

## Transportation Impact Study The Highlands at Clear Spring Knoxville, TENNESSEE

## -Prepared For-

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## EXECUTIVE SUMMARY

## Preface:

Trans South Properties, GP is proposing to develop a subsequent phase of an existing residential development that is nearby to Millertown Pike in northeast Knoxville, TN. The name of this subsequent proposed residential development is "The Highlands at Clear Spring". The initial phase of this residential development was originally approved in 2006 and dozens of homes have been constructed in Phase 1 of the development. The initial phase, Phase 1, ultimately included 111 single-family residential detached lots, 8 condominium units, 14 townhouses and is named Clear Springs Plantation. A concept plan for the subsequent phase, Phase 2, of the development has been submitted to allow for further residential home construction adjacent to Phase 1. With the addition of up to 160 single-family residential detached lots in Phase 2, this report addresses the transportation impacts of both existing Phase 1 and proposed Phase 2 of the entire residential development. The purpose of this study is to determine and evaluate the potential impacts of the residential development on the adjacent transportation system. The study includes a review of the operating characteristics of the transportation system that will provide access to the proposed site. Recommendations and mitigation measures will be analyzed and offered where traffic operations have been estimated to be below traffic engineering standards.

## Study Results:

The findings of this study include the following:

- At full build-out, the Clear Spring residential development of both phases is expected to generate approximately 2,801 new trips on an average weekday. Approximately 216 of these new trips are estimated to occur during the AM peak hour and 276 trips in the PM peak hour at full build-out.
- When both phases in Clear Spring are fully constructed and occupied, two of the intersections studied for this development are anticipated to operate quite well in the projected conditions with respect to vehicular delays up to the year 2022. However, both northbound approaches at the intersection of Millertown Pike at Glen Creek Road and Millertown Pike at Sable Point Lane / Mary Emily Lane were calculated to operate at Level of Service (LOS) F during the PM peak
hour in the projected conditions in the year 2022. The intersection of Millertown Pike at Glen Creek Road was analyzed to see if traffic signal warrants were met for potential traffic signalization. It was determined that based on the projected volumes in the year 2022, the intersection will not meet warrants for signalization. However, as explained in the report, it is expected that the northbound approach at the intersection of Millertown Pike at Glen Creek Road will operate with smaller delays than projected.

The intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane is the only access point for an existing subdivision, Meadows of Millertown, located to the east of the Clear Spring development. This intersection was included in this study since there is a possibility that the two subdivisions could potentially be connected via a new road link. It is projected that the northbound approach of Millertown Pike at Sable Point Lane / Mary Emily Lane will reach LOS F whether or not Phase 2 of the Clear Spring development is constructed.

## Recommendations:

The following recommendations are listed here and offered based on the study analyses:

- An exclusive eastbound right turn lane should be constructed at the intersection of Millertown Pike at Glen Creek Road. The right turn lane should be 100 feet in length and have a 150 -foot taper. If a detailed survey and design determines that there is not enough distance to accommodate these recommended lengths in between Glen Creek Road and an existing driveway at 5528 Millertown Pike, it is recommended that the 150 -foot taper be maintained, and the storage length be reduced to no less than a total of 75 feet.
- The sight distance available looking east and to the west from Glen Creek Road at Millertown Pike has been measured by a licensed land surveyor and it was determined that the sight distance looking to the west (left) is 362 feet and the sight distance looking to the east (right) is 478 feet. The required sight distance at this intersection is 400 feet based on the posted speed limit. It is recommended that the cedar tree limbs on the north side of Millertown Pike and to the west of Glen Creek Road be trimmed to provide a minimum of 400 feet of sight distance.
- Due to the minimal sight distance available looking to the west from Glen Creek Road, it is recommended that a Side Road Sign (W2-2) be installed for eastbound traffic on Millertown Pike just prior to the beginning of the proposed right turn lane. This sign should be located at least 250 feet away to the east of the existing Reverse Turn Sign (W1-3) that is located across from 5521 Millertown Pike. This Side Road Sign is recommended to warn eastbound approaching motorists to the upcoming Glen Creek Road intersection since the intersection sight distance is at a minimum and because the intersection is not clearly visible due to it being located on a horizontal curve.
- 24 " white stop bars should be installed at the northbound approach of Millertown Pike at Glen Creek Road and at the eastbound approach of Old Millertown Pike at Glen Creek Road. Pavement markings also need to be applied at the existing roundabout of Glen Creek Road at Laurel Creek Way / Meadow Wells Drive.
- Vegetation needs continued maintenance within the landscaped island on Glen Creek Road to ensure sight distance is available at the intersection of Old Millertown Pike and at the roundabout.
- A speed limit of 25 mph should be posted on Glen Creek Road just to the south of the intersection of Old Millertown Pike.
- Phase 2 should construct and install sidewalks at a minimum of one side of each roadway. The sidewalks should be 5 feet in width and have ADA compliant ramps at all intersections.
- The Highlands at Clear Spring should include design elements with the appropriate sight distance and appropriate road signage.
- A road link between the Clear Spring Development and the Meadows of Millertown can or could be provided to allow for secondary access to Millertown Pike for both residential developments. It is not expected that providing a road link between these residential subdivisions will result in significant decreased traffic operations to either the intersection of Millertown Pike at Glen Creek Road or at the intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane. If a road connection is provided by extending Parasol Lane to Autumn Creek Drive, a Stop Sign (R1-1) should be installed for the westbound approach of Parasol Lane at Autumn Creek Drive.


## DESCRIPTION OF EXISTING CONDITIONS

## - STUDY AREA:

The proposed location of The Highlands at Clear Spring residential subdivision is shown on a map in Figure 1 and its location relative to Phase 1, Clear Springs Plantation. Phase 2 of the development, The Highlands at Clear Spring, is located to the rear (south) of Phase 1 which is adjacent to Millertown Pike and is in the northeast area of Knoxville, TN. The proposed residential development in Phase 2 is to be comprised of three new internal paved roadways, an extension of two existing roads from Phase 1 and will contain a maximum of 160 single-family residential lots on approximately 63.7 acres. Phase 1 is nearly filled with completed and occupied homes and consists of a total of 8 condominium units, 14 townhouses, and 111 single-family residential detached lots. All the condominium and townhouse units have been constructed and nearly three-quarters of the single-family residential detached homes have been constructed. To analyze the transportation impacts associated with the proposed development, the following roadways and intersections were reviewed where the greatest impact is expected:

```
o Millertown Pike at Glen Creek Road
o Old Millertown Pike at Glen Creek Road
o Glen Creek Road at Laurel Creek Way / Meadow Wells Drive
o Millertown Pike at Sable Point Lane / Mary Emily Lane
```

In the adjacent vicinity of this development, there are several single-family residences, unused/agricultural properties, commercial properties, a church with a cemetery and an electrical substation. Some of the adjacent residential areas are within existing subdivisions and others exist as single residential properties.

The proposed development site of Phase 2 currently consists of woodlands and areas that were partially graded for the future roadways during the initial Phase 1 construction. The roadways and infrastructure for Phase 1 were constructed and developed several years ago. Phase 1 lots are located along Laurel Creek Way (private - joint permanent easement), Meadow Wells Drive, Autumn Creek Drive, and McCampbell Wells Way (private - joint permanent easement). Glen Creek Road was constructed in Phase 1 and provides access in
between Millertown Pike and the Clear Spring residential development.

Phase 2 will be bounded by Phase 1 to the north, Norfolk Southern Railroad to the west, and single-family residential subdivisions to the east and south. The property is also bisected by two electrical transmissions lines.


Figure 1
Location Map

## - Existing Roadways:

Table 1 shows the characteristics of the primary existing roadways included in the study:

TABLE 1
STUDY CORRIDOR CHARACTERISTICS

| NAME | CLASSIFICATION ${ }^{1}$ | SPEED <br> LIMIT | LANES | $\begin{aligned} & \text { ROAD } \\ & \text { WIDTH }{ }^{2} \end{aligned}$ | TRANSIT ${ }^{3}$ | PEDESTRIAN FACILITIES | BICYCLE FACILITIES |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Millertown Pike | Minor Arterial | 40 mph | 2 <br> undivided | 22 feet | None | No sidewalks along roadway | No bike lanes |
| Old Millertown Pike | Local Street | Not Posted | 2 <br> undivided | 16.5 feet | None | No sidewalks along roadway | No bike lanes |
| Glen Creek Road | Local Street | Not Posted | $2$ <br> boulevard | 46 feet | None | 5' sidewalk on one side of roadway | No bike lanes |
| Laurel Creek Way | Local Street (private joint permanent easement) | Not Posted | 2 <br> undivided | 26 feet | None | $5^{\prime}$ sidewalk on one side of roadway | No bike lanes |
| Meadow Wells Drive | Local Street | Not Posted | $2$ <br> undivided | 26 feet | None | No sidewalks along roadway | No bike lanes |
| Sable Point Lane | Local Street | 25 mph | undivided | 26 feet | None | No sidewalks along roadway | No bike lanes |
| Mary Emily Lane | Local Street | Not Posted | $2$ <br> undivided | 25 feet | None | No sidewalks along roadway | No bike lanes |

[^0]Millertown Pike is a minor arterial that traverses in a general northeast-southwest direction. Millertown Pike is nearly 10 miles in total length and runs in between Rutledge Pike (US 11W) from the northeast to Washington Pike to the southwest. Closer to the study area, Millertown Pike provides convenient access to the Knoxville Center Mall area and Interstate 640. Just to the west of the development site on Millertown Pike,


View of Millertown Pike and Old Millertown Pike at Glen Creek Road

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there are numerous shopping and retail centers, restaurants, and grocery stores. Millertown Pike has a 40-mph speed limit in the study area adjacent to the development site but is reduced to 35 mph to the west within the more developed commercial areas closer to Interstate 640 .

For the most part, Millertown Pike has a straight horizontal road alignment and a level vertical road alignment. However, near the intersection of Millertown Pike at Glen Creek Road, Millertown Pike has two successive horizontal curves. Traffic signs (Reverse Turn / W1-3) providing advanced warning of these road curves are provided to the east and west on Millertown


W1-3 Pike. A guardrail is also provided on the south side of Millertown Pike to the west of Glen Creek Road. Traffic movements at the 3-way intersection of Millertown Pike at Glen Creek Road are controlled by a Stop Sign (R1-1) for the Glen Creek Road approach. There are not any street lights at this intersection. Further to the east of this intersection, Millertown Pike has permitted passing zones for eastbound and westbound traffic as designated by the centerline pavement markings. To the west of this intersection, a traffic signal operates at the intersection of Millertown Pike and Mill Road. This signalized intersection is approximately 1,100 feet away from the intersection of Millertown Pike at Glen Creek Road.

Old Millertown Pike is a local street and is the remnants of the turnpike prior to the route re-alignment constructed by the current alignment of Millertown Pike located to the north. The current Millertown Pike alignment provides an overpass over Norfolk Southern Railroad tracks. Old Millertown Pike runs in between Loves Creek Road and Glen Creek Road and is approximately 1,600 feet in length. Old Millertown Pike crosses 2 tracks of Norfolk Southern Railroad at an at-grade crossing. Advanced railroad warning signage is provided but there are not any active warning signals or crossing gates for the crossing. Speed limit signs are not posted on Old Millertown Pike.

Along its length, Old Millertown Pike has 8 single-family residences and a landscape company on the west end at Loves Creek Road. The road alignment is fairly straight except for the last 150 feet on the east end where the roadway makes a sharp horizontal turn and intersects Glen Creek Road approximately 80 feet to the south of the Millertown Pike at Glen Creek Road intersection. This sharp turn and re-alignment of the road was created when Glen Creek Road was constructed for Phase 1. Prior to the re-alignment of Old Millertown Pike and the construction of Glen Creek Road, the roadway intersected Millertown Pike at very undesirable
angle. The 150 feet of Old Millertown Pike that was re-aligned is approximately 26 feet in width. To the west of this realignment section, Old Millertown Pike is reduced in width to approximately 16.5 feet.


View of Old Millertown Pike at Millertown Pike prior to re-alignment (KGIS, 2003 Aerial Map)

Glen Creek Road is a local street that traverses in a general northwest-southeast direction between Millertown Pike on the north side and into the first phase of the Clear Spring development. It currently ends at a roundabout intersection. Glen Creek Road has a boulevard road section with 18 -foot lanes and


Intersection of Glen Creek Road and Laurel Creek Way / Meadow Wells Drive a landscaped 10-foot median that runs in between Millertown Pike and the roundabout intersection. The landscaped median is continuous except for an opening approximately midway that provides access to a TVA and Knoxville Utilities Board electrical substation. Speed limit signs are not posted on Glen Creek Road. Minor residential street lighting is provided within the landscaped median. A 5' sidewalk has been constructed on the west side of Glen Creek Road and runs in between Old Millertown Pike and terminates within the first phase of construction along Laurel Creek Way. The roundabout intersection of Glen Creek Road at Laurel Creek Way / Meadow Wells Drive is controlled by Yield Signs (R1-2) at each approach. The center of the roundabout is landscaped and has a small covered structure.

Laurel Creek Way / Meadow Wells Drive are local streets and both traverse in a general
northeast-southwest direction. Laurel Creek Way is a private drive and operates as a joint private easement. Laurel Creek Way provides access to the condominium and townhouse units from the initial phase of the development. It also provides access to 36 single-family residential detached lots to the west of the existing roundabout.

Meadow Wells Drive is a public street and provides access to single-family residential detached lots. Meadow Wells Drive provides access to Autumn Creek Road and both roads together share 75 single-family residential detached lots. Nearly all the single-family residential lots have homes constructed and occupied on these 2 streets. There are no sidewalks on Meadow Wells Drive or Autumn Creek Road except for one lot near the current end of Autumn Creek Road. Minor residential lighting is provided along Meadow Wells Drive and Autumn Creek Road. Speed limit signs are not posted on either street.

Sable Point Lane / Mary Emily Lane are local streets and both traverse in a general northwest-southeast direction. Sable Point Lane provides access to a fairly large residential subdivision named Meadows of Millertown. Currently, the only access to this subdivision is via Sable Point Lane at Millertown Pike. Sable Point Lane has a short boulevard road section (approximately 100 feet) at the intersection with Millertown Pike. Mary Emily Lane provides access to about a dozen older homes. Its length is approximately 1,800 feet and dead ends abruptly. A single roadway light is provided at the intersection of Millertown Pike at Sable Point Lane /


Intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane Mary Emily Lane. Speed limit signs are not posted on Mary Emily Lane, but Sable Point Lane is posted with a speed limit of 25 mph for the Meadows of Millertown subdivision.

Figure 2 shows the lane configurations of the study area roadways and intersections and shows the study traffic count locations. It also shows the posted speed limits in the area along with distances in between the studied intersections. The pages following Figure 2 give an overview of the site study area with photographs.


## Photo Exhibits






There is one annual vehicular traffic count location adjacent to this project site.
o Existing vehicular roadway traffic:

- Average Daily Traffic (ADT) on Millertown Pike near the project site was reported by the Tennessee Department of Transportation (TDOT) at 7,417 vehicles per day in 2016. From 2006 - 2016, this count station has indicated a $2.1 \%$ average annual growth rate. The researched historical traffic count data for this report can be viewed in Appendix A.
o Existing bicycle and pedestrian volumes: The average daily pedestrian and bicycle traffic along the study corridor is not known. A couple of pedestrians were observed at the intersections during the manual traffic counts. It is reasonably assumed that these volumes are minimal to non-existent in the study area.


## - AdJaCENT RAILROAD SYSTEM:

Norfolk Southern operates a dual railroad track just to the west of the intersection of Old Millertown Road and Glen Creek Road. This railroad line is part of the Alabama Railroad Division of Norfolk Southern. The railroad crossing has Railroad Grade Crossing (crossbuck) signs (R15-1)
 on both approaches but does not have railroad crossing signals or crossing gates. Railroad Grade Crossing Advance Warning (W10-1) signs are posted for both approaches on Old

Millertown Pike. The advance railroad pavement markings are worn away (or non-existent) at both approaches to the railroad crossing.

The railroad crossing on Old Millertown Pike is marked as \#730480D. Appendix B includes the U.S. DOT Crossing Inventory Form from the Federal Railroad Administration for this railroad crossing. According to the railroad forms, an average of 4 trains per day pass through this crossing. Trains on this track operate 24 hours a day, seven days a week, 365 days a year. On average, a quarter of the trains operate from 6 AM to 6 PM and the other three-fourths operates from 6 PM to 6 AM . The maximum track speed is 50 mph for freight trains on this track, but the typical average speed is 30 to 40 mph in this section.

Appendix B also contains a summary of the accident reports at this rail crossing. The past accident record of the railroad crossing included historical data back to 1977. Data indicated that 2 crashes since 1977 were recorded at this crossing and consisted of 2 automobile/train crashes. One of the accidents involved a vehicle stopped at the railroad crossing and the other one involved a vehicle moving across the railroad crossing when being struck. Both accidents occurred in 1977. None of the accidents had injuries or fatalities.

## - On-Street Parking:

Currently, on-street parking is not allowed on Millertown Pike. However, on-street parking was observed and appears to be allowed at all the other studied residential roadways except for Old Millertown Pike.

## - PEDESTRIAN AND BICYCLE FACILITIES:

Bicycle facilities (lanes) and pedestrian sidewalks are not currently available on Millertown Pike, Old Millertown Pike, and nearly all the studied local streets. The only sidewalk that is provided in the study area exists on the west side of Glen Creek Road in between Old Millertown Pike and Laurel Creek Way. Laurel Creek Way continues the sidewalk within the west side of the Phase 1 development.

## - Walk and Transit Score:

A private company offers an online website that grades and gives scores to locations within the United States based on "walkability" and transit availability. According to the website, the numerical value assigned for the Walk Score is based on the distance to the closest amenity in various relevant categories (businesses, schools, parks, etc.) and is graded from 0 to 100. The Transit Score measures how well a location is served by public transit based on distance and type of nearby transit. The Transit Score is also graded from 0 to 100.

Appendix C shows a map and gives information for the Clear Spring development Walk Score and Transit Score at Laurel Creek Way within the first phase of the development. Based on the project location, the site is given a Walk Score of 13. This Walk Score indicates that the site is almost completely dependent on vehicles for errands and travel. This low walkability score is due to the complete absence of sidewalks on Millertown Pike or Old Millertown Pike to outside destinations/amenities even though there are several potential destinations/amenities to the west of the site. Based on the project location, the site is given a Transit Score of 24. This indicates that it is possible to get bus service.

## - Transit Services:

The City of Knoxville has a network of public transit opportunities offered by Knoxville Area Transit (KAT). Bus service is available fairly close to the development site. The overall KAT bus system map is in Appendix D. The closest public transit bus service is located at Wal-Mart approximately 1 mile away to the west via Millertown Pike. This KAT service is Route 23 "Millertown". It operates on weekdays and Saturdays and this route map is also included in Appendix D.

Other transit services include the East Tennessee Human Resource Agency (ETHRA) and Knoxville-Knox County Community Action Committee (CAC) which provides transportation services in Knox County when requested. Other services include private taxis and ride-sharing opportunities (Uber, etc.).

## Project Description

## - Location and Site Plan:

The proposed plan layout for The Highlands at Clear Spring (Phase 2) designed by W. Scott Williams and Associates is shown in Figure 3. As can be seen in the figure, Phase 2 of the development will have two access points via existing roadways. Three completely new streets will be constructed, and these will tie into an extension of Glen Creek Road and Autumn Creek Drive. While not shown in Figure 3, the potential exists for this second phase to include constructing a link in between the Clear Spring development and the existing residential
 development to the east, Meadows of Millertown, by extending Parasol Lane. This would provide both developments with secondary access points to Millertown Pike. While the decision to build this road link has not been made final, this potential connection will be taken into consideration for this traffic study.

The Clear Spring development (both phases) is completely contained within the City of Knoxville limits. The Knoxville city limit exists at the property boundary on the south and east sides.

Phase 2 of the residential development is expected to be comprised of a maximum of 160 single-family residential detached lots on approximately 63.7 acres. The size of the residential lots in Phase 2 will be similar to Phase 1 and will be a minimum of 55 feet wide and 125 feet deep for a total area of 6,875 square feet. Phase 1 is nearly filled with completed and
occupied homes and consists of a total of 8 condominium units, 14 townhouses, and 111 single-family residential detached lots. All the condominium and townhouse units have been constructed and nearly three-quarters of the single-family residential detached homes have been constructed.

The actual schedule for completion of this residential developments is dependent on economic factors and construction timelines. This project is also contingent on permitting, design, and other issues. The developer is expecting continued high demand for housing in the Knoxville market and is estimating full construction and occupancy of both phases occurring within the next 3.5 years. Thus, for the purposes of this study, it was assumed that the total construction build-out and full occupancy of the entire development will occur by the year 2022.

At this point, the development is expected to start construction for Phase 2 as soon as possible and home construction in-filling will continue for the first phase of the development for the remaining undeveloped lots.


Figure 3
Proposed Plan Layout
The Highlands at Clear Spring

## - Proposed Uses and Zoning Requirements:

The second phase of this residential development, The Highlands at Clear Spring, is expected to be comprised of three new internal roadways and an extension of Glen Creek Road and Autumn Creek Drive from Phase 1 with a maximum of 160 lots on approximately 63.7 acres.

