LEGENDS AT WASHINGTON PIKE – PHASE 2 Traffic Impact Study Washington Pike Knoxville, TN

A Traffic Impact Study for the Proposed Legends at Washington Pike – Phase 2

Submitted to

Knoxville – Knox County Metropolitan Planning Commission

Revised August 6, 2018 June 25, 2018 FMA Project No. 616.001



Submitted By:



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Executive Summary

Maddox Companies is proposing a residential development with single family homes and duplex townhomes within the Knoxville city limits. The project is located at the existing intersection of Washington Pike at Rising Oak Way. The development will consist of 179 single family homes and 82 duplex townhomes in addition to the existing Legends at Oak Grove apartment complex located on Rising Oak Way.

The development will connect to the existing Legends at Oak Grove at the end of Rising Oak Way. Construction is proposed to take place this year and this study assumes full buildout for the development will occur in 2021.

In order to maintain or provide an acceptable level-of-service for each of the intersections studied, some recommendations are presented.

Washington Pike at Rising Oak Way

FMA recommends adding a separate right and left turn lane at the intersection with Washington Pike to be built during the Legends at Washington Pike – Phase 2 construction in order for the intersection to operate at an acceptable LOS.

After the completion of the Legends at Washington Pike – Phase 2 including the proposed improvements to the intersection the eastbound approach exiting the development will operate at a LOS D during the AM peak hour and a LOS C during the PM peak hour and the northbound approach will operate at a LOS B during the AM peak hour and a LOS A during the PM peak hour.

A right turn lane warrant is met during the AM peak hour at the intersection of Washington Pike at Rising Oak Way. FMA recommends a 75 foot storage length and a 100 foot taper. The design of the right turn lane should be coordinated with the City of Knoxville engineering department.

Washington Pike at Mill Road

After the completion of the Legends at Washington Pike – Phase 2 the signalized intersection of Washington Pike at Mill Road will operate at a LOS C during AM peak hour and a LOS F during the PM peak hour using the existing signal timing provided by the City of Knoxville.

FMA does not recommend any improvements to the intersection of Washington Pike at Mill Road as a part of the Legends at Washington Pike – Phase 2 development. The highest delay from this intersection is a result of the southbound left turn lane on Washington Pike which is not affected by this development.

1 Introduction

1.1 Project Description

This report provides a summary of a traffic impact study that was performed for the proposed Legends at Washington Pike – Phase 2. The project is located near the existing intersection of Washington Pike at Rising Oak Way in the Knoxville City Limits. The location of the site is shown in Figure 1.

The Legends at Washington Pike – Phase 2 will consist of 179 single family homes and 82 duplex townhomes in addition to the existing Legends at Oak Grove apartment complex located on Rising Oak Way. Construction is proposed to take place this year and this study assumes full build out for the development will occur in 2021.

The development will connect to the existing Legends at Oak Grove at the end of Rising Oak Way. The traffic from the proposed Legends at Washington Pike will enter and exit the site using the existing intersection of Washington Pike at Rising Oak Way. The proposed site layout is shown in Figure 2.

The purpose of this study is to evaluate the impacts to the traffic conditions caused by the proposed development.

Legends at Washington Pike - Phase 2 Traffic Impact Study August 6, 2018



Figure 1: Location Map

Legends at Washington Pike - Phase 2 Traffic Impact Study August 6, 2018





Figure 2: Site Plan

1.2 Existing Site Conditions

The proposed site access will connect to the existing Rising Oak Way. All traffic from the proposed development will enter and exit the site at the existing intersection of Washington Pike at Rising Oak Way.

Rising Oak Way is a two-lane private road with a driveway width of 28 feet at the intersection at Washington Pike. Located at the intersection of Washington Pike at Rising Oak Way is a left turn lane on Washington Pike with a storage length of 80 feet. The intersection of Rising Oak Way at Washington Pike is located 440 feet south of the intersection of Washington Pike at Mill Road. The Knoxville-Knox County Metropolitan Planning Commission does not classify Rising Oak Way; therefore it is considered a local street. The posted speed limit on Rising Oak Way is 20 mph.

The minimum required sight distance for a road with a posted speed limit of 40 mph is 400 feet in each direction in accordance with the "Subdivision Regulations" for Knoxville and Knox County. FMA measured the sight distance at the existing intersection of Washington Pike at Rising Oak Way. At 15 feet from the edge of pavement the sight distance at the existing intersection is 400 feet northbound and 410 feet southbound; however the northbound sight distance is partially blocked due by the tree line.

Washington Pike is a two-lane road south of the intersection of Mill Road. The Knoxville-Knox County Metropolitan Planning Commission classifies Washington Pike between Millertown Pike and Murphy Road as a minor arterial per the Major Road Plan. The posted speed limit on Washington Pike is 40 mph.

Mill Road is a two-lane road between Millertown Pike and Washington Pike. The Knoxville-Knox County Metropolitan Planning Commission classifies Mill Road from Millertown Pike to Washington Pike as a major collector per the Major Road Plan. The posted speed limit on Mill Road is 30 mph.

Aerial photos of the existing intersections are included in Attachment 9.

2 Existing Traffic Volumes

FMA conducted a turning movement count at the intersection of Washington Pike at Mill Road on Tuesday May 15, 2018. FMA also conducted a turning movement count at the intersection of Washington Pike at Rising Oak Way on Wednesday May 16, 2018.

The current AM peak hour and PM peak hour were determined using the turning movement count that FMA conducted. At the intersection of Washington Pike at Mill Road the AM peak hour occurred between 7:15 am and 8:15 am, and the PM peak hour occurred between 5:00 pm and 6:00 pm. At the intersection of Washington Pike at Rising Oak Way the AM peak hour occurred between 7:00 am and 8:00 am, and the PM peak hour occurred between 4:15 pm and 5:15 pm.

The existing volumes including the AM and PM peak hour traffic volumes at the count locations are shown in Figure 3, and the count data collected is included in Attachment 1.



Figure 3: 2018 Existing Peak Hour Traffic

3 Background Growth

The Tennessee Department of Transportation (TDOT) and the Knoxville Regional Transportation Planning Organization (TPO) maintain count stations in the vicinity of the proposed development.

TDOT count station #000041 is located on Mill Road south of the intersection of Washington Pike. The annual traffic growth rate for this station over the last five years is approximately 1.45%.

Knoxville TPO count station ID 093M035 is located on Washington Pike 200 feet west of the intersection with Mill Road. The annual growth rate for this station over the last five years is approximately 1.98%.

For the purpose of this study, an annual growth rate of 2.0% was assumed for traffic at the intersections of Washington Pike at Mill Road and Washington Pike at Rising Oak Way until full occupancy is reached in 2021. Attachment 2 shows the trend line growth charts for the TDOT and TPO count stations.

Figure 4 demonstrates the projected background peak hour volumes at the intersection after applying the background growth rate to the existing conditions.



Figure 4: 2021 Background Peak Hour Traffic

Trip Generation and Trip Distribution 4

The Knoxville-Knox County Metropolitan Planning Commission published a memorandum ("Local Trip Generation Rates for Multi-Family Residential Uses", August 14, 2000) for the purpose of providing locally collected data for all multifamily residential developments. The fitted curve equations from the local study were used to calculate site trips for the duplex townhomes.

Single-Family Detached Housing or Land Use 210 was used to calculate site trips for the proposed Single Family Housing using the fitted curve equations from *Trip* Generation, 9th Edition, published by the Institute of Transportation Engineers. The land use worksheets are included in Attachment 3.

The total combined trips generated by the Legends at Washington Pike – Phase 2 for 179 single family homes and 82 duplex townhomes was estimated to be 2,592 daily trips. The estimated trips are 180 trips during the AM peak hour and 242 trips during the PM peak hour. A trip generation summary is shown in Table 4-1.

| | EC { | Trip Generatio | on Summary | | |
|-----------------------------------|---------------------|-------------------------------|-------------------------|--------------------|--------------------|
| | | Single-Family Det (Land Us | ached Housing e 210) | | |
| | Total New Trips | % Entering | %Exiting | Number Entering | Number Exiting |
| Weekday A.M. Peak P.M. Peak | 1794 135 177 | 50 25 63 | 50 75 37 | 897 34 112 | 897 101 65 |
| | Loo | cal Apartment Trip | Generation Study | / | |
| Weekday A.M. Peak P.M. Peak | 798 45 65 | 50 22 55 | 50 78 45 | 399 10 36 | 399 35 29 |
| | | Total Combi | ned Trips | | |
| Weekday A.M. Peak P.M. Peak | 2,592 180 242 | | | 1,296 44 148 | 1,296 136 94 |

| Table 4-1 |
|--------------------------------------|
| Legends at Washington Pike – Phase 2 |
| Trip Generation Summary |

Thru traffic on Washington Pike at Rising Oak Way has a trip distribution of 20% northbound and 80% southbound during the AM peak hour and 67% northbound and 33% southbound during the PM peak hour.

The directional distribution of the traffic generated by the Legends at Washington Pike – Phase 2 was determined using the existing traffic volumes. Figure 5 shows the AM peak hour trip distribution and Figure 6 shows the PM peak hour trip distribution.

Figure 7 shows the peak hour site traffic and Figure 8 shows the full buildout peak hour traffic.



Figure 5: AM Peak Hour Trip Distribution



Figure 6: PM Peak Hour Trip Distribution



Figure 7: Peak Hour Site Traffic



Figure 8: Peak Hour Full Buildout Traffic

5 **Projected Capacity and Level of Service**

Signalized intersection capacity analyses were performed using Highway Capacity Software (HCS7) with the existing signal timing for the AM and PM peak hours to evaluate the traffic conditions at the intersection of Washington Pike at Mill Road. The existing signal timing was provided by the City of Knoxville and is included in Attachment 4.

Unsignalized intersection capacity analysis was performed using the Highway Capacity Software (HCS7) for the AM and PM peak hours to evaluate the traffic conditions at the intersection of Washington Pike at Rising Oak Way.

The results from the analyses are expressed with a term "level of service" (LOS), which is based on the amount of delay experienced at the intersection. The LOS index ranges from LOS A, indicating excellent traffic conditions with minimal delay, to LOS F indicating very congested conditions with excessive delay. LOS D generally is considered the minimum acceptable condition in urban areas. The HCS7 worksheets are included in Attachments 5, 6, and 7. Table 5-1 shows the results of the capacity analyses.

Table 5-1 Intersection Analysis Level of Service (LOS) Summary

| | | Delay (sec)/LOS | | | | | | | | | |
|--|---|------------------------------|--|--|--|--|--|--|--|--|--|
| | Washington Pike @ Mill Road (Existing 2018) | | | | | | | | | | |
| AM Peak | Intersection | 18.3 / B | | | | | | | | | |
| PM Peak | Intersection | 64.9 / E | | | | | | | | | |
| Washington Pike @ Rising Oak Way (Existing 2018) | | | | | | | | | | | |
| AM Peak | EB Approach NB Approach | 22.2 / C 10.4 / B | | | | | | | | | |
| PM Peak | EB Approach NB Approach | 14.0 / B 8.7 / A | | | | | | | | | |
| | Washington Pike @ Mill Road (Background 2021) | | | | | | | | | | |
| AM Peak | Intersection | 21.0 / C | | | | | | | | | |
| PM Peak | Intersection | 78.6 / E | | | | | | | | | |
| | Washington Pike @ Rising | Oak Way (Background 2021) | | | | | | | | | |
| AM Peak | EB Approach NB Approach | 24.8 / C 10.7 / B | | | | | | | | | |
| PM Peak | EB Approach NB Approach | 14.6 / B 8.9 / A | | | | | | | | | |
| | Washington Pike @ Mil | l Road (Full Buildout 2021) | | | | | | | | | |
| AM Peak | Intersection | 22.8 / C | | | | | | | | | |
| PM Peak | Intersection | 81.7 / F | | | | | | | | | |
| | Washington Pike @ Rising | Oak Way (Full Buildout 2021) | | | | | | | | | |
| AM Peak | EB Approach NB Approach | 28.5 / D 11.0 / B | | | | | | | | | |
| PM Peak | EB Approach NB Approach | 18.6 / C 9.7 / A | | | | | | | | | |

6 Turn Lane Warrant Analysis

The intersection of Washington Pike at Rising Oak Way was evaluated to determine if a southbound right turn lane is warranted. The Knox County Department of Engineering and Public Works handbook, "Access Control and Driveway Design Policy," was used to analyze the information. A right turn lane is warranted on Washington Pike at the intersection of Rising Oak Way during the AM peak hour.

The right-of-way for Washington Pike at the intersection with Rising Oak Way is 88 feet per the Major Road Plan. There is approximately 10 feet between the edge of pavement and the property line for the Oak Grove Zion Church therefore; the owner may need to acquire property from the Oak Grove Zion Church in order to install a right turn lane. Per AASHTO "A Policy on Geometric Design of Highways and Streets" the recommended storage length for the right turn lane is three car lengths (approximately 75 feet) and the recommended taper length is 100 feet. The turn lane warrant worksheets and diagram are included in Attachment 8.

7 Conclusions and Recommendations

7.1 Washington Pike @ Rising Oak Way

Currently at the intersection of Washington Pike at Rising Oak Way the eastbound approach exiting the development operates at a LOS C during the AM peak hour and a LOS B during the PM peak hour and the northbound approach operates at a LOS B during the AM peak hour and a LOS A during the PM peak hour.

It is estimated based on field observations that the existing driveway connection is blocked approximately 10% during the PM peak hour by northbound traffic from the signalized intersection of Washington Pike at Mill Road. The signalized intersection capacity analysis for the intersection of Washington Pike at Mill Road shows an existing 95% queue length for the northbound approach of 159.9 feet during the AM peak hour and 1320.5 feet during the PM peak hour.

The existing northbound left turn lane on Washington Pike measures 125 feet with enough storage space for approximately 5 vehicles. The unsignalized intersection capacity analyses show a 95% queue length of less than one vehicle during both the AM and PM peak hour after the completion of the Legends at Washington Pike – Phase 2, therefore; the existing storage capacity will be adequate.

A turn lane warrant is met for a southbound right turn lane on Washington Pike during the AM peak hour at the intersection of Washington Pike at Rising Oak Way.

Per AASHTO "A Policy on Geometric Design of Highways and Streets" the recommended storage length is three car lengths (approximately 75 feet) and the recommended taper length is 100 feet. The design of the right turn lane should be coordinated with the City of Knoxville engineering department.

FMA recommends adding a separate right and left turn lane at the intersection with Washington Pike to be built during the Legends at Washington Pike – Phase 2 construction in order for the intersection to operate at an acceptable LOS.

After the completion of the Legends at Washington Pike – Phase 2 including the proposed improvements to the intersection the eastbound approach exiting the development will operate at a LOS D during the AM peak hour and a LOS C during the PM peak hour and the northbound approach will operate at a LOS B during the AM peak hour and a LOS A during the PM peak hour.

