | | | 24.5 | | | |
| Intersection Capacity Utiliza | tion | | 55.1% | IC | CU Level of | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Analysis Period (min)
c Critical Lane Group

1: Ebenezer Road/Driveway & Kingston Pike

| | ۶ | - | * | 1 | • | | † | - | ↓ | 1 | |
|-------------------------|------|------|------|------|------|------|----------|------|----------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR | |
| Lane Group Flow (vph) | 10 | 818 | 46 | 75 | 648 | 29 | 122 | 178 | 16 | 11 | |
| v/c Ratio | 0.03 | 0.50 | 0.06 | 0.22 | 0.32 | 0.03 | 0.31 | 0.37 | 0.11 | 0.04 | |
| Control Delay | 21.0 | 22.8 | 0.1 | 13.1 | 13.0 | 0.1 | 35.3 | 7.4 | 44.7 | 0.3 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 21.0 | 22.8 | 0.1 | 13.1 | 13.0 | 0.1 | 35.3 | 7.4 | 44.7 | 0.3 | |
| Queue Length 50th (ft) | 4 | 217 | 0 | 23 | 124 | 0 | 66 | 0 | 10 | 0 | |
| Queue Length 95th (ft) | 16 | 292 | 0 | 46 | 164 | 0 | 118 | 54 | 31 | 0 | |
| Internal Link Dist (ft) | | 551 | | | 715 | | 608 | | 380 | | |
| Turn Bay Length (ft) | | | 140 | | | 100 | | 50 | | 50 | |
| Base Capacity (vph) | 348 | 1634 | 821 | 375 | 2016 | 948 | 392 | 487 | 198 | 314 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.03 | 0.50 | 0.06 | 0.20 | 0.32 | 0.03 | 0.31 | 0.37 | 0.08 | 0.04 | |
| Intersection Summary | | | | | | | | | | | |

| | ۶ | - | * | • | • | • | 1 | † | - | - | ļ | 1 |
|--------------------------------|------------|----------|-------|-------|------------|------------|---------|----------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | 7 | ^ | 7 | | र्स | 7 | | स | 7 |
| Traffic Volume (vph) | 19 | 1277 | 107 | 147 | 1011 | 41 | 104 | 19 | 136 | 104 | 54 | 17 |
| Future Volume (vph) | 19 | 1277 | 107 | 147 | 1011 | 41 | 104 | 19 | 136 | 104 | 54 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | 6.5 | 6.5 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | | 1787 | 1583 | | 1803 | 1583 |
| Flt Permitted | 0.27 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (perm) | 495 | 3539 | 1583 | 132 | 3539 | 1583 | | 1787 | 1583 | | 1803 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 20 | 1359 | 114 | 156 | 1076 | 44 | 111 | 20 | 145 | 111 | 57 | 18 |
| RTOR Reduction (vph) | 0 | 0 | 60 | 0 | 0 | 17 | 0 | 0 | 128 | 0 | 0 | 16 |
| Lane Group Flow (vph) | 20 | 1359 | 54 | 156 | 1076 | 27 | 0 | 131 | 17 | 0 | 168 | 2 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 3 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | | | 3 | | | 4 |
| Actuated Green, G (s) | 56.9 | 56.9 | 56.9 | 74.2 | 74.2 | 74.2 | | 14.0 | 14.0 | | 12.8 | 12.8 |
| Effective Green, g (s) | 56.9 | 56.9 | 56.9 | 74.2 | 74.2 | 74.2 | | 14.0 | 14.0 | | 12.8 | 12.8 |
| Actuated g/C Ratio | 0.47 | 0.47 | 0.47 | 0.62 | 0.62 | 0.62 | | 0.12 | 0.12 | | 0.11 | 0.11 |
| Clearance Time (s) | 6.5 | 6.5 | 6.5 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 234 | 1678 | 750 | 235 | 2188 | 978 | | 208 | 184 | | 192 | 168 |
| v/s Ratio Prot | | c0.38 | | c0.06 | 0.30 | | | c0.07 | | | c0.09 | |
| v/s Ratio Perm | 0.04 | | 0.03 | 0.35 | | 0.02 | | | 0.01 | | | 0.00 |
| v/c Ratio | 0.09 | 0.81 | 0.07 | 0.66 | 0.49 | 0.03 | | 0.63 | 0.09 | | 0.88 | 0.01 |
| Uniform Delay, d1 | 17.3 | 26.9 | 17.2 | 25.2 | 12.6 | 8.9 | | 50.5 | 47.3 | | 52.8 | 47.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.7 | 4.3 | 0.2 | 6.9 | 0.2 | 0.0 | | 13.6 | 1.0 | | 32.8 | 0.0 |
| Delay (s) | 18.0 | 31.3 | 17.4 | 32.1 | 12.7 | 8.9 | | 64.1 | 48.3 | | 85.6 | 48.0 |
| Level of Service | В | С | В | С | В | Α | | Е | D | | F | D |
| Approach Delay (s) | | 30.0 | | | 15.0 | | | 55.8 | | | 82.0 | |
| Approach LOS | | С | | | В | | | Е | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 29.3 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.78 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | S | um of lost | time (s) | | | 25.0 | | | |
| Intersection Capacity Utilizat | tion | | 74.5% | IC | CU Level | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

1: Ebenezer Road/Driveway & Kingston Pike

| | ۶ | - | * | 1 | ← | * | † | - | ↓ | 4 | |
|-------------------------|------|------|------|------|------|------|----------|------|----------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR | |
| Lane Group Flow (vph) | 20 | 1359 | 114 | 156 | 1076 | 44 | 131 | 145 | 168 | 18 | |
| v/c Ratio | 0.09 | 0.81 | 0.14 | 0.66 | 0.49 | 0.04 | 0.63 | 0.46 | 0.88 | 0.06 | |
| Control Delay | 20.5 | 32.4 | 2.2 | 33.7 | 13.6 | 0.1 | 64.9 | 13.1 | 91.9 | 0.4 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 20.5 | 32.4 | 2.2 | 33.7 | 13.6 | 0.1 | 64.9 | 13.1 | 91.9 | 0.4 | |
| Queue Length 50th (ft) | 8 | 455 | 0 | 59 | 225 | 0 | 98 | 0 | 130 | 0 | |
| Queue Length 95th (ft) | 27 | #622 | 22 | 128 | 277 | 1 | #169 | 61 | #257 | 0 | |
| Internal Link Dist (ft) | | 551 | | | 715 | | 608 | | 380 | | |
| Turn Bay Length (ft) | | | 140 | | | 100 | | 50 | | 50 | |
| Base Capacity (vph) | 234 | 1677 | 824 | 361 | 2187 | 1013 | 208 | 312 | 195 | 292 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.09 | 0.81 | 0.14 | 0.43 | 0.49 | 0.04 | 0.63 | 0.46 | 0.86 | 0.06 | |
| | | | | | | | | | | | |