The property for Phase 2 is currently zoned within Knoxville, TN as Planned Residential District (RP-1). This Planned Residential District (RP-1) allows for up to 24 dwelling units per acre. The development property, however, is currently zoned to allow 1 to 3 dwelling units per acre. The current zoning map for the project site is provided in Appendix E. The adjacent surrounding land uses for Phase 2 are the following:

0 The property to the east is located outside the Knoxville city limits (within Knox County, TN) and is zoned as Planned Residential (PR) for the Meadows of Millertown subdivision. The property to the southeast is also outside the Knoxville city limits and is zoned General Residential (RB) and consists of single-family residences.
0 To the west, the development property is bound by Norfolk Southern Railroad. The adjacent property to the southwest of the proposed development is outside the city limits and is zoned Low Density Residential (RA) and is undeveloped. Another adjacent property located to the northwest of the proposed development is within the city limits and is zoned General Agricultural District (A-1) and consists of Spring Place Church and a cemetery.
0 To the south, the adjacent property is zoned General Residential (RB) and consists of the Spring Place subdivision.
0 The property to the north, Clear Springs Plantation (Phase 1), is also zoned Planned Residential District (RP-1) with a density of 1 to 3 dwelling units per acre.

The Planned Residential District (RP-1) zone allows for a variety of land uses primarily within the residential realm. Uses permitted in this zone include single-family dwellings, duplexes, and multi-dwelling structures and developments.

## - DEVELOPMENT DENSITY:

The allowable density by the City of Knoxville for this development is 1 to 3 dwelling units per acre based on the zoning. 160 single-family residential detached lots located on 63.7 acres results in a density of approximately 2.51 dwelling units per acre.

## - On-Site Circulation and Vehicle Parking:

Phase 2 of the proposed residential development is expected to be comprised of three new internal paved roadways and an extension of Glen Creek Road and Autumn Creek Drive from Phase 1. The three new internal roads will consist of cul-de-sacs. The new roads in Phase 2 shown in Figure 3 are labeled as Road "A" thru Road "D". The road extension that connects Glen Creek Road and Autumn Creek Drive is labeled as Road "A" and is approximately 2,173 feet. The three new roads, Road "B", "C", and "D" combined length is approximately 4,224 feet. The total length of all new roadways in Phase 2 will be nearly 6,400 feet.

The internal roadways for the development will be paved, include extruded concrete curbing, and the lane widths will be 13 feet for a total of 26 -foot pavement width within a 50 foot right-of-way. All the home sites will have 2 garage spaces for vehicle parking.

## - SERvice and Delivery Vehicle Access and Circulation:

In addition to passenger vehicles, the proposed internal roadways will also provide access to service, delivery, maintenance, and fire protection vehicles. It is not expected that any of these vehicles will impact off-site adjacent roadway operations other than when these vehicle-types will occasionally enter and exit the development. The internal roadways in all portions of the development are expected to be able to accommodate these types of vehicles along with passenger vehicles.

## Traffic Analysis of Existing and Projected Conditions

## - Existing Traffic Conditions

Traffic counts were conducted at the following existing unsignalized intersections as directed by the MPC:
o Millertown Pike at Glen Creek Road
o Old Millertown Pike at Glen Creek Road
o Glen Creek Road at Laurel Creek Way / Meadow Wells Drive
o Millertown Pike at Sable Point Lane / Mary Emily Lane

Traffic counts were obtained on Thursday, July 26th, 2018. The counts were conducted during the morning, mid-day, and afternoon peak periods. Local schools were not in session when the traffic counts were conducted.

The intersections of Old Millertown Pike at Glen Creek Road, Glen Creek Road at Laurel Creek Way / Meadow Wells Drive, and Millertown Pike at Sable Point Lane / Mary Emily Lane were counted from 7-9 am and 3-6 pm. The intersection of Millertown Pike at Glen Creek Road was counted from $7-9 \mathrm{am}, 11 \mathrm{am}-1 \mathrm{pm}$, and $2-6 \mathrm{pm}$. Based on the traffic volumes counted at the intersections, the AM and PM peak hour of traffic were observed at the following times:
o Millertown Pike at Glen Creek Road
7:15-8:15 AM / 5:00 - 6:00 PM
o Old Millertown Pike at Glen Creek Road
7:15-8:15 AM / 4:30 - 5:30 PM
o Glen Creek Road at Laurel Creek Way / Meadow Wells Drive
7:30 - 8:30 AM / 4:15 - 5:15 PM
o Millertown Pike at Sable Point Lane / Mary Emily Lane
7:15 - 8:15 AM / 5:00 - 6:00 PM

The manual tabulated traffic counts can be reviewed in Appendix F. In Figure 4, the volumes are shown from the existing traffic counts during the AM and PM peak hours
observed at each intersection. Based on the existing traffic counts conducted, and as shown in Figure 4, it appears that there is a significant amount of cut-through traffic utilizing Old Millertown Pike during the PM peak hour to reduce travel times heading east instead of using Millertown Pike. It is assumed that these motorists are coming from south Loves Creek Road or from motorists cutting through prior to the traffic signal at the intersection of Millertown Pike at Loves Creek Road. There were also a handful of motorists using the entrance of Millertown Pike at Glen Creek Road as a U-turn opportunity to change direction on Millertown Pike. Due to the on-going home construction occurring in the first phase of Clear Spring, a fair amount of entering and exiting traffic at Millertown Pike at Glen Creek Road consisted of construction vehicles.

It is expected that the AM and PM peak hour would be observed earlier if this traffic count was conducted while schools were in session. It is also expected that this report will be updated with new traffic counts once schools are back in session in August 2018. The existing counts that are shown in Appendix F have been adjusted in Figure 4 by increasing the observed volumes by $15 \%$ to account for the missing school traffic.


Capacity analyses were undertaken to determine the existing Level of Service (LOS) for the studied intersections with respect to vehicular traffic. The capacity analyses were calculated by following the methods outlined in the Highway Capacity Manual and using Synchro Traffic Software (Version 8). LOS is a qualitative measurement developed by the transportation profession of how well an intersection or roadway performs based on a driver's perception. LOS designations include LOS A through LOS F. The designation of LOS A signifies a roadway or intersection operating at best, while LOS F signifies road operations at the worst. This grading system provides a reliable straightforward means to communicate road operations to the public. The Highway Capacity Manual (HCM) lists level of service criteria for unsignalized intersections and signalized intersections.

For unsignalized intersections, Level of Service is measured in terms of delay (in seconds). This measure is an attempt to quantify delay that includes travel time, driver discomfort, and fuel consumption. The LOS for a two-way

(Source: FDOT) stop (or yield) controlled intersection is defined by the delay for each minor approach and major street left-turn movement. Table 2 lists the level of service criteria for unsignalized intersections.

From the capacity calculations, the results from the existing peak hour vehicular traffic can be seen in Table 3 for the intersections. The intersections in the table are shown with a LOS designation, delay (in seconds), and v/c ratio (volume/capacity) for the AM and PM peak hours. A v/c ratio of 1 would indicate that the traffic volumes are at the roadway capacity. Appendix $G$ includes the worksheets from the capacity analyses for the existing peak hour vehicular traffic. All the studied intersection approaches and intersections are shown to operate at an adequate level during the existing AM and PM peak hours for vehicular traffic except for the northbound approach of Sable Point Lane at Millertown Pike which was calculated to be LOS E in the PM peak hour.

TABLE 2

LEVEL OF SERVICE AND DELAY FOR UNSIGNALIZED INTERSECTIONS

| LEVEL OF <br> SERVICE | DESCRIPTION | DELAY RANGE <br> (seconds /vehicle) |
| :---: | :---: | :---: |
| A | Little or no delay | $\leq 10$ |
| B | Short Traffic Delays | $>10$ and $\leq 15$ |
| C | Average Traffic Delays | $>15$ and $\leq 25$ |
| D | Long Traffic Delays | $>25$ and $\leq 35$ |
| E | Very Long Traffic Delays | $>35$ and $\leq 50$ |
| F | Extreme Traffic Delays | $>50$ |

Source: Highway Capacity Manual

TABLE 3

## 2018 PEAK HOUR LEVEL OF SERVICE \& DELAY - EXISTING TRAFFIC CONDITIONS

| INTERSECTION | TRAFFIC CONTROL | APPROACH | AM PEAK |  |  | PM PEAK |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Los | DELAY <br> (seconds) | V/C | LOS | DELAY <br> (seconds) | v/C |
| Millertown Pike at Glen Creek Road |  | Northbound Left/Right | B | 14.0 | 0.113 | C | 17.3 | 0.285 |
|  |  | Westbound Left | A | 7.7 | 0.014 | A | 8.8 | 0.015 |
|  |  |  |  |  |  |  |  |  |
| Old Millertown Pike at Glen Creek Road |  | Northbound Left | A | 7.3 | 0.005 | A | 7.3 | 0.009 |
|  |  | Eastbound Left/Right | A | 9.0 | 0.013 | A | 9.5 | 0.075 |
|  |  |  |  |  |  |  |  |  |
| Glen Creek Road at Laurel Creek Way / Meadows Well Drive |  | Eastbound Left/Thru/Right | A | 3.3 | 0.009 | A | 3.4 | 0.017 |
|  |  | Westbound Left/Thru/Right | A | 3.5 | 0.037 | A | 3.4 | 0.024 |
|  |  | Northbound Left/Thru/Right | A | 3.3 | 0.000 | A | 3.4 | 0.000 |
|  |  | Southbound Left/Thru/Right | A | 3.5 | 0.032 | A | 3.6 | 0.052 |
| Millertown Pike at Sable Point Lane / Mary Emily Lane |  | Northbound Left/Thru/Right | C | 20.1 | 0.336 | E | 44.9 | 0.550 |
|  |  | Eastbound Left | A | 8.3 | 0.004 | A | 8.1 | 0.023 |
|  |  | Westbound Left | A | 7.6 | 0.011 | A | 9.0 | 0.004 |
|  |  | Southbound Left/Thru/Right | B | 11.4 | 0.014 | C | 15.8 | 0.039 |
|  |  |  |  |  |  |  |  |  |

Note: All analyses were calculated in Synchro 8 software and reported with HCM 2010 methodology for unsignalized intersections

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Transportation Impact Study

The Highlands at Clear Spring
Knoxville, TN

## - Opening Year Traffic Conditions (without project):

Opening year traffic volume estimates represent the future condition the proposed study area is potentially subject to without the proposed project being developed (no-build option). As previously stated, the build-out and full occupancy for this proposed residential development were assumed to occur in the year 2022. This corresponds with nearly 3-1/2 years for the entire development to be constructed and reach full occupancy.

Vehicular traffic over the past 10 years has shown an average annual growth rate of $2.1 \%$ according to the TDOT count station on Millertown Pike (historical traffic data is shown in Appendix A). Currently, there are no known significant upcoming developments adjacent to the proposed site that would indicate large future increased traffic volumes in the study area. To ensure a reasonable traffic growth estimate for this study and to account for any potential traffic growth in the study area, an average annual growth rate of $2.5 \%$ was used to calculate future growth up to the year 2022 for the studied intersections. The results of this growth rate to the existing traffic volumes can be seen in Figure 5. Figure 5 shows the projected opening year traffic volumes in 2022 during the AM and PM peak hours without the project being developed.

The application of opening year traffic to the existing intersections did not appreciably change the LOS designations from the existing traffic volume analysis for the AM and PM peak hours. However, the northbound approach at the intersection of Millertown Pike and Sable Point Lane / Mary Emily Lane was calculated to operate at LOS F in the year 2022 during the PM peak. Table 4 reports the LOS designation, delay (in seconds), and v/c ratio (volume/capacity). Appendix G contains the LOS capacity worksheets for the opening year conditions (without project). It is important to point out that these projected LOS designations for the intersections could potentially exist in the future even without the subsequent proposed residential project being fully constructed and developed.


TABLE 4
2022 PEAK HOUR LEVEL OF SERVICE \& DELAY - OPENING YEAR (WITHOUT PROJECT)

| INTERSECTION | TRAFFIC CONTROL | APPROACH | AM PEAK |  |  | PM PEAK |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Los | $\begin{array}{\|c\|} \hline \text { DELAY } \\ \text { (seconds) } \end{array}$ | v/C | LOS | DELAY <br> (seconds) | v/C |
| Nillertown Pike at |  | Northbound Left/Right | B | 14.9 | 0.133 | C | 19.5 | 0.339 |
| Glen Creek Road |  | Westbound Left | A | 7.7 | 0.015 | A | 9.0 | 0.015 |
|  |  |  |  |  |  |  |  |  |
| Old Millertown Pike at Glen Creek Road |  | Northbound Left | A | 7.3 | 0.007 | A | 7.3 | 0.009 |
|  |  | Eastbound Left/Right | A | 9.0 | 0.018 | A | 9.6 | 0.082 |
|  |  |  |  |  |  |  | § |  |
| Glen Creek Road at Laurel Creek Way / Meadows Well Drive |  | Eastbound Left/Thru/Right | A | 3.3 | 0.011 | A | 3.5 | 0.018 |
|  |  | Westbound Left/Thru/Right | A | 3.6 | 0.040 | A | 3.5 | 0.027 |
|  |  | Northbound Left/Thru/Right | A | 3.3 | 0.000 | A | 3.4 | 0.000 |
|  |  | Southbound Left/Thru/Right | A | 3.5 | 0.036 | A | 3.7 | 0.058 |
| Millertown Pike at Sable Point Lane / Mary Emily Lane |  | Northbound Left/Thru/Right | C | 23.3 | 0.400 | F | 67.3 | 0.703 |
|  |  | Eastbound Left | A | 8.5 | 0.004 | A | 8.2 | 0.028 |
|  |  | Westbound Left | A | 7.6 | 0.011 | A | 9.2 | 0.006 |
|  |  | Southbound Left/Thru/Right | B | 11.9 | 0.020 | C | 17.4 | 0.044 |
|  |  |  |  |  |  |  |  |  |

Note: All analyses were calculated in Synchro 8 software and reported with HCM 2010 methodology for unsignalized intersections

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## - Trip Generation

A generated trip is a single or one-direction vehicle movement that is either entering or exiting the development site. The Trip Generation Manual, a publication of the Institute of Transportation Engineers, is the traditional and most-sourced resource for determining trip generation rates when traffic impact studies are produced. The Manual lists and includes data for a variety of land uses. The estimated amount of traffic that will be generated by the singlefamily detached lots, the condominium units, and townhouses for this entire development (both phases) was calculated based upon rates and equations for peak hour trips provided by Trip Generation Manual, 9th Edition.

The trip generation data and calculations for the proposed land uses are shown in Appendix H. A summary of this information is presented in the following tables. Table 5a shows the overall total potential generated traffic for the entire development that includes Phase 1 and 2 . Tables 5 b and 5 c show the potential generated traffic broken down into the 2 individual land uses in the development.

TABLE 5A
TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT Entire Development

| ITE LAND USE CODE | LAND USE DESCRIPTION | UNITS | GENERATED DAILY TRAFFIC | GENERATED TRAFEIC <br> AM PEAK HOUR |  |  | GENERATED TRAFEIC PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| Total New Volume Site Trips |  |  | 2,801 | 53 | 163 | 216 | 175 | 101 | 276 |

In both phases with a total of 271 single-family detached residential lots, 8 condominiums, and 14 townhouses; based on the calculations, it is estimated that 53 vehicles will enter the development, 163 will exit, for a total of 216 new generated trips during the AM Peak Hour in the year 2022. Similarly, it is estimated that 175 vehicles will enter the development, 101 will exit, for a total of 276 new generated trips during the PM Peak Hour in the year 2022. The calculated trips generated for an average weekday could be expected to be 2,801 vehicles for the entire development. For this study, no trip reductions were included for pass-by or internal trips.

TABLE 5B
TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT
271 Single-Family Detached Homes

| ITE LAND USE CODE | LAND USE DESCRIPTION | UNITS | GENERATED DAILY TRAFFIC | GENERATEDTRAFFICAM PEAK HOUR |  |  | GENERATED TRAFFIC <br> PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| \#210 | Single-Family Detached Housing | 271 Lots | 2,628 | 25\% | 75\% |  | 63\% | 37\% |  |
|  |  |  |  | 50 | 150 | 200 | 163 | 95 | 258 |
| Total New Volume Site Trips |  |  | 2,628 | 50 | 150 | 200 | 163 | 95 | 258 |

ITE Trip Generation Manual, 9th Edition

TABLE 5C
TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT
22 Single-Family Attached Homes ( 8 Condominiums +14 Townhouses)

| ITE LAND USE CODE | LAND USE DESCRIPTION | UNITS | GENERATED DAILY TRAFFIC | GENERATEDTRAFFICAM PEAK HOUR |  |  | GENERATED <br> TRAFFIC <br> PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| \#230 | Residential Condominium / Townhouse | 22 Dwellings | 173 | 17\% | 83\% |  | 67\% | 33\% |  |
|  |  |  |  | 3 | 13 | 16 | 12 | 6 | 18 |
| Total New Volume Site Trips |  |  | 173 | 3 | 13 | 16 | 12 | 6 | 18 |

ITE Trip Generation Manual, 9th Edition

## - Trip Distribution and Assignment

Figure 6 shows the projected distribution for traffic entering and exiting for the entire development (both phases) during the future AM and PM peak hour at the existing intersections of Millertown Pike at Glen Creek Road and at Old Millertown Pike at Glen Creek Road. The percentages shown in the figure only pertain to the trips generated by the existing and proposed single-family detached homes from both phases and the existing condominium and townhouse units in Phase 1 that were calculated from the ITE trip generation rates.

There are a variety of destinations that will potentially "attract" the projected traffic to and from the new development. The vast majority of these will be to and from the west. These destinations will be accessed by utilizing Millertown Pike and Old Millertown Pike. In addition to employment centers and commercial development, traffic will travel to and from a variety of public and private elementary, middle, and high schools. This residential development is zoned for Rita Elementary School, Holston Middle School, and Gibbs High School.

Figure 7 shows the Traffic Assignment of the generated trips by the development at the studied intersections for traffic entering and exiting the development during the future AM and PM peak hours. This is based on the assumed distribution of trips shown in Figure 6 and the total trips generated shown in Table 5a.

The generated trips that are distributed and shown in Figure 7 at the roundabout intersection of Glen Creek Road at Laurel Creek Way / Meadow Wells Drive are based on the location of the various residential types within both phases of the development. The condominiums and townhouses from Phase 1 are all assigned entering and exiting the east side of the roundabout intersection. The single-family residential detached lots are portioned at the roundabout intersection based on 36 lots from Phase 1 located to the west side of the roundabout intersection, 75 lots from Phase 1 located to the east of the roundabout intersection, and the proposed 160 lots for Phase 2 located to the south of the roundabout intersection. These additional "portioning" calculations are shown with the trip generation calculations shown in Appendix H.



## - Opening Year Traffic Conditions (With project)

Overall, several additive steps were taken to estimate the total opening year projected traffic volumes at the studied intersections when the Clear Spring development (Phase 1, Clear Springs Plantation and Phase 2, The Highlands at Clear Spring) is fully constructed and occupied in the year 2022. The steps are illustrated below for clarity:


To calculate the total future projected traffic volumes at the studied intersections, the trips generated (from the ITE trip rates) by the entire residential development (both phases) were added to the 2022 opening year traffic volumes (shown in Figure 5) in accordance with the predicted directional distributions and assignments (shown in Figures 6 and 7). This procedure was necessary to obtain the total projected traffic volumes at the time the development is fully built-out and occupied in the year 2022. Figure 8 shows the projected AM and PM peak hour volumes at the studied intersections for the year 2022 with the development traffic.


Capacity analyses were conducted to determine the projected Level of Service for vehicles at the studied intersections for the year 2022 with the development traffic. Appendix $G$ includes the worksheets for these capacity analyses.

The results of the capacity calculations of the projected 2022 peak hour vehicular traffic volumes at the studied intersections can be seen in Table 6 for the AM and PM peak hour. As can be seen in the table, the northbound turn movements at the intersection of Millertown Pike at Glen Creek Road are projected to operate at LOS F during the PM peak hour in the year 2022. The northbound intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane is also again projected to operate at LOS F in the PM peak hour as previously shown in Table 4 during the projected conditions without the project.

TABLE 6
2022 PEAK HOUR LEVEL OF SERVICE \& DELAY - OPENING YEAR (WITH PROJECT)


Note: All analyses were calculated in Synchro 8 software and reported with HCM 2010 methodology for unsignalized intersections

## - Discussion of Vehicle Crashes on Millertown Pike

As part of the study process, the MPC and the Knox County Engineering Department requested that the vehicle crash history be examined at and near the intersection of Millertown Pike at Glen Creek Road.

