# The Preserve at Greystone Summit Traffic Impact Study Greystone Summit Blvd Knoxville, TN 

Submitted to

# Knoxville - Knox County Metropolitan Planning Commission 

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FMA Project Number: 223.005


Submitted By:


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### 1.0 Site Description

The proposed site access is a single driveway approximately 680 feet west of the intersection of Greystone Summit Boulevard and Solway Road. The proposed Preserve at Greystone Summit Apartments will consist of approximately 296 apartment units by the year 2015. The location of the site is shown in Figure 1 and the site layout is shown in Figure 2.

During a site visit it was determined that Greystone Summit Boulevard is a two-lane road at the point of the proposed single driveway. The Knoxville Regional Transportation Planning Organization (TPO) classifies Greystone Summit Boulevard as a local street. There is not a posted speed limit on Greystone Summit Boulevard; therefore, a speed limit of 25 mph was used for a local street. The intersection site distance at the proposed single driveway was measured to be approximately 325 feet east and approximately 500 feet west of the intersection. The intersection of Greystone Summit Boulevard and Solway Road is currently a T-intersection controlled by a stop sign on the minor approach. The current intersection geometry shows that Solway Road is a two-way two-lane Major Collector. The current speed limit on Solway Road is 40 mph .

### 2.0 EXISTING Traffic CONDITIONS

FMA conducted an eight-hour turning movement count at the intersection of Greystone Summit Blvd and Solway Road on Tuesday, May 1, 2012. The existing volume including the $A M$ and PM peak hour traffic volumes at the count location is shown in Figure 3 and the count data collected is included in Attachment 1.

The current AM peak hour, and PM peak hour were determined using the eight-hour turning movement count. The AM peak hour occurred between 7:30 am and 8:30 am and the PM peak hour occurred between 5:00 pm and 6:00 pm.

### 3.0 Background Growth

The Tennessee Department of Transportation (TDOT) maintains count Station \#000084 on Hardin Valley Road East of Pellissippi Parkway and South of the intersection of Greystone Summit Boulevard and Solway Road. The annual traffic growth rate for Station \#000084

FIGURE 1


LOCATION MAP
THE PRESERVE AT GREYSTONE SUMMIT

KNOX COUNTY, TN

| DRAWN BY | $A L K$ | DATE | 5/21/12 |
| :---: | :---: | :---: | :---: |
| FULGHUM | 10330 HARDIN VALLEY ROAD <br> KNOXVILLE, TN. 37932 <br> OFFICE: (865) 690-6419 <br> FAX: (865) 690-6448 |  |  |

## FIGURE 2



## SITE PLAN

THE PRESERVE AT GREYSTONE SUMMIT

KNOX COUNTY, TN

| DRAWN BY | ALK | DATE | 5/21/12 |
| :---: | :---: | :---: | :---: |
|  | 10330 HARDIN VALLEY ROAD KNOXVILLE, TN. 37932 OFFICE: (865) 690-6419 FAX: (865) 690-6448 |  |  |

FIGURE 3


## LEGEND:

$\longleftarrow 5$ (16)
TURNING MOVEMENT VOLUME AM (PM)

| YEAR 2012 PEAK HOUR TRAFFIC |  |  |  |
| :---: | :---: | :---: | :---: |
| THE PRESERVE AT GREYSTONE SUMMIT |  |  |  |
| KNOX COUNTY, TN |  |  |  |
| DRAWN BY | ALK | DATE | 5/21/12 |
|  | 10330 HARDIN VALLEY ROAD KNOXVILLE, TN. 37932 OFFICE: (865) 690-6419 FAX: (865) 690-6448 |  |  |

between 2001 and 2010 is approximately $5.5 \%$ and is referenced in Attachment 2. There was a greater than $30 \%$ increase between 2010 and 2011 so that point on the graph was not used to determine the average growth rate. For the purpose of this study, an annual growth rate of $5.5 \%$ was assumed until full occupancy is reached in 2015 . Figure 4 demonstrates the projected peak hour volumes at the intersection of Greystone Summit Boulevard and Solway Road after applying this background growth rate to the existing conditions.

### 4.0 Trip Generation and Trip Distribution

Table 3-1 shows the weekday, AM peak hour and PM peak hour trips that the proposed Preserve at Greystone Summit apartments is expected to generate at the point of full occupancy. The Trip Generation, $7^{\text {th }}$ Edition, published by the Institute of Transportation Engineers, was used to estimate volumes based on locally gathered trip generation data. The Knoxville-Knox County Metropolitan Planning Commission published a memorandum ("Local Trip Generation Rates for Multi-Family Residential Uses", August 14, 2000, contained in Attachment 3) for the purpose of providing locally collected data for all multifamily residential developments.

The directional distribution of the traffic generated by the proposed Preserve at Greystone Summit was determined using the traffic data collected for the current conditions. The typical weekday traffic pattern is for traffic to flow heavier in one direction in the morning peak period and then for the traffic to be heavier in the opposite direction during the evening peak period. For Solway Road, the current directional distribution during the AM peak hour is $39 \%$ northbound and $61 \%$ southbound. The directional distribution in the PM peak hour is $53 \%$ northbound and $47 \%$ southbound. Using these percentages the trips generated from The Preserve at Greystone Summit are shown in Figure 5. Figure 6 shows the combined peak hour traffic from the future growth and the proposed development.

FIGURE 4


## LEGEND:

$\longleftarrow 5$ (16)
TURNING MOVEMENT VOLUME AM (PM)

| YEAR 2015 PEAK HOUR TRAFFICWITHOUT DEVELOPMENT WITHOUT DEVELOPMENT |  |  |  |
| :---: | :---: | :---: | :---: |
| THE PRESERVE AT GREYSTONE SUMMIT |  |  |  |
| KNOX COUNTY, TN |  |  |  |
| DRAWN BY | ALK | date | 5/21/12 |
|  | 10330 HARDIN VALLEY ROAD KNOXVILLE, TN. 37932 OFFICE: (865) 690-6419 FAX: (865) 690-6448 |  |  |

## FIGURE 5



LEGEND:
$\longleftarrow 5$ (16)
TURNING MOVEMENT VOLUME AM (PM)
DIRECTIONAL DISTRIBUTION:
SOLWAY ROAD
AM PEAK $39 \%$ NORTHBOUND $\longrightarrow$ $61 \%$ SOUTHBOUND «

PM PEAK
53\% NORTHBOUND $\longrightarrow$
47\% SOUTHBOUND «

| YEAR 2015 PEAK HOUR SITE DEVELOPMENT TRAFFIC |  |  |  |
| :---: | :---: | :---: | :---: |
| THE PRESERVE AT GREYSTONE SUMMIT |  |  |  |
| KNOX COUNTY, TN |  |  |  |
| DRAWN BY | ALK | DATE | 5/21/12 |
| FULGHUM | 10330 HARDIN VALLEY ROAD <br> KNOXVILLE, TN. 37932 <br> OFFICE: (865) 690-6419 <br> FAX: (865) 690-6448 |  |  |