Intersection Summary

Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Attachment 7 Intersection Worksheets – Background AM/PM Peaks

| | ۶ | - | • | • | • | • | • | † | - | - | ļ | 4 |
|-------------------------------|------------|----------|-------|-------|------------|------------|---------|----------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ^ | 7 | 7 | ^ | 7 | | र्स | 7 | | र्स | 7 |
| Traffic Volume (vph) | 10 | 817 | 46 | 75 | 648 | 29 | 108 | 14 | 178 | 10 | 6 | 11 |
| Future Volume (vph) | 10 | 817 | 46 | 75 | 648 | 29 | 108 | 14 | 178 | 10 | 6 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | | 1784 | 1583 | | 1806 | 1583 |
| Flt Permitted | 0.40 | 1.00 | 1.00 | 0.21 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (perm) | 741 | 3539 | 1583 | 384 | 3539 | 1583 | | 1784 | 1583 | | 1806 | 1583 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 10 | 842 | 47 | 77 | 668 | 30 | 111 | 14 | 184 | 10 | 6 | 11 |
| RTOR Reduction (vph) | 0 | 0 | 27 | 0 | 0 | 14 | 0 | 0 | 144 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 10 | 842 | 20 | 77 | 668 | 16 | 0 | 125 | 40 | 0 | 16 | 1 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 3 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | | | 3 | | | 4 |
| Actuated Green, G (s) | 42.2 | 42.2 | 42.2 | 54.2 | 54.2 | 54.2 | | 22.0 | 22.0 | | 4.8 | 4.8 |
| Effective Green, g (s) | 42.2 | 42.2 | 42.2 | 54.2 | 54.2 | 54.2 | | 22.0 | 22.0 | | 4.8 | 4.8 |
| Actuated g/C Ratio | 0.42 | 0.42 | 0.42 | 0.54 | 0.54 | 0.54 | | 0.22 | 0.22 | | 0.05 | 0.05 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 312 | 1493 | 668 | 298 | 1918 | 857 | | 392 | 348 | | 86 | 75 |
| v/s Ratio Prot | | c0.24 | | 0.02 | c0.19 | | | c0.07 | | | c0.01 | |
| v/s Ratio Perm | 0.01 | | 0.01 | 0.12 | | 0.01 | | | 0.03 | | | 0.00 |
| v/c Ratio | 0.03 | 0.56 | 0.03 | 0.26 | 0.35 | 0.02 | | 0.32 | 0.12 | | 0.19 | 0.01 |
| Uniform Delay, d1 | 16.9 | 21.9 | 16.9 | 12.9 | 12.9 | 10.6 | | 32.7 | 31.2 | | 45.7 | 45.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.2 | 1.5 | 0.1 | 0.5 | 0.1 | 0.0 | | 2.1 | 0.7 | | 1.0 | 0.0 |
| Delay (s) | 17.1 | 23.5 | 17.0 | 13.4 | 13.0 | 10.6 | | 34.8 | 31.9 | | 46.8 | 45.4 |
| Level of Service | В | С | В | В | В | В | | С | С | | D | D |
| Approach Delay (s) | | 23.1 | | | 13.0 | | | 33.1 | | | 46.2 | |
| Approach LOS | | С | | | В | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 21.0 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.46 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | um of lost | | | | 24.5 | | | |
| Intersection Capacity Utiliza | ition | | 56.1% | IC | CU Level | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Analysis Period (min)
c Critical Lane Group

1: Ebenezer Road/Driveway & Kingston Pike

| | ۶ | → | * | 1 | ← | | † | - | ↓ | 1 | |
|-------------------------|------|----------|------|------|----------|------|----------|------|----------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR | |
| Lane Group Flow (vph) | 10 | 842 | 47 | 77 | 668 | 30 | 125 | 184 | 16 | 11 | |
| v/c Ratio | 0.03 | 0.52 | 0.06 | 0.24 | 0.33 | 0.03 | 0.32 | 0.37 | 0.11 | 0.04 | |
| Control Delay | 21.0 | 23.1 | 0.1 | 13.2 | 13.1 | 0.1 | 35.4 | 7.4 | 44.7 | 0.3 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 21.0 | 23.1 | 0.1 | 13.2 | 13.1 | 0.1 | 35.4 | 7.4 | 44.7 | 0.3 | |
| Queue Length 50th (ft) | 4 | 226 | 0 | 24 | 129 | 0 | 67 | 0 | 10 | 0 | |
| Queue Length 95th (ft) | 16 | 303 | 0 | 48 | 171 | 0 | 120 | 55 | 31 | 0 | |
| Internal Link Dist (ft) | | 551 | | | 715 | | 608 | | 380 | | |
| Turn Bay Length (ft) | | | 140 | | | 100 | | 50 | | 50 | |
| Base Capacity (vph) | 342 | 1632 | 821 | 366 | 2016 | 948 | 392 | 491 | 198 | 314 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.03 | 0.52 | 0.06 | 0.21 | 0.33 | 0.03 | 0.32 | 0.37 | 0.08 | 0.04 | |
| Intersection Summary | | | | | | | | | | | |