- The Knox County Engineering Department provided traffic crash data for the past 3$1 / 4$ years at and near the intersection of Millertown Pike at Glen Creek Road. The crash data included the individual crash reports that were obtained for 6 crashes reported from the Knox County Sheriffs Department and 1 crash reported by the Tennessee Highway Patrol. Thus, over the past 3-1/4 years, the data showed a total of 7 vehicle crashes occurring at or near the intersection of Millertown Pike at Glen Creek Road. The traffic crash information is summarized in the following and the locations shown in Figure 9:

7 Total Vehicle Crashes from 5/17/15 to 7/25/18:
o Vehicle Crash Categories:
> 4 Vehicle Crashes with no injuries (property damage only)
> 2 Vehicle Crashes with three injuries (one incapacitating, one suspected serious, and one possibly injured)
> 1 Vehicle Crash with one fatality
0 Vehicle Crash Types:
$>3$ Rear-End crashes (no injuries or fatalities)
$>2$ Vehicle Crashes with objects (two injuries in 1 crash)
> 1 Overturning Vehicle Crash (with one fatality)
$>1$ Vehicle Crash involving striking one pedestrian (one incapacitating injury)

Based on evaluating the obtained individual traffic crash reports from Millertown Pike, 5 of the 7 crashes occurred near the intersection and 2 of the crashes occurred at the intersection of Millertown Pike at Glen Creek Road. Based on a review of the 7 crashes; road conditions and weather did not appear to be a causative factor.

Of the three serious crashes involving injuries and the fatality, different factors and causes were contributed to the cause. They are summarized in the following:

0 The fatality accident was a single vehicle crash. According to the traffic crash report, a driver in a concrete mixer truck was traveling westbound at excessive speed, failed to negotiate the road curve on Millertown Pike (west of Glen Creek Road), which caused the vehicle to overturn and strike a guardrail and a utility pole causing the fatality.
o The vehicle crash that caused 2 injuries when striking an object was also a single vehicle crash. According to the traffic crash report, a passenger vehicle was heading eastbound and operated by a driver who was impaired by alcohol. The vehicle left the roadway and struck a tree and injured the driver and a passenger. One of the injuries was "possible" and the other was suspected to be serious.
0 The vehicle crash that involved injuring a pedestrian occurred at night when two pedestrians were attempting to cross Millertown Pike at Glen Creek Road. According to the traffic crash report, a driver in a passenger vehicle heading eastbound attempted to miss hitting the first pedestrian but ended up striking a second pedestrian causing an incapacitating injury.

The less serious vehicle crashes (vehicle property damage only) were rear-end crashes and one crash involving an object in the road. They are summarized in the following:

0 The vehicle crash involving an object was an eastbound single vehicle crash that struck a deer in the roadway.
0 The rear-end crashes occurred at 3 locations at or near the intersection of Millertown Pike at Glen Creek Road. One rear-end crash occurred west of Glen Creek Road due to a westbound vehicle queue from the signalized intersection of Millertown Pike at Mill Road. One rear-end crash occurred at the intersection of Millertown Pike at Glen Creek Road due to a westbound vehicle queue from a vehicle attempting to turn left onto Glen Creek Road. The other rear-end crash occurred due to one driver stopping quickly to avoid hitting a dog on Millertown Pike.


Figure 9
Vehicle Crash Locations
on Millertown Pike

Based on statewide vehicle crash data, TDOT has compiled and calculated statewide crash rates for various types of intersections, road sections, and road spots in Tennessee based on rolling data from the past 3 years of current data. (TDOT defines a spot location as a section of roadway less than or equal to 0.10 mile.) This data is categorized by urban and rural locations, route type (major collector, local, etc.), type of roadway facility (number of lanes, etc.), and location type (intersection, section, or spot). The statewide crash rate tables for intersections, sections, and spots from TDOT was obtained for this study and is provided in Appendix I.

The intersection of Millertown Pike at Glen Creek Road was calculated for an intersection crash rate. Additionally, a section was examined on Millertown Pike from just to the east and to the west of Glen Creek Road where the 7 crashes have occurred in the past 3 years over 0.13 mile.

TDOT has developed a crash analysis file that compares the actual crash rates at roadway intersections, sections, and spots versus the state average. Based on the number of crashes reported at the intersection of Millertown Pike at Glen Creek Road, and the section on Millertown Pike for the past 3 years; it does not appear that the calculated crash rates are considered high enough to obtain TDOT safety funding.

To obtain TDOT safety funding, the ratio of the actual crash rate to the critical crash rate (A/C ratio) would need to be 3.5 or higher. Appendix I includes the crash rate calculations for the intersection and road section. The calculations show the actual crash rate vs. the statewide average crash rate $(\mathrm{A} / \mathrm{S})$ and the ratio of the actual crash rate vs. the critical crash rate (A/C). The critical crash rate (A/C) gives more weight to specific crash severities while the statewide average comparison ( $\mathrm{A} / \mathrm{S}$ ) only considers total numbers. The calculated ratios are shown in the following tables for the intersection and road section respectively:

Table 7
Crash Rates on Millertown Pike

| Millertown Pike, | Knox County |  |  | LM 0.000 |
| :---: | :---: | :---: | :---: | :---: |
| Intersection (Millertown Pike at Glen Creek Road) |  |  |  |  |
| 2 Crashes | - 2015-2018 | Actual | - 0.242 | Acc/MVM |
| State Average | - 0.121 Acc/MVM | Critical | - 0.463 | Acc/MVM |
| A/S Ratio | $=2.00$ | A/C Ratio | $=0.52$ |  |
| 0 Fatal Crash | 1 Incap. Injury Crash |  | 0 Other Injury Crash |  |


| Millertown Pike, | Knox County |  |  | LM 0.000 |
| :---: | :---: | :---: | :---: | :---: |
| Section (east and west of Glen Creek Road) |  |  |  |  |
| 7 Crashes | - 2015-2018 | Actual | - 6.630 | Acc/MVM |
| State Average | - 2.832 Acc/MVM | Critical | - 7.117 | Acc/MVM |
| A/S Ratio | $=2.34$ | A/C Ratio | $=0.93$ |  |
| 1 Fatal Crash | 1 Incap. Injury Crash |  | 2 Other Injury Crash |  |

## - Potential Safety Issues

The study area was investigated for potential safety issues. Several features of the adjacent transportation system were identified and are discussed in the following pages as having potential safety issues.

## - Evaluation of Turn Lane Thresholds

The Millertown Pike at Glen Creek Road intersection was evaluated for the need for separate turn lanes on Millertown Pike for entering vehicles into the development. Based on the projected traffic volumes at the intersection of Millertown Pike at Glen Creek Road and according to "Knox County's Access Control and Driveway Design Policy", a separate left turn lane is not warranted, but a right turn lane is warranted for entering vehicles. The Knox County turn lane policy worksheet is in Appendix J. The results shown in the Appendix are based on the projected volumes during the AM and PM peak hour. The PM peak hour projected traffic volumes are estimated to be at a level that will require the need for a separate right turn lane for eastbound right turns off Millertown Pike onto Glen Creek Road.

The design policy for turn lane warrants relates volume thresholds based on prevailing speeds for two-lane roadways. The speed classification that was chosen for this evaluation was based on the posted speed limit of 40 mph . Therefore, this study evaluation used the Knox County classification for speeds of $36 \mathrm{mph}-45 \mathrm{mph}$ and the calculated projected volumes.

## = Evaluation of Sight Distance

Based on a posted speed limit of 40 mph on Millertown Pike, the required intersection sight distance should be a minimum of 400 feet looking east and west on Millertown Pike from Glen Creek Road based on Knox County policy of requiring 10 feet of sight distance per 1 mph of speed. The sight distance at the intersection of Glen Creek Road at Millertown Pike was measured on September 5th, 2018 by Scott Williams, PE, RLS. The following results were obtained from Glen Creek Road at Millertown Pike: the sight distance looking to the west (left) is 362 feet and the sight distance looking to the east (right) is 478 feet. These measurements were taken on Glen Creek Road 15 feet away from the edge of pavement of

[^1]Millertown Pike. The surveyor believes that 400 feet of sight distance is potentially available looking to the west (left) if tree limbs are removed from the cedar trees located on the north side of Millertown Pike (and west of the intersection). It is believed that the cedar tree limbs are within the right-of-way, however, the trees themselves are located on private property at 5533 Millertown Pike.


## CONCLUSIONS AND RECOMMENDATIONS

The following discussion is an overview of recommendations to minimize the traffic impacts of the proposed development on the surrounding road system while attempting to achieve an acceptable level of traffic flow and safety.

## 1) Millertown Pike at Glen Creek Road

1a) A separate right turn lane on Millertown Pike for turning vehicles onto Glen Creek Road is recommended based on the projected volumes. The Millertown Pike at Glen Creek Road intersection turn lane evaluation was evaluated based on the projected 2022 traffic volumes at the intersection and according to "Knox County's Access Control and Driveway Design Policy".

The traffic impact study for the original development that was conducted in 2005 by Wilbur Smith Associates also recommended a right turn lane be constructed for entering traffic off Millertown Pike onto Glen Creek Road. As recommended in the original study; this current study also recommends that this right turn lane be 100 feet in length with a 150 -foot taper length. As stated in the original traffic study, the length recommended by A Policy on Geometric Design of Highway and Streets by AASHTO (American Association of State Highway and Transportation Officials) is 330 feet to decelerate from 40 mph . However, this recommended length is based on vehicles coming to a complete stop and the right turning vehicles coming off Millertown Pike onto Glen Creek Road will not completely stop. A 100 -foot right turn storage length is a reasonable distance that is consistent with similar developments in Knox County. The taper length is based on 11 -foot wide lanes on Millertown Pike and an approach speed of 40 mph .

There is a residential driveway located to the west of this intersection at 5528 Millertown Pike. This existing residential driveway could reduce the amount of distance available to construct a right turn lane with a recommended 100 feet of storage and a 150 -foot taper length. Once an accurate survey and design is completed, the available right turn lane length will be more defined. If there is not
enough distance in between Glen Creek Road and the residential driveway, it is recommended that the 150 -foot taper be maintained, and the storage length be reduced to no less than a total of 75 feet.

Scott Williams, PE, RLS has completed a rough layout of the right turn lane on Millertown Pike and this layout is included in Figure 10. The construction of this turn lane will involve relocating guardrail, a utility pole, and will also require property acquisition and fill slopes.

The developer is planning on designing and constructing the right turn lane on Millertown Pike as soon as The Highlands at Clear Spring has been approved by the County.


Figure 10
Proposed Right Turn Lane
Millertown Pike at Glen Creek Road
(NTS)

1b) Based on a posted speed limit of 40 mph on Millertown Pike, the required intersection sight distance should be a minimum of 400 feet looking east and west from Glen Creek Road. The sight distance was measured by a licensed land surveyor and determined that the sight distance looking to the west (left) is 362 feet and the sight distance looking to the east (right) is 478 feet. These measurements were taken on Glen Creek Road 15 feet away from the edge of pavement of Millertown Pike. The surveyor believes that 400 feet of sight distance is potentially available looking to the west (left) if tree limbs are removed from the cedar trees located on the north side of Millertown Pike (and west of the intersection). It is believed that the cedar tree limbs are within the right-of-way, however, the trees themselves are located on private property. The images below give an indication of the current view available looking east and west on Millertown Pike from Glen Creek Road and the sight obstructions and potential sight obstructions.



Sight Distance Looking East from Glen Creek Road at Millertown Pike

It is recommended that the limbs from the cedar trees on the north side of Millertown Pike (at 5533 Millertown Pike) be removed/trimmed to increase and maximize the sight distance looking to the west from Glen Creek Road. The sight distance in both directions at this intersection on Millertown Pike will need to be maintained in the future.

In addition, due to the minimal sight distance available looking to the west from Glen Creek Road, it is recommended that a Side Road Sign (W2-2) be installed for eastbound traffic on Millertown Pike just prior to the beginning of the proposed right turn lane. This sign should be located at least 250 feet away to the


W2-2 east of the existing Reverse Turn Sign (W1-3) that is located across from 5521 Millertown Pike. This Side Road Sign is recommended to warn eastbound approaching motorists of the upcoming Glen Creek Road intersection since the intersection sight distance is at a minimum and because the intersection is not readily visible due to it being located on a horizontal curve.

1c) This intersection was calculated currently to operate adequately in 2018 but projected to operate poorly with respect to the level of service for northbound turns during the year 2022 when the development is expected to be fully constructed and
occupied.

Capacity analyses were re-calculated for the intersection of Millertown Pike at Glen Creek Road with an eastbound right turn lane added to the intersection as recommended. Appendix $G$ includes the worksheets for these capacity analyses. The results of the capacity calculations with the projected 2022 peak hour vehicular traffic volumes at this intersection and including an eastbound right turn lane reduced the delay for the northbound approach by over 30 seconds in the PM peak hour. This is due to the large amounts of right turns being removed from the thru lane movement. The results are shown below in Table 8.

TABLE 8
2022 PEAK HOUR LEVEL OF SERVICE \& DELAY - OPENING YEAR (WITH PROJECT) MILLERTOWN PIKE AT GLEN CREEK ROAD WITH ADDED EB RIGHT TURN LANE

| INTERSECTION | TRAFEIC CONTROL | APPROACH | AM PEAK |  |  | PM PEAK |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | DELAY <br> (seconds) | V/C | LOS | DELAY <br> (seconds) | V/C |
| Millertown Pike at |  | Northbound Left/Right | D | 30.2 | 0.675 | F | 54.2 | 0.827 |
| Glen Creek Road |  | Westbound Left | A | 7.6 | 0.018 | A | 8.9 | 0.035 |
|  |  |  |  |  |  |  |  |  |

Note: All analyses were calculated in Synchro 8 software and reported with HCM 2010 methodology for unsignalized intersections

In addition, it is expected that the influence of the traffic signal at Mill Road west of the intersection of Millertown Pike and Glen Creek Road will provide gaps in the traffic flow along Millertown Pike and this will allow greater egress than can be modeled in this analysis. There are also additional factors that would indicate this intersection will operate at a higher level of service in the projected conditions. First, the existing traffic generated by the existing homes in Phase 1 are included in the capacity calculations. Including these volumes in the calculations overestimates (double counts) the projected traffic volumes in the year 2022. Secondly, the existing traffic count showed that a substantial number of eastbound motorists are using Old Millertown Pike as a cut-through or as a time-saving route to head east on Millertown Pike during the PM peak hour. This was observed from the significant amount of eastbound left turns at Old Millertown Pike at Glen Creek Road and subsequent right turns at Millertown Pike at Glen Creek Road. It is suspected that as the Clear Spring development increases in size and increases the
amount of northbound traffic at Millertown Pike at Glen Creek Road, it is expected that fewer motorists will use Old Millertown Pike as a cut-through or as a timesaving route to head east on Millertown Pike. This would then reduce the overall northbound volumes and decrease delay at the intersection of Millertown Pike at Glen Creek Road.

1d) As an investigation into a potential remediation for the projected high northbound vehicle delays, this intersection was examined with the projected 2022 traffic volumes with respect to traffic signal warrants. The traffic counts at this intersection were conducted from $7-9 \mathrm{am}, 11 \mathrm{am}-1 \mathrm{pm}$ and $2-6 \mathrm{pm}$ for a total of 8 hours.

The Manual on Uniform Traffic Control Devices - 2009 Edition (MUTCD) presents 9 different warrants that have been developed by the traffic engineering profession to determine whether a traffic signal is warranted. These warrants cover a broad range of minimum elements required to indicate whether a traffic signal is justified for any particular location. These elements consist of traffic volumes, pedestrian volumes, crash history, and other factors. The MUTCD explicitly states that a traffic control signal should not be installed unless one or more of the signal warrants in the manual are met. However, the satisfaction of a warrant does not entirely in itself justify the need for a traffic signal. Sometimes further engineering studies and judgments also need to be applied before justifying the need for a traffic signal to be installed. These further studies are a very important step in ensuring that an installation of a traffic signal will not actually bring about degradations in safety and efficiencies.

The MUTCD defines 9 different warrants, two of which are potentially applicable for this intersection at this time and are explained below:

- Warrant 1, Eight-Hour Vehicular Volume:

Warrant 1 is comprised of 2 conditions - A and B. The Minimum Vehicular Volume, Condition A, is intended for application where the volume of intersecting traffic is the principal reason for consideration of signal installation. The Interruption of Continuous Traffic, Condition B, is intended for
application at locations where Condition A is not satisfied and where the traffic volume on a major street is so heavy that traffic on a minor intersecting street suffers excessive delay or conflict in entering or crossing the major street.
= Warrant 2, Four-Hour Vehicular Volume:
The Four-Hour Vehicular Volume signal warrant conditions are intended to be applied where the volume of intersecting traffic is the principal reason to consider installing a traffic control signal.

The intersection of Millertown Pike and Glen Creek Road was evaluated for possible justification for a traffic signal based on the MUTCD Warrants listed above and the projected 2022 traffic count volumes. Glen Creek Road was used as the minor side street for the warrant analysis and Millertown Pike was the major street. The analysis shows that this intersection does not meet Warrant 1 or 2 in the projected 2022 conditions. The results of the traffic signal warrant assessment at this intersection for the projected volumes of 2022 are in Appendix K.

1e) As part of the analysis of the intersection, the projected queue length of the northbound lane on Glen Creek Road in the year 2022 was calculated.

To estimate the projected queue length, SimTraffic (Version 8) software was employed. SimTraffic performs micro-simulation and animation of vehicular traffic and calculates various vehicle parameters such as intersection vehicle queue lengths. Based on the projected volumes during the AM and PM peak hours, the $9^{\text {th }}$ percentile queue lengths were calculated. The $95^{\text {th }}$ percentile queue is the recognized measurement in the traffic engineering profession as the design standard used when considering vehicle queue lengths. A 95th percentile queue means that there is a $95 \%$ certainty the queue will not extend beyond that point. The calculated queue results were based on averaging the outcome obtained during 10 traffic simulations. The queue results from the SimTraffic software are in Appendix L.

The results shown in the Appendix indicate that the $95^{\text {th }}$ percentile queue length for the northbound approach of Glen Creek Road at Millertown Pike was
calculated to be 31 feet during the projected AM peak hour and 31 feet during the projected PM peak hour in the year 2022. This would indicate that even though the level of service will be quite poor during these peak hours, the estimated queue lengths are reasonable. A queue length of 31 feet would be just over one car length.

If the projected turns at the northbound approach at the intersection of Millertown Pike at Glen Creek Road were more balanced between left and right turns, an argument could be made to recommend separate left and right turn lanes. Since the vast majority of northbound traffic will turn left to head west, coupled with the minimal queue lengths, it is believed that constructing another lane would not be justified despite the poor level of service during the peak periods.

1f) Based on the number of crashes reported at the intersection of Millertown Pike at Glen Creek Road, and the section on Millertown Pike for the past 3 years; it does not appear that the calculated crash rates are considered high enough to obtain TDOT safety funding.

1g) The approach of Glen Creek Road at Millertown Pike has a Stop Sign (R1-1) installed but it is recommended to also have a 24 " white stop bar installed.

## 2) Old Millertown Pike at Glen Creek Road

2a) The intersection of Old Millertown Pike at Glen Creek Road was calculated to operate very well with respect to level of service under unsignalized conditions in the year 2022.

2b) Vegetation in the landscaped island on Glen Creek Road could cause issues with sight distance if it is not properly maintained. Landscaping will need to be maintained on a regular basis to ensure proper sight distance. The image below gives an indication of the current view available looking south on Glen Creek from Old Millertown Pike.


Sight Distance Looking South from Old Millertown Pike at Glen Creek Road

2c) The approach of Old Millertown Pike at Glen Creek Road has a Stop Sign (R11) installed but it is recommended to also have a 24 " white stop bar installed.

## 3) Glen Creek Road at Laurel Creek Way / Meadow Wells Drive

3a) The intersection of Glen Creek Road at Laurel Creek Way / Meadow Wells Drive was calculated to operate very well with respect to level of service under unsignalized (roundabout) conditions in the year 2022.

3b) The existing roundabout approaches need to be marked with the appropriate pavement markings as shown in Chapter 7 of the Roundabout - An Informational Guide, 2nd Edition and in the MUTCD. At a minimum, it is recommended that the splitter islands be marked with yellow lines on each side of the islands and with a gore area to help delineate the separation of traffic and the presence of the splitter islands. It is also recommended that a wide dotted white extension of the circulatory roadway edge line be installed at each roundabout entering approach. Refer to Chapter 3C, Roundabout Markings in the MUTCD for further details.


3c) Intersection sight distance at the roundabout must not be impacted by future landscaping or signage. The landscaped vegetation will need to be maintained in the future.

## 4) Millertown Pike at Sable Point Lane / Mary Emily Lane

4a) This intersection was calculated to be operating poorly in the PM peak hour with respect to the level of service for the northbound during the existing conditions. The northbound approach was calculated to operate at LOS E currently and estimated to be LOS F in the year 2022. For the analysis of this intersection in the year 2022, no traffic volumes were added or removed except for the thru volumes on Millertown Pike associated with the increased trips generated to and from the east for the Clear Spring development. This intersection currently provides the sole access to Millertown Pike for the Meadows of Millertown subdivision.

This intersection was included in this study due to the possibility for the second phase of Clear Spring to include completing a road link in between the Clear Spring development and the existing residential development to the east, Meadows of

Millertown, by extending Parasol Lane. This would provide both residential developments with secondary access points to and from Millertown Pike. If this link is provided, it is estimated that a portion of the traffic generated by the Meadows of Millertown could shift their driving patterns by utilizing this link. It is assumed that this link will be attractive to some of the Meadows of Millertown residents to reduce their travel times since most of the traffic in the study area travels to and from the west. For the same reason, it is not expected that any traffic to and from the Clear Spring development will utilize this potential link to access the intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane to and from the east.