## FIGURE 6



## LEGEND:

$\longleftarrow 5$ (16)
TURNING MOVEMENT VOLUME AM (PM)

| YEAR 2015 PEAK HOUR TRAFFICWITH DEVELOPMENT |  |  |  |
| :---: | :---: | :---: | :---: |
| THE PRESERVE AT GREYSTONE SUMMIT |  |  |  |
| KNOX COUNTY, TN |  |  |  |
| DRAWN BY | ALK | date | 5/31/12 |
|  | 10330 HARDIN VALLEY ROAD KNOXVILLE, TN. 37932 OFFICE: (865) 690-6419 FAX: (865) 690-6448 |  |  |

Table 3-1
Trip Generation Summary
Rates for Local Apartment Trip Generation Study

|  | Total New <br> Trips | \% Entering | \%Exiting | Number <br> Entering | Number <br> Exiting |
| :--- | :---: | :---: | :---: | :---: | ---: |
| Weekday | 2531 | 50 | 50 | 1266 | 1266 |
| A.M. Peak | 146 | 22 | 78 | 32 | 114 |
| P.M. Peak | 208 | 55 | 45 | 114 | 94 |

### 5.0 TRAFFIC CONDITIONS

Unsignalized intersection capacity analyses were performed for the AM and PM peak hours to evaluate the traffic conditions at the intersection of Greystone Summit Boulevard and Solway Road as well as the intersection of Greystone Summit Boulevard and the proposed single driveway. The capacity analyses were determined from the Highway Capacity Software (HCS 2000) which is based on the 2000 Highway Capacity Manual. The results from the analyses are measured with a term "level of service" (LOS), which is based on the amount of delay experienced at the intersection. The LOS index ranges from LOS A, indicating excellent traffic conditions with minimal delay, to LOS F indicating very congested conditions with excessive delay. LOS D generally is considered the minimum acceptable condition in urban areas. Table 4-1 shows the results of the capacity analyses on both approaches of the intersection and the project entrance driveway.

Table 4-1
Level of Service (LOS) Summary

|  | Current Traffic | Future Traffic | Proposed <br> Traffic |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | AM | PM | AM | PM | AM | PM |  |
| Solway Road \& Greystone Summit Blvd | A | A | A | A | A | A |  |
|  <br> Proposed Driveway | - | - | - |  | - | A | A |

### 6.0 Turn Lane Warrant Analysis

The intersection of Greystone Summit Boulevard and the proposed single driveway was evaluated to determine if a left turn lane into the site or a right turn lane out of the site was warranted. The intersection of Solway Road and Greystone Summit Boulevard was also evaluated to determine if a right turn lane or left turn lane was warranted from the major approach. The Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy," was used to analyze the information. Attachment 8 shows a more detailed evaluation of the turn lane warrants.

Based on these evaluations a right turn lane out of and a left turn lane into The Preserve at Greystone Summit is not warranted for the proposed future traffic. On Solway Road neither a right turn lane from nor left turn lane onto Greystone Summit Blvd, will be warranted with the proposed future development.

### 7.0 CONCLUSIONS and ReCOMmENDAtions

## A. Sight Distance

The minimum required sight distance for a road with a posted speed limit of 25 mph is 275 feet in each direction in accordance with the "Minimum Subdivision Regulations" for Knoxville and Knox County. With a sight distance of approximately 325 ft east and approximately 500 ft west of the intersection, this requirement is met. FMA recommends any necessary landscaping and/or grading that may be involved to maintain this sight distance and continue to comply with Knox County Engineering \& Public Works.
B. Intersection Spacing

Greystone Summit Boulevard is classified as a local street. The minimum intersection spacing required for a local street is approximately 125 feet per the "Minimum Subdivision Regulations" for Knoxville and Knox County. The nearest road intersection to the project entrance is currently 680 feet west at the intersection of Greystone Summit Boulevard and Solway Road.

This intersection exceeds the typical minimum separation of 125 feet between roads on a local street; therefore, no change is necessary.
C. Turn lanes (Proposed Site Driveway and Greystone Summit Boulevard)

A southbound right turn lane and a northbound left turn lane are not warranted at the intersection of Solway Road and Greystone Summit Blvd. An eastbound right turn lane and a westbound left turn lane are not warranted at the intersection of Greystone Summit Blvd and the proposed project entrance.