The 95% queue length on Rising Oak Way for the exiting traffic after the completion of The Legends at Washington Pike – Phase 2 is calculated at 1.3 vehicles in the left turn lane and 3.0 vehicles in the right turn lane during the AM peak hour and less than one vehicle for both the right and left turn lanes during the PM peak hour. Rising Oak Way does have adequate storage capacity for 3 vehicles.

The existing northbound left turn lane on Washington Pike measures 125 feet with enough storage space for approximately 5 vehicles. The unsignalized intersection capacity analyses show a 95% queue length of less than one vehicle during both the AM and PM peak hour after the completion of the Legends at Washington Pike – Phase 2, therefore; the existing storage capacity will be adequate.

The minimum required sight distance for a road with a posted speed limit of 40 mph is 400 feet in each direction in accordance with the "Subdivision Regulations" for Knoxville and Knox County. FMA measured the sight distance at the existing intersection of Washington Pike at Rising Oak Way. At 15 feet from the edge of pavement the sight distance at the existing intersection is 400 feet northbound and 410 feet southbound; however the northbound sight distance is partially blocked due by the tree line.

FMA recommends that the sight distance be re-evaluated in the field after the completion of the proposed intersection improvements to ensure that the sight distance complies with the City of Knoxville Department of Engineering requirements. FMA also recommends any landscaping be installed so as to maintain the sight distance and continue to comply with the City of Knoxville Department of Engineering.

7.2 Washington Pike @ Mill Road

The existing traffic conditions at the signalized intersection of Washington Pike at Mill Road operate at a LOS B during the AM peak hour and a LOS E during the PM peak hour using the existing signal timing provided by the City of Knoxville.

The background traffic conditions at the signalized intersection of Washington Pike at Mill Road operate at a LOS C during the AM peak hour and a LOS E during the PM peak hour using the existing signal timing provided by the City of Knoxville.

After the completion of the Legends at Washington Pike – Phase 2 the signalized intersection of Washington Pike at Mill Road will operate at a LOS C during AM peak hour and a LOS F during the PM peak hour using the existing signal timing provided by the City of Knoxville.

FMA does not recommend any improvements to the intersection of Washington Pike at Mill Road as a part of the Legends at Washington Pike – Phase 2 development. The highest delay from this intersection is a result of the southbound left turn lane on Washington Pike which is not affected by this development.

Attachment 1 Traffic Counts

Project: Legends at Washington Pike Intersection: Washington Pike at Mill Road Date Conducted: 05/15/2018

| [| Ν | ∕ill Road | | Washington Pike | | | Washington Pike | | | |
|----------------------|----------|-----------|-------|-----------------|----------|------------------------|-----------------|----------|-------|------------|
| | Ν | /estbound | | Northbound | | | So | | | |
| Start | Left | Right | Total | Thru | Right | Total | Left | Thru | Total | Int. Total |
| 7:00 AM | 10 | 49 | 59 | 37 | 11 | 48 | 107 | 233 | 340 | 447 |
| 7:15 AM | 9 | 55 | 64 | 61 | 10 | 71 | 131 | 240 | 371 | 506 |
| 7:30 AM | 10 | 73 | 83 | 61 | 12 | 73 | 125 | 252 | 377 | 533 |
| 7:45 AM | 14 | 56 | 70 | 70 | 20 | 90 | 137 | 239 | 376 | 536 |
| Total | 43 | 233 | 276 | 229 | 53 | 282 | 500 | 964 | 1464 | 2022 |
| | | | | | | | | | | |
| 8:00 AM | 13 | 65 | 78 | 65 | 16 | 81 | 156 | 192 | 348 | 507 |
| 8:15 AM | 14 | 79 | 93 | 55 | 11 | 66 | 104 | 185 | 289 | 448 |
| 8:30 AM | 13 | 49 | 62 | 53 | 9 | 62 | 96 | 174 | 270 | 394 |
| 8:45 AM | 8 | 49 | 57 | 53 | 7 | 60 | 106 | 111 | 217 | 334 |
| Total | 48 | 242 | 290 | 226 | 43 | 269 | 462 | 662 | 1124 | 1683 |
| | | | | | | 1 | | | | |
| 11:00 AM | 8 | 58 | 66 | 58 | 13 | 71 | 48 | 84 | 132 | 269 |
| 11:15 AM | 11 | 75 | 86 | 59 | 8 | 67 | 61 | 89 | 150 | 303 |
| 11:30 AM | 9 | 64 | 73 | 63 | 10 | 73 | 54 | 95 | 149 | 295 |
| 11:45 AM | 17 | 64 | 81 | 67 | 12 | 79 | 69 | 84 | 153 | 313 |
| lotal | 45 | 261 | 306 | 247 | 43 | 290 | 232 | 352 | 584 | 1180 |
| 12.00 BM | 0 | E 2 | 61 | 20 | 7 | 06 | EG | 01 | 147 | 204 |
| 12:00 FM 12:15 DM | 0 10 | 22 | 101 | 09 77 | 16 | 90 | 50 | 91 | 147 | 304 |
| 12.13 TM | 12 | 71 | 82 | 73 | 7 | 90 80 | 68 | 80 | 1/12 | 310 |
| 12:30 TM 12:45 PM | 10 | 71 | 85 | 73 | 10 | 87 | 67 | 86 | 140 | 325 |
| Total | 41 | 288 | 329 | 316 | 40 | 356 | 253 | 352 | 605 | 1290 |
| Total | | 200 | 525 | 510 | 10 | 550 | 200 | 552 | 005 | 1200 |
| 2:00 PM | 9 | 88 | 97 | 92 | 22 | 114 | 66 | 88 | 154 | 365 |
| 2:15 PM | 7 | 84 | 91 | 102 | 13 | 115 | 66 | 130 | 196 | 402 |
| 2:30 PM | 8 | 94 | 102 | 79 | 20 | 99 | 85 | 98 | 183 | 384 |
| 2:45 PM | 20 | 90 | 110 | 91 | 16 | 107 | 78 | 89 | 167 | 384 |
| Total | 44 | 356 | 400 | 364 | 71 | 435 | 295 | 405 | 700 | 1535 |
| • | | | • | | | - | | | | |
| 3:00 PM | 13 | 70 | 83 | 103 | 20 | 123 | 100 | 114 | 214 | 420 |
| 3:15 PM | 12 | 130 | 142 | 108 | 23 | 131 | 80 | 101 | 181 | 454 |
| 3:30 PM | 13 | 106 | 119 | 114 | 21 | 135 | 67 | 85 | 152 | 406 |
| 3:45 PM | 9 | 150 | 159 | 136 | 24 | 160 | 78 | 104 | 182 | 501 |
| Total | 47 | 456 | 503 | 461 | 88 | 549 | 325 | 404 | 729 | 1781 |
| | | | 1 | | | | | | | |
| 4:00 PM | 10 | 125 | 135 | 145 | 29 | 174 | 82 | 124 | 206 | 515 |
| 4:15 PM | 18 | 128 | 146 | 152 | 28 | 180 | 71 | 104 | 175 | 501 |
| 4:30 PM | 8 | 115 | 123 | 163 | 28 | 191 | 87 | 89 | 176 | 490 |
| 4:45 PM | 14 | 125 | 139 | 176 | 22 | 198 | 62 | 110 | 172 | 509 |
| Total | 50 | 493 | 543 | 636 | 107 | 743 | 302 | 427 | /29 | 2015 |
| 5.00 PM | 5 | 121 | 126 | 207 | 17 | 224 | 65 | 86 | 151 | 511 |
| 5.15 PM | 5 15 | 120 | 150 | 207 107 | 20 | 22 4 217 | 54 | 00 80 | 1/12 | 511 |
| 5.30 PM | 13 | 139 | 154 | 101 | 20 | ∠1 4 214 | 54 | 09 | 156 | 525 |
| 5.45 PM | ∠J 22 | 150 | 177 | 191 | ∠3 07 | ∠1 4 010 | 66 | 105 | 150 | 560 |
| LetoT | 67 | 555 | 622 | 777 | 87 | 864 | 250 | 371 | 621 | 2107 |
| TUtai | 07 | 555 | 022 | /// | 07 | 004 | 250 | 371 | 021 | 210/ |
| | | | | | | | | | | |
| Grand Total | 385 | 2884 | 3269 | 3256 | 532 | 3788 | 2619 | 3937 | 6556 | 13613 |
| Approach % | 11.8 | 88.2 | | 86.0 | 14.0 | | 39.9 | 60.1 | | |
| Total % | 2.8 | 21.2 | 24.0 | 23.9 | 3.9 | 27.8 | 19.2 | 28.9 | 48.2 | |
| | | | | | | | | | | |

Project: Legends at Washington Pike Date Conducted: 5/15/2018

| AM Peak Hour | 7:15 AM - 8:15 AM | 2082 |
|--------------|-------------------|------|
| PM Peak Hour | 5:00 PM - 6:00 PM | 2107 |

| | Mill Road | | | Wa | shington F | Pike | Wa | | | |
|---------------------------|-------------|-------------|------------|------------|------------|------------|------|------|------------|------------|
| | , | Westbound | k | Northbound | | | S | | | |
| Start | Left | Right | App. Total | Thru | Right | App. Total | Left | Thru | App. Total | Int. Total |
| Peak Hour Analysis from 7 | :00 AM to 9 | :00 AM | | | | | | | | |
| AM Peak Hour begins at 7: | 15 AM | | | | | | | | | |
| 7:15 AM | 9 | 55 | 64 | 61 | 10 | 71 | 131 | 240 | 371 | 506 |
| 7:30 AM | 10 | 73 | 83 | 61 | 12 | 73 | 125 | 252 | 377 | 533 |
| 7:45 AM | 14 | 56 | 70 | 70 | 20 | 90 | 137 | 239 | 376 | 536 |
| 8:00 AM | 13 | 65 | 78 | 65 | 16 | 81 | 156 | 192 | 348 | 507 |
| Total Volume | 46 | 249 | 295 | 257 | 58 | 315 | 549 | 923 | 1472 | 2082 |
| Future (2% over 3 yrs) | 49 | 264 | 313 | 273 | 62 | 334 | 583 | 979 | 1562 | 2209 |
| PHF | 0.82 | 0.85 | | 0.92 | 0.73 | | 0.88 | 0.92 | | 0.97 |
| Peak Hour Analysis from 3 | :00 PM to 6 | :00 PM | | | | | | | | |
| PM Peak Hour begins at 5: | 00 PM | | | | | | | | | |
| 5:00 PM | 5 | 131 | 136 | 207 | 17 | 224 | 65 | 86 | 151 | 511 |
| 5:15 PM | 15 | 139 | 154 | 194 | 20 | 214 | 54 | 89 | 143 | 511 |
| 5:30 PM | 25 | 130 | 155 | 191 | 23 | 214 | 65 | 91 | 156 | 525 |
| 5:45 PM | 22 | 155 | 177 | 185 | 27 | 212 | 66 | 105 | 171 | 560 |
| Total Volume | 67 | 555 | 622 | 777 | 87 | 864 | 250 | 371 | 621 | 2107 |
| Future (2% over 3 yrs) | 71 | <u>5</u> 89 | 660 | 825 | 92 | 917 | 265 | 394 | 659 | 2236 |
| PHF | 0.67 | 0.90 | | 0.94 | 0.81 | | 0.95 | 0.88 | | 0.94 |

Project: Legends at Washington Pike Intersection: Washington Pike at Rising Oak Way Date Conducted: 05/16/2018

| | Risii | ng Oak W | /ay | Washington Pike | | | Was | I | | |
|-------------|-------|----------|--------|-----------------|------|----------|------|-----------|-------|------------|
| | E | astbound | - | Northbound | | | So | outhbound | | |
| Start | Left | Right | Total | Left | Thru | Total | Thru | Right | Total | Int. Total |
| 7:00 AM | 12 | 10 | 22 | 1 | 41 | 42 | 222 | 5 | 227 | 291 |
| 7:15 AM | 12 | 14 | 26 | 2 | 45 | 47 | 260 | 1 | 261 | 334 |
| 7:30 AM | 8 | 17 | 25 | 1 | 61 | 62 | 254 | 3 | 257 | 344 |
| 7:45 AM | 6 | 14 | 20 | 1 | 81 | 82 | 227 | 7 | 234 | 336 |
| Total | 38 | 55 | 93 | 5 | 228 | 233 | 963 | 16 | 979 | 1305 |
| I | | _ | 1 | _ | | | | - | | |
| 8:00 AM | 4 | 7 | 11 | 3 | 60 | 63 | 173 | 0 | 173 | 247 |
| 8:15 AM | 3 | 6 | 9 | 3 | 76 | 79 | 184 | 1 | 185 | 273 |
| 8:30 AM | 2 | 8 | 10 | 3 | 55 | 58 | 184 | 0 | 184 | 252 |
| 8:45 AM | 4 | 5 | 9 | 10 | 59 | 60 | 128 | 2 | 130 | 199 |
| Iotal | 13 | 26 | 39 | 10 | 250 | 260 | 669 | 3 | 672 | 971 |
| 11.00 414 | 0 | 1 | 1 | 1 | 60 | 70 | 105 | 2 | 108 | 179 |
| 11.00 AM | 3 | 1 | 7 | 5 | 82 | 70 87 | 105 | 5 1 | 100 | 200 |
| 11.13 AM | 1 | | 1 | 1 | 79 | 80 | 00 | 5 | 100 | 188 |
| 11:45 AM | 3 | 2 | | 1 | 107 | 108 | 92 | 0 | 92 | 205 |
| Total | 7 | 10 | 17 | 8 | 337 | 345 | 401 | 9 | 410 | 772 |
| Total | , | 10 | .71 | Ũ | 557 | 515 | 101 | 5 | 110 | ,,,_ |
| 12:00 PM | 1 | 5 | 6 | 1 | 84 | 85 | 104 | 1 | 105 | 196 |
| 12:15 PM | 2 | 2 | 4 | 6 | 114 | 120 | 101 | 5 | 106 | 230 |
| 12:30 PM | 2 | 2 | 4 | 2 | 94 | 96 | 98 | 7 | 105 | 205 |
| 12:45 PM | 4 | 4 | 8 | 6 | 104 | 110 | 81 | 6 | 87 | 205 |
| Total | 9 | 13 | 22 | 15 | 396 | 411 | 384 | 19 | 403 | 836 |
| | | | | | | | | | | |
| 2:00 PM | 1 | 4 | 5 | 3 | 92 | 95 | 92 | 1 | 93 | 193 |
| 2:15 PM | 2 | 10 | 12 | 3 | 128 | 131 | 111 | 2 | 113 | 256 |
| 2:30 PM | 2 | 2 | 4 | 5 | 112 | 117 | 102 | 2 | 104 | 225 |
| 2:45 PM | 0 | 6 | 6 | 2 | 105 | 107 | 91 | 1 | 92 | 205 |
| Total | 5 | 22 | 27 | 13 | 437 | 450 | 396 | 6 | 402 | 8/9 |
| 3.00 PM | Э | 4 | 6 | 2 | 137 | 130 | 110 | 11 | 172 | 268 |
| 3.15 PM | 2 | | 11 | 5 | 137 | 1/2 | 100 | 2 | 123 | 200 |
| 3.13 PM | 3 | 2 4 | 7 | 5 | 137 | 133 | 90 | 2 | 97 | 235 |
| 3:45 PM | 2 | 3 | , 5 | 10 | 166 | 176 | 107 | 7 | 114 | 295 |
| Total | 16 | 13 | 29 | 23 | 567 | 590 | 409 | 27 | 436 | 1055 |
| | | | 1 | | | | | | | |
| 4:00 PM | 6 | 3 | 9 | 10 | 164 | 174 | 129 | 7 | 136 | 319 |
| 4:15 PM | 1 | 8 | 9 | 5 | 205 | 210 | 127 | 2 | 129 | 348 |
| 4:30 PM | 1 | 5 | 6 | 7 | 296 | 303 | 126 | 2 | 128 | 437 |
| 4:45 PM | 2 | 1 | 3 | 10 | 210 | 220 | 98 | 4 | 102 | 325 |
| Total | 10 | 17 | 27 | 32 | 875 | 907 | 480 | 15 | 495 | 1429 |
| | | | 1 | | | 1 | | | | I |
| 5:00 PM | 3 | 7 | 10 | 14 | 212 | 226 | 108 | 8 | 116 | 352 |
| 5:15 PM | 2 | 8 | 10 | 11 | 210 | 221 | 107 | 1 | 108 | 339 |
| 5:30 PM | / | 2 | 9 | 15 | 202 | 217 | 125 | / | 132 | 358 |
| 5:45 PM | 10 | 10 | 3 | <u> </u> | 208 | 220 | 112 | 5 | 11/ | 340 |
| Total | 13 | 19 | 32 | 52 | 832 | 884 | 452 | 21 | 4/3 | 1389 |
| | | | | | | | | | | |
| Grand Total | 111 | 175 | 286 | 158 | 3922 | 4080 | 4154 | 116 | 4270 | 8636 |
| Approach % | 38.8 | 61.2 | | 3.9 | 96.1 | | 97.3 | 2.7 | 0 | |
| Total % | 1.3 | 2.0 | 3.3 | 1.8 | 45.4 | 47.2 | 48.1 | 1.3 | 49.4 | |
| | | | | | | | | | | - |