Based on projected travel times, at most, it is estimated that 50 homes (some of the homes on Parasol Lane, and the homes on Mosaic Lane, Grasswalk Lane, Gateswalk Lane, and Wallflower Lane) out of the existing 201 lots of Meadows of Millertown would consider traveling to and from the Clear Spring development to reduce travel time and distance. 50 single-family detached homes would result in an additional 45 trips during the AM peak hour and 57 trips during the PM peak hour traveling to the intersection of Millertown Pike at Glen Creek Road via Parasol Lane and would cause a similar reduction of the number of trips at the intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane.

However, it is theorized that some of these residents using the new route via Parasol Lane would reconsider and return to using the intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane. As more residents use this new road link and delays increase at the intersection of Millertown Pike at Glen Creek Road, the residents will perceive that the travel time and distance saved is negated and will revert to the intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane.

4b) As part of the analysis of the intersection, the projected queue length of the northbound lane on Sable Point Lane at Millertown Pike in the year 2022 was calculated. To estimate the projected queue length, SimTraffic (Version 8) software was employed. Based on the projected volumes during the AM and PM peak hours, the $95^{\text {th }}$ percentile queue distance was calculated. The calculated queue results were
based on averaging the outcome obtained during 10 traffic simulations. The queue results from the SimTraffic software are in Appendix L.

The results shown in the Appendix indicate that the $95^{\text {th }}$ percentile queue length for the northbound approach of Sable Point Lane at Millertown Pike was calculated to be 65 feet during the projected AM peak hour and 61 feet during the projected PM peak hour in the year 2022. This would indicate that even though the level of service will be quite poor during the peak hours, the estimated queue lengths are reasonable. A queue length of 68 feet would be around three car lengths.

If the projected turns at the northbound approach at the intersection of Millertown Pike at Sable Point Lane / Mary Emily Lane were more balanced between left and right turns, an argument could be made to recommend separate left and right turn lanes. Since the vast majority of northbound traffic will turn left to head west, coupled with the minimal queue lengths, it is believed that constructing another lane would not be justified despite the poor level of service during the peak periods.

## 5) Parasol Lane Road Connection

As described earlier, with the construction of The Highlands at Clear Spring, the developer is offering to provide a connection between the existing residential subdivisions of Clear Springs Plantation and the Meadows of Millertown. This link would provide a
 secondary access point
for each subdivision to Millertown Pike.

The proposed road connection link will occur in between Autumn Creek Drive and Parasol Lane. Parasol Lane will need to be extended approximately 215 feet. The corridor where the road connection would traverse in between the two subdivisions is currently an empty lot in the Clear Springs Plantation subdivision. The road connection (via the extension of Parasol Lane) will require a Stop Sign (R1-1) be installed for the westbound approach at Autumn Creek Drive. Based on a posted speed limit of 25 mph within the subdivision, sight distance at this intersection will need to be provided to ensure that there is at least 250 feet of sight distance looking north and south from Parasol Lane on Autumn Creek Drive. This may require obtaining a sight distance easement for the properties to the northwest due to the sharp horizontal curve of Autumn Creek Drive.


## 6) The Highlands at Clear Spring Subdivision Internal Roads

The current concept plan shows three new roads and the extension of two existing roads being constructed within The Highlands at Clear Spring as shown in Figure 3.

6a) It is recommended that a $25-\mathrm{mph}$ speed limit be posted at the entrance of the Clear Spring development on Glen Creek Road just to the south of Old Millertown Pike.

6b) Stop Signs (R1-1) should be installed at the internal intersections as shown below:


6c) All drainage grates and covers for the residential development need to be pedestrian and bicycle-safe.

6d) Sight distance at the new internal intersections must not be impacted by new signage, future landscaping, or parked vehicles.

6e) The internal sidewalks that are proposed for the development should have appropriate ADA compliant curbed ramps at intersection corners and the sidewalks are recommended to be 5 feet minimum in width.

6f) All road grade and intersection elements internally and externally should be designed to AASHTO, TDOT, and Knoxville Engineering specifications and guidelines to ensure proper operation.

APPENDIX A
Historical Traffic Count Data

## Historical Traffic Counts

Organization: TDOT
Station ID \#: 000261
Location: Millertown Pike (North of John Sevier)


2006-2016 Growth Rate $=\quad 22.0 \%$
Average Annual Growth Rate = $2.1 \%$

## Traffic History



## APPENDIX B

RAILROAD INFORMATION

## U. S. DOT CROSSING INVENTORY FORM

## DEPARTMENT OF TRANSPORTATION

FEDERAL RAILROAD ADMINISTRATION
OMB No. 2130-0017

Instructions for the initial reporting of the following types of new or previously unreported crossings: For public highway-rail grade crossings, complete the entire inventory Form. For private highway-rail grade crossings, complete the Header, Parts I and II, and the Submission Information section. For public pathway grade crossings (including pedestrian station grade crossings), complete the Header, Parts I and II, and the Submission Information section. For Private pathway grade crossings, complete the Header, Parts I and II, and the Submission Information section. For grade-separated highway-rail or pathway crossings (including pedestrian station crossings), complete the Header, Part I, and the Submission Information section. For changes to existing data, complete the Header, Part I Items 1-3, and the Submission Information section, in addition to the updated data fields. Note: For private crossings only, Part I Item 20 and Part III Item 2.K. are required unless otherwise noted. An asterisk * denotes an optional field.

| A. Revision Date | B. Reporting Agency |  | C. Reason for Update (Select only one) |  |  | $\square$ No Train | $\square$ Quiet | D. DOT Crossing Inventory Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (MM/DD/YYYY) | $\pm$ Railroad | $\square$ Transit | $\mathbf{x}$ Change in | $\square$ New | $\square$ Closed |  |  |  |
|  | $\square$ State | $\square$ Other | Data <br> $\square$ Re-Open | Crossing <br> $\square$ Date | $\square$ Change in Primary | Traffic <br> $\square$ Admin. | Zone Update | 730480D |
|  |  |  |  | Change Only | Operating RR | Correction |  |  |

## Part I: Location and Classification Information



## U. S. DOT CROSSING INVENTORY FORM



DFPARTMFNT OF TRANSPORTATION
HIGHWAY-RAIL GRADF CROSSING
ACCIDENT/INCIDENT REPORT
FEDERAL RAILROAD ADMINISTRATION (FRA)
OMB Approval No. 2130-0500


20c. State the name and quantity of the hazardous material released, if any


42. Driver Passed Standing
Code
43. View of Track Obscured by (primary obstruction)

Highway Vehicle

| 1. Yes | 2. No $\quad$ 3. Unknown | 2 |
| :--- | :--- | :--- |


| Casualties to: | Killed | Injured | 44. Driver was <br> 1. Killed 2. Injured $\quad$ 3. Uninjured | 3 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| 45. Was Driver in the Vehicle? <br> 1. Yes 2. No |
| :--- |

DFPARTMENT OF TRANSPORTATION
HIGHWAY-RAII GRADF CROSSING
ACCIDENT/INCIDENT REPORT
FEDERAL RAILROAD ADMINISTRATION (FRA)
OMB Approval No. 2130-0500


20c. State the name and quantity of the hazardous material released, if any



## APPENDIX C

WALk Score

## Walk Score

(from walkscore.com)

| Walk S | core ${ }^{\circ}$ | Ger Scores | Find Aparments | My Favorties | Add to Your stie |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (3) Type an address, nelghborhood or cty co |  |  |  |  |  |
| 5431 Laurel Creek Way <br> Knoxville, Tennessee, 37924 <br> Commute to Downtown Knoxville <br> © 14 min 46 min (क) $43 \mathrm{~min} \quad 60+\mathrm{min}$ View Routes |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| More atour 54311 aurel Creek Way me |  |  |  |  |  |
| Car-Dependent |  |  |  |  |  |
| Minimal Transit <br> 24 <br> It is possible to get on a bus. |  |  |  |  |  |
| About your score |  |  |  |  |  |
| Add scores to your site |  |  |  |  |  |

## Scores for 5431 Laurel Creek Way





| Walk Score | Transit Score | Bike Score |
| ---: | :--- | :--- |
| Transit Score measures how well a location is served by public transit |  |  |
| based on the distance and type of nearby transit lines. |  |  |

## Travel Time Map

Explore how far you can travel by car, bus, bike and foot from 5431 Laurel Creek Way.



APPENDIX D
Knoxville Area Transit Map and Information



## SERVES:

A Broadway Towers
A Carmike 10 Cinemas
A. Knoxville Center Mall
$\star$ Knoxville Station/Downtown

# Regal Knoxville Center 10 

 Walmart: Millertown Pike
## Weekday Schedule Route 23: Millertown




## Saturday-Sunday Schedule Route 23: Millertown

|  | Going away from downtown |  |  |  |  |  |  | Going toward downtown |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (T) Transfer to: |  |  |  |  | Rt. 90 <br> Westbound <br> Knoxville <br> Center Mall <br> (Arrives) <br> 6 | $\begin{gathered} \text { Bus Goes } \\ \text { OnTo } \\ \text { Serve } \\ \hline \end{gathered}$ | Knoxville Center Mall (Leaves) 6 | Walmart | Washington at Fairview | Broadway Towers | Sixth at Grainger | Knoxville Station |
|  | Knoxville StationPlatform I | Grainger at Sixth | Broadway Towers | Nadine at Washington Pk | Walmart |  |  |  |  |  |  |  |  |
| SATURDAY SCHEDULE |  |  |  |  |  |  |  |  |  |  |  |  |  |
| A.M. | - | - | - | - | - | - | - | 7:30 | 7:37 | 7:49 | - | 7:56 | 8:10 |
|  | 7:15 | 7:24 | - | 7:29 | 7:45 | 7:55 | Rt. 33 | 8:30 | 8:37 | 8:49 | - | 8:56 | 9:10 |
|  | 8:15 | 8:24 | - | 8:29 | 8:45 | 8:55 | Rt. 33 | 9:30 | 9:37 | 9:49 | - | 9:56 | 10:10 |
|  | 9:15 | 9:24 | - | 9:29 | 9:45 | 9:55 | Rt. 33 | 10:30 | 10:37 | 10:49 | - | 10:56 | 11:10 |
|  | 10:15 | 10:24 | - | 10:29 | 10:45 | 10:55 | Rt. 33 | 11:30 | 11:37 | 11:49 | - | 11:56 | 12:10 |
|  | 11:15 | 11:24 | - | 11:29 | 11:45 | 11:55 | Rt. 33 | 12:30 | 12:37 | 12:49 | - | 12:56 | 1:10 |
| P.M. | 12:15 | 12:24 | - | 12:29 | 12:45 | 12:55 | Rt. 33 | 1:30 | 1:37 | 1:49 | - | 1:56 | 2:10 |
|  | 1:15 | 1:24 | - | 1:29 | 1:45 | 1:55 | Rt. 33 | 2:30 | 2:37 | 2:49 | - | 2:56 | 3:10 |
|  | 2:15 | 2:24 | - | 2:29 | 2:45 | 2:55 | Rt. 33 | 3:30 | 3:37 | 3:49 | - | 3:56 | 4:10 |
|  | 3:15 | 3:24 | - | 3:29 | 3:45 | 3:55 | Rt. 33 | 4:30 | 4:37 | 4:49 | - | 4:56 | 5:10 |
|  | 4:15 | 4:24 | - | 4:29 | 4:45 | 4:55 | Rt. 33 | 5:30 | 5:37 | 5:49 | - | 5:56 | 6:10 |
|  | 5:15 | 5:24 | - | 5:29 | 5:45 | 5:55 | Rt. 33 | 6:30 | 6:37 | 6:49 | - | 6:56 | 7:10 |
|  | 6:15 | 6:24 | - | 6:29 | 6:45 | 6:55 | Rt. 33 | 7:30 | 7:37 | 7:49 | - | 7:56 | 8:10 |
|  | 7:15 | 7:24 | - | 7:29 | 7:45 | 7:55 | Rt. 33 | 8:30 | 8:37 | 8:49 | - | 8:56 | 9:10 |
|  | 8:15 | 8:24 | - | 8:29 | 8:45 | 8:55 | Rt. 33 | 9:30 | 9:37 | 9:49 | - | 9:56 | 10:10 |
|  | 9:15 | 9:24 | - | 9:29 | 9:45 | 9:55 | Rt. 33 | 10:30 | 10:37 | 10:49 | - | 10:56 | 11:10 |
|  | 10:15 | 10:24 | - | 10:29 | 10:45 | 10:55 | - | 1-40 to Dow | wntown | - | - | - | 11:10 |
|  | 11:15 | 11:24 | - | 11:29 | 11:45 | To Garage |  |  |  |  |  |  |  |
| SUNDAY SCHEDULE |  |  |  |  |  |  |  |  |  |  |  |  |  |
| A.M. | - | - | - | - | - | - | - | 7:30 | 7:37 | 7:49 | - | 7:56 | 8:10 |
|  | - | - | - | - | - | - | - | 8:30 | 8:37 | 8:49 | - | 8:56 | 9:10 |
|  | 8:15 | 8:24 | - | 8:29 | 8:45 | 8:55 | Rt. 33 | 9:30 | 9:37 | 9:49 | - | 9:56 | 10:10 |
|  | 9:15 | 9:24 | - | 9:29 | 9:45 | 9:55 | Rt. 33 | 10:30 | 10:37 | 10:49 | - | 10:56 | 11:10 |
|  | 10:15 | 10:24 | - | 10:29 | 10:45 | 10:55 | Rt. 33 | 11:30 | 11:37 | 11:49 | - | 11:56 | 12:10 |
|  | 11:15 | 11:24 | - | 11:29 | 11:45 | 11:55 | Rt. 33 | 12:30 | 12:37 | 12:49 | - | 12:56 | 1:10 |
| P.M. | 12:15 | 12:24 | - | 12:29 | 12:45 | 12:55 | Rt. 33 | 1:30 | 1:37 | 1:49 | - | 1:56 | 2:10 |
|  | 1:15 | 1:24 | - | 1:29 | 1:45 | 1:55 | Rt. 33 | 2:30 | 2:37 | 2:49 | - | 2:56 | 3:10 |
|  | 2:15 | 2:24 | - | 2:29 | 2:45 | 2:55 | Rt. 33 | 3:30 | 3:37 | 3:49 | - | 3:56 | 4:10 |
|  | 3:15 | 3:24 | - | 3:29 | 3:45 | 3:55 | Rt. 33 | 4:30 | 4:37 | 4:49 | - | 4:56 | 5:10 |
|  | 4:15 | 4:24 | - | 4:29 | 4:45 | 4:55 | Rt. 33 | 5:30 | 5:37 | 5:49 | - | 5:56 | 6:10 |
|  | 5:15 | 5:24 | - | 5:29 | 5:45 | 5:55 | Rt. 33 | 6:30 | 6:37 | 6:49 | - | 6:56 | 7:10 |
|  | 6:15 | 6:24 | - | 6:29 | 6:45 | 6:55 | Rt. 33 | 7:30 | 7:37 | 7:49 | - | 7:56 | 8:10 |
|  | 7:15 | 7:24 | - | 7:29 | 7:45 | 7:55 | - | To Garage |  |  |  |  |  |
|  | 8:15 | 8:24 | - | 8:29 | 8:45 | 8:55 | - | To Garage |  |  |  |  |  |

Need help reading this schedule?
Need other general information on how to ride?
Click here to Download the General Schedule Information pdf available from katbus.com

## APPENDIX E

ZONING MAP


## APPENDIX F

Manual Traffic Count Data

TRAFFIC COUNT DATA

|  | Millertown Pike |  | Glen Creek Road |  | Millertown Pike |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { TIME } \\ \text { BEGIN } \\ \hline \end{gathered}$ | WESTBOUND |  | NORTHBOUND |  | EASTBOUND |  | VEHICLE TOTAL | PEAK HOUR |
|  | LT | THRU | LT | RT | THRU | RT |  |  |
| 7:00 AM | 0 | 79 | 8 | 0 | 27 | 1 | 115 |  |
| 7:15 AM | 2 | 117 | 6 | 1 | 31 | 3 | 160 | 7:15 AM - 8:15 AM |
| 7:30 AM | 3 | 127 | 3 | 1 | 30 | 8 | 172 |  |
| 7:45 AM | 4 | 104 | 10 | 1 | 27 | 5 | 151 |  |
| 8:00 AM | 1 | 80 | 7 | 1 | 37 | 6 | 132 |  |
| 8:15 AM | 2 | 76 | 3 | 1 | 34 | 5 | 121 |  |
| 8:30 AM | 1 | 77 | 8 | 1 | 24 | 3 | 114 |  |
| 8:45 AM | 1 | 69 | 8 | 2 | 35 | 4 | 119 |  |
| TOTAL | 14 | 729 | 53 | 8 | 245 | 35 | 1084 |  |
|  |  |  |  |  |  |  |  |  |
| 11:00 AM | 0 | 51 | 6 | 2 | 41 | 3 | 103 |  |
| 11:15 AM | 0 | 51 | 4 | 3 | 52 | 6 | 116 |  |
| 11:30 AM | 2 | 57 | 3 | 1 | 58 | 4 | 125 |  |
| 11:45 AM | 0 | 47 | 4 | 3 | 50 | 2 | 106 |  |
| 12:00 PM | 0 | 73 | 12 | 0 | 70 | 5 | 160 | 12:00 PM - 1:00 PM |
| 12:15 PM | 4 | 69 | 5 | 2 | 70 | 10 | 160 |  |
| 12:30 PM | 0 | 56 | 7 | 2 | 81 | 9 | 155 |  |
| 12:45 PM | 3 | 54 | 6 | 1 | 63 | 6 | 133 |  |
| TOTAL | 9 | 458 | 47 | 14 | 485 | 45 | 1058 |  |
|  |  |  |  |  |  |  |  |  |
| 2:00 PM | 1 | 65 | 8 | 4 | 75 | 4 | 157 |  |
| 2:15 PM | 1 | 52 | 3 | 4 | 61 | 5 | 126 |  |
| 2:30 PM | 1 | 48 | 6 | 3 | 68 | 5 | 131 |  |
| 2:45 PM | 0 | 50 | 5 | 1 | 82 | 11 | 149 |  |
| 3:00 PM | 0 | 59 | 5 | 4 | 88 | 9 | 165 |  |
| 3:15 PM | 3 | 69 | 5 | 4 | 85 | 4 | 170 |  |
| 3:30 PM | 2 | 61 | 4 | 3 | 79 | 4 | 153 |  |
| 3:45 PM | 2 | 45 | 9 | 2 | 83 | 9 | 150 |  |
| 4:00 PM | 0 | 48 | 7 | 2 | 95 | 7 | 159 |  |
| 4:15 PM | 1 | 69 | 9 | 4 | 127 | 11 | 221 |  |
| 4:30 PM | 0 | 73 | 5 | 7 | 112 | 7 | 204 |  |
| 4:45 PM | 3 | 51 | 7 | 6 | 98 | 7 | 172 |  |
| 5:00 PM | 3 | 64 | 11 | 10 | 127 | 6 | 221 | 5:00 PM - 6:00 PM |
| 5:15 PM | 2 | 65 | 7 | 14 | 116 | 4 | 208 |  |
| 5:30 PM | 0 | 83 | 7 | 7 | 116 | 8 | 221 |  |
| 5:45 PM | 0 | 106 | 6 | 7 | 99 | 4 | 222 |  |
| TOTAL | 16 | 793 | 82 | 70 | 1225 | 80 | 2266 |  |

Existing Traffic Volumes were collected and tabulated using CountCam System
Unadjusted School Volumes

|  | Millertown Pike |  | Glen Creek Road |  | Millertown Pike |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | WESTBOUND |  | NORTHBOUND |  | EASTBOUND |  |
| BEGIN | LT | THRU | LT | RT | THRU | RT |
| 7:15 AM | 2 | 117 | 6 | 1 | 31 | 3 |
| 7:30 AM | 3 | 127 | 3 | 1 | 30 | 8 |
| $7: 45 \mathrm{AM}$ | 4 | 104 | 10 | 1 | 27 | 5 |
| 8:00 AM | 1 | 80 | 7 | 1 | 37 | 6 |
| TOTAL | 10 | 428 | 26 | 4 | 125 | 22 |
| PHF | 0.63 | 0.84 | 0.65 | 1.00 | 0.84 | 0.69 |

Unadjusted School Volumes

## 2018 Mid-Day Peak Hour

12:00 PM - 1:00 PM

|  | Millertown Pike |  | Glen Creek Road |  | Millertown Pike |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | WESTBOUND |  | NORTHBOUND |  | EASTBOUND |  |
|  | LT | THRU | LT | RT | THRU | RT |
| 12:00 PM | 0 | 73 | 12 | 0 | 70 | 5 |
| 12:15 PM | 4 | 69 | 5 | 2 | 70 | 10 |
| 12:30 PM | 0 | 56 | 7 | 2 | 81 | 9 |
| 12:45 PM | 3 | 54 | 6 | 1 | 63 | 6 |
| TOTAL | 7 | 252 | 30 | 5 | 284 | 30 |
| PHF | 0.44 | 0.86 | 0.63 | 0.63 | 0.88 | 0.75 |