Attachment 1
Traffic Counts

Project: The Preserve at Greystone Summit
Date Conducted: 5/1/2012

|  | Solway Road Northbound |  |  | Solway Road Southbound |  |  | Greystone Summit Blvd Eastbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | Thru | Left | Total | Right | Thru | Total | Right | Left | Total | Int. Total |
| 7:00 AM | 8 | 2 | 10 | 0 | 39 | 39 | 15 | 2 | 17 | 66 |
| 7:15 AM | 10 | 0 | 10 | 0 | 28 | 28 | 22 | 4 | 26 | 64 |
| 7:30 AM | 17 | 2 | 19 | 0 | 45 | 45 | 22 | 1 | 23 | 87 |
| 7:45 AM | 18 | 9 | 27 | 0 | 32 | 32 | 18 | 2 | 20 | 79 |
| Total | 53 | 13 | 66 | 0 | 144 | 144 | 77 | 9 | 86 | 296 |
| 8:00 AM | 13 | 5 | 18 | 2 | 32 | 34 | 13 | 1 | 14 | 66 |
| 8:15 AM | 21 | 4 | 25 | 0 | 27 | 27 | 12 | 1 | 13 | 65 |
| 8:30 AM | 9 | 2 | 11 | 0 | 15 | 15 | 11 | 1 | 12 | 38 |
| 8:45 AM | 6 | 2 | 8 | 0 | 17 | 17 | 10 | 0 | 10 | 35 |
| Total | 49 | 13 | 62 | 2 | 91 | 93 | 46 | 3 | 49 | 204 |
| 11:00 AM | 15 | 2 | 17 | 0 | 15 | 15 | 3 | 1 | 4 | 36 |
| 11:15 AM | 15 | 3 | 18 | 0 | 16 | 16 | 4 | 2 | 6 | 40 |
| 11:30 AM | 11 | 3 | 14 | 1 | 19 | 20 | 11 | 0 | 11 | 45 |
| 11:45 AM | 17 | 1 | 18 | 0 | 12 | 12 | 4 | 0 | 4 | 34 |
| Total | 58 | 9 | 67 | 1 | 62 | 63 | 22 | 3 | 25 | 155 |
| 12:00 PM | 21 | 8 | 29 | 3 | 20 | 23 | 5 | 2 | 7 | 59 |
| 12:15 PM | 11 | 9 | 20 | 1 | 18 | 19 | 6 | 1 | 7 | 46 |
| 12:30 PM | 18 | 4 | 22 | 2 | 23 | 25 | 9 | 0 | 9 | 56 |
| 12:45 PM | 15 | 10 | 25 | 1 | 13 | 14 | 4 | 0 | 4 | 43 |
| Total | 65 | 31 | 96 | 7 | 74 | 81 | 24 | 3 | 27 | 204 |
| 2:00 PM | 14 | 6 | 20 | 0 | 13 | 13 | 3 | 0 | 3 | 36 |
| 2:15 PM | 14 | 8 | 22 | 1 | 16 | 17 | 3 | 0 | 3 | 42 |
| 2:30 PM | 16 | 6 | 22 | 1 | 18 | 19 | 6 | 1 | 7 | 48 |
| 2:45 PM | 18 | 6 | 24 | 1 | 15 | 16 | 7 | 1 | 8 | 48 |
| Total | 62 | 26 | 88 | 3 | 62 | 65 | 19 | 2 | 21 | 174 |
| 3:00 PM | 14 | 5 | 19 | 0 | 13 | 13 | 5 | 0 | 5 | 37 |
| 3:15 PM | 23 | 4 | 27 | 1 | 25 | 26 | 7 | 0 | 7 | 60 |
| 3:30 PM | 27 | 7 | 34 | 1 | 13 | 14 | 5 | 0 | 5 | 53 |
| 3:45 PM | 28 | 11 | 39 | 2 | 27 | 29 | 5 | 0 | 5 | 73 |
| Total | 92 | 27 | 119 | 4 | 78 | 82 | 22 | 0 | 22 | 223 |
| 4:00 PM | 25 | 18 | 43 | 1 | 19 | 20 | 7 | 0 | 7 | 70 |
| 4:15 PM | 27 | 18 | 45 | 3 | 22 | 25 | 7 | 0 | 7 | 77 |
| 4:30 PM | 31 | 12 | 43 | 4 | 33 | 37 | 10 | 0 | 10 | 90 |
| 4:45 PM | 36 | 9 | 45 | 2 | 31 | 33 | 4 | 0 | 4 | 82 |
| Total | 119 | 57 | 176 | 10 | 105 | 115 | 28 | 0 | 28 | 319 |
| 5:00 PM | 26 | 7 | 33 | 2 | 37 | 39 | 13 | 1 | 14 | 86 |
| 5:15 PM | 34 | 18 | 52 | 5 | 39 | 44 | 9 | 1 | 10 | 106 |
| 5:30 PM | 35 | 14 | 49 | 3 | 25 | 28 | 14 | 0 | 14 | 91 |
| 5:45 PM | 28 | 11 | 39 | 5 | 36 | 41 | 17 | 0 | 17 | 97 |
| Total | 123 | 50 | 173 | 15 | 137 | 152 | 53 | 2 | 55 | 380 |
| Grand Total | 621 | 226 | 847 | 42 | 753 | 795 | 291 | 22 | 313 | 1955 |
| Approach \% | 73.3 | 26.7 |  | 5.3 | 94.7 |  | 93.0 | 7.0 |  |  |
| Total \% | 31.8 | 11.6 | 43.3 | 2.1 | 38.5 | 40.7 | 14.9 | 1.1 | 16.0 |  |

Project: The Preserve at Greystone Summit
Date Conducted: 5/1/2012

| AM Peak Hour | $7: 30-8: 30$ | 297 |
| :--- | :---: | :---: |
| Lunch Peak Hour | $12: 00-1: 00$ | 204 |
| PM Peak Hour | $5: 00-6: 00$ | 380 |


|  | Solway Road Northbound |  |  | Solway Road Southbound |  |  | Greystone Summit Blvd Eastbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | Thru | Left | App. Total | Right | Thru | App. Total | Right | Left | App. Total | Int. Total |
| Peak Hour Analysis from 7:00 AM to 9:00 AM |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hour begins at 7:45 AM |  |  |  |  |  |  |  |  |  |  |
| 7:30 AM | 17 | 2 | 19 | 0 | 45 | 45 | 22 | 1 | 23 | 87 |
| 7:45 AM | 18 | 9 | 27 | 0 | 32 | 32 | 18 | 2 | 20 | 79 |
| 8:00 AM | 13 | 5 | 18 | 2 | 32 | 34 | 13 | 1 | 14 | 66 |
| 8:15 AM | 21 | 4 | 25 | 0 | 27 | 27 | 12 | 1 | 13 | 65 |
| Total Volume | 69 | 20 | 89 | 2 | 136 | 138 | 65 | 5 | 70 | 297 |
| Future (5.5\% over 3 yrs ) | 81 | 23 |  | 2 | 160 |  | 76 | 6 |  | 349 |
| PHF | 0.82 | 0.56 |  | 0.25 | 0.76 |  | 0.74 | 0.63 |  | 0.85 |
| Peak Hour Analysis from 11:00 AM to 1:00 PM |  |  |  |  |  |  |  |  |  |  |
| Lunch Peak Hour begins at 11:45 AM |  |  |  |  |  |  |  |  |  |  |
| 12:00 PM | 21 | 8 | 29 | 3 | 20 | 23 | 5 | 2 | 7 | 59 |
| 12:15 PM | 11 |  | 20 | 1 | 18 | 19 | 6 | 1 | 7 | 46 |
| 12:30 PM | 18 | 4 | 22 | 2 | 23 | 25 | 9 | 0 | 9 | 56 |
| 12:45 PM | 15 | 10 | 25 | 1 | 13 | 14 | 4 | 0 | 4 | 43 |
| Total Volume | 65 | 31 | 96 | 7 | 74 | 81 | 24 | 3 | 27 | 204 |
| Future (5.5\% over 3 yrs ) | 76 | 36 |  | 8 | 87 |  | 28 | 4 |  | 240 |
| PHF | 0.77 | 0.78 |  | 0.58 | 0.80 |  | 0.67 | 0.38 |  | 0.86 |
| Peak Hour Analysis from 2:00 PM to 6:00 PM |  |  |  |  |  |  |  |  |  |  |
| PM Peak Hour begins at 4:15 PM |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM | 26 | 7 | 33 | 2 | 37 | 39 | 13 | 1 | 14 | 86 |
| 5:15 PM | 34 | 18 | 52 | 5 | 39 | 44 | 9 | 1 | 10 | 106 |
| 5:30 PM | 35 | 14 | 49 | 3 | 25 | 28 | 14 | 0 | 14 | 91 |
| 5:45 PM | 28 | 11 | 39 | 5 | 36 | 41 | 17 | 0 | 17 | 97 |
| Total Volume | 123 | 50 | 173 | 15 | 137 | 152 | 53 | 2 | 55 | 380 |
| Future (5.5\% over 3 yrs ) | 144 | 59 |  | 18 | 161 |  | 62 | 2 |  | 446 |
| PHF | 0.88 | 0.69 |  | 0.75 | 0.88 |  | 0.78 | 0.50 |  | 0.90 |

Attachment 2
ADT Trends


Attachment 3
Local Apartment Trip Generation Study

## MEMORANDUM

To: $\quad$ Traffic Impact Study Reviewers and Preparers (see attached list)
From: Mike Conger $10{ }^{\circ}$
Date: August 14, 2000
Subject: Local Trip Generation Rates for Multi-Family Residential Uses

Attached please find a summary of the final report with data plots for the Knox County Local Apartment Trip Generation Study. As you will recall, this report was discussed when the traffic impact study group last convened this past February. A consensus was reached at that meeting that the trip generation rates developed in the local study should be used for new apartment complexes and any other "multi-family" residential uses that are being proposed.