Project: Legends at Washington Pike Date Conducted: 5/16/2018

| AM Peak Hour | 7:00 AM - 8:00 AM | 1305 |
|--------------|-------------------|------|
| PM Peak Hour | 4:15 PM - 5:15 PM | 1462 |

| | Rising Oak Way | | | Wa | Washington Pike | | | Washington Pike | | | |
|---------------------------|----------------|-----------|------------|------|-----------------|------------|------------|-----------------|------------|------------|--|
| | | Eastbound | | Ν | orthboun | d | Southbound | | | | |
| Start | Left | Right | App. Total | Left | Thru | App. Total | Thru | Right | App. Total | Int. Total | |
| Peak Hour Analysis from 7 | :00 AM to 9: | 00 AM | | | | | | | | | |
| AM Peak Hour begins at 7: | :15 AM | | | | | | | | | | |
| 7:00 AM | 12 | 10 | 22 | 1 | 41 | 42 | 222 | 5 | 227 | 291 | |
| 7:15 AM | 12 | 14 | 26 | 2 | 45 | 47 | 260 | 1 | 261 | 334 | |
| 7:30 AM | 8 | 17 | 25 | 1 | 61 | 62 | 254 | 3 | 257 | 344 | |
| 7:45 AM | 6 | 14 | 20 | 1 | 81 | 82 | 227 | 7 | 234 | 336 | |
| Total Volume | 38 | 55 | 93 | 5 | 228 | 233 | 963 | 16 | 979 | 1305 | |
| Future (2% over 3 yrs) | 40 | 58 | | 5 | 242 | | 1022 | 17 | | 1385 | |
| PHF | 0.79 | 0.81 | | 0.63 | 0.70 | | 0.93 | 0.57 | | 0.95 | |
| Peak Hour Analysis from 3 | :00 PM to 6: | 00 PM | | | | | | | | | |
| PM Peak Hour begins at 5: | 00 PM | | | | | | | | | | |
| 4:15 PM | 1 | 8 | 9 | 5 | 205 | 210 | 127 | 2 | 129 | 348 | |
| 4:30 PM | 1 | 5 | 6 | 7 | 296 | 303 | 126 | 2 | 128 | 437 | |
| 4:45 PM | 2 | 1 | 3 | 10 | 210 | 220 | 98 | 4 | 102 | 325 | |
| 5:00 <u>PM</u> | 3 | 7 | 10 | 14 | 212 | 226 | 108 | 8 | 116 | 352 | |
| Total Volume | 7 | 21 | 28 | 36 | 923 | 959 | 459 | 16 | 475 | 1462 | |
| Future (2% over 3 yrs) | 7 | 22 | | 38 | 979 | | 487 | 17 | | 1551 | |
| PHF | 0.58 | 0.66 | | 0.64 | 0.78 | | 0.90 | 0.50 | | 0.84 | |

Attachment 2 ADT Trends



| Most Recent | Trend | Line Growth |
|-------------|-------|-------------|
| | Year | ADT |
| | 2012 | 11700 |
| | 2016 | 12860 |

Annual Percent Growth

1.98%

| | | Adjusted Average Daily | | | | | | | | | | | |
|----|------|---------------------------|-------|--------|----|----------|--------|--------|--------|-------|------|----|----|
| | Year | Traffic | | | | | | | | | | | |
| 1 | 2000 | 6734 | | | | | | | | | | | |
| 2 | 2001 | 6663 | | | AD | T Tre | nd - T | DOT | Statio | n #00 | 0041 | | |
| 3 | 2002 | 7062 | | | | Mill R | oad - | S of V | Vashir | noton | Pk | | |
| 4 | 2003 | 7287 | | | | VIIII IX | oau - | 501 | vasim | ISTON | | | |
| 5 | 2004 | 7378 | 12000 | | | | | | | | | | |
| 6 | 2005 | 8359 | 10000 | | | | | | | | | | |
| 7 | 2006 | 8578 | | | | | | | | | | | |
| 8 | 2007 | 8701 | 8000 | | | | | | | | | | |
| 9 | 2008 | 9894 | 6000 | • | • | | | | | | | | |
| 10 | 2009 | 9901 | | | | | | | | | | | |
| 11 | 2010 | 9756 | 4000 | | | | | | | | | | |
| 12 | 2011 | 9793 | 2000 | | | | | | | | | | |
| 13 | 2012 | 10623 | | | | | | | | | | | |
| 14 | 2013 | 10133 | 0 | ີ ງ | 2 | 1 | 6 | 8 | 10 | 12 | 1/ | 16 | 18 |
| 15 | 2014 | 10611 | | 0 | 2 | 4 | 0 | 0 | 10 | 12 | 74 | 10 | 10 |
| 16 | 2015 | 10870 | | | | | | | | | | | |
| 17 | 2016 | 11392 | | | | | | | | | | | |

| Most Recent Trend | Line Growth |
|-------------------|-------------|
| Year | ADT |
| 2012 | 10623 |
| 2016 | 11392 |

Annual Percent Growth 1.45%

Attachment 3 Trip Generation

Project: Legends at Washington Pike Date Conducted: 8/2/2018

> Local Apartment Trip Generation Study 82 Duplex Townhomes

Average Daily Traffic

 $T = 15.193 (X)^{0.899}$ T = 15.193 (82) ^0.899 T = 798

Peak Hour of Adjacent Street Traffic

One Hour Between 7 and 9 a.m.

 $T = 0.758 (X) ^0.924$ $T = 0.758 (82) ^0.924$

T = 45

Peak Hour of Adjacent Street Traffic One Hour Between 4 and 6 p.m.

T = 0.669 (X) + 10.069T = 0.669 (82) + 10.069 T = 65

| | | Percent | | Number | | |
|--------------------|--------------------|---------|------|--------|------|--|
| Time Period | Total Trips | Enter | Exit | Enter | Exit | |
| Weekday (24 hours) | 798 | 50% | 50% | 399 | 399 | |
| AM Peak Hour | 45 | 22% | 78% | 10 | 35 | |
| PM Peak Hour | 65 | 55% | 45% | 36 | 29 | |

Project: Legends at Washington Pike Date Conducted: 8/2/2018

Single-Family Detached Housing (LUC 210) 179 Single Family

Average Daily Traffic

Ln(T) = 0.92Ln(X) + 2.72 Ln(T) = 0.92Ln(179) + 2.72T = 1794

Peak Hour of Adjacent Street Traffic One Hour Between 7 and 9 a.m.

T = 0.70(X) + 9.74T = 0.70(179) + 9.74 T = 135

Peak Hour of Adjacent Street Traffic One Hour Between 4 and 6 p.m.

Ln(T) = 0.90Ln(X) + 0.51 Ln(T) = 0.90Ln(179) + 0.51T = 177

| | | Per | cent | Number | | |
|--------------------|--------------------|-------|------|--------|------|--|
| Time Period | Total Trips | Enter | Exit | Enter | Exit | |
| Weekday (24 hours) | 1794 | 50% | 50% | 897 | 897 | |
| AM Peak Hour | 135 | 25% | 75% | 34 | 101 | |
| PM Peak Hour | 177 | 63% | 37% | 112 | 65 | |



MEMORANDUM

To: Traffic Impact Study Reviewers and Preparers (see attached list)

From: Mike Conger

Date: August 14, 2000

Subject: Local Trip Generation Rates for Multi-Family Residential Uses

Attached please find a summary of the final report with data plots for the Knox County Local Apartment Trip Generation Study. As you will recall, this report was discussed when the traffic impact study group last convened this past February. A consensus was reached at that meeting that the trip generation rates developed in the local study should be used for new apartment complexes <u>and</u> any other "multi-family" residential uses that are being proposed.

The MPC voted at its July 2000 meeting to officially amend the Traffic Impact Study Guidelines with language which reads that "trip generation rates for proposed uses shall be calculated using the latest edition of the ITE Trip Generation Manual, or using local data when it is available". This amendment allows the full implementation of the new rates, and they should be used for future proposed multi-family developments unless it can be demonstrated otherwise.

Thanks for your assistance and cooperation in this matter, if there are any questions or comments, please let me know.

Suite 403 • City County Building 4 0 0 M a i n S t r e e t Knoxville, Tennessee 37902 8 6 5 • 2 1 5 • 2 5 0 0 F A X • 2 1 5 • 2 0 6 8 w w • k n o x m p c • o r g

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KNOX COUNTY LOCAL APARTMENT TRIP GENERATION STUDY

PURPOSE

A Traffic Impact Study (TIS) is currently required in Knox County when a proposed development is projected to generate in excess of 750 trips per day. The determinations of when the threshold is met as well as all subsequent analyses in the TIS are performed using the rates and equations given in the Institute of Transportation Engineers (ITE) Trip Generation Manual. Local governmental agencies rely heavily on the accuracy of these trip generation rates in order to correctly predict the impacts of a proposed development on the transportation system. Therefore, in certain instances, it is logical to verify whether the "national" rates and equations given in the ITE Trip Generation Manual are appropriate for use in a specific local area or region.

The decision was made to study the local trip-making characteristics of apartments because of the discrepancy between the trip generation rates for apartments and single family residential land uses as given in the ITE Trip Generation Manual. While these two land uses are similar in nature, the Trip Generation Manual predicts about three less trips per dwelling unit generated by apartments for the average weekday. Additionally the Trip Generation Manual points out that due to the age of their database, which dates back to the 1960's, "the rates for apartments probably had changed over time". It is also assumed that some of the ITE data had come from larger metropolitan areas with denser development and greater transit use than Knox County, which would contribute to lower trip generation Manual or generate new ones that can be applied to locally proposed apartment developments.

PROCEDURE

The procedures recommended by ITE in conducting local trip generation studies were generally followed for this study, along with some important assumptions that have made. ITE has published a proposed recommended practice entitled "Trip Generation Handbook" which specifically outlines procedures for conducting local trip generation studies and establishing new rates and equations.

The first step in the study was to define the number and location of the sites to be studied, as well as the counting methodology. Initially 14 sites were selected, although one apartment complex – the College Park Apartments – was later omitted due to uncharacteristically high traffic generation numbers. The number of sites used in this study far exceeds the recommended minimum amount suggested by ITE, which is five sites. Traffic counts were taken for week-long periods at 15-minute intervals between July 22, 1996 and August 9, 1996 at the access points to the apartment complexes. A Technical Appendix to this report contains the traffic count data collected at each apartment complex.

RESULTS

The traffic count data was analyzed using spreadsheets in order to determine the weighted average rates and regression equations. In order to be considered valid, the local rates and equations for each time period of analysis that were generated must meet certain statistical criteria. First, the standard deviation of the independent variable (dwelling units) should be no more than 110 percent of the weighted average rate; and secondly, the regression equations require a computed coefficient of determination (\mathbb{R}^2) value of at least 0.75 before good data fit is indicated. This statistical criteria is met by the local data results, and in fact it often exceeds the level of data fit given by their counterparts in the ITE Trip Generation Manual. Finally, in order to simplify the use of the local data, plots were generated that appear identical to the actual ones in the ITE Trip Generation Manual.

The resulting rates and equations calculated from the local data indicate that the average weekday trip generation of apartments in this area is well above the national rates reported in the ITE manual. For example, the locally computed average rate for number of trips generated during a weekday is 35% higher than the rate given by ITE (increase from 6.63 trips per dwelling unit to 9.03 trips per dwelling unit). The trip generation rates do not increase as much for the AM and PM peak hours however. The local rate is roughly 8% higher for the AM peak, and 16% higher for the PM peak. The plots from the ITE Trip Generation Manual are included in the Technical Appendix for comparison purposes.

ASSUMPTIONS MADE

Some important assumptions have been made which may affect the results of the local data that was collected:

- It is important to note that the local trip generation rates were computed for the *total* number of dwelling units in the apartment complex, and <u>not</u> necessarily for the number of *occupied* dwelling units. There are several reasons why this was done, chiefly because of the need for comparability with the rates given in ITE Trip Generation Manual, as it does not specify whether the dwelling units are occupied. According to ITE procedures the selected sites must only be of "reasonably full occupancy (i.e. at least 85%)". The Apartment Association of Greater Knoxville (AAGK) publishes quarterly reports on occupancy levels of apartment complexes, and the report covering the period of the data collection was reviewed to determine occupancy levels. According to the AAGK report from July 1, 1996 September 30, 1996 all of the apartment complexes surveyed in this study met the minimum 85% occupancy level, with an average occupancy rate for all sites studied of 94%.
- The count data that was collected at each apartment complex was used "raw" meaning that it was not factored for possible daily or seasonal variations. Once again, according to an ITE representative it is not known whether the data used in the Trip Generation Manual was factored or not, so therefore in order to be able to compare

local rates to those in the manual you must assume that count data should not be factored. Additionally, it was felt that apartment complexes would generally not be as susceptible to major seasonal fluctuations as other land uses might be. The local rates were also developed using count data that was collected and averaged over an entire week, which should limit some of the daily variations. Finally, reliable local daily and seasonal variation factors do not truly exist.