Unadjusted School Volumes

2018 PM Peak Hour
5:00 PM - 6:00 PM

|  | Millertown Pike |  | Glen Creek Road |  | Millertown Pike |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | WESTBOUND |  | NORTHBOUND |  | EASTBOUND |  |
|  | LTG | THRU | LT | RT | THRU | RT |
| 5:00 PM | 3 | 64 | 11 | 10 | 127 | 6 |
| 5:15 PM | 2 | 65 | 7 | 14 | 116 | 4 |
| 5:30 PM | 0 | 83 | 7 | 7 | 116 | 8 |
| 5:45 PM | 0 | 106 | 6 | 7 | 99 | 4 |
| TOTAL | 5 | 318 | 31 | 38 | 458 | 22 |
| PHF | 0.42 | 0.75 | 0.70 | 0.68 | 0.90 | 0.69 |

Unadjusted School Volumes

|  | Glen Creek Road |  |  | Glen Creek Road |  | Old Millertown Pike |  | VEHICLE TOTAL | PEAK HOUR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | SOUTHBOUND |  |  | NORTHBOUND |  | EASTBOUND |  |  |  |
| BEGIN | THRU | RT | U-TURN | LT | THRU | LT | RT |  |  |
| 7:00 AM | 1 | 0 | 0 | 1 | 8 | 0 | 0 | 10 |  |
| 7:15 AM | 3 | 2 | 0 | 0 | 7 | 0 | 0 | 12 | 7:15 AM - 8:15 AM |
| 7:30 AM | 8 | 2 | 1 | 2 | 3 | 1 | 1 | 18 |  |
| 7:45 AM | 7 | 3 | 0 | 1 | 9 | 2 | 0 | 22 |  |
| 8:00 AM | 5 | 1 | 1 | 0 | 7 | 0 | 1 | 15 |  |
| 8:15 AM | 5 | 1 | 1 | 0 | 3 | 0 | 1 | 11 |  |
| 8:30 AM | 2 | 2 | 0 | 2 | 8 |  | 2 | 17 |  |
| 8:45 AM | 3 | 1 | 1 | 0 | 7 | 2 | 0 | 14 |  |
| TOTAL | 34 | 12 | 0 | 6 | 52 | 6 | 5 | 115 |  |
|  |  |  |  |  |  |  |  |  |  |
| 3:00 PM | 5 | 3 | 1 | 0 | 4 | 4 | 1 | 18 |  |
| 3:15 PM | 4 | 2 | 1 | 0 | 7 | 1 | 0 | 15 |  |
| 3:30 PM | 3 | 2 | 1 | 0 | 3 | 5 | 1 | 15 |  |
| 3:45 PM | 6 | 3 | 2 | 0 | 7 | 2 | 1 | 21 |  |
| 4:00 PM | 7 | 0 | 0 | 1 | 6 | 2 | 1 | 17 |  |
| 4:15 PM | 10 | 1 | 1 | 0 | 8 | 4 | 0 | 24 |  |
| 4:30 PM | 7 | 0 | 0 | 3 | 6 | 6 | 3 | 25 | 4:30 PM - 5:30 PM |
| 4:45 PM | 8 | 2 | 0 | 0 | 8 | 5 | 3 | 26 |  |
| 5:00 PM | 4 | 4 | 1 | 1 | 11 | 9 | 3 | 33 |  |
| 5:15 PM | 6 | 0 | 0 | 1 | 12 | 11 | 0 | 30 |  |
| 5:30 PM | 7 | 0 | 1 | 0 | 4 | 7 | 1 | 20 |  |
| 5:45 PM | 5 | 0 | 0 | 0 | 6 | 7 | 2 | 20 |  |
| TOTAL | 72 | 17 | 8 | 6 | 82 | 63 | 16 | 264 |  |

Existing Traffic Volumes were collected and tabulated using CountCam System
Unadjusted School Volumes
2018 AM Peak Hour
7:15 AM - 8:15 AM

|  | Glen Creek Road |  |  | Glen Creek Road |  | Old Millertown Pike |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | SOUTHBOUUND |  | NORTHBOUND |  | EASTBOUND |  |  |
|  | BEGIN | THRU | RT | U-TURN | LT | THRU | LT |
| 7:15 AM | 3 | 2 | 0 | 0 | 7 | 0 | 0 |
| 7:30 AM | 8 | 2 | 1 | 2 | 3 | 1 | 1 |
| $7: 45 \mathrm{AM}$ | 7 | 3 | 0 | 1 | 9 | 2 | 0 |
| 8:00 AM | 5 | 1 | 1 | 0 | 7 | 0 | 1 |
| TOTAL | 23 | 8 | 2 | 3 | 26 | 3 | 2 |
| PHF | 0.72 | 0.67 | 0.50 | 0.38 | 0.72 | 0.38 | 0.50 |

Unadjusted School Volumes
2018 PM Peak Hour
4:30 PM - 5:30 PM

|  | Glen Creek Road |  |  | Glen Creek Road |  | Old Millertown Pike |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | SOUTHBOUND |  | NORTHBOUND |  | EASTBOUND |  |  |
| BEGGI | THRU | RT | U-TURN | LT | THRU | LT | RT |
| 4:30 PM | 7 | 0 | 0 | 3 | 6 | 6 | 3 |
| 4:45 PM | 8 | 2 | 0 | 0 | 8 | 5 | 3 |
| 5:00 PM | 4 | 4 | 1 | 1 | 11 | 9 | 3 |
| 5:15 PM | 6 | 0 | 0 | 1 | 12 | 11 | 0 |
| TOTAL | 25 | 6 | 1 | 5 | 37 | 31 | 9 |
| PHF | 0.78 | 0.38 | 0.25 | 0.42 | 0.77 | 0.70 | 0.75 |

Unadjusted School Volumes

|  | Glen Creek Road |  |  | Meadow Wells Drive |  |  | Glen Creek Road |  |  | Laurel Creek Way |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \hline \text { TIME } \\ \text { BEGIN } \end{gathered}$ | SOUTHBOUND |  |  | WESTBOUND |  |  | NORTHBOUND |  |  | EASTBOUND |  |  | VEHICLE TOTAL | $\begin{aligned} & \hline \hline \text { PEAK } \\ & \text { HOUR } \end{aligned}$ |
|  | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT |  |  |
| 7:00 AM | 0 | 0 | 2 | 0 | 0 | 6 | 0 | 0 | 0 | 3 | 0 | 0 | 11 |  |
| 7:15 AM | 1 | 0 | 2 | 0 | 1 | 5 | 0 | 0 | 0 | 2 | 0 | 0 | 11 |  |
| 7:30 AM | 1 | 0 | 5 | 0 | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 12 | 7:30 AM - 8:30 AM |
| 7:45 AM | 3 | 0 | 4 | 0 | 0 | 9 | 0 | 0 | 0 | 1 | 0 | 0 | 17 |  |
| 8:00 AM | 1 | 0 | 4 | 0 | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 0 | 12 |  |
| 8:15 AM | 3 | 0 | 5 | 0 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 12 |  |
| 8:30 AM | 2 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 10 |  |
| 8:45 AM | 1 | 0 | 2 | 0 | 0 | 6 | 0 | 0 | 0 | 2 | 0 | 0 | 11 |  |
| TOTAL | 12 | 0 | 24 | 0 | 1 | 41 | 0 | 0 | 0 | 18 | 0 | 0 | 96 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM | 4 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 1 | 0 | 11 |  |
| 3:15 PM | 1 | 0 | 2 | 0 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 0 | 10 |  |
| 3:30 PM | 3 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 8 |  |
| 3:45 PM | 4 | 0 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 0 | 14 |  |
| 4:00 PM | 5 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 6 | 1 | 0 | 15 |  |
| 4:15 PM | 6 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 4 | 0 | 0 | 18 | 4:15 PM - 5:15 PM |
| 4:30 PM | 6 | 0 | 5 | 0 | 0 | 6 | 0 | 0 | 0 | 4 | 0 | 0 | 21 |  |
| 4:45 PM | 8 | 0 | 3 | 0 | 0 | 6 | 0 | 0 | 0 | 2 | 0 | 0 | 19 |  |
| 5:00 PM | 3 | 0 | 3 | 0 | 0 | 5 | 0 | 0 | 0 | 4 | 0 | 0 | 15 |  |
| 5:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 7 | 0 | 0 | 17 |  |
| 5:30 PM | 7 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 0 | 12 |  |
| 5:45 PM | 4 | 0 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 0 | 14 |  |
| TOTAL | 56 | 0 | 29 | 0 | 0 | 47 | 0 | 0 | 0 | 39 | 3 | 0 | 174 |  |

Existing Traffic Volumes were collected and tabulated using CountCam System
Unadjusted School Volumes

2018 AM Peak Hour
7:30 AM - 8:30 AM


Unadjusted School Volumes

2018 PM Peak Hour
4:15 PM - 5:15 PM

|  | Glen Creek Road |  |  | Meadow Wells Drive |  |  | Glen Creek Road |  |  | Laurel Creek Way |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | SOUTHBOUND |  |  | WESTBOUND |  |  | NORTHBOUND |  |  | EASTBOUND |  |  |
| BEGIN | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT |
| 4:15 PM | 6 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 4 | 0 | 0 |
| 4:30 PM | 6 | 0 | 5 | 0 | 0 | 6 | 0 | 0 | 0 | 4 | 0 | 0 |
| 4:45 PM | 8 | 0 | 3 | 0 | 0 | 6 | 0 | 0 | 0 | 2 | 0 | 0 |
| 5:00 PM | 3 | 0 | 3 | 0 | 0 | 5 | 0 | 0 | 0 | 4 | 0 | 0 |
| TOTAL | 23 | 0 | 15 | 0 | 0 | 21 | 0 | 0 | 0 | 14 | 0 | 0 |
| PHF | 0.72 | - | 0.75 | - | - | 0.88 | - | - | - | 0.88 | - | - |

Unadjusted School Volumes

|  | Mary Emily Lane |  |  | Millertown Pike |  |  | Sable Point Lane |  |  | Millertown Pike |  |  | VEHICLE TOTAL | PEAK HOUR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | SOUTHBOUND |  |  | WESTBOUND |  |  | NORTHBOUND |  |  | EASTBOUND |  |  |  |  |
| BEGIN | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT |  |  |
| 7:00 AM | 0 | 0 | 2 | 0 | 58 | 0 | 16 | 0 | 1 | 0 | 26 | 2 | 105 |  |
| 7:15 AM | 0 | 0 | 1 | 3 | 85 | 0 | 23 | 0 | 0 | 0 | 23 | 3 | 138 | 7:15 AM - 8:15 AM |
| 7:30 AM | 0 | 0 | 2 | 0 | 106 | 0 | 25 | 0 | 0 | 1 | 24 | 5 | 163 |  |
| 7:45 AM | 0 | 0 | 0 | 0 | 77 | 0 | 25 | 0 | 1 | 0 | 28 | 3 | 134 |  |
| 8:00 AM | 0 | 0 | 0 | 1 | 64 | 0 | 17 | 0 | 0 | 0 | 33 | 3 | 118 |  |
| 8:15 AM | 0 | 0 | 2 | 1 | 63 | 1 | 12 | 0 | 3 | 0 | 26 | 4 | 112 |  |
| 8:30 AM | 1 | 0 | 2 | 1 | 53 | 0 | 18 | 0 | 0 | 1 | 21 | 4 | 101 |  |
| 8:45 AM | 0 | 0 | 0 | 0 | 55 | 0 | 19 | 0 | 2 | 1 | 24 | 12 | 113 |  |
| TOTAL | 1 | 0 | 9 | 6 | 561 | 1 | 155 | 0 | 7 | 3 | 205 | 36 | 984 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM | 0 | 0 | 1 | 1 | 48 | 1 | 6 | 1 | 1 | 3 | 86 | 8 | 156 |  |
| 3:15 PM | 1 | 0 | 1 | 2 | 57 | 0 | 8 | 0 | 0 | 2 | 66 | 11 | 148 |  |
| 3:30 PM | 0 | 0 | 0 | 1 | 58 | 1 | 8 | 0 | 0 | 0 | 65 | 15 | 148 |  |
| 3:45 PM | 0 | 0 | 0 | 0 | 38 | 0 | 10 | 0 | 1 | 0 | 69 | 15 | 133 |  |
| 4:00 PM | 0 | 0 | 1 | 2 | 38 | 0 | 1 | 0 | 0 | 0 | 94 | 6 | 142 |  |
| 4:15 PM | 0 | 0 | 0 | 0 | 57 | 0 | 12 | 0 | 0 | 1 | 100 | 13 | 183 |  |
| 4:30 PM | 0 | 0 | 0 | 0 | 62 | 0 | 11 | 0 | 0 | 1 | 104 | 20 | 198 |  |
| 4:45 PM | 0 | 0 | 1 | 0 | 52 | 0 | 2 | 0 | 0 | 1 | 82 | 10 | 148 |  |
| 5:00 PM | 0 | 0 | 0 | 1 | 53 | 0 | 8 | 0 | 0 | 1 | 99 | 23 | 185 | 5:00 PM - 6:00 PM |
| 5:15 PM | 0 | 0 | 1 | 0 | 55 | 0 | 10 | 0 | 1 | 2 | 121 | 20 | 210 |  |
| 5:30 PM | 1 | 0 | 2 | 1 | 71 | 1 | 9 | 1 | 1 | 1 | 104 | 17 | 209 |  |
| 5:45 PM | 0 | 0 | 2 | 1 | 81 | 0 | 21 | 0 | 1 | 2 | 89 | 18 | 215 |  |
| TOTAL | 2 | 0 | 9 | 9 | 670 | 3 | 106 | 2 | 5 | 14 | 1079 | 176 | 2075 |  |

Existing Traffic Volumes were collected and tabulated using CountCam System
Unadjusted School Volumes

2018 AM Peak Hour
7:15 AM - 8:15 AM

|  | Mary Emily Lane |  |  | Millertown Pike |  |  | Sable Point Lane |  |  | Millertown Pike |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | SOUTHBOUND |  |  | WESTBOUND |  |  | NORTHBOUND |  |  | EASTBOUND |  |  |
| BEGIN | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT | LT | THRU | RT |
| 7:15 AM | 0 | 0 | 1 | 3 | 85 | 0 | 23 | 0 | 0 | 0 | 23 | 3 |
| 7:45 AM | 0 | 0 | 2 | 0 | 106 | 0 | 25 | 0 | 0 | 1 | 24 | 5 |
| 8:00 AM | 0 | 0 | 0 | 0 | 77 | 0 | 25 | 0 | 1 | 0 | 28 | 3 |
| 8:15 AM | 0 | 0 | 0 | 1 | 64 | 0 | 17 | 0 | 0 | 0 | 33 | 3 |
| TOTAL | 0 | 0 | 3 | 4 | 332 | 0 | 90 | 0 | 1 | 1 | 108 | 14 |
| PHF | - | - | 0.38 | 0.33 | 0.78 | - | 0.90 | - | 0.25 | 0.25 | 0.82 | 0.70 |

Unadjusted School Volumes

2018 PM Peak Hour
5:00 PM - 6:00 PM


Unadjusted School Volumes

## APPENDIX G

Capacity Analyses - HCM Worksheets (Synchro 8)

| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 3.5 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | EB |  | WB |  | NB |  | SB |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 12 |  | 45 |  | 0 |  | 41 |
| Demand Flow Rate, veh/h |  | 12 |  | 45 |  | 0 |  | 41 |
| Vehicles Circulating, veh/h |  | 15 |  | 12 |  | 27 |  | 0 |
| Vehicles Exiting, veh/h |  | 26 |  | 15 |  | 0 |  | 57 |
| Follow-Up Headway, s |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.186 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 3.3 |  | 3.6 |  | 0.0 |  | 3.5 |
| Approach LOS |  | A |  | A |  | - |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Critical Headway, s | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Entry Flow, veh/h | 12 |  | 45 |  | 0 |  | 41 |  |
| Cap Entry Lane, veh/h | 1113 |  | 1116 |  | 1100 |  | 1130 |  |
| Entry HV Adj Factor | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Flow Entry, veh/h | 12 |  | 45 |  | 0 |  | 41 |  |
| Cap Entry, veh/h | 1113 |  | 1116 |  | 1100 |  | 1130 |  |
| V/C Ratio | 0.011 |  | 0.040 |  | 0.000 |  | 0.036 |  |
| Control Delay, s/veh | 3.3 |  | 3.6 |  | 3.3 |  | 3.5 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 0 |  | 0 |  | 0 |  | 0 |  |



| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.2 | 14.9 |
| HCM LOS |  |  | B |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Vol, veh/h | 1 | 135 | 18 | 5 | 415 | 0 | 113 | 0 | 1 | 0 | 0 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - |  | - | - | - |  | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 2 | - | - | -2 | - | - | 0 | - | - | 2 |  |
| Peak Hour Factor | 25 | 82 | 70 | 33 | 78 | 90 | 90 | 90 | 25 | 90 | 90 | 38 |
| Heavy Vehicles, \% | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 4 | 165 | 26 | 15 | 532 | 0 | 126 | 0 | 4 | 0 | 0 | 11 |


| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 532 | 0 | 0 | 190 | 0 | 0 | 753 | 747 | 177 | 749 | 760 | 532 |
| Stage 1 | - | - | - | - | - | - | 185 | 185 |  | 562 | 562 |  |
| Stage 2 | - | - | - | - | - | - | 568 | 562 |  | 187 | 198 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.5 | 6.9 | 6.4 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1046 | - | - | 1396 | - | - | 329 | 344 | 871 | 304 | 311 | 535 |
| Stage 1 | - | - | - | - | - | - | 821 | 751 |  | 484 | 482 |  |
| Stage 2 | - | - | - | - | - | - | 511 | 513 |  | 803 | 725 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1046 | - | - | 1396 | - | - | 318 | 337 | 871 | 298 | 305 | 535 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 318 | 337 | - | 298 | 305 |  |
| Stage 1 | - | - | - | - | - | - | 818 | 748 | - | 482 | 475 |  |
| Stage 2 | - | - | - | - | - | - | 493 | 505 | - | 796 | 722 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.2 | 0.2 | 23.3 | 11.9 |
| HCM LOS |  | $C$ | $B$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 324 | 1046 | - | -1396 | - | - | 535 |  |
| HCM Lane V/C Ratio | 0.4 | 0.004 | - | -0.011 | - | -0.02 |  |  |
| HCM Control Delay (s) | 23.3 | 8.5 | 0 | - | 7.6 | 0 | -11.9 |  |
| HCM Lane LOS | C | A | A | - | A | A | - | B |
| HCM 95th \%tile Q(veh) | 1.9 | 0 | - | - | 0 | - | - | 0.1 |


| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 3.5 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | EB |  | WB |  | NB |  | SB |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 10 |  | 41 |  | 0 |  | 36 |
| Demand Flow Rate, veh/h |  | 10 |  | 41 |  | 0 |  | 36 |
| Vehicles Circulating, veh/h |  | 13 |  | 10 |  | 23 |  | 0 |
| Vehicles Exiting, veh/h |  | 23 |  | 13 |  | 0 |  | 51 |
| Follow-Up Headway, s |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.186 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 3.3 |  | 3.5 |  | 0.0 |  | 3.5 |
| Approach LOS |  | A |  | A |  | - |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Critical Headway, s | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Entry Flow, veh/h | 10 |  | 41 |  | 0 |  | 36 |  |
| Cap Entry Lane, veh/h | 1115 |  | 1119 |  | 1104 |  | 1130 |  |
| Entry HV Adj Factor | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Flow Entry, veh/h | 10 |  | 41 |  | 0 |  | 36 |  |
| Cap Entry, veh/h | 1115 |  | 1119 |  | 1104 |  | 1130 |  |
| V/C Ratio | 0.009 |  | 0.037 |  | 0.000 |  | 0.032 |  |
| Control Delay, s/veh | 3.3 |  | 3.5 |  | 3.3 |  | 3.5 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 0 |  | 0 |  | 0 |  | 0 |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Vol, veh/h | 144 | 25 | 12 | 492 | 30 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | -5 | - | - | -2 | -5 | - |
| Peak Hour Factor | 84 | 69 | 63 | 84 | 65 | 100 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 171 | 36 | 19 | 586 | 46 | 5 |
| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| Conflicting Flow All | 0 | 0 | 208 | 0 | 814 | 190 |
| Stage 1 | - | - | - | - | 190 | - |
| Stage 2 | - | - | - | - | 624 | - |
| Critical Hdwy | - | - | 4.1 | - | 5.4 | 5.7 |
| Critical Hdwy Stg 1 | - | - | - | - | 4.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 4.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1375 | - | 439 | 880 |
| Stage 1 | - | - | - | - | 893 | - |
| Stage 2 | - | - | - | - | 640 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1375 | - | 430 | 880 |
| Mov Cap-2 Maneuver | - | - | - | - | 430 | - |
| Stage 1 | - | - | - | - | 893 | - |
| Stage 2 | - | - | - | - | 627 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.2 | 14 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 453 | - | -1375 | - |  |
| HCM Lane V/C Ratio | 0.113 | - | -0.014 | - |  |
| HCM Control Delay (s) | 14 | - | - | 7.7 | 0 |
| HCM Lane LOS | B | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.4 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Vol, veh/h | 1 | 124 | 16 | 5 | 382 | 0 | 104 | 0 | 1 | 0 | 0 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - |  | - | - | - | - | - |  | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 2 | - | - | -2 | - | - | 0 | - | - | 2 |  |
| Peak Hour Factor | 25 | 82 | 70 | 33 | 78 | 90 | 90 | 90 | 25 | 90 | 90 | 38 |
| Heavy Vehicles, \% | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 4 | 151 | 23 | 15 | 490 | 0 | 116 | 0 | 4 | 0 | 0 | 8 |
| Major/Minor | Major1 |  |  | Major2 |  |  | inor1 |  |  | inor2 |  |  |
| Conflicting Flow All | 490 | 0 | 0 | 174 | 0 | 0 | 695 | 691 | 163 | 693 | 702 | 490 |
| Stage 1 | - | - | - | - | - | - | 171 | 171 | - | 520 | 520 |  |
| Stage 2 | - | - | - | - |  | - | 524 | 520 | - | 173 | 182 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.5 | 6.9 | 6.4 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.5 | 5.9 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.5 | 5.9 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1084 | - | - | 1415 | - | - | 359 | 370 | 887 | 334 | 338 | 567 |
| Stage 1 | - | - | - | - | - | - | 836 | 761 | - | 512 | 505 | - |
| Stage 2 | - | - | - | - | - | - | 540 | 535 | - | 818 | 738 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1084 | - | - | 1415 | - | - | 349 | 363 | 887 | 328 | 332 | 567 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 349 | 363 | - | 328 | 332 | - |
| Stage 1 | - | - | - | - | - | - | 833 | 758 | - | 510 | 497 |  |
| Stage 2 | - | - | - | - | - | - | 524 | 527 | - | 811 | 735 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.2 | 0.2 | 20.1 | 11.4 |
| HCM LOS |  |  | $C$ | $B$ |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 356 | 1084 | - | -1415 | - | - | 567 |  |
| HCM Lane V/C Ratio | 0.336 | 0.004 | - | -0.011 | - | -0.014 |  |  |
| HCM Control Delay (s) | 20.1 | 8.3 | 0 | - | 7.6 | 0 | - | 11.4 |
| HCM Lane LOS | C | A | A | - | A | A | - | B |
| HCM 95th \%tile Q(veh) | 1.4 | 0 | - | - | 0 | - | - | 0 |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Vol, veh/h | 3 | 2 | 3 | 30 | 26 | 9 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 5 | - | - | -5 | 5 | - |
| Peak Hour Factor | 38 | 50 | 38 | 72 | 72 | 67 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 8 | 4 | 8 | 42 | 36 | 13 |
| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| Conflicting Flow All | 100 | 43 | 50 | 0 | - | 0 |
| Stage 1 | 43 | - | - | - | - | - |
| Stage 2 | 57 | - | - | - | - | - |
| Critical Hdwy | 7.4 | 6.7 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 6.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | 879 | 1027 | 1570 | - | - | - |
| Stage 1 | 973 | - | - | - | - | - |
| Stage 2 | 955 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 875 | 1027 | 1570 | - | - | - |
| Mov Cap-2 Maneuver | 875 | - | - | - | - | - |
| Stage 1 | 973 | - | - | - | - | - |
| Stage 2 | 950 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 9 | 1.2 | 0 |
| HCM LOS | A |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1570 | -921 | - | - |  |
| HCM Lane V/C Ratio | 0.005 | -0.013 | - | - |  |
| HCM Control Delay (s) | 7.3 | 0 | 9 | - | - |
| HCM Lane LOS | A | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0 | - | - |


| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 3.5 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | EB |  | WB |  | NB |  | SB |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 18 |  | 27 |  | 0 |  | 59 |
| Demand Flow Rate, veh/h |  | 18 |  | 27 |  | 0 |  | 59 |
| Vehicles Circulating, veh/h |  | 36 |  | 18 |  | 54 |  | 0 |
| Vehicles Exiting, veh/h |  | 23 |  | 36 |  | 0 |  | 45 |
| Follow-Up Headway, s |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.186 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 3.4 |  | 3.4 |  | 0.0 |  | 3.6 |
| Approach LOS |  | A |  | A |  | - |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Critical Headway, s | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Entry Flow, veh/h | 18 |  | 27 |  | 0 |  | 59 |  |
| Cap Entry Lane, veh/h | 1090 |  | 1110 |  | 1071 |  | 1130 |  |
| Entry HV Adj Factor | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Flow Entry, veh/h | 18 |  | 27 |  | 0 |  | 59 |  |
| Cap Entry, veh/h | 1090 |  | 1110 |  | 1071 |  | 1130 |  |
| V/C Ratio | 0.017 |  | 0.024 |  | 0.000 |  | 0.052 |  |
| Control Delay, s/veh | 3.4 |  | 3.4 |  | 3.4 |  | 3.6 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 0 |  | 0 |  | 0 |  | 0 |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.7 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Vol, veh/h | 527 | 25 | 6 | 366 | 36 | 44 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | -5 | - | - | -2 | -5 | - |
| Peak Hour Factor | 90 | 69 | 42 | 75 | 70 | 68 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 586 | 36 | 14 | 488 | 51 | 65 |
| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| Conflicting Flow All | 0 | 0 | 622 | 0 | 1121 | 604 |
| Stage 1 | - | - | - | - | 604 | - |
| Stage 2 | - | - | - | - | 517 | - |
| Critical Hdwy | - | - | 4.1 | - | 5.4 | 5.7 |
| Critical Hdwy Stg 1 | - | - | - | - | 4.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 4.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 969 | - | 314 | 546 |
| Stage 1 | - | - | - | - | 650 | - |
| Stage 2 | - | - | - | - | 696 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 969 | - | 308 | 546 |
| Mov Cap-2 Maneuver | - | - | - | - | 308 | - |
| Stage 1 | - | - | - | - | 650 | - |
| Stage 2 | - | - | - | - | 682 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.2 | 17.3 |
| HCM LOS |  |  | C |




| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 378 | 0 | 0 | 708 | 0 | 0 | 1089 | 1086 | 644 | 1088 | 1148 | 376 |
| Stage 1 | - | - | - | - | - | - | 700 | 700 | - | 384 | 384 |  |
| Stage 2 | - | - | - | - | - | - | 389 | 386 |  | 704 | 764 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.5 | 6.9 | 6.4 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.5 | 5.9 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.5 | 5.9 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1192 | - | - | 900 | - | - | 195 | 218 | 476 | 173 | 176 | 661 |
| Stage 1 | - | - | - | - | - | - | 433 | 444 | - | 616 | 589 |  |
| Stage 2 | - | - | - | - | - | - | 639 | 614 | - | 398 | 382 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1192 | - | - | 900 | - | - | 185 | 208 | 476 | 163 | 168 | 661 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 185 | 208 | - | 163 | 168 |  |
| Stage 1 | - | - | - | - | - | - | 416 | 426 | - | 591 | 585 |  |
| Stage 2 | - | - | - | - | - | - | 626 | 610 | - | 375 | 367 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.3 | 0.1 | 44.9 | 15.8 |
| HCM LOS |  |  | E | C |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 190 | 1192 | - | - | 900 | - | - | 347 |
| HCM Lane V/C Ratio | 0.55 | 0.023 | - | -0.004 | - | -0.039 |  |  |
| HCM Control Delay (s) | 44.9 | 8.1 | 0 | - | 9 | 0 | - | 15.8 |
| HCM Lane LOS | E | A | A | - | A | A | - | C |
| HCM 95th \%tile Q(veh) | 2.9 | 0.1 | - | - | 0 | - | - | 0.1 |



| Approach | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, S | 9.5 | 1.5 | 0 |
| HCM LOS | A |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1562 | -864 | - | - |  |
| HCM Lane V/C Ratio | 0.009 | -0.075 | - | - |  |
| HCM Control Delay (s) | 7.3 | 0 | 9.5 | - | - |
| HCM Lane LOS | A | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.2 | - | - |

Opening Year Traffic Conditions (Without Project)

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Vol, veh/h | 4 | 3 | 4 | 33 | 29 | 10 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 5 | - | - | -5 | 5 | - |
| Peak Hour Factor | 38 | 50 | 38 | 72 | 72 | 67 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 11 | 6 | 11 | 46 | 40 | 15 |
| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| Conflicting Flow All | 115 | 48 | 55 | 0 | - | 0 |
| Stage 1 | 48 | - | - | - | - | - |
| Stage 2 | 67 | - | - | - | - | - |
| Critical Hdwy | 7.4 | 6.7 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 6.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | 858 | 1020 | 1563 | - | - | - |
| Stage 1 | 967 | - | - | - | - | - |
| Stage 2 | 943 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 852 | 1020 | 1563 | - | - | - |
| Mov Cap-2 Maneuver | 852 | - | - | - | - | - |
| Stage 1 | 967 | - | - | - | - | - |
| Stage 2 | 936 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 9 | 1.4 | 0 |
| HCM LOS | A |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1563 | -906 | - | - |  |
| HCM Lane V/C Ratio | 0.007 | -0.018 | - | - |  |
| HCM Control Delay (s) | 7.3 | 0 | 9 | - | - |
| HCM Lane LOS | A | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | - | - |


| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 3.6 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | EB |  | WB |  | NB |  | SB |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 20 |  | 30 |  | 0 |  | 65 |
| Demand Flow Rate, veh/h |  | 20 |  | 30 |  | 0 |  | 65 |
| Vehicles Circulating, veh/h |  | 40 |  | 20 |  | 60 |  | 0 |
| Vehicles Exiting, veh/h |  | 25 |  | 40 |  | 0 |  | 50 |
| Follow-Up Headway, s |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.186 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 3.5 |  | 3.5 |  | 0.0 |  | 3.7 |
| Approach LOS |  | A |  | A |  | - |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Critical Headway, s | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Entry Flow, veh/h | 20 |  | 30 |  | 0 |  | 65 |  |
| Cap Entry Lane, veh/h | 1086 |  | 1108 |  | 1064 |  | 1130 |  |
| Entry HV Adj Factor | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Flow Entry, veh/h | 20 |  | 30 |  | 0 |  | 65 |  |
| Cap Entry, veh/h | 1086 |  | 1108 |  | 1064 |  | 1130 |  |
| V/C Ratio | 0.018 |  | 0.027 |  | 0.000 |  | 0.058 |  |
| Control Delay, s/veh | 3.5 |  | 3.5 |  | 3.4 |  | 3.7 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 0 |  | 0 |  | 0 |  | 0 |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.9 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Vol, veh/h | 573 | 28 | 6 | 398 | 39 | 48 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | -5 | - | - | -2 | -5 | - |
| Peak Hour Factor | 90 | 69 | 42 | 75 | 70 | 68 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 637 | 41 | 14 | 531 | 56 | 71 |
| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| Conflicting Flow All | 0 | 0 | 677 | 0 | 1216 | 657 |
| Stage 1 | - | - | - | - | 657 | - |
| Stage 2 | - | - | - | - | 559 | - |
| Critical Hdwy | - | - | 4.1 | - | 5.4 | 5.7 |
| Critical Hdwy Stg 1 | - | - | - | - | 4.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 4.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 924 | - | 283 | 513 |
| Stage 1 | - | - | - | - | 624 | - |
| Stage 2 | - | - | - | - | 673 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 924 | - | 277 | 513 |
| Mov Cap-2 Maneuver | - | - | - | - | 277 | - |
| Stage 1 | - | - | - | - | 624 | - |
| Stage 2 | - | - | - | - | 659 | - |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.2 | 19.5 |
| HCM LOS |  |  | C |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 6.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Vol, veh/h | 8 | 517 | 98 | 4 | 325 | 1 | 60 | 1 | 4 | 1 | 0 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - |  | - | - | - |  | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 2 | - | - | -2 | - | - | 0 | - | - | 2 |  |
| Peak Hour Factor | 25 | 82 | 70 | 75 | 80 | 25 | 57 | 25 | 75 | 25 | 90 | 63 |
| Heavy Vehicles, \% | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 32 | 630 | 140 | 5 | 406 | 4 | 105 | 4 | 5 | 4 | 0 | 10 |


| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 410 | 0 | 0 | 770 | 0 | 0 | 1188 | 1185 | 700 | 1188 | 1253 | 408 |
| Stage 1 | - | - | - | - | - | - | 764 | 764 | - | 419 | 419 |  |
| Stage 2 | - | - | - | - | - | - | 424 | 421 | - | 769 | 834 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.5 | 6.9 | 6.4 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1160 | - | - | 854 | - | - | 167 | 191 | 443 | 146 | 151 | 633 |
| Stage 1 | - | - | - | - | - | - | 399 | 416 | - | 588 | 566 |  |
| Stage 2 | - | - | - | - | - | - | 612 | 592 | - | 364 | 352 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1160 | - | - | 854 | - | - | 157 | 180 | 443 | 136 | 142 | 633 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 157 | 180 | - | 136 | 142 |  |
| Stage 1 | - | - | - | - | - | - | 379 | 395 | - | 559 | 561 |  |
| Stage 2 | - | - | - | - | - | - | 598 | 587 | - | 338 | 334 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.3 | 0.1 | 67.3 | 17.4 |
| HCM LOS |  | $F$ | $C$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 163 | 1160 | - | -854 | - | -304 |  |
| HCM Lane V/C Ratio | 0.703 | 0.028 | - | -0.006 | - | -0.044 |  |
| HCM Control Delay (s) | 67.3 | 8.2 | 0 | - | 9.2 | 0 | -17.4 |
| HCM Lane LOS | F | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 4.2 | 0.1 | - | - | 0 | - | - |
| C | 0.1 |  |  |  |  |  |  |



| Approach | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 9.6 | 1.4 | 0 |
| HCM LOS | A |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1555 | -855 | - | - |  |
| HCM Lane V/C Ratio | 0.009 | -0.082 | - | - |  |
| HCM Control Delay (s) | 7.3 | 0 | 9.6 | - | - |
| HCM Lane LOS | A | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.3 | - | - |

Opening Year Traffic Conditions (With Project)

| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 4.4 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | EB |  | WB |  | NB |  | SB |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 61 |  | 117 |  | 98 |  | 116 |
| Demand Flow Rate, veh/h |  | 61 |  | 117 |  | 98 |  | 116 |
| Vehicles Circulating, veh/h |  | 79 |  | 159 |  | 97 |  | 0 |
| Vehicles Exiting, veh/h |  | 37 |  | 36 |  | 43 |  | 276 |
| Follow-Up Headway, s |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.186 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 4.0 |  | 4.9 |  | 4.4 |  | 4.1 |
| Approach LOS |  | A |  | A |  | A |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Critical Headway, s | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Entry Flow, veh/h | 61 |  | 117 |  | 98 |  | 116 |  |
| Cap Entry Lane, veh/h | 1044 |  | 964 |  | 1025 |  | 1130 |  |
| Entry HV Adj Factor | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Flow Entry, veh/h | 61 |  | 117 |  | 98 |  | 116 |  |
| Cap Entry, veh/h | 1044 |  | 964 |  | 1025 |  | 1130 |  |
| V/C Ratio | 0.058 |  | 0.121 |  | 0.096 |  | 0.103 |  |
| Control Delay, s/veh | 4.0 |  | 4.9 |  | 4.4 |  | 4.1 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 0 |  | 0 |  | 0 |  | 0 |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 7.8 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Vol, veh/h | 156 | 73 | 16 | 535 | 172 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | -5 | - | - | -2 | -5 | - |
| Peak Hour Factor | 84 | 100 | 63 | 84 | 65 | 100 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 186 | 73 | 25 | 637 | 265 | 13 |
| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| Conflicting Flow All | 0 | 0 | 259 | 0 | 910 | 222 |
| Stage 1 | - | - | - | - | 222 | - |
| Stage 2 | - | - | - | - | 688 | - |
| Critical Hdwy | - | - | 4.1 | - | 5.4 | 5.7 |
| Critical Hdwy Stg 1 | - | - | - | - | 4.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 4.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1317 | - | 396 | 848 |
| Stage 1 | - | - | - | - | 872 | - |
| Stage 2 | - | - | - | - | 608 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1317 | - | 385 | 848 |
| Mov Cap-2 Maneuver | - | - | - | - | 385 | - |
| Stage 1 | - | - | - | - | 872 | - |
| Stage 2 | - | - | - | - | 590 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.3 | 33 |
| HCM LOS |  |  | D |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Vol, veh/h | 1 | 143 | 18 | 5 | 418 | 0 | 113 | 0 | 1 | 0 | 0 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - |  |  | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 2 | - | - | -2 | - | - | 0 | - | - | 2 |  |
| Peak Hour Factor | 25 | 82 | 70 | 33 | 78 | 90 | 90 | 90 | 25 | 90 | 90 | 38 |
| Heavy Vehicles, \% | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 4 | 174 | 26 | 15 | 536 | 0 | 126 | 0 | 4 | 0 | 0 | 11 |


| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 536 | 0 | 0 | 200 | 0 | 0 | 766 | 761 | 187 | 763 | 774 | 536 |
| Stage 1 | - | - | - | - | - | - | 195 | 195 | - | 566 | 566 |  |
| Stage 2 | - | - | - | - | - | - | 571 | 566 | - | 197 | 208 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.5 | 6.9 | 6.4 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1042 | - | - | 1384 | - | - | 322 | 337 | 860 | 297 | 304 | 532 |
| Stage 1 | - | - | - |  | - | - | 811 | 743 | - | 481 | 480 |  |
| Stage 2 | - | - | - | - | - | - | 509 | 511 | - | 792 | 717 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1042 | - | - | 1384 | - | - | 311 | 331 | 860 | 291 | 298 | 532 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 311 | 331 | - | 291 | 298 |  |
| Stage 1 | - | - | - | - | - | - | 808 | 740 | - | 479 | 473 |  |
| Stage 2 | - | - | - | - | - | - | 491 | 503 | - | 785 | 714 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.2 | 0.2 | 24 | 11.9 |
| HCM LOS |  |  | C | B |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 317 | 1042 | - | -1384 | - | - | 532 |
| HCM Lane V/C Ratio | 0.409 | 0.004 | - | -0.011 | - | -0.02 |  |
| HCM Control Delay (s) | 24 | 8.5 | 0 | - | 7.6 | 0 | -11.9 |
| HCM Lane LOS | C | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 1.9 | 0 | - | - | 0 | - | - |
| B | 0.1 |  |  |  |  |  |  |



| Approach | EB | NB | SB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 10.6 | 1.3 | 0 |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1478 | -668 | - | - |  |
| HCM Lane V/C Ratio | 0.036 | - | 0.04 | - | - |
| HCM Control Delay (s) | 7.5 | 0 | 10.6 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.1 | - | - |


| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 5.2 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | EB |  | WB |  | NB |  | SB |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 42 |  | 59 |  | 62 |  | 307 |
| Demand Flow Rate, veh/h |  | 42 |  | 59 |  | 62 |  | 307 |
| Vehicles Circulating, veh/h |  | 236 |  | 104 |  | 145 |  | 0 |
| Vehicles Exiting, veh/h |  | 71 |  | 103 |  | 133 |  | 163 |
| Follow-Up Headway, s |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.186 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 4.5 |  | 4.0 |  | 4.2 |  | 5.7 |
| Approach LOS |  | A |  | A |  | A |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Critical Headway, s | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Entry Flow, veh/h | 42 |  | 59 |  | 62 |  | 307 |  |
| Cap Entry Lane, veh/h | 892 |  | 1018 |  | 977 |  | 1130 |  |
| Entry HV Adj Factor | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Flow Entry, veh/h | 42 |  | 59 |  | 62 |  | 307 |  |
| Cap Entry, veh/h | 892 |  | 1018 |  | 977 |  | 1130 |  |
| V/C Ratio | 0.047 |  | 0.058 |  | 0.063 |  | 0.272 |  |
| Control Delay, s/veh | 4.5 |  | 4.0 |  | 4.2 |  | 5.7 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 0 |  | 0 |  | 0 |  | 1 |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 13.3 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Vol, veh/h | 573 | 177 | 14 | 398 | 125 | 53 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | -5 | - | - | -2 | -5 | - |
| Peak Hour Factor | 90 | 69 | 42 | 75 | 70 | 68 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 637 | 257 | 33 | 531 | 179 | 78 |
| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| Conflicting Flow All | 0 | 0 | 893 | 0 | 1362 | 765 |
| Stage 1 | - | - | - | - | 765 | - |
| Stage 2 | - | - | - | - | 597 | - |
| Critical Hdwy | - | - | 4.1 | - | 5.4 | 5.7 |
| Critical Hdwy Stg 1 | - | - | - | - | 4.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 4.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 768 | - | 241 | 452 |
| Stage 1 | - | - | - | - | 572 | - |
| Stage 2 | - | - | - | - | 654 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 768 | - | 226 | 452 |
| Mov Cap-2 Maneuver | - | - | - | - | 226 | - |
| Stage 1 | - | - | - | - | 572 | - |
| Stage 2 | - | - | - | - | 614 | - |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.6 | 87.6 |
| HCM LOS |  |  | F |




| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 420 | 0 | 0 | 777 | 0 | 0 | 1205 | 1202 | 707 | 1204 | 1270 | 418 |
| Stage 1 | - | - | - | - | - | - | 771 | 771 | - | 429 | 429 |  |
| Stage 2 | - | - | - | - | - | - | 434 | 431 | - | 775 | 841 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.5 | 6.9 | 6.4 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  | 6.5 | 5.9 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1150 | - | - | 848 | - | - | 162 | 186 | 439 | 142 | 147 | 625 |
| Stage 1 | - | - | - | - | - | - | 396 | 413 | - | 580 | 560 |  |
| Stage 2 | - | - | - | - | - | - | 604 | 586 | - | 361 | 349 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1150 | - | - | 848 | - | - | 153 | 175 | 439 | 132 | 139 | 625 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 153 | 175 | - | 132 | 139 |  |
| Stage 1 | - | - | - | - | - | - | 376 | 392 | - | 551 | 556 |  |
| Stage 2 | - | - | - | - | - | - | 590 | 581 | - | 335 | 332 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.3 | 0.1 | 71.1 | 17.7 |
| HCM LOS |  | $F$ | $C$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 159 | 1150 | - | - | 848 | - | -297 |
| HCM Lane V/C Ratio | 0.721 | 0.028 | - | -0.006 | - | -0.046 |  |
| HCM Control Delay (s) | 71.1 | 8.2 | 0 | - | 9.3 | 0 | -17.7 |
| HCM Lane LOS | F | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 4.3 | 0.1 | - | - | 0 | - | - |
| C | 0.1 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.7 |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Vol, veh/h | 39 | 29 | 16 | 137 | 188 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 5 | - | - | -5 | 5 | - |
| Peak Hour Factor | 70 | 75 | 42 | 77 | 78 | 38 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 56 | 39 | 38 | 178 | 241 | 21 |
| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| Conflicting Flow All | 506 | 252 | 262 | 0 | - | 0 |
| Stage 1 | 252 | - | - | - | - | - |
| Stage 2 | 254 | - | - | - | - | - |
| Critical Hdwy | 7.4 | 6.7 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 6.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | 460 | 764 | 1314 | - | - | - |
| Stage 1 | 741 | - | - | - | - | - |
| Stage 2 | 739 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 445 | 764 | 1314 | - | - | - |
| Mov Cap-2 Maneuver | 445 | - | - | - | - | - |
| Stage 1 | 741 | - | - | - | - | - |
| Stage 2 | 715 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 13.1 | 1.4 | 0 |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1314 | -537 | - | - |  |
| HCM Lane V/C Ratio | 0.029 | -0.176 | - | - |  |
| HCM Control Delay (s) | 7.8 | 0 | 13.1 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.6 | - | - |