The MPC voted at its July 2000 meeting to officially amend the Traffic Impact Study Guidelines with language which reads that "trip generation rates for proposed uses shall be calculated using the latest edition of the ITE Trip Generation Manual, or using local data when it is available". This amendment allows the full implementation of the new rates, and they should be used for future proposed multi-family developments unless it can be demonstrated otherwise.

Thanks for your assistance and cooperation in this matter, if there are any questions or comments, please let me know.

## TRAFFIC IMPACT STUDY REVIEWER \& PREPARER GROUP

| Name | Organization | Phone Number |
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| Daniel Armstrong | Wilbur Smith | $584-8584$ |
| Rusty Baksa | Land Dev. Solutions | $671-2281$ |
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| Alan Childers | Cannon \& Cannon | $988-4818$ |
| Steve Drummer | Barge Waggoner | $637-2810$ |
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| Barbara Hatcher | SITE, inc. | $693-5010$ |
| John Heid | AR/TEC | $681-8848$ |
| Bill Kervin | Allen Hoshall | $694-1834$ |
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| Jim Snowden | Knox County | $215-5800$ |
| Darcy Sullivan | SITE, inc. | $693-5010$ |
| Jeff Welch | MPC | $215-2500$ |

## KNOX COUNTY <br> LOCAL APARTMENT TRIP GENERATION STUDY

## PURPOSE

A Traffic Impact Study (TIS) is currently required in Knox County when a proposed development is projected to generate in excess of 750 trips per day. The determinations of when the threshold is met as well as all subsequent analyses in the TIS are performed using the rates and equations given in the Institute of Transportation Engineers (ITE) Trip Generation Manual. Local governmental agencies rely heavily on the accuracy of these trip generation rates in order to correctly predict the impacts of a proposed development on the transportation system. Therefore, in certain instances, it is logical to verify whether the "national" rates and equations given in the ITE Trip Generation Manual are appropriate for use in a specific local area or region.

The decision was made to study the local trip-making characteristics of apartments because of the discrepancy between the trip generation rates for apartments and single family residential land uses as given in the ITE Trip Generation Manual. While these two land uses are similar in nature, the Trip Generation Manual predicts about three less trips per dwelling unit generated by apartments for the average weekday. Additionally the Trip Generation Manual points out that due to the age of their database, which dates back to the 1960 's, "the rates for apartments probably had changed over time". It is also assumed that some of the ITE data had come from larger metropolitan areas with denser development and greater transit use than Knox County, which would contribute to lower trip generation rates. Therefore, this study will be used to either verify the rates given in the Trip Generation Manual or generate new ones that can be applied to locally proposed apartment developments.

## PROCEDURE

The procedures recommended by ITE in conducting local trip generation studies were generally followed for this study, along with some important assumptions that have made. ITE has published a proposed recommended practice entitled "Trip Generation Handbook" which specifically outlines procedures for conducting local trip generation studies and establishing new rates and equations.

The first step in the study was to define the number and location of the sites to be studied, as well as the counting methodology. Initially 14 sites were selected, although one apartment complex - the College Park Apartments - was later omitted due to uncharacteristically high traffic generation numbers. The number of sites used in this study far exceeds the recommended minimum amount suggested by ITE, which is five sites. Traffic counts were taken for week-long periods at 15 -minute intervals between July 22, 1996 and August 9, 1996 at the access points to the apartment complexes. A Technical Appendix to this report contains the traffic count data collected at each apartment complex.

## RESULTS

The traffic count data was analyzed using spreadsheets in order to determine the weighted average rates and regression equations. In order to be considered valid, the local rates and equations for each time period of analysis that were generated must meet certain statistical criteria. First, the standard deviation of the independent variable (dwelling units) should be no more than 110 percent of the weighted average rate; and secondly, the regression equations require a computed coefficient of determination ( $\mathrm{R}^{2}$ ) value of at least 0.75 before good data fit is indicated. This statistical criteria is met by the local data results, and in fact it often exceeds the level of data fit given by their counterparts in the ITE Trip Generation Manual. Finally, in order to simplify the use of the local data, plots were generated that appear identical to the actual ones in the ITE Trip Generation Manual.

The resulting rates and equations calculated from the local data indicate that the average weekday trip generation of apartments in this area is well above the national rates reported in the ITE manual. For example, the locally computed average rate for number of trips generated during a weekday is $35 \%$ higher than the rate given by ITE (increase from 6.63 trips per dwelling unit to 9.03 trips per dwelling unit). The trip generation rates do not increase as much for the AM and PM peak hours however. The local rate is roughly $8 \%$ higher for the AM peak, and $16 \%$ higher for the PM peak. The plots from the ITE Trip Generation Manual are included in the Technical Appendix for comparison purposes.

## ASSUMPTIONS MADE

Some important assumptions have been made which may affect the results of the local data that was collected:
$>$ It is important to note that the local trip generation rates were computed for the total number of dwelling units in the apartment complex, and not necessarily for the number of occupied dwelling units. There are several reasons why this was done, chiefly because of the need for comparability with the rates given in ITE Trip Generation Manual, as it does not specify whether the dwelling units are occupied. According to ITE procedures the selected sites must only be of "reasonably full occupancy (i.e. at least 85\%)". The Apartment Association of Greater Knoxville (AAGK) publishes quarterly reports on occupancy levels of apartment complexes, and the report covering the period of the data collection was reviewed to determine occupancy levels. According to the AAGK report from July 1, 1996 - September 30, 1996 all of the apartment complexes surveyed in this study met the minimum $85 \%$ occupancy level, with an average occupancy rate for all sites studied of $94 \%$.
$>$ The count data that was collected at each apartment complex was used "raw" meaning that it was not factored for possible daily or seasonal variations. Once again, according to an ITE representative it is not known whether the data used in the Trip Generation Manual was factored or not, so therefore in order to be able to compare
local rates to those in the manual you must assume that count data should not be factored. Additionally, it was felt that apartment complexes would generally not be as susceptible to major seasonal fluctuations as other land uses might be. The local rates were also developed using count data that was collected and averaged over an entire week, which should limit some of the daily variations. Finally, reliable local daily and seasonal variation factors do not truly exist.