| | ۶ | - | • | • | • | • | 4 | † | - | - | Ţ | 1 |
|--------------------------------|-----------|----------|-------|-------|------------|------------|---------|----------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ^ | 7 | 7 | ^ | 7 | | र्स | 7 | | ર્ન | 7 |
| Traffic Volume (vph) | 20 | 1316 | 110 | 151 | 1042 | 42 | 107 | 20 | 140 | 107 | 56 | 18 |
| Future Volume (vph) | 20 | 1316 | 110 | 151 | 1042 | 42 | 107 | 20 | 140 | 107 | 56 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | 6.5 | 6.5 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | | 1787 | 1583 | | 1804 | 1583 |
| Flt Permitted | 0.26 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (perm) | 479 | 3539 | 1583 | 119 | 3539 | 1583 | | 1787 | 1583 | | 1804 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 21 | 1400 | 117 | 161 | 1109 | 45 | 114 | 21 | 149 | 114 | 60 | 19 |
| RTOR Reduction (vph) | 0 | 0 | 62 | 0 | 0 | 17 | 0 | 0 | 128 | 0 | 0 | 17 |
| Lane Group Flow (vph) | 21 | 1400 | 55 | 161 | 1109 | 28 | 0 | 135 | 21 | 0 | 174 | 2 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 3 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | | | 3 | | | 4 |
| Actuated Green, G (s) | 56.4 | 56.4 | 56.4 | 74.0 | 74.0 | 74.0 | | 14.0 | 14.0 | | 13.0 | 13.0 |
| Effective Green, g (s) | 56.4 | 56.4 | 56.4 | 74.0 | 74.0 | 74.0 | | 14.0 | 14.0 | | 13.0 | 13.0 |
| Actuated g/C Ratio | 0.47 | 0.47 | 0.47 | 0.62 | 0.62 | 0.62 | | 0.12 | 0.12 | | 0.11 | 0.11 |
| Clearance Time (s) | 6.5 | 6.5 | 6.5 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 225 | 1663 | 744 | 232 | 2182 | 976 | | 208 | 184 | | 195 | 171 |
| v/s Ratio Prot | | c0.40 | | c0.07 | 0.31 | | | c0.08 | | | c0.10 | |
| v/s Ratio Perm | 0.04 | | 0.03 | 0.36 | | 0.02 | | | 0.01 | | | 0.00 |
| v/c Ratio | 0.09 | 0.84 | 0.07 | 0.69 | 0.51 | 0.03 | | 0.65 | 0.11 | | 0.89 | 0.01 |
| Uniform Delay, d1 | 17.6 | 27.9 | 17.5 | 29.1 | 12.8 | 9.0 | | 50.7 | 47.4 | | 52.8 | 47.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.8 | 5.4 | 0.2 | 8.7 | 0.2 | 0.0 | | 14.6 | 1.3 | | 36.1 | 0.0 |
| Delay (s) | 18.4 | 33.2 | 17.7 | 37.8 | 13.0 | 9.0 | | 65.3 | 48.7 | | 88.9 | 47.8 |
| Level of Service | В | С | В | D | В | Α | | Е | D | | F | D |
| Approach Delay (s) | | 31.9 | | | 15.9 | | | 56.6 | | | 84.9 | |
| Approach LOS | | С | | | В | | | Е | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 30.7 | H | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.80 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | Sı | um of lost | time (s) | | | 25.0 | | | |
| Intersection Capacity Utilizat | ion | | 76.1% | IC | CU Level | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

1: Ebenezer Road/Driveway & Kingston Pike

| | • | → | * | 1 | ← | * | † | 1 | ↓ | 1 | |
|-------------------------|------|----------|------|------|------|------|----------|------|----------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR | |
| Lane Group Flow (vph) | 21 | 1400 | 117 | 161 | 1109 | 45 | 135 | 149 | 174 | 19 | |
| v/c Ratio | 0.09 | 0.84 | 0.14 | 0.69 | 0.51 | 0.04 | 0.65 | 0.48 | 0.89 | 0.07 | |
| Control Delay | 20.9 | 34.4 | 2.4 | 38.5 | 13.9 | 0.1 | 66.0 | 14.0 | 94.7 | 0.4 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 20.9 | 34.4 | 2.4 | 38.5 | 13.9 | 0.1 | 66.0 | 14.0 | 94.7 | 0.4 | |
| Queue Length 50th (ft) | 9 | 481 | 0 | 69 | 236 | 0 | 101 | 3 | 135 | 0 | |
| Queue Length 95th (ft) | 28 | #691 | 24 | 139 | 288 | 1 | #180 | 65 | #268 | 0 | |
| Internal Link Dist (ft) | | 551 | | | 715 | | 608 | | 380 | | |
| Turn Bay Length (ft) | | | 140 | | | 100 | | 50 | | 50 | |
| Base Capacity (vph) | 224 | 1663 | 818 | 355 | 2182 | 1011 | 208 | 312 | 195 | 292 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.09 | 0.84 | 0.14 | 0.45 | 0.51 | 0.04 | 0.65 | 0.48 | 0.89 | 0.07 | |

Intersection Summary # 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Attachment 8 Intersection Worksheets – Full Buildout AM/PM Peaks