Opening Year Traffic Conditions (With Project) Millertown Pike at Glen Creek Road with EB Right Turn Lane

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 7.2 |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Vol, veh/h | 156 | 73 | 16 | 535 | 172 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 100 | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | -5 | - | - | -2 | -5 | - |
| Peak Hour Factor | 84 | 100 | 63 | 84 | 65 | 100 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 186 | 73 | 25 | 637 | 265 | 13 |
| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| Conflicting Flow All | 0 | 0 | 186 | 0 | 874 | 186 |
| Stage 1 | - | - | - | - | 186 | - |
| Stage 2 | - | - | - | - | 688 | - |
| Critical Hdwy | - | - | 4.1 | - | 5.4 | 5.7 |
| Critical Hdwy Stg 1 | - | - | - | - | 4.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 4.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1401 | - | 412 | 884 |
| Stage 1 | - | - | - | - | 896 | - |
| Stage 2 | - | - | - | - | 608 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1401 | - | 400 | 884 |
| Mov Cap-2 Maneuver | - | - | - | - | 400 | - |
| Stage 1 | - | - | - | - | 896 | - |
| Stage 2 | - | - | - | - | 591 | - |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.3 | 30.2 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 411 | - | -1401 | - |  |
| HCM Lane V/C Ratio | 0.675 | - | -0.018 | - |  |
| HCM Control Delay (s) | 30.2 | - | - | 7.6 | 0 |
| HCM Lane LOS | D | - | - | A | A |
| HCM 95th \%tile Q(veh) | 4.8 | - | - | 0.1 | - |



| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.5 | 54.2 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL |
| :--- | ---: | ---: | ---: | ---: | WBT | W |
| :--- |
| Capacity (veh/h) |
| 310 |

## APPENDIX H

ITE Trip Generation Rates

# Land Use: 210 Single-Family Detached Housing 

## Description

Single-family detached housing includes all single-family detached homes on individual lots. A typical site surveyed is a suburban subdivision.

## Additional Data

The number of vehicles and residents had a high correlation with average weekday vehicle trip ends. The use of these variables was limited, however, because the number of vehicles and residents was often difficult to obtain or predict. The number of dwelling units was generally used as the independent variable of choice because it was usually readily available, easy to project and had a high correlation with average weekday vehicle trip ends.

This land use included data from a wide variety of units with different sizes, price ranges, locations and ages. Consequently, there was a wide variation in trips generated within this category. Other factors, such as geographic location and type of adjacent and nearby development, may also have had an effect on the site trip generation.

Single-family detached units had the highest trip generation rate per dwelling unit of ail residential uses because they were the largest units in size and had more residents and more vehicles per unit than other residential land uses; they were generally located farther away from shopping centers, employment areas and other trip attractors than other residential land uses; and they generally had fewer alternative modes of transportation available because they were typically not as concentrated as other residential land uses.

The peak hour of the generator typically coincided with the peak hour of the adjacent street traffic.
The sites were surveyed between the late 1960s and the 2000s throughout the United States and Canada.

## Source Numbers

$1,4,5,6,7,8,11,12,13,14,16,19,20,21,26,34,35,36,38,40,71,72,84,91,98,100,105$,
$108,110,114,117,119,157,167,177,187,192,207,211,246,275,283,293,300,319,320,357$,
$384,435,550,552,579,598,601,603,611,614,637,711,735$

## Single-Family Detached Housing

(210)

## Average Vehicle Trip Ends vs: Dwelling Units <br> On a: Weekday

Number of Studies: 355
Avg. Number of Dwelling Units: 198
Directional Distribution: 50\% entering, 50\% exiting
Trip Generation per Dwelling Unit

| Average Rate |  | Range of Rates | Standard Deviation |
| :---: | :---: | :---: | :---: |
| 9.52 | $4.31-21.85$ | 3.70 |  |

## Data Plot and Equation



# Single-Family Detached Housing <br> (210) 

## Average Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Number of Studies: 292
Avg. Number of Dwelling Units: 194
Directional Distribution: $25 \%$ entering, $75 \%$ exiting

## Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.75 | $0.33-2.27$ | 0.90 |

## Data Plot and Equation



## Single-Family Detached Housing <br> (210)

Average Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Number of Studies: 321
Avg. Number of Dwelling Units: 207
Directional Distribution: 63\% entering, 37\% exiting
Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.00 | $0.42-2.98$ | 1.05 |

## Data Plot and Equation



## Land Use: 230 Residential Condominium/Townhouse

## Description

Residential condominiums/townhouses are defined as ownership units that have at least one other owned unit within the same building structure. Both condominiums and townhouses are included in this land use. The studies in this land use did not identify whether the condominiums/townhouses were low-rise or high-rise. Low-rise residential condominium/townhouse (Land Use 231), high-rise residential condominium/townhouse (Land Use 232) and luxury condominium/townhouse (Land Use 233) are related uses.

## Additional Data

The number of vehicles and the number of residents had a high correlation with average weekday vehicle trip ends. The use of these variables was limited, however, because the number of vehicles and residents was often difficult to obtain or predict. The number of dwelling units was generally used as the independent variable of choice because it is usually readily available, easy to project and had a high correlation with average weekday vehicle trip ends.

The peak hour of the generator typically coincided with the peak hour of the adjacent street traffic.
The sites were surveyed between the mid-1970s and the 2000s throughout the United States and Canada.

## Source Numbers

$4,92,94,95,97,100,105,106,114,168,186,204,237,253,293,319,320,321,390,412,418$, 561, 562, 583, 638

# Residential Condominium/Townhouse (230) 

Average Vehicle Trip Ends vs: Dwelling Units
On a: Weekday

Number of Studies: 56
Avg. Number of Dwelling Units: 179
Directional Distribution: 50\% entering, 50\% exiting

## Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: | :---: |
| 5.81 | $1.53-11.79$ | 3.11 |

## Data Plot and Equation



# Residential Condominium/Townhouse (230) 

## Average Vehicle Trip Ends vs: Dwelling Units

Ona: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Number of Studies: 59
Avg. Number of Dwelling Units: 213
Directional Distribution: $17 \%$ entering, $83 \%$ exiting
Trip Generation per Dwelling Unit

| Average Rate | Range of Rates |  | Standard Deviation |
| :---: | :---: | :---: | :---: |
| 0.44 | $0.15-1.61$ | 0.69 |  |

## Data Plot and Equation



# Residential Condominium/Townhouse (230) 

## Average Vehicle Trip Ends vs: Dwelling Units <br> On a: Weekday, <br> Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Number of Studies: 62
Avg. Number of Dwelling Units: 205
Directional Distribution: 67\% entering, 33\% exiting
Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.52 | $0.18-1.24$ | 0.75 |

## Data Plot and Equation



Fitted Curve Equation: $\operatorname{Ln}(T)=0.82 \operatorname{Ln}(X)+0.32$ $\mathrm{R}^{2}=0.80$

TABLE 5A
TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT
Entire Development

| ITE LAND USE CODE | LAND USE DESCRIPTION | UNITS | ```GENERATED DAILY TRAFFIC``` | GENERATED <br> TRAFFIC <br> AM PEAK HOUR |  |  | GENERATED <br> TRAFFIC <br> PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ENT'ER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| Total New Volume Site Trips |  |  | 2,801 | 53 | 163 | 216 | 175 | 101 | 276 |

TABLE 5B
TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT
271 Single-Family Detached Homes

| ITE LAND USE CODE | LAND USE DESCRIPTION | UNITS | $\begin{array}{\|l} \text { GENERATED } \\ \text { DAILY } \\ \text { TRAFFIC } \end{array}$ | GENERATED TRAFFIC <br> AM PEAK HOUR |  |  | GENERATED TRAFFIC <br> PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| \#210 | Single-Family Detached Housing | 271 Lots | 2,628 | 25\% | 75\% |  | 63\% | 37\% |  |
|  |  |  |  | 50 | 150 | 200 | 163 | 95 | 258 |
| Total New Volume Site Trips |  |  | 2,628 | 50 | 150 | 200 | 163 | 95 | 258 |

ITE Trip Generation Manual, 9th Edition

36 single family detached homes - East side of Phase 1

| AM | ENTER | 36 lots out of | 271 lots = | 0.13 | * | $50=$ | 7 | trips |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EXIT | 36 lots out of | 271 lots = | 0.13 | * | $150=$ | 20 | trips |
| PM | ENTER | 36 lots out of | 271 lots = | 0.13 |  | $163=$ | 22 | trips |
|  | EXIT | 36 lots out of | 271 lots = | 0.13 | * | $95=$ | 13 | trips |
| 75 si | detach | - West side of P | ase 1 |  |  |  |  |  |
| AM | ENTER | 75 lots out of | 271 lots = | 0.28 | * | $50=$ | 14 | trips |
|  | EXIT | 75 lots out of | 271 lots = | 0.28 |  | $150=$ | 42 | trips |
| PM | ENTER | 75 lots out of | 271 lots = | 0.28 |  | $163=$ | 45 | trips |
|  | EXIT | 75 lots out of | 271 lots = | 0.28 | * | $95=$ | 26 | trips |
| 160 | ily detach | Phase 2 |  |  |  |  |  |  |
| AM | ENTER | 160 lots out of | 271 lots = | 0.59 | * | $50=$ | 30 | trips |
|  | EXIT | 160 lots out of | 271 lots = | 0.59 | * | $150=$ | 89 | trips |
| PM | ENTER | 160 lots out of | 271 lots = | 0.59 | * | $163=$ | 96 | trips |
|  | EXIT | 160 lots out of | 271 lots = | 0.59 | * | $95=$ | 56 | trips |

## TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT

271 single family detached homes

## 271 Residential Units $=\mathbf{X}$

## Weekday:

Fitted Curve Equation:

$$
\operatorname{Ln}(\mathrm{T})=0.92 \operatorname{Ln}(\mathrm{X})+2.72
$$

$$
\begin{aligned}
\operatorname{Ln}(\mathrm{T}) & =0.92 * 5.60+2.72 \\
\operatorname{Ln}(\mathrm{~T}) & =7.87 \\
\mathbf{T} & =\mathbf{2 , 6 2 8} \text { trips }
\end{aligned}
$$

## Peak Hour of Adjacent Traffic between 7 and 9 am:

Fitted Curve Equation:

$$
\begin{aligned}
& \mathrm{T}=0.70(\mathrm{X})+9.74 \\
& \mathrm{~T}=\quad 0.70 * 271+9.74 \\
& \mathrm{~T}=\quad \mathbf{2 0 0} \text { trips }
\end{aligned}
$$

## Peak Hour of Adjacent Traffic between 4 and 6 pm :

Fitted Curve Equation:

$$
\operatorname{Ln}(\mathrm{T})=0.90 \operatorname{Ln}(\mathrm{X})+0.51
$$

$$
\begin{aligned}
\operatorname{Ln}(\mathrm{T}) & =0.90 * 5.60+0.51 \\
\operatorname{Ln}(\mathrm{~T}) & =5.55 \\
\mathbf{T} & =\mathbf{2 5 8} \text { trips }
\end{aligned}
$$

TABLE 5C
TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT
22 Single-Family Attached Homes
(8 Condominiums +14 Townhouses)

| ITE LAND USE CODE | LAND USE DESCRIPTION | UNITS | $\begin{aligned} & \text { GENERATED } \\ & \text { DAILY } \\ & \text { TRAFFIC } \end{aligned}$ | GENERATED TRAFFIC <br> AM PEAK HOUR |  |  | GENERATEDTRAFFICPM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| \#230 | ResidentialCondominium /Townhouse | 22 Dwellings | 173 | 17\% | 83\% |  | 67\% | 33\% |  |
|  |  |  |  | 3 | 13 | 16 | 12 | 6 | 18 |
| Total New Volume Site Trips |  |  | 173 | 3 | 13 | 16 | 12 | 6 | 18 |

ITE Trip Generation Manual, 9th Edition

22 attached homes - East side of Phase 1

| AM | ENTER | 3 | trips |
| :--- | :--- | :---: | :--- |
|  | EXIT | 13 | trips |
| PM | ENTER | 12 | trips |
|  | EXIT | 6 | trips |

TRIP GENERATION FOR CLEAR SPRING DEVELOPMENT
22 attached homes

## 22 Dwelling Units $=X$

## Weekday:

Fitted Curve Equation:

$$
\operatorname{Ln}(\mathrm{T})=0.87 \operatorname{Ln}(\mathrm{X})+2.46
$$

$$
\begin{aligned}
\operatorname{Ln}(\mathrm{T}) & =0.87 * 3.09+2.46 \\
\operatorname{Ln}(\mathrm{~T}) & =5.15 \\
\mathbf{T} & =\mathbf{1 7 3} \text { trips }
\end{aligned}
$$

## Peak Hour of Adjacent Traffic between 7 and 9 am:

Fitted Curve Equation:

$$
\begin{aligned}
\operatorname{Ln}(T) & =0.80 \operatorname{Ln}(\mathrm{X})+0.26 \\
\operatorname{Ln}(\mathrm{~T}) & =0.80 * 3.09+0.26 \\
\operatorname{Ln}(\mathrm{~T}) & =2.73 \\
\mathbf{T} & =16 \text { trips }
\end{aligned}
$$

## Peak Hour of Adjacent Traffic between 4 and 6 pm :

Fitted Curve Equation:

$$
\begin{aligned}
\operatorname{Ln}(T) & =0.82 \operatorname{Ln}(\mathrm{X})+0.32 \\
\operatorname{Ln}(\mathrm{~T}) & =0.82 * 3.09+0.32 \\
\operatorname{Ln}(\mathrm{~T}) & =2.85 \\
\mathbf{T} & =18 \text { trips }
\end{aligned}
$$

## APPENDIX I

TDOT Statewide Crash Rates \& Spreadsheet Calculations




| 11/20/2017 9:39 AM |  |  |  |  |  |  |  |  |  | Page 3 of 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tennessee Department of Transportation |  |  |  |  |  |  |  |  |  |  |
| Statewide Average Crash Rates for Sections and Spots |  |  |  |  |  |  |  |  |  |  |
| Study: OFFICIAL HSIP STUDY 2014-2016 |  |  |  |  |  |  |  |  |  |  |
| Begin Date: 1/1/2014 End Date: 12/31/2016 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  | Total |
| Route Type | Rural / Urban | Location Type | Highway Type | Fatal Rate | Incap. Rate | Other Inj. Rate | Pd. Rate | Total Rate | Severe Crash Rate | Veh. Miles (in millions) |
| High Risk Rural Roads |  |  |  |  |  |  |  |  |  |  |
| MAJOR COL. | Rural | Section | 2 OR 3 LN | 0.029 | 0.151 | 0.533 | 1.470 | 2.183 | 0.181 | 7,712 |
| MAJOR COL. | Rural | Section | 2 OR 3 LN W/TL | 0.016 | 0.087 | 0.309 | 1.774 | 2.186 | 0.103 | 126 |
| MAJOR COL. | Rural | Section | 4 OR MORE UNDIV | 0.001 | 0.214 | 0.357 | 1.928 | 2.500 | 0.214 | 14 |
| MAJOR COL. | Rural | Section | 4 OR MORE DIV | 0.001 | 0.001 | 0.687 | 1.899 | 2.585 | 0.001 | 25 |
| MAJOR COL. | Rural | Section | 4 OR MORE W TL | 0.018 | 0.071 | 0.285 | 1.017 | 1.391 | 0.089 | 56 |
| MAJOR COL. | Rural | Section | FREEWAY | 0.001 | 0.001 | 0.535 | 2.407 | 2.942 | 0.001 | 4 |
| MAJOR COL. | Rural | Spot | 2 OR 3 LN | 0.010 | 0.053 | 0.187 | 0.517 | 0.767 | 0.063 | 22,204 |
| MAJOR COL. | Rural | Spot | 2 OR 3 LN W/TL | 0.002 | 0.016 | 0.062 | 0.357 | 0.437 | 0.018 | 675 |
| MAJOR COL. | Rural | Spot | 4 OR MORE UNDIV | 0.001 | 0.036 | 0.072 | 0.346 | 0.453 | 0.036 | 84 |
| MAJOR COL. | Rural | Spot | 4 OR MORE DIV | 0.001 | 0.001 | 0.159 | 0.484 | 0.642 | 0.001 | 126 |
| MAJOR COL. | Rural | Spot | 4 OR MORE W TL | 0.003 | 0.012 | 0.047 | 0.186 | 0.249 | 0.015 | 338 |
| MAJOR COL. | Rural | Spot | FREEWAY | 0.001 | 0.001 | 0.071 | 0.318 | 0.388 | 0.001 | 28 |
| MIN COL. | Rural | Section | 2 OR 3 LN | 0.034 | 0.180 | 0.663 | 1.891 | 2.768 | 0.214 | 6,421 |
| MIN COL. | Rural | Section | 2 OR 3 LN W/TL | 0.001 | 0.081 | 0.269 | 1.022 | 1.372 | 0.081 | 37 |
| MIN COL. | Rural | Section | 4 OR MORE UNDIV | 0.001 | 0.001 | 1.814 | 4.405 | 6.219 | 0.001 | 4 |
| MIN COL. | Rural | Section | 4 OR MORE DIV | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0 |
| MIN COL. | Rural | Section | 4 OR MORE W TL | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0 |
| MIN COL. | Rural | Section | FREEWAY | 0.001 | 2.484 | 2.484 | 4.968 | 9.936 | 2.484 | 0 |
| MIN COL. | Rural | Spot | 2 OR 3 LN | 0.017 | 0.089 | 0.327 | 0.934 | 1.366 | 0.105 | 13,065 |
| MIN COL. | Rural | Spot | 2 OR 3 LN W/TL | 0.001 | 0.018 | 0.053 | 0.260 | 0.331 | 0.018 | 169 |
| MIN COL. | Rural | Spot | 4 OR MORE UNDIV | 0.001 | 0.041 | 0.326 | 0.856 | 1.223 | 0.041 | 25 |
| MIN COL. | Rural | Spot | FREEWAY | 0.001 | 0.483 | 0.483 | 1.448 | 2.414 | 0.483 | 2 |

## TENNESSEE DEPARTMENT OF TRANSPORTATION



| Millertown Pike Intersection (Mi | Knox County ike at Glen Cree | Road) | LM 0.000 |
| :---: | :---: | :---: | :---: |
| 2 Crashes | - 2015-2018 | Actual | 0.242 Acc/MVM |
| State Average A/S Ratio | $\begin{aligned} & =0.121 \mathrm{Acc} / \mathrm{MVM} \\ & =2.00 \end{aligned}$ |  | $\begin{aligned} & =0.463 \mathrm{Acc} / \mathrm{MVM} \\ & =0.52 \end{aligned}$ |

TENNESSEE DEPARTMENT OF TRANSPORTATION

Millertown Pike, Knox County LM 0.000

Section (east and west of Glen Creek Road)

| 7 Crashes | $-2015-2018$ | Actual | -6.630 Acc/MVM |
| :--- | :--- | :--- | :--- |
| State Average | -2.832 Acc/MVM | Critical | -7.117 Acc/MVM |
| A/S Ratio | $=2.34$ | A/C Ratio | $=0.93$ |

## APPENDIX J

## Knox County Turn Lane Volume Threshold Worksheet

TABLE 5A
LEFT-TURN LANE VOLUME THRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH
(If the left-turn volume exceeds the table value a left -turn lane is needed)

| $\begin{gathered} \text { OPPOSING } \\ \text { VOLUME } \end{gathered}$ | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100-149 | 150-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ | $\begin{aligned} & 250 \\ & 200 \end{aligned}$ | $\begin{aligned} & 180 \\ & 140 \end{aligned}$ | $\begin{aligned} & 140 \\ & 105 \end{aligned}$ | $\begin{gathered} 110 \\ 90 \end{gathered}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ | $\begin{aligned} & 70 \\ & 60 \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 160 \\ & 130 \end{aligned}$ | $\begin{aligned} & 115 \\ & 100 \end{aligned}$ | $\begin{aligned} & 85 \\ & 75 \end{aligned}$ | $\begin{aligned} & 75 \\ & 65 \end{aligned}$ | $\begin{aligned} & 65 \\ & 60 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & 110 \\ & 100 \end{aligned}$ | $\begin{aligned} & 90 \\ & 80 \\ & \hline \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ |
| $\begin{array}{r} 400-449 \\ 450-499 \end{array}$ | $\begin{aligned} & 90 \\ & 80 \end{aligned}$ | $\begin{aligned} & 70 \\ & 65 \\ & \hline \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \\ & \hline \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ |
| $\begin{array}{r} 500-549 \\ 550-599 \\ \hline \end{array}$ | $\begin{array}{r} 70 \\ , \quad 65 \\ \hline \end{array}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{array}{r} 35 \\ 35 \\ \hline \end{array}$ | $\begin{aligned} & 35 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ |
| $\begin{aligned} & 600-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 45 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ |
| $\begin{gathered} 700-749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 50 \\ & 45 \end{aligned}$ | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ |



* Or through volume only if a right-turn lane exists

RIGHT-TURN LANE VOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH

| RIGHT-TURN <br> VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $<100$ | 100-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{aligned} & \text { Fewer Than } 25 \\ & \begin{array}{c} 25-49 \\ \hline 50-99 \\ \hline \end{array} \end{aligned}$ |  |  |  |  |  |  |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  | $n$ Pike |  |  |  |  |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ |  | reek Road <br> cted AM |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{array}{r} 300-349 \\ 350-399 \\ \hline \end{array}$ |  | Turns $=73$ <br> Turn Lane | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ |  | Warranted | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |


| RIGHT-TURN VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | 400-449 | 450-499 | 500-549 | 550-600 | $+I>600$ |
| $\begin{gathered} \text { Fewer Than } 25 \\ 25-49 \\ 50-99 \end{gathered}$ |  | * |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{array}{r} 200-249 \\ 250-299 \\ \hline \end{array}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes | Yes <br> Yes | Yes Yes | Yes Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{array}{r} 400-449 \\ 450-499 \end{array}$ | Yes Yes | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \\ & \hline \end{aligned}$ | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |

* Or through volume only if a left-turn lane exists.