## CONCLUSION

The local apartment study methodology and results were distributed for comment to a group of local transportation professionals who are directly responsible for either preparing or reviewing traffic impact studies. A meeting was held between this group on February 16, 2000 in order to gather comments and discuss the study in greater detail. The following conclusions are based on the discussion and consensus reached at this meeting:

1. The trip generation rates and equations meet statistical requirements and resulted from a study that followed accepted procedures; therefore they should be adopted for future use. Furthermore, the rates and equations are recommended for use in reviewing the traffic impact of any development termed as "multi-family", such as townhouse and condominium developments due to their similarity to apartment complexes.
2. The Traffic Access and Impact Study Guidelines and Procedures adopted by MPC should be amended with the language that local data should be used when available, which will allow the implementation of these new multi-family trip generation rates.
3. The following suggestions were made for future consideration:

- This study should be updated with data collected from local townhouse and condominium developments in order to further justify the use of the new trip generation rates.
- A statistical comparison should be made between any newly developed rates and the ITE single family trip generation rates to determine if there is a significant difference. If there is no difference then perhaps ITE single-family rates could be used for any residential development proposed in Knox County.


# Local Apartment Trip Generation Study 

Average Vehicle Trip Ends vs: Dwelling Units On a: Weekday

Number of Studies: 13<br>Average Number of Dwelling Units: 193<br>Directional Distribution: $50 \%$ entering, $50 \%$ exiting

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 9.03 | $6.59-17.41$ | 2.47 |

Data Plot and Equation


# Local Apartment Trip Generation Study 

Average Vehlcle Trip Ends vs: Dwelling Units<br>On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.<br>Number of Studies: 13<br>Average Number of Dwelling Units: 193<br>Directional Distribution: $22 \%$ entering, $78 \%$ exiting

Trip Generation Per Dwelling Unlt

| Average Rate | Ranges of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.55 | $0.14-0.78$ | 0.18 |

Data Plot and Equation


# Local Apartment Trip Generation Study 

| Average Vehicle Trip Ends vs: |  |
| ---: | :--- |
| On a: | Dwelling Units <br> Weekday, <br> Peak Hour of Adjacent Street Traffic, <br> One Hour Between 4 and 6 p.m. |
|  |  |
| Number of Studies: | 13 |
| Average Number of Dwelling Units: | 193 |
| Directional Distribution: | $55 \%$ entering, $45 \%$ exiting |

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.72 | $0.32-1.66$ | 0.25 |

Data Plot and Equation


Attachment 4
Unsignalized Intersection Worksheet Current AM/PM Peaks

| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | ALK | Intersection | Solway/Greystone Summit |
| Agency/Co. | Fulghum, MacIndoe \& Assoc. | Jurisdiction | Knox County |
| Date Performed | 5/9/2012 | Analysis Year | 2012 |
| Analysis Time Period | AM Peak |  |  |
| Project Description 223.005-Current Traffic |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: Solway Road |  |
| Intersection Orientation: North-South |  | Study Period (hrs) |  |

Vehicle Volumes and Adjustments

| Major Street | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 20 | 69 |  |  | 136 | 2 |
| Peak-Hour Factor, PHF | 0.56 | 0.82 | 1.00 | 1.00 | 0.76 | 0.25 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 35 | 84 | 0 | 0 | 178 | 8 |
| Percent Heavy Vehicles | 1 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration | LT |  |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Eastbound |  |  | Westbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 5 |  | 65 |  |  |  |
| Peak-Hour Factor, PHF | 0.63 | 1.00 | 0.74 | 1.00 | 1.00 | 1.00 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 7 | 0 | 87 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 1 | 0 | 1 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |

Delay, Queue Length, and Level of Service

| Approach | Northbound | Southbound | Westbound |  |  | Eastbound |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | $L T$ |  |  |  |  |  | $L R$ |  |
| V (veh/h) | 35 |  |  |  |  |  | 94 |  |
| C (m) (veh/h) | 1395 |  |  |  |  |  | 842 |  |
| V/c | 0.03 |  |  |  |  |  | 0.11 |  |
| $95 \%$ queue length | 0.08 |  |  |  |  |  | 0.38 |  |
| Control Delay (s/veh) | 7.6 |  |  |  |  |  | 9.8 |  |
| LOS | A |  |  |  |  |  | A |  |
| Approach Delay (s/veh) | -- | -- | 9.8 |  |  |  |  |  |
| Approach LOS | -- | -- | $A$ |  |  |  |  |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | ALK | Intersection | Solway/Greystone Summit |
| Agency/Co. | Fulghum, MacIndoe \& Assoc. | Jurisdiction | Knox County |
| Date Performed | 5/9/2012 | Analysis Year | 2012 |
| Analysis Time Period | PM Peak |  |  |
| Project Description 223.005 - Current Traffic |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: Solway Road |  |
| Intersection Orientation: North-South |  | Study Period (hrs) |  |

Vehicle Volumes and Adjustments

| Major Street | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 50 | 123 |  |  | 137 | 15 |
| Peak-Hour Factor, PHF | 0.69 | 0.88 | 1.00 | 1.00 | 0.88 | 0.75 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 72 | 139 | 0 | 0 | 155 | 20 |
| Percent Heavy Vehicles | 1 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration | LT |  |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Eastbound |  |  | Westbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 2 |  | 53 |  |  |  |
| Peak-Hour Factor, PHF | 0.50 | 1.00 | 0.78 | 1.00 | 1.00 | 1.00 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 4 | 0 | 67 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 1 | 0 | 1 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |

Delay, Queue Length, and Level of Service

| Approach | Northbound | Southbound | Westbound |  |  | Eastbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | LT |  |  |  |  |  | LR |  |
| v (veh/h) | 72 |  |  |  |  |  | 71 |  |
| C (m) (veh/h) | 1407 |  |  |  |  |  | 852 |  |
| v/c | 0.05 |  |  |  |  |  | 0.08 |  |
| 95\% queue length | 0.16 |  |  |  |  |  | 0.27 |  |
| Control Delay (s/veh) | 7.7 |  |  |  |  |  | 9.6 |  |
| LOS | A |  |  |  |  |  | A |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 9.6 |  |
| Approach LOS | -- | -- |  |  |  |  | A |  |

Attachment 5
Unsignalized Intersection Worksheet Future AM/PM Peaks

| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | ALK | Intersection | Solway/Greystone Summit |
| Agency/Co. | Fulghum, MacIndoe \& Assoc. | Jurisdiction | Knox County |
| Date Performed | 5/9/2012 | Analysis Year | 2015 |
| Analysis Time Period | AM Peak |  |  |
| Project Description 223.005 - Future Traffic w/o Development |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: Solway Road |  |
| Intersection Orientation: North-South |  | Study Period (hrs) |  |