CONCLUSION

The local apartment study methodology and results were distributed for comment to a group of local transportation professionals who are directly responsible for either preparing or reviewing traffic impact studies. A meeting was held between this group on February 16, 2000 in order to gather comments and discuss the study in greater detail. The following conclusions are based on the discussion and consensus reached at this meeting:

- 1. The trip generation rates and equations meet statistical requirements and resulted from a study that followed accepted procedures; therefore they should be adopted for future use. Furthermore, the rates and equations are recommended for use in reviewing the traffic impact of any development termed as "multi-family", such as townhouse and condominium developments due to their similarity to apartment complexes.
- 2. The Traffic Access and Impact Study Guidelines and Procedures adopted by MPC should be amended with the language that local data should be used when available, which will allow the implementation of these new multi-family trip generation rates.
- 3. The following suggestions were made for future consideration:
 - This study should be updated with data collected from local townhouse and condominium developments in order to further justify the use of the new trip generation rates.
 - A statistical comparison should be made between any newly developed rates and the ITE single family trip generation rates to determine if there is a significant difference. If there is no difference then perhaps ITE single-family rates could be used for any residential development proposed in Knox County.
Local Apartment Trip Generation Study

Average Vehicle Trip Ends vs: On a:

Dwelling Units Weekday

| 13 |
|---------------------------|
| 193 |
| 50% entering, 50% exiting |
| |

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 9.03 | 6.59 - 17.41 | 2.47 |

Data Plot and Equation



Local Apartment Trip Generation Study

| Average | Vehicle | Trip | Ends vs: | |
|---------|---------|------|----------|--|
| | | | On a: | |

Dwelling Units Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Number of Studies: Average Number of Dwelling Units: Directional Distribution: 13 193 22% entering, 78% exiting

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 0.55 | 0.14 - 0.78 | 0.18 |

Data Plot and Equation



Local Apartment Trip Generation Study

| Average Vehicle Trip Ends vs: On a: | Dwelling Units Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. |
|--|--|
| Number of Studies: | 13 |
| Average Number of Dwelling Units: | 193 |
| Directional Distribution: | 55% entering, 45% exiting |

Trip Generation Per Dwelling Unit

| Average Rate | Ranges of Rates | Standard Deviation |
|--------------|-----------------|--------------------|
| 0.72 | 0.32 - 1.66 | 0.25 |



Data Plot and Equation







| Attachment 4 |
|---------------|
| Signal Timing |

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| ¥ Databa | ase | Prir | ntout | of | 1880 | DEL | Local | | | | | | | | | Page | e: 5 |
| Inters | sect | i on: Í Í Í Í | IANIN W | ASHI Í Í Í Í | NGT(Í Í Í Í | ≞∟ DN/M ÍÍÍÍÍ | ILL ´ Í Í Í Í Í Í | 11/22 111/1 | 2/11 Í Í Í Í Í | [[[[[| [[[[| - | Tue No ÍÍÍÍÍ | ov 15 ÍÍÍÍÍÍ | 13:1 [[[[| 8: 22 Í Í Í Í Í | 2016 Í Í Í Í |
| Split Split Split Split Split Split Split Split Split Split Split Split | $\begin{array}{c}1&2&3&4&5&6\\7&8&9&0&1&1&2\\1&1&1&1&1&1&1\\1&1&1&1&1&1\\1&1&1&1&$ | 45 29 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | $ \begin{array}{r} 30 \\ 40 \\ 52 \\ 0 \\ $ | 000000000000000000000000000000000000000 | $\begin{array}{c} 25\\ 31\\ 32\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\$ | 000000000000000000000000000000000000000 | 75 69 68 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 000000000000000000000000000000000000000 | | 20 20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 30 30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 40 40 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | |

Split Matrix:



WASHMI LL. TXT 1 2 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 4 0 0 0 0 0 5 0 0 0 0 0 6 0 0 0 0 0 Cycle Times: Cycl e 90 sec. 1 2 3 70 sec. 150 sec. 4 0 sec. 5 0 sec. 6 0 sec. Database Printout of 1880EL Local Page: 6 Filename: DATA\INT#1101.EL Intersection: WASHINGTON/MILL 11/22/11 Tue Nov 15 13:18:22 2016 Sync Reference: 00:00 Time: Sync with Event Time? NO City Zero: Active? NO Reference Time Cycle 1 0 2 3 0 0 4 5 0 0 6 0 Closed Loop Options: TOD Flash/Aux? NO Free w/ Ckt 0? YES Report Channel Failures to Central Conflict Flash Occurence and Resume Normal (3) Manual /Auto Flash (3) (3) Occurence and Resume Normal Occurence and Resume Normal MCE (3) Preempt Occurence and Resume Normal Auto-log only Auto-log only Channel # 5 (0)Channel # 6 (0)Channel # Auto-log only 7 (0)Channel # 8 Auto-log only (0)Occurence and Resume Normal Door Open (3)Main Street Phs for Out of Step Test Ring 1 - 2 2 - 0 Speed Trap Sensor Pairs 1-2 3-4 5-6 7-8 NO NO NO NO Standard Overlaps: Page 5

WASHMI LL. TXT

f

| HCS7 Two-Way Stop-Control Report | | | | | | | | | | |
|----------------------------------|--|----------------------------|-------------------------|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Washington @ Rising Oak | | | | | | | |
| Agency/Co. | FMA | Jurisdiction | City of Knoxville | | | | | | | |
| Date Performed | 6/3/2018 | East/West Street | Rising Oak Way | | | | | | | |
| Analysis Year | 2018 | North/South Street | Washington Pike | | | | | | | |
| Time Analyzed | Existing AM Peak | Peak Hour Factor | 0.95 | | | | | | | |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 | | | | | | | |
| Project Description | Project Description 616.001 Legends at Washington Pike - Phase 2 | | | | | | | | | |
| | | | | | | | | | | |



Major Street: North-South

| Vehicle Volumes and Adj | ustmo | ents | | | | | | | | | | | | | | |
|---|----------|---------|-------|-------|------|------|-------|---|----|-------|-------|----|----|-------|-------|----|
| Approach | | Eastb | ound | | | West | oound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration | | | LR | | | | | | | L | Т | | | | | TR |
| Volume, V (veh/h) | | 38 | | 55 | | | | | | 5 | 228 | | | | 963 | 16 |
| Percent Heavy Vehicles (%) | | 2 | | 2 | | | | | | 2 | | | | | | |
| Proportion Time Blocked | | 0.000 | | 0.000 | | | | | | 0.000 | | | | | | |
| Percent Grade (%) | 0 | | | | | | | | | | | | | | | |
| Right Turn Channelized | No No No | | | | | | | | | | Ν | 10 | | | | |
| Median Type/Storage | | | | Left | Only | | | | 5 | | | | | | | |
| Critical and Follow-up He | eadwa | iys | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | 7.1 | | 6.2 | | | | | | 4.1 | | | | | | |
| Critical Headway (sec) | | 6.42 | | 6.22 | | | | | | 4.12 | | | | | | |
| Base Follow-Up Headway (sec) | | 3.5 | | 3.3 | | | | | | 2.2 | | | | | | |
| Follow-Up Headway (sec) | | 3.52 | | 3.32 | | | | | | 2.22 | | | | | | |
| Delay, Queue Length, and | d Leve | el of S | ervic | e | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | 98 | | | | | | | 5 | | | | | | |
| Capacity, c (veh/h) | | | 306 | | | | | | | 674 | | | | | | |
| v/c Ratio | | | 0.32 | | | | | | | 0.01 | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | 1.3 | | | | | | | 0.0 | | | | | | |
| Control Delay (s/veh) | | | 22.2 | | | | | | | 10.4 | | | | | | |
| Level of Service, LOS | | | С | | | | | | | В | | | | | | |
| Approach Delay (s/veh) | | 22 | 2.2 | - | | - | | | | 0 | .2 | - | | | - | |
| Approach LOS | | (| C | | | | | | | | | | | | | |

| HCS7 Two-Way Stop-Control Report | | | | | | | | | | | |
|--|------------------|--------------------|-------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Washington @ Rising Oak | | | | | | | | |
| Agency/Co. | FMA | Jurisdiction | City of Knoxville | | | | | | | | |
| Date Performed | 6/3/2018 | East/West Street | Rising Oak Way | | | | | | | | |
| Analysis Year | 2018 | North/South Street | Washington Pike | | | | | | | | |
| Time Analyzed | Existing PM Peak | Peak Hour Factor | 0.84 | | | | | | | | |
| Intersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | | | |
| Project Description 616.001 Legends at Washington Pike - Phase 2 | | | | | | | | | | | |
| | | | | | | | | | | | |



Major Street: North-South

| Vehicle Volumes and Ad | ustm | ents | | | | | | | | | | | | | | |
|---|--------|---------|-------|-------|------|------|-------|---|----|-------|-------|---|----|-------|-------|----|
| Approach | | Eastb | ound | | | West | bound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration | | | LR | | | | | | | L | Т | | | | | TR |
| Volume, V (veh/h) | | 7 | | 21 | | | | | | 36 | 923 | | | | 459 | 16 |
| Percent Heavy Vehicles (%) | | 2 | | 2 | | | | | | 2 | | | | | | |
| Proportion Time Blocked | | 0.100 | | 0.000 | | | | | | 0.000 | | | | | | |
| Percent Grade (%) | | (| C | | | | | | | | | | | | | |
| Right Turn Channelized | | Ν | lo | | | Ν | lo | | | Ν | lo | | | Ν | lo | |
| Median Type/Storage | | | | Left | Only | | | 5 | | | | | | | | |
| Critical and Follow-up Ho | eadwa | ays | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | 7.1 | | 6.2 | | | | | | 4.1 | | | | | | |
| Critical Headway (sec) | | 6.42 | | 6.22 | | | | | | 4.12 | | | | | | |
| Base Follow-Up Headway (sec) | | 3.5 | | 3.3 | | | | | | 2.2 | | | | | | |
| Follow-Up Headway (sec) | | 3.52 | | 3.32 | | | | | | 2.22 | | | | | | |
| Delay, Queue Length, an | d Leve | el of S | ervic | e | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | 33 | | | | | | | 43 | | | | | | |
| Capacity, c (veh/h) | | | 431 | | | | | | | 1006 | | | | | | |
| v/c Ratio | | | 0.08 | | | | | | | 0.04 | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | 0.2 | | | | | | | 0.1 | | | | | | |
| Control Delay (s/veh) | | | 14.0 | | | | | | | 8.7 | | | | | | |
| Level of Service, LOS | | | В | | | | | | | А | | | | | | |
| Approach Delay (s/veh) | | 14 | 1.0 | - | | - | - | | | 0 | .3 | - | | - | - | |
| Approach LOS | | I | 3 | | | | | | | | | | | | | |

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HCS7™ TWSC Version 7.2.1 Existing PM Peak_Rising Oak Way.xtw

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| | | | r erg | | • | 01000 | | | | | | | | | | |
|------------------------------------|---|------------------------|----------|-----------|------------|----------|-------|------|----------|-------|--------|--------|------|----------|-----------|---------|
| General Inform | nation | | | | | | | | Inters | ectio | n Info | rmatic | n | U | * 7 * † † | L. |
| Agency | | FMA | | | | | | | Duratio | on h | | 0.25 | | | ţĻ | |
| Analyst | | Addie Kirkham | | Analys | is Date | Jun 3 | 2018 | | Area T | vne | | Other | | | | بر ج |
| Jurisdiction | | City of Knoxville | | Time F | | Fxisti | | eak | PHE | ypo | | 0 97 | | * | w‡e | ∕≂ |
| Lirban Street | | Washington Pike | | Analys | is Vear | 2018 | | Cak | | is Po | ariod | 1 7.0 | 0 | ** | | |
| Intersection | | Washington Pike at | Mill | | mo | Evicti | | ook | Mill Roa | d vue | - | 127.0 | | | | ~ |
| Project Descript | tion | 616 001 Legends at | Washi | naton Pi | | | | | | u.xua | 5 | | | - | 41473 | |
| T Toject Descrip | | 010.001 Legends al | . washii | ngton i i | KC - I I | 1036 2 | | | | | | | | | | |
| Demand Inform | nation | | | | EB | | | W | /B | | | NB | | | SB | |
| Approach Move | ment | | | L | Т | R | L | - | T F | र | L | Т | R | L | Т | R |
| Demand (v), v | eh/h | | | | | 1 | 46 | | 24 | 49 | | 257 | 58 | 549 | 923 | |
| | | | | | | | | | | | | | | | | |
| Signal Informa | tion | | | | l ↓ | 17 | n n | _ | | | | l | L | | | |
| Cycle, s | 90.0 | Reference Phase | 2 | | ↑ 2 | • | 6 | | | | | | | P | 2 | 4 |
| Offset, s | 0 | Reference Point | End | Green | 48.6 | 8.0 | 15.4 | 0. | 0 0. | 0 | 0.0 | | | | 3 | ĸ |
| Uncoordinated | No | Simult. Gap E/W | On | Yellow | 4.0 | 4.0 | 4.0 | 0. | 0 0. | 0 | 0.0 | | | | | |
| Force Mode | Fixed | Simult. Gap N/S | On | Red | 2.0 | 2.0 | 2.0 | 0. | 0 0. | 0 | 0.0 | | 5 | 6 | 7 | 8 |
| | | | | | | | | | | | | | | | | |
| Timer Results | | | | EBL | - | EBT | WBI | - | WBT | | NBL | | NBT | SBL | | SBT |
| Assigned Phase | Э | | | | | | | | 8 | | | | 2 | 1 | | 6 |
| Case Number | | | | | | | | | 9.0 | | | | 8.3 | 1.0 | | 4.0 |
| Phase Duration | Phase Duration, s Change Period, (Y+R c), s | | | | | | | | 21.4 | | | | 54.6 | 14.0 | | 58.6 |
| Change Period, | Change Period, (Y+R c), s | | | | | | | | 6.0 | | | | 6.0 | 6.0 | | 6.0 |
| Max Allow Head | dway(<i>I</i> | <i>MAH</i>), s | | | | | | | 3.8 | | | | 0.0 | 3.6 | | 0.0 |
| Queue Clearan | ce Time | (g s), s | | | | | | | 14.6 | | | | | 2.0 | | |
| Green Extensio | n Time | (ge), s | | | | | | | 0.8 | | | | 0.0 | 5.5 | | 0.0 |
| Phase Call Prol | oability | | | | | | | | 1.00 | | | | | 1.00 | | |
| Max Out Proba | bility | | | | | | | | 0.00 | | | | | 0.14 | | |
| Movement Gro | un Res | ults | | | FB | | | \//I | R | | | NB | | | SB | |
| Approach Move | ment | | | | Т | R | | Т | R | | I | Т | R | | Т | R |
| Assigned Move | ment | | | | | | 3 | • | 18 | | - | 2 | 12 | 1 | 6 | |
| Adjusted Flow F | Rate (v |), veh/h | _ | | | | 47 | | 257 | 7 | | 325 | | 566 | 952 | |
| Adjusted Satura | ation Flo | w Rate (s), veh/h/l | n | | | | 1810 | | 161 | 0 | | 1839 | | 1810 | 1900 | |
| Queue Service | Time (d | g s), S | | | | | 2.0 | | 12.0 | 6 | | 8.9 | | 0.0 | 27.5 | |
| Cvcle Queue C | learance | e Time (q c), s | | | | | 2.0 | | 12.0 | 6 | | 8.9 | | 0.0 | 27.5 | |
| Green Ratio (o | /C) | | | | | | 0.17 | | 0.20 | 6 | | 0.54 | | 0.61 | 0.70 | |
| Capacity (c), v | /eh/h | | | | | | 310 | | 419 | 3 | | 993 | | 690 | 1321 | |
| Volume-to-Cap | acity Ra | tio (X) | | | | | 0.153 | | 0.61 | 3 | | 0.327 | | 0.820 | 0.720 | |
| Back of Queue | (Q), ft/ | In (95 th percentile) | | | | | 39.2 | | 210. | .4 | | 159.9 | | 433.3 | 375.5 | |
| Back of Queue | (Q), ve | eh/In (95 th percenti | le) | | | | 1.6 | | 8.4 | | | 6.4 | | 17.3 | 15.0 | |
| Queue Storage | Ratio (| RQ) (95 th percent | ile) | | | 1 | 0.26 | | 0.0 | 0 | | 0.00 | | 0.00 | 0.00 | |
| Uniform Delay (| (d1), s | /veh | | | | | 31.7 | | 29.3 | 3 | | 11.6 | | 22.4 | 8.4 | |
| Incremental De | lay (d 2 |), s/veh | | | | 1 | 0.2 | | 1.1 | | | 0.9 | | 3.6 | 3.4 | |
| Initial Queue Delay (d z), s/veh | | | | | | | 0.0 | | 0.0 |) | | 0.0 | | 0.0 | 0.0 | |
| Control Delay (d), s/veh | | | | | | | 31.9 | | 30.4 | 4 | | 12.4 | | 26.0 | 11.8 | |
| Level of Service (LOS) | | | | | | | С | | С | | | В | | С | В | |
| Approach Delay | Approach Delay, s/veh / LOS | | | | | | 30.6 | | С | | 12.4 | | В | 17.1 | | В |
| Intersection De | ntersection Delay, s/veh / LOS | | | | | 18 | 3.3 | | | | | | | В | | |
| | | | | | | | | | | | | | | | | |
| Multimodal Re | sults | // 00 | | | EB | D | 0.0 | W | 8 | | 0.0 | NB | _ | 0.5 | SB | _ |
| Pedestrian LOS | Score | / LUS | | 2.1 | | В | 2.3 | | В | | 2.3 | | В | 0.7 | _ | A |
| BICYCIE LOS SC | ore / LC | 15 | | | | | | | F | | 1.0 | | А | 3.0 | | C |