| | ۶ | - | • | • | • | • | 1 | † | / | - | Ţ | 4 |
|-------------------------------|------------|----------|-------|-------|-------------|------------|---------|----------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ^ | 7 | * | ^ | 7 | | र्स | 7 | | ર્ન | 7 |
| Traffic Volume (vph) | 10 | 817 | 58 | 97 | 648 | 29 | 149 | 20 | 249 | 10 | 8 | 11 |
| Future Volume (vph) | 10 | 817 | 58 | 97 | 648 | 29 | 149 | 20 | 249 | 10 | 8 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | | 1784 | 1583 | | 1812 | 1583 |
| Flt Permitted | 0.40 | 1.00 | 1.00 | 0.20 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (perm) | 741 | 3539 | 1583 | 378 | 3539 | 1583 | | 1784 | 1583 | | 1812 | 1583 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 10 | 842 | 60 | 100 | 668 | 30 | 154 | 21 | 257 | 10 | 8 | 11 |
| RTOR Reduction (vph) | 0 | 0 | 35 | 0 | 0 | 14 | 0 | 0 | 158 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 10 | 842 | 25 | 100 | 668 | 16 | 0 | 175 | 99 | 0 | 18 | 1 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 3 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | | | 3 | | | 4 |
| Actuated Green, G (s) | 41.6 | 41.6 | 41.6 | 54.2 | 54.2 | 54.2 | | 22.0 | 22.0 | | 4.8 | 4.8 |
| Effective Green, g (s) | 41.6 | 41.6 | 41.6 | 54.2 | 54.2 | 54.2 | | 22.0 | 22.0 | | 4.8 | 4.8 |
| Actuated g/C Ratio | 0.42 | 0.42 | 0.42 | 0.54 | 0.54 | 0.54 | | 0.22 | 0.22 | | 0.05 | 0.05 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 308 | 1472 | 658 | 303 | 1918 | 857 | | 392 | 348 | | 86 | 75 |
| v/s Ratio Prot | | c0.24 | | 0.02 | c0.19 | | | c0.10 | | | c0.01 | |
| v/s Ratio Perm | 0.01 | | 0.02 | 0.16 | | 0.01 | | | 0.06 | | | 0.00 |
| v/c Ratio | 0.03 | 0.57 | 0.04 | 0.33 | 0.35 | 0.02 | | 0.45 | 0.28 | | 0.21 | 0.01 |
| Uniform Delay, d1 | 17.3 | 22.4 | 17.3 | 13.2 | 12.9 | 10.6 | | 33.7 | 32.4 | | 45.8 | 45.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.2 | 1.6 | 0.1 | 0.6 | 0.1 | 0.0 | | 3.6 | 2.0 | | 1.2 | 0.0 |
| Delay (s) | 17.5 | 24.0 | 17.4 | 13.8 | 13.0 | 10.6 | | 37.4 | 34.5 | | 47.0 | 45.4 |
| Level of Service | В | С | В | В | В | В | | D | С | | D | D |
| Approach Delay (s) | | 23.5 | | | 13.0 | | | 35.7 | | | 46.4 | |
| Approach LOS | | С | | | В | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 22.4 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.50 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | um of lost | | | | 24.5 | | | |
| Intersection Capacity Utiliza | tion | | 60.5% | IC | CU Level of | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

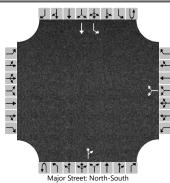
Analysis Period (min)
c Critical Lane Group

1: Ebenezer Road/Driveway & Kingston Pike

| | ۶ | → | • | • | • | • | † | - | ļ | 4 | |
|-------------------------|------|----------|------|------|------|------|----------|------|------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR | |
| Lane Group Flow (vph) | 10 | 842 | 60 | 100 | 668 | 30 | 175 | 257 | 18 | 11 | |
| v/c Ratio | 0.03 | 0.52 | 0.07 | 0.30 | 0.33 | 0.03 | 0.45 | 0.51 | 0.12 | 0.04 | |
| Control Delay | 21.8 | 23.8 | 0.2 | 13.9 | 13.1 | 0.1 | 38.0 | 12.5 | 44.9 | 0.3 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 21.8 | 23.8 | 0.2 | 13.9 | 13.1 | 0.1 | 38.0 | 12.5 | 44.9 | 0.3 | |
| Queue Length 50th (ft) | 4 | 230 | 0 | 31 | 129 | 0 | 97 | 28 | 11 | 0 | |
| Queue Length 95th (ft) | 16 | 310 | 0 | 59 | 171 | 0 | 163 | 101 | 33 | 0 | |
| Internal Link Dist (ft) | | 551 | | | 715 | | 608 | | 380 | | |
| Turn Bay Length (ft) | | | 140 | | | 100 | | 50 | | 50 | |
| Base Capacity (vph) | 336 | 1609 | 812 | 364 | 2015 | 948 | 392 | 506 | 199 | 314 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.03 | 0.52 | 0.07 | 0.27 | 0.33 | 0.03 | 0.45 | 0.51 | 0.09 | 0.04 | |
| Intersection Summary | | | | | | | | | | | |

| HCS Two-Way Stop-Control Report | | | | | | | | | | | |
|--|-----------------------|--------------------|-------------------------------------|--|--|--|--|--|--|--|--|
| General Information Site Information | | | | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Ebenezer Road at Apartment Driveway | | | | | | | | |
| Agency/Co. | Ardurra | Jurisdiction | Knox County | | | | | | | | |
| Date Performed | 4/13/2024 | East/West Street | Apartment Driveway | | | | | | | | |
| Analysis Year | 2027 | North/South Street | Ebenezer Road | | | | | | | | |
| Time Analyzed | Full Buildout AM Peak | Peak Hour Factor | 0.92 | | | | | | | | |
| Intersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | | | |
| Project Description 330.029 - Ebenezer Subdivision | | | | | | | | | | | |

Lanes

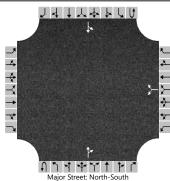


| Major Street: North-South | | | | | | | | | | | | | | | | |
|---|--------|--------------|--------|----|---|-------|-------|------|----|-------|-------|----|----|-------|-------|---|
| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | |
| Approach | Τ | Eastk | oound | | | Westl | bound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 |
| Configuration | | | | | | | LR | | | | | TR | | L | Т | |
| Volume (veh/h) | | | | | | 32 | | 75 | | | 343 | 9 | | 21 | 142 | |
| Percent Heavy Vehicles (%) | | | | | | 2 | | 2 | | | | | | 2 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | 0 | | | | | | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | Undivided | | | | | | | | | | | | | | |
| Critical and Follow-up H | eadwa | ys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.1 | | 6.2 | | | | | | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.42 | | 6.22 | | | | | | 4.12 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.52 | | 3.32 | | | | | | 2.22 | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 116 | | | | | | | 23 | | |
| Capacity, c (veh/h) | | | | | | | 593 | | | | | | | 1176 | | |
| v/c Ratio | | | | | | | 0.20 | | | | | | | 0.02 | | |
| 95% Queue Length, Q ₉₅ (veh) | | 0.7 | | | | | | | | 0.1 | | | | | | |
| Control Delay (s/veh) | | 12.5 8.1 0.1 | | | | | | | | | | | | | | |
| Level of Service (LOS) | | B A A | | | | | | | | | | | | | | |
| Approach Delay (s/veh) | | | | | | 12 | 2.5 | | | | | | | 1 | .2 | |
| Approach LOS | | B A | | | | | | | | | | | | | | |