Vehicle Volumes and Adjustments

| Major Street | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 23 | 81 |  |  | 160 | 2 |
| Peak-Hour Factor, PHF | 0.56 | 0.82 | 1.00 | 1.00 | 0.76 | 0.25 |
| Hourly Flow Rate, HFR (veh/h) | 41 | 98 | 0 | 0 | 210 | 8 |
| Percent Heavy Vehicles | 1 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration | LT |  |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Eastbound |  |  | Westbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 6 |  | 76 |  |  |  |
| Peak-Hour Factor, PHF | 0.63 | 1.00 | 0.74 | 1.00 | 1.00 | 1.00 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 9 | 0 | 102 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 1 | 0 | 1 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |

Delay, Queue Length, and Level of Service

| Approach | Northbound | Southbound | Westbound |  |  | Eastbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | LT |  |  |  |  |  | LR |  |
| v (veh/h) | 41 |  |  |  |  |  | 111 |  |
| C (m) (veh/h) | 1358 |  |  |  |  |  | 803 |  |
| v/c | 0.03 |  |  |  |  |  | 0.14 |  |
| 95\% queue length | 0.09 |  |  |  |  |  | 0.48 |  |
| Control Delay (s/veh) | 7.7 |  |  |  |  |  | 10.2 |  |
| LOS | A |  |  |  |  |  | B |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 10.2 |  |
| Approach LOS | -- | -- |  |  |  |  | B |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | ALK | Intersection | Solway/Greystone Summit |
| Agency/Co. | Fulghum, MacIndoe \& Assoc. | Jurisdiction | Knox County |
| Date Performed | 5/9/2012 | Analysis Year | 2015 |
| Analysis Time Period | PM Peak |  |  |
| Project Description 223.005 - Future Traffic w/o Development |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: Solway Road |  |
| Intersection Orientation: North-South |  | Study Period (hrs) |  |

Vehicle Volumes and Adjustments

| Major Street | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 59 | 144 |  |  | 161 | 18 |
| Peak-Hour Factor, PHF | 0.69 | 0.88 | 1.00 | 1.00 | 0.88 | 0.75 |
| Hourly Flow Rate, HFR (veh/h) | 85 | 163 | 0 | 0 | 182 | 24 |
| Percent Heavy Vehicles | 1 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration | LT |  |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Eastbound |  |  | Westbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 2 |  | 62 |  |  |  |
| Peak-Hour Factor, PHF | 0.50 | 1.00 | 0.78 | 1.00 | 1.00 | 1.00 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 4 | 0 | 79 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 1 | 0 | 1 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |

Delay, Queue Length, and Level of Service

| Approach | Northbound | Southbound | Westbound |  |  | Eastbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | LT |  |  |  |  |  | LR |  |
| v (veh/h) | 85 |  |  |  |  |  | 83 |  |
| C (m) (veh/h) | 1371 |  |  |  |  |  | 820 |  |
| v/c | 0.06 |  |  |  |  |  | 0.10 |  |
| 95\% queue length | 0.20 |  |  |  |  |  | 0.34 |  |
| Control Delay (s/veh) | 7.8 |  |  |  |  |  | 9.9 |  |
| LOS | A |  |  |  |  |  | A |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 9.9 |  |
| Approach LOS | -- | -- |  |  |  |  | A |  |

Attachment 6
Unsignalized Intersection Worksheet
Future AM/PM Peaks + Development

| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | ALK | Intersection | Solway/Greystone Summit |
| Agency/Co. | Fulghum, MacIndoe \& Assoc. | Jurisdiction | Knox County |
| Date Performed | 5/31/2012 | Analysis Year | 2015 |
| Analysis Time Period | AM Peak |  |  |
| Project Description 223.005 - Future Traffic with Development |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: Solway Road |  |
| Intersection Orientation: North-South |  | Study Period (hrs) |  |

Vehicle Volumes and Adjustments

| Major Street | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 35 | 81 |  |  | 160 | 22 |
| Peak-Hour Factor, PHF | 0.85 | 0.85 | 1.00 | 1.00 | 0.85 | 0.85 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 41 | 95 | 0 | 0 | 188 | 25 |
| Percent Heavy Vehicles | 1 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration | LT |  |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Eastbound |  |  | Westbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 12 |  | 184 |  |  |  |
| Peak-Hour Factor, PHF | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 14 | 0 | 216 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 1 | 0 | 1 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |

Delay, Queue Length, and Level of Service

| Approach | Northbound | Southbound | Westbound |  |  | Eastbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | LT |  |  |  |  |  | LR |  |
| v (veh/h) | 41 |  |  |  |  |  | 230 |  |
| C (m) (veh/h) | 1363 |  |  |  |  |  | 824 |  |
| v/c | 0.03 |  |  |  |  |  | 0.28 |  |
| 95\% queue length | 0.09 |  |  |  |  |  | 1.14 |  |
| Control Delay (s/veh) | 7.7 |  |  |  |  |  | 11.1 |  |
| LOS | A |  |  |  |  |  | B |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 11.1 |  |
| Approach LOS | -- | -- |  |  |  |  | B |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst | ALK | Intersection | Solway/Greystone Summit |
| Agency/Co. | Fulghum, MacIndoe \& Assoc. | Jurisdiction | Knox County |
| Date Performed | 5/9/2012 | Analysis Year | 2015 |
| Analysis Time Period | PM Peak |  |  |
| Project Description 223.005 - Future Traffic with Development |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: Solway Road |  |
| Intersection Orientation: North-South |  | Study Period (hrs) |  |

Vehicle Volumes and Adjustments

| Major Street | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 119 | 144 |  |  | 161 | 72 |
| Peak-Hour Factor, PHF | 0.90 | 0.90 | 1.00 | 1.00 | 0.90 | 0.90 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 132 | 160 | 0 | 0 | 178 | 80 |
| Percent Heavy Vehicles | 1 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration | LT |  |  |  |  | TR |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Eastbound |  |  | Westbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 7 |  | 151 |  |  |  |
| Peak-Hour Factor, PHF | 0.90 | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 7 | 0 | 167 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 1 | 0 | 1 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |

Delay, Queue Length, and Level of Service

| Approach | Northbound | Southbound | Westbound |  |  | Eastbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration | LT |  |  |  |  |  | LR |  |
| v (veh/h) | 132 |  |  |  |  |  | 174 |  |
| C (m) (veh/h) | 1313 |  |  |  |  |  | 790 |  |
| v/c | 0.10 |  |  |  |  |  | 0.22 |  |
| 95\% queue length | 0.33 |  |  |  |  |  | 0.84 |  |
| Control Delay (s/veh) | 8.0 |  |  |  |  |  | 10.8 |  |
| LOS | A |  |  |  |  |  | B |  |
| Approach Delay (s/veh) | -- | -- |  |  |  |  | 10.8 |  |
| Approach LOS | -- | -- |  |  |  |  | B |  |