| General Inform | nation | | | | | | | | | Inte | ersecti | ion Info | ormati | on | L. | 47411 | L. |
|--|--------------------------------|---------------------------|------|----------------------|---------------|-----|---------|----------|---------------|--------|-------------|----------|------------|------|------------|-----------|--------|
| Agency | | FMA | | | | | | | | Dui | ration, | h | 0.25 | | | . ↓ L | |
| Analvst | | Addie Kirkham | | Analvs | is Da | ate | Jun 3. | 2018 | | Are | ea Type | ; | Othe | r | | | \ |
| Jurisdiction | | City of Knoxville | | Time P | erioc | ł | Existir | na PM P | eak | PH | IF | | 0.94 | | - → * | W E | • , |
| Urban Street | | Washington Pike | | Analvs | is Ye | ar | 2018 | 5 | | Ana | alvsis F | Period | 1> 7: | 00 | 1 | | - |
| Intersection | | Washington Pike at Mill. | | File Na | ame | | Existir | na PM P | eak | Mill F | , Road.x | us | | | | tr | |
| Project Descrip | tion | 616.001 Legends at Wa | shir | ngton Pi | ke - I | Pha | ise 2 | 5 | | | | | | | | 11471 | * (* |
| ., | | | | J | - | | | | | | | | | | | | |
| Demand Inform | nation | | | | EE | В | | | ٧ | ٧B | | | NB | | | SB | |
| Approach Move | ement | | | L | Т | · | R | L | | Т | R | L | Т | R | L | Т | R |
| Demand (v), v | /eh/h | | | | | | | 67 | | | 555 | | 777 | 87 | 250 | 371 | |
| | | | | | 1 1: | | | | 1 | | | _ | _ | | | | |
| Signal Informa | ation | | | | 45 | | 17 | ~ ~ | | | | | Į | L | * - | | |
| Cycle, s | 150.0 | Reference Phase 2 | | | · | tal | | 1 e | | | | | | 1 | 2 | 3 | 4 |
| Offset, s | 0 | Reference Point En | d | Green | 72.0 | 0 | 18.0 | 42.0 | 0. | 0 | 0.0 | 0.0 | | | | | 5 |
| Uncoordinated | No | Simult. Gap E/W O | n | Yellow | 4.0 | | 4.0 | 4.0 | 0. | 0 | 0.0 | 0.0 | | | | | |
| Force Mode | Fixed | Simult. Gap N/S O | n | Red | 2.0 | | 2.0 | 2.0 | 0. | 0 | 0.0 | 0.0 | | 5 | 6 | 7 | 8 |
| | | | | EDI | | _ | DT | | | | (D.T. | | | NET | 0.51 | | 0.D.T. |
| Timer Results | | | _ | EBL | | E | BI | VVBI | - + | | BI | NBL | | NBI | SBI | - | SBI |
| Assigned Phase | e | | _ | | \rightarrow | | | | - | 3 | 8 | | + | 2 | 1 | | 6 |
| Case Number | | | _ | | \rightarrow | | | | - | 9. | .0 | | _ | 8.3 | 1.0 | | 4.0 |
| Phase Duration | n, s | \ \ | _ | | _ | | | <u> </u> | _ | 48 | 3.0 | | | 78.0 | 24.0 |) 1 | 02.0 |
| Change Period,(Y+ <i>R</i> ɛ), s Max Allow Headway(<i>MAH</i>), s | | | | | | | | <u> </u> | \rightarrow | 6. | .0 | | _ | 6.0 | 6.0 | | 6.0 |
| Max Allow Head | Max Allow Headway (MAH), s | | | | \rightarrow | | | <u> </u> | _ | 3. | .8 | | | 0.0 | 3.6 | | 0.0 |
| Queue Clearan | | e (gs), s | | | \rightarrow | | | | \rightarrow | 44 | 4.0 | | | | 20.0 |) | |
| Green Extensio | on lime | (ge), S | _ | | \rightarrow | | | | \rightarrow | 0. | .0 | | | 0.0 | 0.0 | | 0.0 |
| Phase Call Pro | bability | | | | \rightarrow | | | | | 1.0 | 00 | | | | 1.00 |) | |
| Max Out Proba | bility | | | | | | | | | 1.0 | 00 | | | | 1.00 |) | |
| Movement Gro | oup Res | sults | ٦ | | EB | 3 | | | W | В | | _ | NB | | | SB | |
| Approach Move | ement | | | L | Т | | R | L | Т | | R | L | Т | R | L | Т | R |
| Assigned Move | ment | | | | | | | 3 | | | 18 | | 2 | 12 | 1 | 6 | |
| Adjusted Flow I | Rate (v |), veh/h | | | | | | 71 | | | 590 | | 919 | | 266 | 395 | |
| Adjusted Satura | ation Flo | ow Rate (s), veh/h/ln | | | | | | 1810 | | 1 | 1610 | | 1866 | | 1810 | 1900 | |
| Queue Service | Time (| g s), S | | | | | | 4.4 | | | 42.0 | | 72.0 | | 18.0 | 14.2 | |
| Cycle Queue C | learanc | e Time (<i>g c</i>), s | | | | | | 4.4 | | | 42.0 | | 72.0 | | 18.0 | 14.2 | |
| Green Ratio (g | ŋ∕C) | | | | | | | 0.28 | | | 0.40 | | 0.48 | | 0.59 | 0.64 | |
| Capacity (c), v | /eh/h | | | | | | | 507 | | | 644 | | 896 | | 265 | 1216 | |
| Volume-to-Cap | acity Ra | itio (X) | | | | | | 0.141 | | 0 | 0.917 | | 1.026 | | 1.003 | 0.325 | |
| Back of Queue | (Q), ft | /In (95 th percentile) | | | | | | 90.3 | | 5 | 550.5 | | 1320. 5 | | 510.6 | 256.1 | |
| Back of Queue | (Q), ve | eh/In (95 th percentile) | | | | | | 3.6 | | | 22.0 | | 52.8 | | 20.4 | 10.2 | |
| Queue Storage | Ratio (| RQ) (95 th percentile) | | | | | | 0.60 | | | 0.00 | | 0.00 | | 0.00 | 0.00 | |
| Uniform Delay | (d 1), s | /veh | | | | | | 40.5 | | - | 42.6 | | 39.0 | | 64.4 | 12.3 | |
| Incremental Delay (<i>d</i> ₂), s/veh | | | | | | | | 0.1 | | | 17.9 | | 36.9 | | 56.1 | 0.7 | |
| Initial Queue Delay (d 3), s/veh | | | | | | | | 0.0 | | | 0.0 | | 0.0 | | 0.0 | 0.0 | |
| Control Delay (d), s/veh | | | | | | | | 40.6 | | | 60.5 | | 75.9 | | 120.4 | 13.0 | |
| Level of Service (LOS) | | | | | | | | D | | | E | | F | | F | В | |
| Approach Delay, s/veh / LOS | | | | 0.0 | | | | 58.4 | | E | E | 75.9 | | Е | 56.2 | 2 | Е |
| Intersection De | ntersection Delay, s/veh / LOS | | | | | | 64 | 1.9 | | | | | | | E | | |
| Multimodel De | eulte | | | | ED | 2 | | | 14/ | D | | | ND | | | CD | |
| Pedestrian LOS | Score | /105 | - | <u></u> | | , | B | 2.2 | VV | | B | 2.2 | ND | B | 0.7 | 30 | Δ |
| Riovela LOS Co | | | | 2.2 | | | 0 | 2.3 | | C | | 2.3 | | B | 0.7 | | |
| Dicycle LOS SC | | | | | | | | | | г | | 2.0 | | D | 1.0 | | D |

Attachment 6 Intersection Worksheets – Background AM/PM Peaks

| HCS7 Two-Way Stop-Control Report | | | | | | | | | | | |
|--|---|--------------------|-------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Washington @ Rising Oak | | | | | | | | |
| Agency/Co. | FMA | Jurisdiction | City of Knoxville | | | | | | | | |
| Date Performed | 6/3/2018 | East/West Street | Rising Oak Way | | | | | | | | |
| Analysis Year | 2021 | North/South Street | Washington Pike | | | | | | | | |
| Time Analyzed | Background AM Peak | Peak Hour Factor | 0.95 | | | | | | | | |
| Intersection Orientation | ersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | | |
| Project Description 616.001 Legends at Washington Pike - Phase 2 | | | | | | | | | | | |
| | | | | | | | | | | | |



Major Street: North-South

| Vehicle Volumes and Adj | ustme | ents | | | | | | | | | | | | | | |
|---|--------|---------|-------|-------|------|------|-------|---|----|-------|-------|---|----|-------|-------|----|
| Approach | | Eastb | ound | | | West | oound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 10 | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration | | | LR | | | | | | | L | Т | | | | | TR |
| Volume, V (veh/h) | | 40 | | 58 | | | | | | 5 | 242 | | | | 1022 | 17 |
| Percent Heavy Vehicles (%) | | 2 | | 2 | | | | | | 2 | | | | | | |
| Proportion Time Blocked | | 0.000 | | 0.000 | | | | | | 0.000 | | | | | | |
| Percent Grade (%) | | (| C | | | | | | | | | | | | | |
| Right Turn Channelized | | N | lo | | | Ν | 10 | | | Ν | lo | | | Ν | 10 | |
| Median Type/Storage | | | | Left | Only | | | | | | | | 5 | | | |
| Critical and Follow-up Headways | | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | 7.1 | | 6.2 | | | | | | 4.1 | | | | | | |
| Critical Headway (sec) | | 6.42 | | 6.22 | | | | | | 4.12 | | | | | | |
| Base Follow-Up Headway (sec) | | 3.5 | | 3.3 | | | | | | 2.2 | | | | | | |
| Follow-Up Headway (sec) | | 3.52 | | 3.32 | | | | | | 2.22 | | | | | | |
| Delay, Queue Length, and | d Leve | el of S | ervic | e | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | 103 | | | | | | | 5 | | | | | | |
| Capacity, c (veh/h) | | | 283 | | | | | | | 638 | | | | | | |
| v/c Ratio | | | 0.36 | | | | | | | 0.01 | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | 1.6 | | | | | | | 0.0 | | | | | | |
| Control Delay (s/veh) | | | 24.8 | | | | | | | 10.7 | | | | | | |
| Level of Service, LOS | | | С | | | | | | | В | | | | | | |
| Approach Delay (s/veh) | | 24.8 | | | | | | | | 0 | .2 | | | | | |
| Approach LOS | | (| 2 | | | | | | | | | | | | | |

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HCS7™ TWSC Version 7.2.1

Generated: 8/4/2018 2:49:03 PM

| HCS7 Two-Way Stop-Control Report | | | | | | | | | | | |
|--|--|--------------------|-------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Washington @ Rising Oak | | | | | | | | |
| Agency/Co. | FMA | Jurisdiction | City of Knoxville | | | | | | | | |
| Date Performed | 6/3/2018 | East/West Street | Rising Oak Way | | | | | | | | |
| Analysis Year | 2021 | North/South Street | Washington Pike | | | | | | | | |
| Time Analyzed | Background PM Peak | Peak Hour Factor | 0.84 | | | | | | | | |
| Intersection Orientation | rsection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | | |
| Project Description 616.001 Legends at Washington Pike - Phase 2 | | | | | | | | | | | |
| | | | | | | | | | | | |