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| HCS Two-Way Stop-Control Report | | | | | | | | | | | |
|--|-----------------------|--------------------|---------------------------|--|--|--|--|--|--|--|--|
| General Information Site Information | | | | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Ebenezer Road at Driveway | | | | | | | | |
| Agency/Co. | Ardurra | Jurisdiction | Knox County | | | | | | | | |
| Date Performed | 4/13/2024 | East/West Street | Subdivision Driveway | | | | | | | | |
| Analysis Year | 2027 | North/South Street | Ebenezer Road | | | | | | | | |
| Time Analyzed | Full Buildout AM Peak | Peak Hour Factor | 0.92 | | | | | | | | |
| Intersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | | | |
| Project Description 330.029 - Ebenezer Subdivision | | | | | | | | | | | |

Lanes



| | | | | | Majo | Street: Nor | th-South | | | | | | | | | |
|---|--------|-----------|--------|----|------|-------------|----------|------|------------|---|-----|-----|------------|------|-----|---|
| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | |
| Approach | Π | Eastk | ound | | | Westbound | | | Northbound | | | | Southbound | | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration | | | | | | | LR | | | | | TR | | LT | | |
| Volume (veh/h) | | | | | | 19 | | 43 | | | 309 | 7 | | 15 | 159 | |
| Percent Heavy Vehicles (%) | | | | | | 2 | | 2 | | | | | | 2 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | Undivided | | | | | | | | | | | | | | |
| Critical and Follow-up Headways | | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.1 | | 6.2 | | | | | | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.42 | | 6.22 | | | | | | 4.12 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.52 | | 3.32 | | | | | | 2.22 | | |
| Delay, Queue Length, and | d Leve | l of S | ervice | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 67 | | | | | | | 16 | | |
| Capacity, c (veh/h) | | | | | | | 621 | | | | | | | 1216 | | |
| v/c Ratio | | | | | | | 0.11 | | | | | | | 0.01 | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 0.4 | | | | | | | 0.0 | | |
| Control Delay (s/veh) | | | | | | | 11.5 | | | | | | | 8.0 | 0.1 | |
| Level of Service (LOS) | | | | | | | В | | | | | | | А | А | |
| Approach Delay (s/veh) | | | | | 11.5 | | | | | | | 0.8 | | | | |
| Approach LOS | | | | | | | В | | | | | А | | | | |

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|-----------------------------------|---------|----------|-------------|-------|------------|------------|---------|----------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ^ | 7 | 1 | ^ | 7 | | स | 7 | | ર્ન | 7 |
| Traffic Volume (vph) | 20 | 1316 | 153 | 226 | 1042 | 42 | 138 | 26 | 194 | 107 | 63 | 18 |
| Future Volume (vph) | 20 | 1316 | 153 | 226 | 1042 | 42 | 138 | 26 | 194 | 107 | 63 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | 6.5 | 6.5 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | | 1788 | 1583 | | 1806 | 1583 |
| FIt Permitted | 0.26 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | | 0.96 | 1.00 | | 0.97 | 1.00 |
| Satd. Flow (perm) | 479 | 3539 | 1583 | 128 | 3539 | 1583 | | 1788 | 1583 | | 1806 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 21 | 1400 | 163 | 240 | 1109 | 45 | 147 | 28 | 206 | 114 | 67 | 19 |
| RTOR Reduction (vph) | 0 | 0 | 80 | 0 | 0 | 17 | 0 | 0 | 128 | 0 | 0 | 17 |
| Lane Group Flow (vph) | 21 | 1400 | 83 | 240 | 1109 | 28 | 0 | 175 | 78 | 0 | 181 | 2 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Perm | Split | NA | Perm | Split | NA | Perm |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 3 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | | | 3 | | | 4 |
| Actuated Green, G (s) | 52.1 | 52.1 | 52.1 | 74.0 | 74.0 | 74.0 | | 14.0 | 14.0 | | 13.0 | 13.0 |
| Effective Green, g (s) | 52.1 | 52.1 | 52.1 | 74.0 | 74.0 | 74.0 | | 14.0 | 14.0 | | 13.0 | 13.0 |
| Actuated g/C Ratio | 0.43 | 0.43 | 0.43 | 0.62 | 0.62 | 0.62 | | 0.12 | 0.12 | | 0.11 | 0.11 |
| Clearance Time (s) | 6.5 | 6.5 | 6.5 | 5.5 | 6.0 | 6.0 | | 6.0 | 6.0 | | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 207 | 1536 | 687 | 296 | 2182 | 976 | | 208 | 184 | | 195 | 171 |
| v/s Ratio Prot | | c0.40 | | c0.11 | 0.31 | | | c0.10 | | | c0.10 | |
| v/s Ratio Perm | 0.04 | | 0.05 | 0.39 | | 0.02 | | | 0.05 | | | 0.00 |
| v/c Ratio | 0.10 | 0.91 | 0.12 | 0.81 | 0.51 | 0.03 | | 0.84 | 0.42 | | 0.93 | 0.01 |
| Uniform Delay, d1 | 20.1 | 31.8 | 20.3 | 35.2 | 12.8 | 9.0 | | 51.9 | 49.2 | | 53.0 | 47.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.0 | 9.7 | 0.4 | 15.4 | 0.2 | 0.0 | | 31.8 | 7.0 | | 44.0 | 0.0 |
| Delay (s) | 21.1 | 41.5 | 20.6 | 50.5 | 13.0 | 9.0 | | 83.7 | 56.2 | | 97.1 | 47.8 |
| Level of Service | С | D | С | D | В | Α | | F | E | | F | D |
| Approach Delay (s) | | 39.1 | | | 19.4 | | | 68.8 | | | 92.4 | |
| Approach LOS | | D | | | В | | | Е | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 37.5 | H | CM 2000 | Level of S | Service | | D | | | |
| HCM 2000 Volume to Capacity | / ratio | | 0.89 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | Sı | um of lost | time (s) | | | 25.0 | | | |
| Intersection Capacity Utilization | | | | | | | | | | | | |
| | n | | 80.6% 15 | IC | U Level (| of Service | | | D | | | |