Attachment 7
Unsignalized Intersection Worksheet
Project Entrance - Future AM/PM Peaks + Development

| TWO-WAY STOP CONTROL SUMMARY |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |  |
| Analyst | ALK | Intersection |  | Greystone Summit/Driveway |
| Agency/Co. | Fulghum, MacIndoe \& | \| Jurisdiction |  | Knox County |
| Date Performed | 5/10/2012 | Analysis Year |  | 2015 |
| Analysis Time Period | AM Peak |  |  |  |
| Project Description 223.005 - The Preserve at Greystone Summit Driveway |  |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: | Drive |  |
| Intersection Orientation: East-West |  | Study Period (hrs): | 0.25 |  |

Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) |  | 82 | 0 | 32 | 25 |  |
| Peak-Hour Factor, PHF | 1.00 | 0.90 | 0.90 | 0.90 | 0.90 | 1.00 |
| $\begin{array}{l}\text { Hourly Flow Rate, HFR } \\ \text { (veh/h) }\end{array}$ | 0 | 91 | 0 | 35 | 27 | 0 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration |  |  | TR | $L T$ |  |  |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 0 |  | 114 |  |  |  |
| Peak-Hour Factor, PHF | 0.90 | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 |
| Hourly Flow Rate, HFR (veh/h) | 0 | 0 | 126 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | - 0 |  |  | 0 |  |  |
| Flared Approach |  | $N$ |  |  | $N$ |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |


| Delay, Queue Length, and Level of Service |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration |  | $L T$ |  | $L R$ |  |  |  |  |
| $\mathrm{v}(\mathrm{veh} / \mathrm{h})$ |  | 35 |  | 126 |  |  |  |  |
| $\mathrm{C}(\mathrm{m})(\mathrm{veh} / \mathrm{h})$ |  | 1517 |  | 972 |  |  |  |  |
| V c |  | 0.02 |  | 0.13 |  |  |  |  |
| $95 \%$ queue length |  | 0.07 |  | 0.44 |  |  |  |  |
| Control Delay (s/veh) |  | 7.4 |  | 9.3 |  |  |  |  |
| LOS |  | $A$ |  | A |  |  |  |  |
| Approach Delay (s/veh) | -- | -- | 9.3 |  |  |  |  |  |
| Approach LOS | -- | -- | A |  |  |  |  |  |


| TWO-WAY STOP CONTROL SUMMARY |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |  |
| Analyst | ALK | Intersection |  | Greystone Summit/Driveway |
| Agency/Co. | Fulghum, MacIndoe \& | \| Jurisdiction |  | Knox County |
| Date Performed | As/10/2012 | Analysis Year |  | 2015 |
| Analysis Time Period | PM Peak |  |  |  |
| Project Description 223.005 - The Preserve at Greystone Summit Driveway |  |  |  |  |
| East/West Street: Greystone Summit Blvd |  | North/South Street: | Drive |  |
| Intersection Orientation: East-West |  | Study Period (hrs): | 0.25 |  |

Vehicle Volumes and Adjustments

| Major Street | Eastbound |  |  | Westbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | 1 | 2 | 3 | 4 | 5 | 6 |
|  | L | T | R | L | T | R |
| Volume (veh/h) |  | 64 | 0 | 114 | 77 |  |
| Peak-Hour Factor, PHF | 1.00 | 0.90 | 0.90 | 0.90 | 0.90 | 1.00 |
| Hourly Flow Rate, HFR (veh/h) | 0 | 71 | 0 | 126 | 85 | 0 |
| Percent Heavy Vehicles | 0 | -- | -- | 0 | -- | -- |
| Median Type | Undivided |  |  |  |  |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 |
| Configuration |  |  | TR | LT |  |  |
| Upstream Signal |  | 0 |  |  | 0 |  |
| Minor Street | Northbound |  |  | Southbound |  |  |
| Movement | 7 | 8 | 9 | 10 | 11 | 12 |
|  | L | T | R | L | T | R |
| Volume (veh/h) | 0 |  | 94 |  |  |  |
| Peak-Hour Factor, PHF | 0.90 | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 |
| Hourly Flow Rate, HFR (veh/h) | 0 | 0 | 104 | 0 | 0 | 0 |
| Percent Heavy Vehicles | 0 | 0 | 0 | 0 | 0 | 0 |
| Percent Grade (\%) | 0 |  |  | 0 |  |  |
| Flared Approach |  | N |  |  | N |  |
| Storage |  | 0 |  |  | 0 |  |
| RT Channelized |  |  | 0 |  |  | 0 |
| Lanes | 0 | 0 | 0 | 0 | 0 | 0 |
| Configuration |  | LR |  |  |  |  |


| Delay, Queue Length, and Level of Service |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Eastbound | Westbound | Northbound |  |  | Southbound |  |  |
| Movement | 1 | 4 | 7 | 8 | 9 | 10 | 11 | 12 |
| Lane Configuration |  | LT |  | LR |  |  |  |  |
| v (veh/h) |  | 126 |  | 104 |  |  |  |  |
| C (m) (veh/h) |  | 1542 |  | 997 |  |  |  |  |
| v/c |  | 0.08 |  | 0.10 |  |  |  |  |
| 95\% queue length |  | 0.27 |  | 0.35 |  |  |  |  |
| Control Delay (s/veh) |  | 7.5 |  | 9.0 |  |  |  |  |
| LOS |  | A |  | A |  |  |  |  |
| Approach Delay (s/veh) | -- | -- |  | 9.0 |  |  |  |  |
| Approach LOS | -- | -- |  | A |  |  |  |  |

Attachment 8 Turn Lane Warrants

## Attachment 8

Turn Lane Warrant Analysis

## Project: The Preserve at Greystone Summit

Solway Road at Greyston Summit Blvd

Greystone Summit Blvd at Proposed Driveway LEFT TURN
Proposed AM PM

RIGHT TURN
Proposed AM
PM

| LEFT TURN | \%LT | Opposing | LT | LT MAX | Warrant Met |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Proposed AM | 31\% | 182 | 35 | 200 | NO |
| PM | 46\% | 233 | 119 | 160 | NO |
| RIGHT TURN | \%RT | Opposing | RT | RT MAX | Warrant Met |
| Proposed AM | 12\% | 116 | 22 | 449 | NO |
| PM | 31\% | 263 | 72 | 299 | NO |

VOLUMES

| VOLUMES |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| \%LT | Opposing | LT | LT MAX | Warrant Met |
| 56\% | 82 | 32 | 300 | NO |
| 60\% | 64 | 114 | 300 | NO |


| $\%$ RT | Opposing | RT | RT MAX | Warrant Met |
| :---: | :---: | :---: | :---: | :---: |
| $100 \%$ | 57 | 114 | 599 | NO |
| $100 \%$ | 191 | 94 | 599 | NO |