Major Street: North-South

| Vehicle Volumes and Adj | ustme | ents | | | | | | | | | | | | | | |
|---|--------|---------|-------|-------|------|------|-------|---|----|-------|-------|---|----|-------|-------|----|
| Approach | | Eastb | ound | | | West | oound | | | North | bound | | | South | bound | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 10 | 1 | 2 | 3 | 4U | 4 | 5 | 6 |
| Number of Lanes | | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| Configuration | | | LR | | | | | | | L | Т | | | | | TR |
| Volume, V (veh/h) | | 7 | | 22 | | | | | | 38 | 979 | | | | 487 | 17 |
| Percent Heavy Vehicles (%) | | 2 | | 2 | | | | | | 2 | | | | | | |
| Proportion Time Blocked | | 0.100 | | 0.000 | | | | | | 0.000 | | | | | | |
| Percent Grade (%) | | (| C | | | | | | | | | | | | | |
| Right Turn Channelized | | N | lo | | | Ν | 10 | | | Ν | lo | | | Ν | lo | |
| Median Type/Storage | | | | Left | Only | | | | | | | | 5 | | | |
| Critical and Follow-up Headways | | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | 7.1 | | 6.2 | | | | | | 4.1 | | | | | | |
| Critical Headway (sec) | | 6.42 | | 6.22 | | | | | | 4.12 | | | | | | |
| Base Follow-Up Headway (sec) | | 3.5 | | 3.3 | | | | | | 2.2 | | | | | | |
| Follow-Up Headway (sec) | | 3.52 | | 3.32 | | | | | | 2.22 | | | | | | |
| Delay, Queue Length, and | d Leve | el of S | ervic | e | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | | 34 | | | | | | | 45 | | | | | | |
| Capacity, c (veh/h) | | | 409 | | | | | | | 976 | | | | | | |
| v/c Ratio | | | 0.08 | | | | | | | 0.05 | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | | 0.3 | | | | | | | 0.1 | | | | | | |
| Control Delay (s/veh) | | | 14.6 | | | | | | | 8.9 | | | | | | |
| Level of Service, LOS | | | В | | | | | | | А | | | | | | |
| Approach Delay (s/veh) | | 14 | 1.6 | | | | | | | 0 | .3 | | | | | |
| Approach LOS | | E | 3 | | | | | | | | | | | | | |

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| General Inform | nation | | | | | | | | Inters | ecti | on Info | ormatio | on | | 4741 | × (, |
|---|--------------------------------|-------------------------|---------|----------|--------|------------------|----------|-----|----------|---------|----------|---------|----------|---|---------------|------------------|
| Agency | allon | FMA | | | | | | | Durati | ion I | h | 0.25 | | | . ↓ Ľ | |
| Analyst | | Addie Kirkham | | Analys | is Dat | e Jun : | 3 2018 | | Area | Tvne | | Other | | -* -* | | |
| Jurisdiction | | City of Knoxville | | Time P | eriod | Back | around A | M | PHF | Typo | | 0.97 | | | ₩ ₩ + E | ~ _~ |
| | | | | | | Peak | | | | | | 0.07 | | 14 17 | | 1 1 1 1 |
| Urban Street | | Washington Pike | | Analys | is Yea | r 2021 | | | Analys | sis F | Period | 1> 7:0 | 00 | | * | |
| Intersection | | Washington Pike at | Mill | File Na | ime | Back | ground A | M P | eak Mill | Roa | ad.xus | | | The second se | 4 1 4 7 1 | * (* |
| Project Descrip | tion | 616.001 Legends a | t Washi | ngton Pi | ke - P | hase 2 | | | | | | | | | | |
| Demons d la ferra | | | | | 50 | | | | | | 1 | ND | | | 00 | |
| Demand Inform | nation | | | | EB | | <u> </u> | V | | D | | | | _ | SB | D |
| Approach Move | ement | | | <u> </u> | | ĸ | | + | | R C4 | <u> </u> | 070 | R CO | L | 070 | ĸ |
| Demand (V), V | /en/n | | | | | | 49 | | 2 | 64 | | 273 | 62 | 583 | 979 | |
| Signal Informa | ation | | | | L. | JL | 5 5 | 1 | | | | | t. | | | |
| Cycle, s | 90.0 | Reference Phase | 2 | 1 | | я ^{т ч} | - E | | | | | | _ | 7 | | |
| Offset, s | 0 | Reference Point | End | Croon | 46.0 | | 16.0 | | 0 0 | 0 | 0.0 | | 1 | 2 | 3 | 4 |
| Uncoordinated | No | Simult. Gap E/W | On | Yellow | 40.0 | 9.2 | 4 0 | 0 | 0 0 | 0 | 0.0 | - | | | | \rightarrow |
| Force Mode | Fixed | Simult. Gap N/S | On | Red | 2.0 | 2.0 | 2.0 | 0 | .0 0 | .0 | 0.0 | | 5 | 6 | 7 | 8 |
| | | | | 1. | | | | | | | | | | | | |
| Timer Results | imer Results | | | | | EBT | WB | L | WBT | • | NBL | - | NBT | SBI | _ | SBT |
| Assigned Phase | ssigned Phase | | | | | | | | 8 | | | | 2 | 1 | | 6 |
| Case Number | Case Number | | | | | | | | 9.0 | | | | 8.3 | 1.0 | | 4.0 |
| Phase Duration | hase Duration, s | | | | | | | | 22.0 | | | | 52.8 | 15.2 | 2 | 68.0 |
| Change Period | , (Y+R | c), S | | | | | | | 6.0 | | | | 6.0 | 6.0 | | 6.0 |
| Max Allow Hea | dway(<i>I</i> | MAH), s | | | | | | | 3.8 | | | | 0.0 | 3.6 | | 0.0 |
| Queue Clearan | ce Time | e (g s), s | | | | | | | 15.2 | | | | | 5.9 | | |
| Green Extensio | on Time | (g _e),s | | | | | | | 0.8 | | | | 0.0 | 3.3 | | 0.0 |
| Phase Call Pro | bability | | | | | | | | 1.00 | | | | | 1.00 |) | |
| Max Out Proba | bility | | | | | | | | 0.00 | | | | | 0.28 | 3 | |
| Movement Gro | | sulte | | | EB | | | \٨/ | 'B | | | NB | | | SB | |
| Approach Move | ement | build | | | т | R | | т Т | · R | | 1 | Т | R | 1 | Т | R |
| Assigned Move | mont | | | | - | | 3 | | 19 | 2 | - | 2 | 12 | 1 | 6 | |
| Adjusted Flow | Rate (v | () veh/h | | | | | 51 | | 27 | 2 | | 2/5 | 12 | 601 | 1009 | |
| Adjusted Satura | ation Flo |), ven/n | n | | | | 1810 | | 161 | 10 | | 1839 | | 1810 | 1900 | |
| Queue Service | Time (| (α_s) , s | | | | | 2.1 | | 13. | 2 | | 10.0 | | 3.9 | 31.7 | |
| Cvcle Queue C | learanc | e Time (<i>a</i> c). s | | | | | 2.1 | | 13. | .2 | | 10.0 | | 3.9 | 31.7 | |
| Green Ratio (g | r/C) | | | | | | 0.18 | | 0.2 | 28 | | 0.52 | | 0.60 | 0.69 | |
| Capacity (c), v | /eh/h | | | | | | 321 | | 45 | 0 | | 957 | | 672 | 1309 | |
| Volume-to-Cap | acity Ra | atio (X) | | | | | 0.157 | | 0.60 | 05 | | 0.361 | | 0.895 | 0.771 | |
| Back of Queue | (Q), ft | /In (95 th percentile) |) | | | | 41.5 | | 216 | 6.6 | | 182.7 | | 478.7 | 431.2 | |
| Back of Queue | (Q), ve | eh/In (95 th percenti | le) | | | | 1.7 | | 8.7 | 7 | | 7.3 | | 19.1 | 17.2 | |
| Queue Storage | Ratio (| RQ) (95 th percent | tile) | | | | 0.28 | | 0.0 | 0 | | 0.00 | | 0.00 | 0.00 | |
| Uniform Delay | (d 1), s | /veh | | | | | 31.3 | | 28. | .1 | | 12.7 | | 24.7 | 9.3 | |
| Incremental Delay (<i>d z</i>), s/veh | | | | | | | 0.2 | | 1.(| 0 | | 1.1 | | 8.3 | 4.4 | |
| Initial Queue Delay (d 3), s/veh | | | | | | | 0.0 | | 0.0 | 0 | | 0.0 | | 0.0 | 0.0 | |
| Control Delay (d), s/veh | | | | | | | 31.5 | | 29. | .1 | | 13.8 | | 33.0 | 13.7 | |
| Level of Service (LOS) | | | | | | | С | | C | | | В | | С | В | |
| Approach Delay, s/veh / LOS | | | | 0.0 | | | 29.5 | 5 | С | | 13.8 | | В | 20.9 |) | С |
| Intersection De | ntersection Delay, s/veh / LOS | | | | | 2 | 21.0 | | | | | | | С | | |
| Multimedal D- | oulto | | | | ED | | | 104 | D | | | | | | 00 | |
| Pedestrian LOS | Soore | /1.05 | | 0.1 | EB | P | | VV | P | | 2.2 | | B | 07 | 30 | Δ |
| Bicycle LOS Sc | core / I C |)S | | 2.1 | | 5 | 2.3 | | F | | 2.5 | | A | 3.1 | | C |
| , 5.0 _00 00 | | | | | | | | | | | | | · · | 0.1 | | - |

| General Inform | nation | | | | | | | | Inters | oction | n Info | rmatio | n | | 4241 | × (, |
|-----------------------------|--------------------------------|--------------------------|---------|----------|----------|--------|--------------------|-------|----------|--------|--------|---------------|----------|----------|-------|-----------|
| | ation | EMA | | | | | | | Duratio | on h | | 0.25 | /11 | | ţĻ | |
| Apolyet | | Addia Kirkham | | Apolyc | ic Dote | | 2019 | | | | | 0.20 Othor | | | | |
| Analyst | | | | Time D | | Bock | , 2010 around E | DN / | | ype | | | | | w + E | ₹_ |
| Junsaiction | | | | Timer | enou | Peak | | | | | | 0.94 | | A M | | |
| Urban Street | | Washington Pike | | Analys | is Year | 2021 | | | Analys | sis Pe | riod | 1> 7:0 | 0 | | * | |
| Intersection | | Washington Pike at | Mill | File Na | ime | Back | ground F | P M P | eak Mill | Road | l.xus | | | | 41491 | * 10 |
| Project Descrip | tion | 616.001 Legends a | t Washi | ngton Pi | ke - Pł | nase 2 | | | | | | | | | | |
| Demand Inform | nation | | | | EB | | | V | VB | | | NB | | | SB | |
| Approach Move | ement | | | L | Т | R | L | T · | T F | २ | L | Т | R | L | Т | R |
| Demand (v), v | /eh/h | | | | | | 71 | | 58 | 39 | | 825 | 92 | 265 | 394 | |
| | | | | 16 | | | | | | | | | | | | |
| Signal Informa | ation | | | | 1 | | R R | 4 | | | | | L | _ | | |
| Cycle, s | 150.0 | Reference Phase | 2 | | ti | | Ľ | | | | | | 1 | N | 2 | 4 |
| Offset, s | 0 | Reference Point | End | Green | 72.0 | 18.0 | 42.0 | 0. | 0 0. | 0 | 0.0 | | | | 5 | ĸ |
| Uncoordinated | No | Simult. Gap E/W | On | Yellow | 4.0 | 4.0 | 4.0 | 0. | 0 0. | 0 | 0.0 | | | | | ` |
| Force Mode | Fixed | Simult. Gap N/S | On | Red | 2.0 | 2.0 | 2.0 | 0. | 0 0. | 0 | 0.0 | | 5 | 6 | 7 | 8 |
| | | | | | | | | 11 | | | | Ŧ | | | T | |
| Timer Results | | EBL | | EBT | WB | - | WBT | | NBL | | NBT | SBL | - | SBT | | |
| Assigned Phase | е | | | | | | | | 8 | | | | 2 | 1 | | 6 |
| Case Number | | | | | | | | | 9.0 | | | | 8.3 | 1.0 | | 4.0 |
| Phase Duration | Phase Duration, s | | | | | | | | 48.0 | | | | 78.0 | 24.0 |) 1 | 02.0 |
| Change Period | Change Period, ($Y+Rc$), s | | | | | | | | 6.0 | | | | 6.0 | 6.0 | | 6.0 |
| Max Allow Hea | dway(<i>I</i> | MAH), s | | | | | | | 3.8 | | | | 0.0 | 3.6 | | 0.0 |
| Queue Clearan | ce Time | e (g s), s | | | | | | | 44.0 | | | | | 20.0 |) | |
| Green Extensio | on Time | (g _e),s | | | | | | | 0.0 | | | | 0.0 | 0.0 | | 0.0 |
| Phase Call Pro | bability | | | | | | | | 1.00 | | | | | 1.00 |) | |
| Max Out Proba | bility | | | | | | | | 1.00 | | | | | 1.00 |) | |
| Movement Gro | oup Res | sults | | | EB | | | W | В | Т | | NB | | | SB | |
| Approach Move | ement | | | L | Т | R | L | Т | R | | L | Т | R | L | Т | R |
| Assigned Move | ment | | | | | | 3 | | 18 | | | 2 | 12 | 1 | 6 | |
| Adjusted Flow I | Rate (v | ′), veh/h | | | | | 76 | | 627 | 7 | | 976 | | 282 | 419 | |
| Adjusted Satura | ation Flo | ow Rate (s), veh/h/l | n | | | | 1810 | | 161 | 0 | | 1866 | | 1810 | 1900 | |
| Queue Service | Time (g | g s), S | | | | | 4.7 | | 42.0 | 0 | | 72.0 | | 18.0 | 15.3 | |
| Cycle Queue C | learanc | e Time (<i>g c</i>), s | | | | | 4.7 | | 42.0 | 0 | | 72.0 | | 18.0 | 15.3 | |
| Green Ratio (g | r/C) | | | | | | 0.28 | | 0.40 | 0 | | 0.48 | | 0.59 | 0.64 | |
| Capacity (c), v | /eh/h | | | | | | 507 | | 644 | 1 | | 896 | | 265 | 1216 | |
| Volume-to-Cap | acity Ra | atio (X) | | | | | 0.149 | | 0.97 | '3 | | 1.089 | | 1.063 | 0.345 | |
| Back of Queue | (Q), ft/ | /In (95 th percentile) | | | | | 96 | | 669. | .1 | | 1534. 9 | | 563 | 272.5 | |
| Back of Queue | (Q), ve | eh/In (95 th percenti | le) | | | | 3.8 | | 26.8 | 8 | | 61.4 | | 22.5 | 10.9 | |
| Queue Storage | Ratio (| RQ) (95 th percent | ile) | | | | 0.64 | | 0.00 | 0 | | 0.00 | | 0.00 | 0.00 | |
| Uniform Delay | (d1), s | /veh | | | | | 40.6 | | 44.2 | 2 | | 39.0 | | 64.4 | 12.5 | |
| Incremental De | | | | | 0.1 | | 28.6 | 6 | | 57.2 | | 73.0 | 0.8 | | | |
| Initial Queue D | | | | | 0.0 | | 0.0 |) | | 0.0 | | 0.0 | 0.0 | | | |
| Control Delay (| | | | | 40.7 | | 72.8 | 8 | | 96.2 | | 137.3 | 13.2 | | | |
| Level of Service (LOS) | | | | | | | D | | E | | | F | | F | В | |
| Approach Delay, s/veh / LOS | | | | 0.0 | | | 69.3 | 6 | E | | 96.2 | | F | 63.2 | 2 | E |
| Intersection De | ntersection Delay, s/veh / LOS | | | | | 7 | 8.6 | | | | | | | E | | |
| Multiment | | | | | | | | 14/ | D | | | | | | 00 | |
| Nuttimodal Re | suits | (1.02 | | 0.0 | EB | | 0.0 | VV | | | 0.0 | NB | | 0.7 | 58 | ^ |
| Pedestrian LOS | S Score | / 105 | | 2.2 | | В | 2.3 | | Б | | 2.3 | | В | 0.7 | | A |
| BICYCIE LOS SC | ore / LC | 75 | | | | | | | F | | 2.1 | | В | 1.6 | | В |