c Critical Lane Group

1: Ebenezer Road/Driveway & Kingston Pike

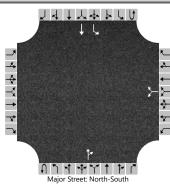
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|-------------------------|------|----------|------|------|------|------|----------|------|----------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBT | NBR | SBT | SBR | |
| Lane Group Flow (vph) | 21 | 1400 | 163 | 240 | 1109 | 45 | 175 | 206 | 181 | 19 | |
| v/c Ratio | 0.10 | 0.91 | 0.21 | 0.81 | 0.51 | 0.04 | 0.84 | 0.66 | 0.93 | 0.07 | |
| Control Delay | 23.9 | 42.5 | 6.1 | 49.3 | 13.9 | 0.1 | 84.3 | 27.6 | 101.5 | 0.4 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 23.9 | 42.5 | 6.1 | 49.3 | 13.9 | 0.1 | 84.3 | 27.6 | 101.5 | 0.4 | |
| Queue Length 50th (ft) | 10 | 530 | 10 | 128 | 236 | 0 | 135 | 44 | 141 | 0 | |
| Queue Length 95th (ft) | 29 | #731 | 54 | 215 | 288 | 1 | #259 | 127 | #281 | 0 | |
| Internal Link Dist (ft) | | 551 | | | 715 | | 608 | | 380 | | |
| Turn Bay Length (ft) | | | 140 | | | 100 | | 50 | | 50 | |
| Base Capacity (vph) | 208 | 1537 | 767 | 360 | 2182 | 1011 | 208 | 312 | 195 | 292 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.10 | 0.91 | 0.21 | 0.67 | 0.51 | 0.04 | 0.84 | 0.66 | 0.93 | 0.07 | |

Intersection Summary
95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

| HCS Two-Way Stop-Control Report | | | | | | | | | | |
|---------------------------------|--------------------------------|----------------------------|-------------------------------------|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Ebenezer Road at Apartment Driveway | | | | | | | |
| Agency/Co. | Ardurra | Jurisdiction | Knox County | | | | | | | |
| Date Performed | 4/13/2024 | East/West Street | Apartment Driveway | | | | | | | |
| Analysis Year | 2027 | North/South Street | Ebenezer Road | | | | | | | |
| Time Analyzed | Full Buildout PM Peak | Peak Hour Factor | 0.92 | | | | | | | |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 | | | | | | | |
| Project Description | 330.029 - Ebenezer Subdivision | | | | | | | | | |

Lanes

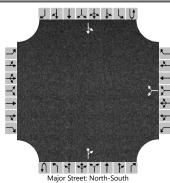


| | | | | | Majo | r Street: Nor | th-South | J | | | | | | | | | |
|---|--------|-----------|--------|----|------|---------------|----------|------|------------|---|-----|------------|----|------|-----|---|--|
| Vehicle Volumes and Adj | ustme | nts | | | | | | | | | | | | | | | |
| Approach | Τ | Eastk | oound | | | Westbound | | | Northbound | | | Southbound | | | | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | |
| Configuration | | | | | | | LR | | | | | TR | | L | Т | | |
| Volume (veh/h) | | | | | | 26 | | 62 | | | 296 | 32 | | 76 | 367 | | |
| Percent Heavy Vehicles (%) | | | | | | 2 | | 2 | | | | | | 2 | | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | | |
| Median Type Storage | | Undivided | | | | | | | | | | | | | | | |
| Critical and Follow-up Headways | | | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | | | | | 7.1 | | 6.2 | | | | | | 4.1 | | | |
| Critical Headway (sec) | | | | | | 6.42 | | 6.22 | | | | | | 4.12 | | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | | |
| Follow-Up Headway (sec) | | | | | | 3.52 | | 3.32 | | | | | | 2.22 | | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | | | | | 96 | | | | | | | 83 | | | |
| Capacity, c (veh/h) | | | | | | | 492 | | | | | | | 1202 | | | |
| v/c Ratio | | | | | | | 0.19 | | | | | | | 0.07 | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 0.7 | | | | | | | 0.2 | | | |
| Control Delay (s/veh) | | | | | | | 14.1 | | | | | | | 8.2 | 0.4 | | |
| Level of Service (LOS) | | | | | | | В | | | | | | | А | А | | |
| Approach Delay (s/veh) | | | | | | 14 | 4.1 | | | | | 1.7 | | | | | |
| Approach LOS | | | | | | | В | | | | | А | | | | | |

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| HCS Two-Way Stop-Control Report | | | | | | | | | | |
|---------------------------------|--------------------------------|----------------------------|---------------------------|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Ebenezer Road at Driveway | | | | | | | |
| Agency/Co. | Ardurra | Jurisdiction | Knox County | | | | | | | |
| Date Performed | 4/13/2024 | East/West Street | Subdivision Driveway | | | | | | | |
| Analysis Year | 2027 | North/South Street | Ebenezer Road | | | | | | | |
| Time Analyzed | Full Buildout PM Peak | Peak Hour Factor | 0.92 | | | | | | | |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 | | | | | | | |
| Project Description | 330.029 - Ebenezer Subdivision | | | | | | | | | |