Greystone Summit Blva at Proposed Drineway
TABLE 4A

## LEFT-TURN LANE VOLUME THRESHOLDS

FOR TWO-LANE ROADWAYS WITH A PREVALING SPEED OF 35 MPH OR LESS
(If the left-turn volume excceds the table value a left -turn lane is needed)

| OPPOSING VOLUME | THIROUGH VOLUME PLUS RIGHT-TURN VOLUNE * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{ccc} \text { AM } \\ 15 & 100-109 & 78 \\ \hline \end{array}$ | 150-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{array}{\|ccc} \hline A M & 100-149 & \mathrm{Pm} \\ 82 & 150-199 & 64 \end{array}$ | ${\frac{(300)}{}{ }^{245}}^{\text {Am }+8 p}$ | $\begin{aligned} & 235 \\ & 200 \end{aligned}$ | $\begin{aligned} & 185 \\ & 160 \end{aligned}$ | $\begin{aligned} & 145 \\ & 130 \end{aligned}$ | $\begin{aligned} & 120 \\ & 110 \end{aligned}$ | $\begin{aligned} & 100 \\ & 90 \end{aligned}$ |
| $\begin{aligned} & 200-2.49 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 205 \\ & 175 \end{aligned}$ | $\begin{aligned} & 170 \\ & 150 \end{aligned}$ | $\begin{aligned} & 140 \\ & 125 \end{aligned}$ | $\begin{aligned} & 115 \\ & 105 \end{aligned}$ | $\begin{gathered} 100 \\ 90 \end{gathered}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & 155 \\ & 135 \end{aligned}$ | $\begin{aligned} & 135 \\ & 120 \end{aligned}$ | $\begin{aligned} & 110 \\ & 100 \end{aligned}$ | $\begin{aligned} & 95 \\ & 85 \end{aligned}$ | $\begin{gathered} 50 \\ 70 \end{gathered}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ |
| $\begin{aligned} & 400-490 \\ & 450-4019 \end{aligned}$ | $\begin{aligned} & 120 \\ & 105 \end{aligned}$ | $\begin{aligned} & 105 \\ & 20 \end{aligned}$ | $\begin{aligned} & 90 \\ & 80 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ |
| $\begin{aligned} & 5(K)-549 \\ & 550-50) \end{aligned}$ | $\begin{aligned} & 95 \\ & 85 \end{aligned}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 65 \\ & 61 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ |
| $\begin{aligned} & 600-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 75 \\ & 70 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ |
| $\begin{gathered} 700-749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |


| OPPOSING <br> VOLUME | THROUGF VOLUME PLUS RIGET-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | 400-749 | 450-499 | 500-549 | 550-599 | $=1>600$ |
| $\begin{array}{r} 100-149 \\ 150-199 \\ \hline \end{array}$ | $\begin{gathered} 100 \\ 90 \end{gathered}$ | $\begin{aligned} & 80 \\ & 75 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \\ & \hline \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ | $\begin{aligned} & 72 \\ & 65 \end{aligned}$ | $\begin{gathered} 460 \\ 55 \end{gathered}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \\ & \hline \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 600-649 \\ & 650-699 \end{aligned}$ | $\begin{array}{r} 40 \\ 35 \end{array}$ | $\begin{aligned} & 35 \\ & 35 \\ & \hline \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |
| $\begin{gathered} 700-749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 30 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \\ & \hline \end{aligned}$ | 30 30 | 30 30 | 30 30 |

* Or through volume only if a right-turn lane exists.

Greystone Summit Blid at Proposed Driveway

TABLE 4B
RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 35 MPH OR LESS

| RIGHT-TURN VOLUME | THROUGH VOLUNE PLUS LEET-TURN VOLUME *- |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{AN} \\ 0<100 \mathrm{PM} \\ 0 \end{gathered}$ | 100-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & \text { Tewer Than } 25 \\ & 25-49 \\ & 50-9994 \\ & \hline \end{aligned}$ | PM Peak |  |  |  |  |  |
| $\begin{aligned} & 100-149114 \\ & 150-199 \end{aligned}$ | Am Peak |  |  |  |  |  |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ |  |  |  | . |  | Yes |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | , - |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ |  |  | $\begin{aligned} & \text { Yes } \\ & \text { Y'es } \end{aligned}$ | Y'es <br> Y'es | Yes Yes | Yes Yes |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ |  | Ycs <br> Yes | $\begin{aligned} & \text { Y'es } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |


| RIGHT-TURN VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | $400 \cdot 449$ | $450-499$ | 500-549 | $550 \cdot 600$ | $+1>600$ |
| $\begin{aligned} & \text { Tewer Than } 25 \\ & 25-49 \\ & 50-99 \end{aligned}$ |  |  |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Ycs } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or Mort | Yes | Yes | Yes | Yes | Yes | Yes |

* Or through volume only if a left-turn lane exists.

TABLE 5A
LEFT-TURN LANE VOLUME TKRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH
(If the left-turn volume exceeds the table value a left -turn lane is needed)

| OPPOSING <br> VOLUME | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Am 100.149 PM | 150-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & 100-149 \\ & 150-199 \\ & \hline \end{aligned}$ | $250$ | $\begin{aligned} & 180 \\ & 140 \\ & \hline \end{aligned}$ | $\begin{aligned} & 140 \\ & 105 \\ & \hline \end{aligned}$ | $110$ | $\begin{aligned} & 80 \\ & 70 \\ & \hline \end{aligned}$ | $\begin{array}{r} 70 \\ 60 \\ \hline \end{array}$ |
| $2(0)-249233$ $250-299$ | $\frac{160}{130}-\mathrm{mm}$ | $\begin{aligned} & 115 \\ & 100 \end{aligned}$ | $\begin{aligned} & 85 \\ & 75 \end{aligned}$ | $\begin{aligned} & 75 \\ & 65 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & 110 \\ & 100 \end{aligned}$ | $\begin{array}{r} 90 \\ 80 \\ \hline \end{array}$ | $\begin{array}{r} 70 \\ 65 \\ \hline \end{array}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ |
| $\begin{aligned} & 400-40 \\ & 450-409 \end{aligned}$ | $\begin{aligned} & 90 \\ & 80 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ |
| $\begin{aligned} & 500-54 y \\ & 550-599 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ |
| $\begin{aligned} & 600-699 \\ & 650-699 \end{aligned}$ | $\begin{array}{r} 60 \\ 55 \\ \hline \end{array}$ | $\begin{aligned} & 45 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{array}{r} 25 \\ 25 \\ \hline \end{array}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ |
| $\begin{gathered} 700-749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | 20 20 | 20 20 |


| OPPOSING VOLUME | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | 400-449 | 450-499 | 500-549 | 550-509 | $=1>600$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ | $\begin{aligned} & 70 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 . \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ |
| $\begin{aligned} & 600-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ |
| $\begin{gathered} 700 \cdot 749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{array}{r} 20 \\ \cdot \quad 20 \end{array}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ |

[^0]TABLE SB
RIGHT-TURN LANE VOLUME THRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH



* Or through volume only if a left-turn lane exists.


[^0]:    * Or through volume only if a right-turn lane exists