Attachment 7 Intersection Worksheets – Full Buildout AM/PM Peaks

| HCS7 Two-Way Stop-Control Report | | | | | | | | | | | |
|--|-----------------------|--------------------|-------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Washington @ Rising Oak | | | | | | | | |
| Agency/Co. | FMA | Jurisdiction | City of Knoxville | | | | | | | | |
| Date Performed | 6/3/2018 | East/West Street | Rising Oak Way | | | | | | | | |
| Analysis Year | 2021 | North/South Street | Washington Pike | | | | | | | | |
| Time Analyzed | Full Buildout AM Peak | Peak Hour Factor | 0.95 | | | | | | | | |
| Intersection Orientation North-South Analysis Time Period (hrs) 0.25 | | | | | | | | | | | |
| Project Description 616.001 Legends at Washington Pike - Phase 2 | | | | | | | | | | | |
| | | | | | | | | | | | |



Major Street: North-South

| Vehicle Volumes and Adj | ustmo | ents | | | | | | | | | | | | | | | |
|---|--------|---------|-------|-------|------|------|-------|---|-----|-------|-------|---|----|-------|-------|----|--|
| Approach | | Eastb | ound | | | West | bound | | | North | bound | | | South | bound | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 1U | 1 | 2 | 3 | 4U | 4 | 5 | 6 | |
| Number of Lanes | | 1 | 0 | 1 | | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | |
| Configuration | | L | | R | | | | | | L | Т | | | | Т | R | |
| Volume, V (veh/h) | | 96 | | 138 | | | | | | 16 | 242 | | | | 1022 | 50 | |
| Percent Heavy Vehicles (%) | | 2 | | 2 | | | | | | 2 | | | | | | | |
| Proportion Time Blocked | | 0.000 | | 0.000 | | | | | | 0.000 | | | | | | | |
| Percent Grade (%) | 0 | | | | | | | | | | | | | | | | |
| Right Turn Channelized | | N | lo | | | Ν | 10 | | | Ν | lo | | No | | | | |
| Median Type/Storage | | | | Left | Only | | | | | | | | 5 | | | | |
| Critical and Follow-up He | eadwa | iys | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | 7.1 | | 6.2 | | | | | | 4.1 | | | | | | | |
| Critical Headway (sec) | | 6.42 | | 6.22 | | | | | | 4.12 | | | | | | | |
| Base Follow-Up Headway (sec) | | 3.5 | | 3.3 | | | | | | 2.2 | | | | | | | |
| Follow-Up Headway (sec) | | 3.52 | | 3.32 | | | | | | 2.22 | | | | | | | |
| Delay, Queue Length, and | d Leve | el of S | ervic | е | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | 101 | | 145 | | | | | | 17 | | | | | | | |
| Capacity, c (veh/h) | | 321 | | 266 | | | | | | 619 | | | | | | | |
| v/c Ratio | | 0.31 | | 0.54 | | | | | | 0.03 | | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | 1.3 | | 3.0 | | | | | | 0.1 | | | | | | | |
| Control Delay (s/veh) | | 21.3 | | 33.5 | | | | | | 11.0 | | | | | | | |
| Level of Service, LOS | | С | | D | | | | | | В | | | | | | | |
| Approach Delay (s/veh) | | 28 | 3.5 | | | - | - | | 0.7 | | | | | | | | |
| Approach LOS | | [|) | | | | | | | | | | | | | | |

| HCS7 Two-Way Stop-Control Report | | | | | | | | | | | |
|----------------------------------|--|----------------------------|-------------------------|--|--|--|--|--|--|--|--|
| General Information | | Site Information | | | | | | | | | |
| Analyst | Addie Kirkham | Intersection | Washington @ Rising Oak | | | | | | | | |
| Agency/Co. | FMA | Jurisdiction | City of Knoxville | | | | | | | | |
| Date Performed | 6/3/2018 | East/West Street | Rising Oak Way | | | | | | | | |
| Analysis Year | 2021 | North/South Street | Washington Pike | | | | | | | | |
| Time Analyzed | Full Buildout PM Peak | Peak Hour Factor | 0.84 | | | | | | | | |
| Intersection Orientation | North-South | Analysis Time Period (hrs) | 0.25 | | | | | | | | |
| Project Description | 616.001 Legends at Washington Pike - Phase | 2 | | | | | | | | | |
| | | | | | | | | | | | |



Major Street: North-South

| Vehicle Volumes and Adj | ustme | ents | | | | | | | | | | | | | | | | |
|---|--------|---------|-------|-------|------|-----------|----|---|-----|-------|-------|---|----|-------|-------|----|--|--|
| Approach | | Eastb | ound | | | Westbound | | | | North | bound | | | South | bound | | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | | |
| Priority | | 10 | 11 | 12 | | 7 | 8 | 9 | 10 | 1 | 2 | 3 | 4U | 4 | 5 | 6 | | |
| Number of Lanes | | 1 | 0 | 1 | | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 1 | | |
| Configuration | | L | | R | | | | | | L | Т | | | | Т | R | | |
| Volume, V (veh/h) | | 30 | | 93 | | | | | | 140 | 979 | | | | 487 | 63 | | |
| Percent Heavy Vehicles (%) | | 2 | | 2 | | | | | | 2 | | | | | | | | |
| Proportion Time Blocked | | 0.100 | | 0.000 | | | | | | 0.000 | | | | | | | | |
| Percent Grade (%) | | 0 | | | | | | | | | | | | | | | | |
| Right Turn Channelized | | No | | | | Ν | 10 | | No | | | | No | | | | | |
| Median Type/Storage | | | | Left | Only | | | | | | | | 5 | | | | | |
| Critical and Follow-up He | eadwa | iys | | | | | | | | | | | | | | | | |
| Base Critical Headway (sec) | | 7.1 | | 6.2 | | | | | | 4.1 | | | | | | | | |
| Critical Headway (sec) | | 6.42 | | 6.22 | | | | | | 4.12 | | | | | | | | |
| Base Follow-Up Headway (sec) | | 3.5 | | 3.3 | | | | | | 2.2 | | | | | | | | |
| Follow-Up Headway (sec) | | 3.52 | | 3.32 | | | | | | 2.22 | | | | | | | | |
| Delay, Queue Length, and | d Leve | el of S | ervic | e | | | | | | | | | | | | | | |
| Flow Rate, v (veh/h) | | 36 | | 111 | | | | | | 167 | | | | | | | | |
| Capacity, c (veh/h) | | 164 | | 514 | | | | | | 932 | | | | | | | | |
| v/c Ratio | | 0.22 | | 0.22 | | | | | | 0.18 | | | | | | | | |
| 95% Queue Length, Q ₉₅ (veh) | | 0.8 | | 0.8 | | | | | | 0.7 | | | | | | | | |
| Control Delay (s/veh) | | 32.9 | | 13.9 | | | | | | 9.7 | | | | | | | | |
| Level of Service, LOS | | D | | В | | | | | | А | | | | | | | | |
| Approach Delay (s/veh) | | 18 | 3.6 | | | | | | 1.2 | | | | | | | | | |
| Approach LOS | | (| 2 | | | | | | | | | | | | | | | |

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HCS7[™] TWSC Version 7.2.1

| General Inform | nation | | | | | | | | | Inte | ersecti | ion Infe | ormati | on | | 47411 | L. |
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| Analyst | | Addie Kirkham | | Analys | is Dat | | 3 | 2018 | | Διο | a Type | <u>دا</u> | Othe | r | -* | | ч. А |
| Jurisdiction | | City of Knoxville | | Time Period Full | | | i 5, I Ri | uildout A | PHE | F | | 0 97 | | - → * | w‡e | •* | |
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| Project Descrip | tion | 616.001 Legends a | t Washi | ngton Pi | ke - P | hase 2 | 2 | | | | | | | | | | |
| Demand Inform | nation | | | | ER | | | | V | /B | | 1 | NB | | | SB | |
| Approach Movement | | | 1 | Т | F | 2 | | V | т | R | | Т | R | 1 | Т | R | |
| Demand (y) yeb/b | | | <u> </u> | | + ' | ` ` | 51 | ┢ | <u> </u> | 264 | | 310 | 72 | 583 | 1010 | | |
| | en/m | | | | | | | 51 | | | 204 | | 513 | 12 | 505 | 1010 | |
| Signal Informa | tion | | | | | ŢŢ | 5. | 7 | - | | | | | Ĺ | • | | |
| Cycle, s | 90.0 | Reference Phase | 2 | | • ا | | | Ľ | 1 | | | | | | P | | |
| Offset, s | 0 | Reference Point | End | Green | 447 | 11 | 8 | 15.5 | 0 | 0 | 0.0 | 0.0 | | 1 | 2 | 3 | 4 |
| Uncoordinated | No | Simult. Gap E/W | On | Yellow | 4.0 | 4.0 |) | 4.0 | 0. | 0 | 0.0 | 0.0 | | | | | \sim |
| Force Mode | Fixed | Simult. Gap N/S | On | Red | 2.0 | 2.0 |) | 2.0 | 0. | 0 | 0.0 | 0.0 | | 5 | 6 | 7 | 8 |
| | | | | | Ŧ | | | | | | | | Ŧ | | 7 | | |
| Timer Results | | | | EBL | · | EBT | | WBL | - | WE | BT | NBL | - | NBT | SBI | | SBT |
| Assigned Phase | e | | | | | | 4 | | | 8 | 3 | | | 2 | 1 | | 6 |
| Case Number | | | | | | | | | | 9. | .0 | | | 8.3 | 1.0 | | 4.0 |
| Phase Duration | , S | | | | | | 4 | | | 21 | .5 | | | 50.7 | 17.8 | 3 | 58.5 |
| Change Period, (Y+R c), s | | | | | | | | | 6. | .0 | | | 6.0 | 6.0 | | 6.0 | |
| Max Allow Headway (MAH), s | | | | | _ | | | 3. | .8 | | | 0.0 | 3.6 | | 0.0 | | |
| Queue Clearance Time (g_s), s | | | | | | | | 14 | .8 | | | | 10.2 | 2 | | | |
| Green Extension Time (g_e), s | | | | | | _ | | _ | 0. | .7 | | | 0.0 | 1.6 | | 0.0 | |
| Phase Call Prol | bability | | | | | | | | | 1.0 | 00 | | | | 1.00 |) | |
| Max Out Proba | bility | | | | | | | | | 0.0 | 02 | | | | 0.46 | 5 | |
| Movement Gro | oup Res | sults | | EB | | | | | W | В | | | NB | | | SB | |
| Approach Move | ement | | | L | Т | R | | L | Т | | R | L | Т | R | L | Т | R |
| Assigned Move | ment | | | | | | | 3 | | | 18 | | 2 | 12 | 1 | 6 | |
| Adjusted Flow F | Rate (v |), veh/h | | | | | | 53 | | | 272 | | 403 | 1 | 601 | 1041 | |
| Adjusted Satura | ation Flo | w Rate (s), veh/h/l | n | | | | | 1810 | | 1 | 610 | | 1839 | | 1810 | 1900 | |
| Queue Service | Time (g | g s), S | | | | | | 2.2 | | 1 | 12.8 | | 12.7 | | 8.2 | 33.3 | |
| Cycle Queue C | learanc | e Time (<i>g c</i>), s | | | | | | 2.2 | | 1 | 12.8 | | 12.7 | | 8.2 | 33.3 | |
| Green Ratio (g | /C) | | | | | | | 0.17 | | 0 | 0.30 | | 0.50 | | 0.61 | 0.69 | |
| Capacity (c), v | /eh/h | | | | | | | 311 | | 4 | 488 | | 914 | | 649 | 1320 | |
| Volume-to-Capa | acity Ra | tio(X) | | | | | | 0.169 | | 0 | .557 | | 0.441 | | 0.925 | 0.789 | |
| Back of Queue | (Q), ft/ | In (95 th percentile) | | | | | | 43.6 | | 2 | 209.4 | | 226 | | 503.4 | 447.9 | |
| Back of Queue | (Q), ve | eh/In (95 th percenti | le) | | | | _ | 1.7 | | _ | 8.4 | | 9.0 | | 20.1 | 17.9 | |
| Queue Storage | Ratio (| RQ) (95 th percent | ile) | | | | 4 | 0.29 | | 0 | 0.00 | | 0.00 | | 0.00 | 0.00 | |
| Uniform Delay (| (d1), S | /veh | | | | | 4 | 31.8 | | - 2 | 26.3 | | 14.6 | | 26.4 | 9.3 | |
| Incremental Delay (d_2), s/veh | | | | | _ | - | 0.2 | | | 0.7 | | 1.5 | | 13.1 | 4.9 | | |
| Initial Queue Delay (d 3), s/veh | | | | | | | 0.0 | | | 0.0 | | 0.0 | | 0.0 | 0.0 | | |
| Control Delay (α), s/veh | | | | | | | 32.0 | | | 21.0 | | 10.1 D | | 39.5 | 14.1 D | | |
| Level of Service (LOS) | | | | | | | | | | | 16.4 | В | D | | В | <u> </u> | |
| Approaction Delay | y, s/ven | / LUS | | 0.0 | | | 22 | 27.8 8 | | | | 10.1 | | D | 23.4 C | | U |
| milersection De | iay, 5/VE | an / LOS | | | | | 22 | .0 | | | | | | | | | |
| Multimodal Re | sults | | | | EB | | | | W | В | | | NB | | | SB | |
| Pedestrian LOS | Score | / LOS | | 2.1 | | В | | 2.3 | | В | 3 | 2.3 | | В | 0.7 | | А |
| Bicycle LOS Sc | ore / LC | DS | | | | | | | | F | - | 1.2 | | А | 3.2 | | С |