Lanes



| | | | | | Majo | r Street: Nor | th-South | , | | | | | | | | |
|---|--------------------|-----------|--------|----|------|---------------|----------|------|------------|---|-----|----|------------|------|-----|---|
| Vehicle Volumes and Ad | justme | nts | | | | | | | | | | | | | | |
| Approach | T | Eastk | oound | | | Westbound | | | Northbound | | | | Southbound | | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration | | | | | | | LR | | | | | TR | | LT | | |
| Volume (veh/h) | | | | | | 12 | | 29 | | | 299 | 21 | | 50 | 343 | |
| Percent Heavy Vehicles (%) | | | | | | 2 | | 2 | | | | | | 2 | | |
| Proportion Time Blocked | | | | | | | | | | | | | | | | |
| Percent Grade (%) | | | | | | (| 0 | | | | | | | | | |
| Right Turn Channelized | | | | | | | | | | | | | | | | |
| Median Type Storage | | Undivided | | | | | | | | | | | | | | |
| Critical and Follow-up H | Follow-up Headways | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | T | | | | | 7.1 | | 6.2 | | | | | | 4.1 | | |
| Critical Headway (sec) | | | | | | 6.42 | | 6.22 | | | | | | 4.12 | | |
| Base Follow-Up Headway (sec) | | | | | | 3.5 | | 3.3 | | | | | | 2.2 | | |
| Follow-Up Headway (sec) | | | | | | 3.52 | | 3.32 | | | | | | 2.22 | | |
| Delay, Queue Length, an | d Leve | l of S | ervice | • | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | T | | | | | | 45 | | | | | | | 54 | | |
| Capacity, c (veh/h) | | | | | | | 526 | | | | | | | 1211 | | |
| v/c Ratio | | | | | | | 0.08 | | | | | | | 0.04 | | |
| 95% Queue Length, Q ₉₅ (veh) | | | | | | | 0.3 | | | | | | | 0.1 | | |
| Control Delay (s/veh) | | | | | | | 12.5 | | | | | | | 8.1 | 0.5 | |
| Level of Service (LOS) | | | | | | | В | | | | | | | Α | А | |
| Approach Delay (s/veh) | | | | | | 12 | 2.5 | | | | | | | 1 | .4 | |
| Approach LOS | | | | | | | В | | | | | | | , | 4 | |

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Attachment 9 Turn Lane Warrants

Project: Ebenezer Road Subdivision

| | _ | = |
|---------------|---|---------|
| Ebenezer Road | | VOLUMES |

at Apartment Roadway

| LEFT TURN | Opposing | Thru | LT | LT MAX | Warrant Met |
|-----------|----------|------|----|--------|-------------|
| AM | 352 | 142 | 21 | 135 | NO |
| PM | 328 | 367 | 76 | 65 | YES |

Ebenezer Road VOLUMES

at Apartment Roadway

| RIGHT TURN | Thru | RT | RT MAX | Warrant Met |
|------------|------|----|--------|-------------|
| AM | 343 | 9 | 299 | NO |
| PM | 296 | 32 | 349 | NO |

Ebenezer Road at Subdivision Roadway

Ebenezer Road VOLUMES

at Subdivision Roadway

| LEFT TURN | Opposing | Thru | LT | LT MAX | Warrant Met |
|-----------|----------|------|----|--------|-------------|
| AM | 316 | 159 | 15 | 135 | NO |
| PM | 320 | 343 | 50 | 80 | NO |

Ebenezer Road VOLUMES

at Subdivision Roadway RIGHT TURN

| RIGHT TURN | I hru | RI | RIMAX | Warrant Met |
|------------|-------|----|-------|-------------|
| AM | 309 | 7 | 299 | NO |
| PM | 299 | 21 | 349 | NO |

TABLE 4A

LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

(If the left-turn volume exceeds the table value a left -turn lane is needed)

| OPPOSING | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * | | | | | | |
|------------------------|---|-----------------|------------|-----------|------------------|-----------|--|
| VOLUME | 100 - 149 | 150 - 199 | 200 - 249 | 250 - 299 | 300 - 349 | 350 - 399 | |
| 100 - 149 | 300 | 235 | 185 | 145 | 120 | 100 | |
| 150 - 199 | 245 | 200 | 160 | 130 | 110 | 90 | |
| 200 - 249 | 205 | 170 | 140 | 115 | 100 | 80 | |
| 250 - 299 | 175 | 150 | 125 | 105 | 90 | 70 | |
| 300 - 349 350 - 399 | 155 (135) AM F | 135 Peak 120 | 110 100 | , , | PM Peak 76 LT | 65 | |
| 400 - 449 | 120 | 105 | 90 | 75 | 65 | 55 | |
| 450 - 499 | 105 | 90 | 80 | 70 | 60 | 50 | |
| 5(K) - 549 | 95 | 80 | 70 | 65 | 55 | 50 | |
| 550 - 599 | 85 | 70 | 65 | 60 | 50 | 45 | |
| 600 - 649 | 75 | 65 | 60 | 55 | 45 | 40 | |
| 650 - 699 | 70 | 60 | 55 | 50 | 40 | 35 | |
| 700 - 749 | 65 | 55 | 50 | 45 | 35 | 30 | |
| 750 or More | 60 | 50 | 45 | 40 | 35 | 30 | |

| OPPOSING | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * | | | | | | | |
|-------------|---|-----------|-----------|-----------|-----------|-----------|--|--|
| VOLUME | 350 - 399 | 400 - 449 | 450 - 499 | 500 - 549 | 550 - 599 | = / > 600 | | |
| 100 - 149 | 100 | 80 | 70 | 60 | 55 | 50 | | |
| 150 - 199 | 90 | 75 | 65 | 55 | 50 | 45 | | |
| 200 - 249 | 80 | 72 | 460 | 55 | 50 | 45 | | |
| 250 - 299 | 70 | 65 | 55 | 50 | 45 | 40 | | |
| 300 - 349 | 65 | 60 | 50 | 50 | 45 | 40 | | |
| 350 - 399 | 60 | 55 | 50 | 45 | 40 | 40 | | |
| 400 - 449 | 55 | 50 | 45 | 45 | 40 | 35 | | |
| 450 - 499 | 50 | 45 | 45 | 40 | 35 | 35 | | |
| 500 - 549 | 50 | 45 | 40 | 40 | 35 | 35 | | |
| 550 - 599 | 45 | 40 | 40 | 35 | 35 | 35 | | |
| 600 - 649 | 40 | 35 | 35 | 35 | 35 | 30 | | |
| 650 - 699 | | 35 | 35 | 30 | 30 | 30 | | |
| 700 - 749 | 30 | 30 | 30 | 30 | 30 | 30 | | |
| 750 or More | 30 | 30 | 30 | 30 | 30 | 30 | | |

^{*} Or through volume only if a right-turn lane exists.

TABLE 4B RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | | |
|-------------------------------------|--|------------|------------|------------|------------|---------------|--|--|
| VOLUME | <100 | 100 - 199 | 200 - 249 | 250 - 299 | 300 - 349 | 350 - 399 | | |
| Fewer Than 25 25 - 49 50 - 99 | | | PM Pe | eak | | AM Peak RT | | |
| 100 - 149 150 - 199 | | | 32 RT | | | | | |
| 200 - 249 250 - 299 | | | | | | Yes | | |
| 300 - 349 350 - 399 | | | | Yes | Yes Yes | Yes Yes | | |
| 400 - 449 450 - 499 | | | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 500 - 549 550 - 599 | | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | | |

| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | |
|-------------------------------------|--|------------|------------|------------|------------|--------------|--|
| VOLUME | 350 - 399 | 400 - 449 | 450 - 499 | 500 - 549 | 550 - 600 | + / > 600 | |
| Fewer Than 25 25 - 49 50 - 99 | | | | | Yes | Yes Yes | |
| 100 - 149 150 - 199 | | | Yes | Yes Yes | Yes Yes | Yes Yes | |
| 200 - 249 250 - 299 | Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | |
| 300 - 349 350 - 399 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | |
| 400 - 449 450 - 499 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | |
| 500 - 549 550 - 599 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes . Yes | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | |

^{*} Or through volume only if a left-turn lane exists.

TABLE 4A

LEFT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

(If the left-turn volume exceeds the table value a left -turn lane is needed)

| OPPOSING | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * | | | | | | |
|-------------|---|-----------|-----------|-----------|-----------|-----------|--|
| VOLUME | 100 - 149 | 150 - 199 | 200 - 249 | 250 - 299 | 300 - 349 | 350 - 399 | |
| 100 - 149 | 300 | 235 | 185 | 145 | 120 | 100 | |
| 150 - 199 | 245 | 200 | 160 | 130 | 110 | 90 | |
| 200 - 249 | 205 | 170 | 140 | 115 | 100 | 80 | |
| 250 - 299 | 175 | 150 | 125 | 105 | 90 | 70 | |
| 300 - 349 | 155 | 135 AM | Peak | 95 | i i | 65 | |
| 350 - 399 | 135 | 15 L | T 100 | 85 | | PM Peak | |
| 400 - 449 | 120 | 105 | 90 | 75 | 65 | 80 LT | |
| 450 - 499 | 105 | 90 | 80 | 70 | 60 | 50 | |
| 5(K) - 549 | 95 | 80 | 70 | 65 | 55 | 50 | |
| 550 - 599 | 85 | 70 | 65 | 60 | 50 | 45 | |
| 600 - 649 | 75 | 65 | 60 | 55 | 45 | 40 | |
| 650 - 699 | 70 | 60 | 55 | 50 | 40 | 35 | |
| 700 - 749 | 65 | 55 | 50 | 45 | 35 | 30 | |
| 750 or More | 60 | 50 | 45 | 40 | 35 | 30 | |

| OPPOSING | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * | | | | | | | |
|-------------|---|-----------|-----------|-----------|-----------|-----------|--|--|
| VOLUME | 350 - 399 | 400 - 449 | 450 - 499 | 500 - 549 | 550 - 599 | = / > 600 | | |
| 100 - 149 | 100 | 80 | 70 | 60 | 55 | 50 | | |
| 150 - 199 | 90 | 75 | 65 | 55 | 50 | 45 | | |
| 200 - 249 | 80 | 72 | 460 | 55 | 50 | 45 | | |
| 250 - 299 | 70 | 65 | 55 | 50 | 45 | 40 | | |
| 300 - 349 | 65 | 60 | 50 | 50 | 45 | 40 | | |
| 350 - 399 | 60 | 55 | 50 | 45 | 40 | 40 | | |
| 400 - 449 | 55 | 50 | 45 | 45 | 40 | 35 | | |
| 450 - 499 | 50 | 45 | 45 | 40 | 35 | 35 | | |
| 500 - 549 | 50 | 45 | 40 | 40 | 35 | 35 | | |
| 550 - 599 | 45 | 40 | 40 | 35 | 35 | 35 | | |
| 600 - 649 | 40 | 35 | 35 | 35 | 35 | 30 | | |
| 650 - 699 | | 35 | 35 | 30 | 30 | 30 | | |
| 700 - 749 | 30 | 30 | 30 | 30 | 30 | 30 | | |
| 750 or More | 30 | 30 | 30 | 30 | 30 | 30 | | |

^{*} Or through volume only if a right-turn lane exists.

TABLE 4B RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | | |
|-------------------------------------|--|------------|-----------------|------------|------------|--------------|--|--|
| VOLUME | <100 | 100 - 199 | 200 - 249 | 250 - 299 | 300 - 349 | 350 - 399 | | |
| Fewer Than 25 25 - 49 50 - 99 | | | PM Pea 21 RT | ak | | M Peak LT | | |
| 100 - 149 150 - 199 | | | | | | | | |
| 200 - 249 250 - 299 | | | | | | Yes | | |
| 300 - 349 350 - 399 | | | | Yes | Yes Yes | Yes Yes | | |
| 400 - 449 450 - 499 | | | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 500 - 549 550 - 599 | | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | | |

| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | | |
|-------------------------------------|--|------------|------------|------------|------------|--------------|--|--|
| VOLUME | 350 - 399 | 400 - 449 | 450 - 499 | 500 - 549 | 550 - 600 | + / > 600 | | |
| Fewer Than 25 25 - 49 50 - 99 | | | | | Yes | Yes Yes | | |
| 100 - 149 150 - 199 | | | Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 200 - 249 250 - 299 | Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 300 - 349 350 - 399 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 400 - 449 450 - 499 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | |
| 500 - 549 550 - 599 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes . Yes | | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | | |

^{*} Or through volume only if a left-turn lane exists.

Attachment 10 Sight Distance



Ebenezer Road at Subdivision Roadway – Looking Left (Southbound)



Ebenezer Road at Subdivision Roadway – Looking Right (Northbound)