| | | | l eig | | u III | | 000 | | | anto | oan | inner j | , | | | | |
|-------------------------------------|------------------|--------------------------|----------|---------------|---------------|-----------|--------------|------------------|----------|--------|---------|----------|------------|------------|------------|---------------|---------|
| General Inform | nation | | | | | | | | | Into | rsoct | ion Infr | ormati | 2 2 | | 4741 | L. |
| | lation | | | | | | | | | Dur | ation | | 0.25 | 511 | | ĻĻ | |
| Appliet | | Addia Kirkham | | Analyza | | to l | 1.00.2 | 2010 | | Area | | | Otho | | | | 1. A |
| Analyst | | | | | Time Period | | | Full Buildout PM | | | | | | | - | "Ĭ. | • |
| Junsaiction | | City of Knoxville | | Time P | renoo | 1 | Peak | | | | | | 0.94 | | 14 14 1 | | |
| Urban Street | | Washington Pike | | Analys | 2021 | | | Ana | alysis F | Period | 1> 7: | 00 | | * | | | |
| Intersection | | Washington Pike at | Mill | File Na | ame | | Full B | uildout F | PM P | eak N | Mill Ro | ad.xus | | | | * 1 *** *** 1 | · /* |
| Project Descrip | tion | 616.001 Legends a | t Washi | ngton Pi | ke - F | Pha | se 2 | | | | | | | | | | |
| Demand Inform | nation | | | | EE | 3 | | | V | VB | | | NB | | | SB | |
| Approach Move | ement | | | L | Т | · | R | L | <u> </u> | Т | R | L | Т | R | L | Т | R |
| Demand (v), veh/h | | | | | | | 78 | | | 589 | | 846 | 94 | 265 | 433 | | |
| 0 | <i></i> | | | r | 1 | | | | 1 | | | _ | | • | | | |
| Signal Informa | | Defenses Dises | 0 | | +s | • | $\uparrow P$ | S () | 1 | | | | Į | | t a | | |
| Cycle, s | 150.0 | Reference Phase | 2 | - | · | <u>†7</u> | | Ľ | | | | | | 1 | 2 | 3 | 4 |
| Offset, s | 0 | Reference Point | End | Green | 72.0 | 0 | 18.0 | 42.0 | 0. | 0 | 0.0 | 0.0 | | | | | ~ |
| Uncoordinated | No | Simult. Gap E/W | On | Yellow | 4.0 | | 4.0 | 4.0 | 0. | 0 | 0.0 | 0.0 | _ | | | | |
| Force Mode | Fixed | Simult. Gap N/S | On | Red | 2.0 | | 2.0 | 2.0 | 0. | 0 | 0.0 | 0.0 | | 5 | 6 | 7 | 8 |
| Times Desults | | | _ | EDI | _ | - | DT | | 1 | 14/5 | DT | NDI | _ | NDT | | _ | ODT |
| Timer Results | | | | EBL | | E | BI | VVBL | - | VVE | Ы | NBL | | NBI | SBL | - | SBI |
| Assigned Phase | | | | | \rightarrow | | | <u> </u> | _ | 8 | 6 | | _ | 2 | 1 | _ | 6 |
| Case Number | | | | <u> </u> | | | | <u> </u> | | 9.0 | 0 | | | 8.3 | 1.0 | | 4.0 |
| Phase Duration | i, S | | | | _ | | | | _ | 48 | .0 | | | 78.0 | 24.0 |) 1 | 02.0 |
| Change Period, (Y+R c), s | | | <u> </u> | | | | <u> </u> | | 6. | 0 | | | 6.0 | 6.0 | _ | 6.0 | |
| Max Allow Headway (MAH), s | | | | _ | | | | _ | 3. | 8 | | | 0.0 | 3.6 | | 0.0 | |
| Queue Clearance Time (g_s), s | | | | _ | | | | _ | 44 | .0 | | _ | | 20.0 |) | | |
| Green Extension Time (ge), s | | | | \rightarrow | | | | | 0. | 0 | | _ | 0.0 | 0.0 | | 0.0 | |
| Phase Call Probability | | | | | | | | | _ | 1.0 | 00 | | | | 1.00 |) | |
| Max Out Proba | bility | | | | | | | | | 1.0 | 00 | | | | 1.00 | | |
| Movement Gro | oup Res | sults | | | EB | 3 | | | W | В | | | NB | | | SB | |
| Approach Move | ement | | | L | Т | | R | L | Т | | R | L | Т | R | L | Т | R |
| Assigned Move | ment | | | | | | | 3 | | | 18 | | 2 | 12 | 1 | 6 | |
| Adjusted Flow F | Rate (v |), veh/h | | | | | | 83 | | (| 627 | | 1000 | | 282 | 461 | |
| Adjusted Satura | ation Flo | ow Rate (s), veh/h/l | n | | | | | 1810 | | 1 | 610 | | 1866 | | 1810 | 1900 | |
| Queue Service | Time (g | g s), s | | | | | | 5.2 | | 4 | 12.0 | | 72.0 | | 18.0 | 17.3 | |
| Cycle Queue C | learanc | e Time (<i>g</i> c), s | | | | | | 5.2 | | 4 | 12.0 | | 72.0 | | 18.0 | 17.3 | |
| Green Ratio (g | ı/C) | | | | | | | 0.28 | | C | 0.40 | | 0.48 | | 0.59 | 0.64 | |
| Capacity (c), v | /eh/h | | | | | | | 507 | | (| 644 | | 896 | | 265 | 1216 | |
| Volume-to-Capa | acity Ra | itio(X) | | | | | | 0.164 | | 0 | .973 | | 1.116 | | 1.063 | 0.379 | |
| Back of Queue | (Q), ft/ | In (95 th percentile) | | | | | | 105.9 | | 6 | 69.2 | | 1639. 1 | | 563 | 301.3 | |
| Back of Queue | (Q), ve | eh/In (95 th percenti | le) | | | | _ | 4.2 | | 2 | 26.8 | | 65.6 | | 22.5 | 12.1 | |
| Queue Storage | Ratio (| RQ) (95 th percent | ile) | | | + | | 0.71 | | C | 0.00 | | 0.00 | | 0.00 | 0.00 | |
| Uniform Delay (| (d1), s | /veh | - / | | | | | 40.7 | | 4 | 14.2 | | 39.0 | | 64.4 | 12.8 | |
| Incremental De | lay (<i>d</i> 2 |), s/veh | | | | + | | 0.1 | | 2 | 28.6 | | 67.3 | | 73.0 | 0.9 | |
| Initial Queue Delay (d_2) , siven | | | | | + | | 0.0 | | | 0.0 | | 0.0 | | 0.0 | 0.0 | | |
| Control Delay (<i>d</i>), s/veh | | | | | + | | 40.9 | | 7 | 72.8 | | 106.3 | | 137.3 | 13.7 | | |
| Level of Service (LOS) | | | | | + | | D | | | E | | F | | F | В | | |
| Approach Delay, s/veh / LOS | | | 0.0 | | | | 69.1 | | E | | 106.3 | 3 | F | 60.7 | · | E | |
| Intersection De | lay, s/ve | eh / LOS | | | | | 81 | .7 | | | | | | | F | | |
| | | | | | | | | | | | 1 | | | | | | |
| Multimodal Re | sults | | | | EB | 3 | | | W | В | | NB | | B | | SB | |
| Pedestrian LOS | S Score | / LOS | | 2.2 | | | В | 2.3 | | В | 3 | 2.3 | | В | 0.7 | | A |
| Bicycle LOS Sc | ore / LC | DS | | | | | | | | F | - | 2.1 | | В | 1.7 | | В |

Attachment 8 Turn Lane Warrant Analysis

Project: Legends at Washington Pike - Phase 2

| Washington Pike | VOLUMES | | | | |
|-------------------|---------|------|----|--------|-------------|
| at Rising Oak Way | | | | | |
| RIGHT TURN | | Thru | RT | RT MAX | Warrant Met |
| AM | _ | 1022 | 50 | 25 | YES |
| PM | | 487 | 63 | 49 | NO |

Washington Pike at Rising Oak Way

TABLE 5B

RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH

| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | | | | | | | | |
|-------------------------------------|--|---------------------------------------|------------|------------|------------|------------|--|--|--|--|--|--|--|--|
| VOLUME | < 100 | 100 - 199 | 200 - 249 | 250 - 299 | 300 - 349 | 350 - 399 | | | | | | | | |
| Fewer Than 25 25 - 49 50 - 99 | | | | | | | | | | | | | | |
| 100 - 149 150 - 199 | | · · · · · · · · · · · · · · · · · · · | ļ | | | <u> </u> | | | | | | | | |
| 200 - 249 250 - 299 | | | <u> </u> | <u> </u> | Yes | Yes Yes | | | | | | | | |
| 300 - 349 350 - 399 | | | Yes | Ves Yes | Yes Yes | Yes Yes | | | | | | | | |
| 400 - 449 450 - 499 | | Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | | | | | | | |
| 500 - 549 550 - 599 | Yes | Ves Yes | Yes Yes | Yts Yes | Yes Yes | Yes Yes | | | | | | | | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | | | | | | | | |

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| RIGHT-TURN | THROUGH VOLUME PLUS LEFT-TURN VOLUME * | | | | | | | | | | | |
|-------------------------------------|--|------------|------------|------------|---------------|------------|--|--|--|--|--|--|
| VOLUME | 350 - 399 | 400 - 449 | 450 - 499 | 500 - 549 | 550 - 600 | + / > 600 | | | | | | |
| Fewer Than 25 25 - 49 50 - 99 | | PM Peak | 63 RT | Yes | Yes Yes | Yes | | | | | | |
| 100 - 149 150 - 199 | | Yes | Yes Yes | Yes Yes | AM Pea Yes | ak 50 RT | | | | | | |
| 200 - 249 250 - 299 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | | | | | |
| 300 - 349 350 - 399 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | | | | | |
| 400 - 449 450 - 499 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | | | | | |
| 500 - 549 550 - 599 | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | Yes Yes | | | | | | |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes | | | | | | |

* Or through volume only if a left-turn lane exists.



| Attachment 9 | |
|----------------------|--|
| Aerial Photos | |



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Washington Pike at Rising Oak Way



Knoxville - Knox County - KUB Geographic Information System

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Date: August 6, 2018

Project Name: Legends at Washington Pike – Phase 2

To: MPC and City of Knoxville Engineering Department

Subject: TIS Comment Response Document for the Legends at Washington Pike – Phase 2 Review Comments Dated August 2, 2018.

Dear MPC and City of Knoxville staff,

The following comment response document is submitted to address comments dated August 2, 2018:

<u>Reviewer Comment:</u> On page 3 under Washington Pike at Rising Oak Way, correct the first paragraph to read "the eastbound approach exiting the development will operate at a LOS F". In the second paragraph capitalize 'Pike'.

Response: Added "exiting the development" and capitalized "Pike".

Reviewer Comment: In the last paragraph of this page, the report says a LOS E during the PM at the signalized intersection of Washington Pike and Mill Road. With a delay of this type, there needs to be recommended mitigations if this is due to the development. Also, existing timing should be used at the signal and should not be optimized.

<u>Response:</u> Removed the optimized signal timing from the report and added "FMA does not recommend any improvements to the intersection of Washington Pike at Mill Road as a part of the Legends at Washington Pike – Phase 2 development. The highest delay from this intersection is a result of the southbound left turn lane on Washington Pike which is not affected by this development."

Reviewer Comment: On page 7, mention that Rising Oak Way is a private road. Mention in the third paragraph what the required sight distance is for the intersection of Washington Pike at Rising Oak Way. At the end of this paragraph, remove the last sentence discussing sight distance measured 20 ft back from the edge of pavement. City of Knoxville policy is 15 ft from the edge of pavement and that is already discussed.

<u>Response</u>: Added "Rising Oak Way is a two-lane private road" and "The minimum required sight distance for a road with a posted speed limit of 40 mph is 400 feet in each direction in accordance with the "Subdivision Regulations" for Knoxville and Knox County." to page 7 and removed the last sentence regarding sight distance measured from 20 ft back.

Ms. Barrett August 6, 2018 Page 2 of 4

Reviewer Comment: In Figure 3 (pg 9), correct the through AM westbound traffic at the intersection of Washington Pike and Rising Oak Way. The TMC for this direction is different than what is in the Figure.

<u>Response:</u> Revised Figure 3 to match the TMC at the intersection of Washington Pike at Rising Oak Way.

Reviewer Comment: On page 10 fourth paragraph, the report mentioned 2% annual growth rate was used at the intersection of Washington Pike at Rising Oak Way. After review of this in the appendix, the review team noticed 3% was used. Please check.

<u>Response:</u> The 2% growth rate at the intersection of Washington Pike at Rising Oak Way is correct. I updated Figure 4 to reflect the changes.

Reviewer Comment: Figure 4 on page 11 needs to be corrected if this is the case.

<u>Response:</u> Revised Figure 4 to show 2% growth rate at the intersection of Washington Pike at Rising Oak Way.

Reviewer Comment: In Table 4-1 (pg 12), correct the Weekday Total Local Apartment Trips. The table says 573 trips, but the equation gives 754 trips. This would also change the Total Combined trips.

Response: Revised Table 4-1 with the correct weekday total local apartment trips.

Reviewer Comment: For Full Buildout in Table 5-1, show LOS summary for existing and optimized timing plans. Please provide signal timing plan for optimized if used.

Response: Removed the optimized signal timing from the report.

Reviewer Comment: For Washington Pike at Rising Oak Way (Full Buildout 2021), please correct the approach in the PM Peak from SB to NB. This would be consistent with the HCS worksheets.

<u>Response:</u> Revised Table 5-1 for Washington Pike at Rising Oak Way (Full Buildout 2021) to NB approach.

Reviewer Comment: In the Turn Lane Warrant Analysis (pg 20), please provide discussion on if there is enough ROW for the recommended right-turn lane. What are storage and bay taper dimensions?

<u>Response:</u> Added "The right-of-way for Washington Pike at the intersection with Rising Oak Way is 88 feet per the Major Road Plan. There is approximately 10 feet between the edge of pavement and the property line for the Oak Grove Zion Church therefore; the owner may need to acquire property from the Oak Grove Zion Church in order to install a right turn lane. Per AASHTO "A Policy on
Geometric Design of Highways and Streets" the recommended storage length for the right turn lane is three car lengths (approximately 75 feet) and the recommended taper length is 100 feet." to the turn lane warrant analysis.

Reviewer Comment: In the Conclusions and Recommendations second paragraph (pg 20), please provide a queue length for the blocked driveway.

<u>Response:</u> Added the following to the Conclusions and Recommendations "The signalized intersection capacity analysis for the intersection of Washington Pike at Mill Road shows an existing 95% queue length for the northbound approach of 159.9 feet during the AM peak hour and 1320.5 feet during the PM peak hour."

Reviewer Comment: On page 21 first paragraph first sentence, which right-turn lane is being discussed?

<u>Response:</u> Revised to say "A turn lane warrant is met for a southbound right turn lane on Washington Pike"

Reviewer Comment: In second paragraph, remove "Minimum" from "Minimum Subdivision Regulations".

Response: Removed the word "Minimum".

Reviewer Comment: In third paragraph, the report recommends landscaping to be minimum to keep sight distance at intersection. Does the sight distance line extend onto private property? Show in a diagram with the turn lane and dimensions.

Response: Added a diagram to Attachment 8.

Reviewer Comment: Under Washington Pike at Mill Road, mention if there are improvements recommended or not and use the existing timing plan at this location, not optimized. This can be received through the City of Knoxville Traffic Office.

<u>Response:</u> Added "FMA does not recommend any improvements to the intersection of Washington Pike at Mill Road as a part of the Legends at Washington Pike – Phase 2 development. The highest delay from this intersection is a result of the southbound left turn lane on Washington Pike which is not affected by this development."

Ms. Barrett August 6, 2018 Page 4 of 4

Sincerely,



Addie Kirkham, P.E.