TABLE 5A
LEFT-TURN LANE VOLUME THRESHOLDS
FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPE
(If the left-turn volume exceeds the table value a left -turn lane is needed)


| OPPOSING VOLUME | THROUGH VOLUME PLUS RIGHT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | 400-449 | 450-499 | 500-549 | 550-599 | $=f>600$ |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ | $\begin{aligned} & 70 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 55 \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | $\begin{aligned} & 55 \\ & 50 \\ & \hline \end{aligned}$ | $\begin{aligned} & 50 \\ & 45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 35 \end{aligned}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ |
| $\begin{array}{r} 400-449 \\ 450-499 \\ \hline \end{array}$ | $\begin{aligned} & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & \mathbf{3 0} \\ & \mathbf{2 5} \\ & \hline \end{aligned}$ | $\begin{array}{r} 30 \\ 25 \\ \hline \end{array}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ |
| $\begin{array}{r} 500-549 \\ 550-599 \\ \hline \end{array}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ |
| $\begin{aligned} & 600-649 \\ & 650-699 \end{aligned}$ | $\begin{aligned} & 25 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{array}{r} 20 \\ 20 \\ \hline \end{array}$ | $\begin{aligned} & 15 \\ & 15 \\ & \hline \end{aligned}$ |
| $\begin{gathered} 700-749 \\ 750 \text { or More } \end{gathered}$ | $\begin{aligned} & 20 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ |

* Or through volume only if a right-turn lane exists

RIGHT-TURN LANE YOLUME THRESHOLDS FOR TWO-LANE ROADWAYS WITH A PREVAILING SPEED OF 36 TO 45 MPH

| RIGHT-TURN VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $<100$ | 100-199 | 200-249 | 250-299 | 300-349 | 350-399 |
| $\begin{gathered} \text { Fewer Than } 25 \\ 25-49 \\ 50-99 \end{gathered}$ |  |  |  |  |  |  |
| $\begin{aligned} & 100-149 \\ & 150-199 \end{aligned}$ |  |  |  |  |  |  |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ |  |  |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ |  |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 400-449 \\ & 450-499 \end{aligned}$ |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |


| RIGHT-TURN VOLUME | THROUGH VOLUME PLUS LEFT-TURN VOLUME * |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 350-399 | 400-449 | 450-499 | 500-549 | 550-600 | $+I>600$ |
| $\begin{gathered} \text { Fewer Than } 25 \\ 25-49 \\ 50-99 \end{gathered}$ |  | * |  | Yes | $\begin{aligned} & \text { yes } \\ & \text { yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $100-149$ <br> $150-199$ |  | Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 200-249 \\ & 250-299 \end{aligned}$ | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |  | $\underbrace{\mathrm{Yes}_{\text {Pr }}}_{\text {wn Pike at }}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{aligned} & 300-349 \\ & 350-399 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |  | reek Road cted PM | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| $\begin{array}{r} 400-449 \\ 450-499 \end{array}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Rig | Turn Lane | Yes <br> Yes |
| $\begin{aligned} & 500-549 \\ & 550-599 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\mathcal{C u}_{\text {Yes }}$ | ranted Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 600 or More | Yes | Yes | Yes | Yes | Yes | Yes |

* Or through volume only if a left-turn lane exists.


## APPENDIX K

Traffic Signalization Warrants

|  | Millertown Pike |  | Glen Creek Road |  | Millertown Pike |  | Growth Rate of 2.5\% at 3.5 Years |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { TIME } \\ \text { BEGIN } \\ \hline \end{gathered}$ | WESTBOUND |  | NORTHBOUND |  | EASTBOUND |  |  |
|  | LT | THRU | LT | RT | THRU | RT |  |
| 7:00 AM | 0 | 79 | 8 | 0 | 27 | 1 |  |
| 7:15 AM | 2 | 117 | 6 | 1 | 31 | 3 |  |
| 7:30 AM | 3 | 127 | 3 | 1 | 30 | 8 |  |
| 7:45 AM | 4 | 104 | 10 | 1 | 27 | 5 |  |
| SUM | 9 | 427 | 27 | 3 | 115 | 17 |  |
|  | 0.7875 | 37.3625 | 2.3625 | 0.2625 | 10.0625 | 1.4875 |  |
|  | 10 | 464 | 29 | 3 | 125 | 18 | Growth Rate of 2.5\% at 3.5 Years |
| Year 2022 | 1 | 464 | 66 | 4 | 125 | 22 |  |
| 8:00 AM | 1 | 80 | 7 | 1 | 37 | 6 |  |
| 8:15 AM | 2 | 76 | 3 | 1 | 34 | 5 |  |
| 8:30 AM | 1 | 77 | 8 | 1 | 24 |  |  |
| 8:45 AM | 1 | 69 | 8 | 2 | 35 | 4 |  |
| SUM | 5 | 302 | 26 | 5 | 130 | 18 |  |
|  | 0.4375 | 26.425 | 2.275 | 0.4375 | 11.375 | 1.575 |  |
|  | 5 | 328 | 28 | 5 | 141 | 20 | Growth Rate of 2.5\% at 3.5 Years |
| Year 2022 | 1 | 328 | 48 | 3 | 141 | 16 |  |
| 11:00 AM | 0 | 51 | 6 | 2 | 41 | 3 |  |
| 11:15 AM | 0 | 51 | 4 | 3 | 52 | 6 |  |
| 11:30 AM | 2 | 57 |  | 1 | 58 | 4 |  |
| 11:45 AM | 0 | 47 | 4 | 3 | 50 | 2 |  |
| SUM | 2 | 206 | 17 | 9 | 201 | 15 |  |
|  | 0.175 | 18.025 | 1.4875 | 0.7875 | 17.5875 | 1.3125 |  |
|  | 2 | 224 | 18 | 10 | 219 | 16 | Growth Rate of 2.5\% at 3.5 Years |
| Year 2022 | 1 | 224 | 44 | 3 | 219 | 15 |  |
| 12:00 PM | 0 | 73 | 12 | 0 | 70 | 5 |  |
| 12:15 PM | 4 | 69 | 5 | 2 | 70 | 10 |  |
| 12:30 PM | 0 | 56 | 7 | 2 | 81 |  |  |
| 12:45 PM | 3 | 54 | 6 | 1 | 63 | 6 |  |
| SUM | 7 | 252 | 30 | 5 | 284 | 30 |  |
|  | 0.6125 | 22.05 | 2.625 | 0.4375 | 24.85 | 2.625 |  |
|  | 8 | 274 | 33 | 5 | 309 | 33 | Growth Rate of 2.5\% at 3.5 Years |
| Year 2022 | 1 | 274 | 59 | 3 | 309 | 20 |  |
| 2:00 PM | 1 | 65 | 8 | 4 | 75 | 4 |  |
| 2:15 PM | 1 | 52 | 3 | 4 | 61 | 5 |  |
| 2:30 PM | 1 | 48 | 6 | 3 | 68 | 5 |  |
| 2:45 PM | 0 | 50 | 5 | 1 | 82 | 11 |  |
| SUM | 3 | 215 | 22 | 12 | 286 | 25 |  |
|  | 0.2625 | 18.8125 | 1.925 | 1.05 | 25.025 | 2.1875 |  |
|  | 3 | 234 | 24 | 13 | 311 | 27 | Growth Rate of $2.5 \%$ at 3.5 Years |
| Year 2022 | 1 | 234 | 59 | 3 | 311 | 20 |  |
| 3:00 PM | 0 | 59 | 5 | 4 | 88 | 9 |  |
| 3:15 PM | 3 | 69 | 5 | 4 | 85 | 4 |  |
| 3:30 PM | 2 | 61 | 4 | 3 | 79 | 4 |  |
| 3:45 PM | 2 | 45 | 9 | 2 | 83 | 9 |  |
| SUM | 7 | 234 | 23 | 13 | 335 | 26 |  |
|  | 0.6125 | 20.475 | 2.0125 | 1.1375 | 29.3125 | 2.275 |  |
|  | 8 | 254 | 25 | 14 | 364 | 28 | Growth Rate of 2.5\% at 3.5 Years |
| Year 2022 | 1 | 254 | 74 | 4 | 364 | 25 |  |
| 4:00 PM | 0 | 48 | 7 | 2 | 95 | 7 |  |
| 4:15 PM | 1 | 69 | 9 | 4 | 127 | 11 |  |
| 4:30 PM | 0 | 73 | 5 | 7 | 112 | 7 |  |
| 4:45 PM | 3 | 51 | 7 | 6 | 98 | 7 |  |
| SUM | 4 | 241 | 28 | 19 | 432 | 32 |  |
|  | 0.35 | 21.0875 | 2.45 | 1.6625 | 37.8 | 2.8 |  |
|  |  | 262 | 30 | 21 | 470 | 35 |  |
| Year 2022 | 2 | 262 | 83 | 5 | 470 | 28 |  |
| 5:00 PM | 3 | 64 | 11 | 10 | 127 | 6 |  |
| 5:15 PM | 2 | 65 | 7 | 14 | 116 | 4 |  |
| 5:30 PM | 0 | 83 | 7 | 7 | 116 | 8 |  |
| 5:45 PM | 0 | 106 | 6 | 7 | 99 | 4 |  |
| SUM | 5 | 318 | 31 | 38 | 458 | 22 | Growth Rate of $2.5 \%$ at 3.5 Years |
|  | 0.4375 | 27.825 | 2.7125 | 3.325 | 40.075 | 1.925 |  |
|  | 5 | 424 | 37 | 45 | 557 | 26 |  |
| Year 2022 | 2 | 424 | 85 | 5 | 557 | 28 |  |



## Traffic Signal Warrant Analysis

| Project Name | The Highlands at Clear Spring |
| :--- | :---: |
| Project/File \# | 1808 |
| Scenario | 2022 - Projected Traffic Volumes |


| Intersection Information |  |
| :---: | :---: |
| Major Street Name | Millertown Pike |
| North/South or East/West | E/W |
| Speed Limit > 40 mph | Yes |
| \# of Approach Lanes | 1 |
| \% of Right Turn Traffic to Include | $100 \%$ |
|  |  |
| Minor Street Name | Glen Creek Road |
| \# of Approach Lanes | 1 |
| \% of Right Turn Traffic to Include | $100 \%$ |
| Isolated Community < 10,000 pop | No |

Additional Warrants to Consider

| Warrant 3, Peak Hour (A - Volume and Delay) | No |
| :--- | :--- |
| All-Way Stop Warrant | No |

## Traffic Signal Warrant Analysis

Millertown Pike (Major Street) Volume

| Eastbound Volume by Hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Time | Left Turns | Through | Right Turns | Peds/Bikes |
| 12-1 AM |  |  |  |  |
| 1-2 AM |  |  |  |  |
| 2-3 AM |  |  |  |  |
| 3-4 AM |  |  |  |  |
| 4-5 AM |  |  |  |  |
| 5-6 AM |  |  |  |  |
| 6-7 AM |  |  |  |  |
| 7-8 AM |  | 125 | 22 |  |
| 8-9 AM |  | 141 | 20 |  |
| 9-10 AM |  |  |  |  |
| 10-11 AM |  |  |  |  |
| 11-12 PM |  | 219 | 16 |  |
| 12-1 PM |  | 309 | 33 |  |
| 1-2 PM |  |  |  |  |
| 2-3 PM |  | 311 | 27 |  |
| 3-4PM |  | 364 | 28 |  |
| 4-5 PM |  | 470 | 35 |  |
| 5-6 PM |  | 557 | 28 |  |
| 6-7 PM |  |  |  |  |
| 7-8 PM |  |  |  |  |
| 8-9 PM |  |  |  |  |
| 9-10 PM |  |  |  |  |
| 10-11 PM |  |  |  |  |
| 11-12 AM |  |  |  |  |
| Tota | hicles (una | ted) | 2,705 | 0 |


| Westbound Volume by Hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Time | Left Turns | Through | Right Turns | Peds/Bikes |
| 12-1 AM |  |  |  |  |
| 1-2 AM |  |  |  |  |
| 2-3 AM |  |  |  |  |
| 3-4 AM |  |  |  |  |
| 4-5 AM |  |  |  |  |
| 5-6 AM |  |  |  |  |
| 6-7 AM |  |  |  |  |
| 7-8 AM | 10 | 464 |  |  |
| 8-9 AM | 5 | 328 |  |  |
| 9-10 AM |  |  |  |  |
| 10-11 AM |  |  |  |  |
| 11-12 PM | 2 | 224 |  |  |
| 12-1 PM | 8 | 274 |  |  |
| 1-2 PM |  |  |  |  |
| 2-3 PM | 3 | 234 |  |  |
| 3-4 PM | 8 | 254 |  |  |
| 4-5 PM | 4 | 262 |  |  |
| 5-6 PM | 5 | 424 |  |  |
| 6-7 PM |  |  |  |  |
| 7-8 PM |  |  |  |  |
| 8-9 PM |  |  |  |  |
| 9-10 PM |  |  |  |  |
| 10-11 PM |  |  |  |  |
| 11-12 AM |  |  |  |  |
| Total | hicles (unad | sted) | 2,509 | 0 |

Glen Creek Road (Minor Street) Volume

| Northbound Volume by Hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Time | Left Turns | Through | Right Turns | Peds/Bikes |
| 12-1 AM |  |  |  |  |
| 1-2 AM |  |  |  |  |
| 2-3 AM |  |  |  |  |
| 3-4 AM |  |  |  |  |
| 4-5 AM |  |  |  |  |
| 5-6 AM |  |  |  |  |
| 6-7 AM |  |  |  |  |
| 7-8 AM | 66 |  | 4 |  |
| 8-9 AM | 48 |  | 5 |  |
| 9-10 AM |  |  |  |  |
| 10-11 AM |  |  |  |  |
| 11-12 PM | 44 |  | 10 |  |
| 12-1 PM | 59 |  | 5 |  |
| 1-2 PM |  |  |  |  |
| 2-3 PM | 59 |  | 13 |  |
| 3-4 PM | 74 |  | 14 |  |
| 4-5 PM | 83 |  | 21 |  |
| 5-6 PM | 85 |  | 45 |  |
| 6-7 PM |  |  |  |  |
| 7-8 PM |  |  |  |  |
| 8-9 PM |  |  |  |  |
| 9-10 PM |  |  |  |  |
| 10-11 PM |  |  |  |  |
| 11-12 AM |  |  |  |  |
| Tota | hicles (unad | ted) | 635 | 0 |


| Southbound Volume by Hour |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- |
| Time | Left Turns | Through | Right Turns | Peds/Bikes |
| $12-1$ AM |  |  |  |  |
| $1-2 \mathrm{AM}$ |  |  |  |  |
| $2-3 \mathrm{AM}$ |  |  |  |  |
| $3-4 \mathrm{AM}$ |  |  |  |  |
| $4-5 \mathrm{AM}$ |  |  |  |  |
| $5-6 \mathrm{AM}$ |  |  |  |  |
| $6-7 \mathrm{AM}$ |  |  |  |  |
| $7-8 \mathrm{AM}$ |  |  |  |  |
| $8-9 \mathrm{AM}$ |  |  |  |  |
| $9-10 \mathrm{AM}$ |  |  |  |  |
| $10-11 \mathrm{AM}$ |  |  |  |  |
| $11-12 \mathrm{PM}$ |  |  |  |  |
| $12-1 \mathrm{PM}$ |  |  |  |  |
| $1-2 \mathrm{PM}$ |  |  |  |  |
| $2-3 \mathrm{PM}$ |  |  |  |  |
| $3-4 \mathrm{PM}$ |  |  |  |  |
| $4-5 \mathrm{PM}$ |  |  |  |  |
| $5-6 \mathrm{PM}$ |  |  |  |  |
| $6-7 \mathrm{PM}$ |  |  |  |  |
| $7-8 \mathrm{PM}$ |  |  |  |  |
| $8-9 \mathrm{PM}$ |  |  |  |  |
| $9-10 \mathrm{PM}$ |  |  |  |  |
| $10-11 \mathrm{PM}$ |  |  |  |  |
| $11-12 \mathrm{AM}$ |  |  |  |  |

## Traffic Signal Warrant Analysis

Warrants 1-3 (Volume Warrants)

| Project Name | The Highlands at Clear Spring |
| :--- | :---: |
| Project/File \# | 1808 |
| Scenario | 2022 - Projected Traffic Volumes |


| Intersection Information |  |  |  |
| :--- | :---: | :--- | :---: |
| Major Street (E/W Road) | Millertown Pike | Minor Street (N/S Road) | Glen Creek Road |
| Analyzed with | 1 approach lane | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 5214 vehicles | Total Approach Volume | 635 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 0 percent applied |

Reduction applied to warrant thresholds due to high speed on Millertown Pike

| Warrant 1, Eight Hour Vehicular Volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not satisfied | Not satisfied | Not satisfied |
| Required values reached for | 1 hour | 6 hours | 3 (Cond. A) \& (Cond. B) |
| Criteria - Major Street (veh/hr) | 350 | 525 | 280 (Cond. A) \& 420 (Cond. B) |
| Criteria - Minor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be applied only after an adequate trail of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Warrant 2, Four Hour Vehicular Volume |  |  |
| ---: | :---: | :---: |
|  |  |  |
| Condition Satisfied? | Not satisfied |  |
| Required values reached for | 3 hours |  |
| Criteria | See Figure Below |  |


| Warrant 3, Peak Hour Vehicular Volume |  |  |
| ---: | :---: | :---: |
| Condition Satisfied? | Condition A | Condition B |
| Required values reached for |  | Satisfied |
| Criteria - Total Approach Volume (veh in one hour) |  | 1 hour |
| Criteria - Minor Street High Side Volume (veh in one hour) |  | See Figure Below |
| Criteria - Minor Street High Side Delay (veh-hrs) |  |  |

Figure 4C-2 (Warrant 2-70\% Factor) \& Figure 4C-4 (Warrant 3-70\% Factor)


## APPENDIX L

## SimTraffic Queue Length Calculations

Intersection: 2: Glen Creek Road \& Millertown Pike

| Movement | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | R | LT | LR |
| Maximum Queue (tt) | 4 | 62 | 30 |
| Average Queue (ft) | 0 | 6 | 30 |
| 95th Queue (ft) | 3 | 32 | 31 |
| Link Distance (ft) |  | 218 | 5 |
| Upstream Blk Time (\%) |  |  | 32 |
| Queuing Penalty (veh) |  |  | 58 |
| Storage Bay Dist (ft) | 100 |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

Intersection: 12: Sable Point Lane/Mary Emily Lane \& Millertown Pike

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 6 | 24 | 78 | 33 |
| Average Queue (ft) | 0 | 1 | 40 | 4 |
| 95th Queue (ft) | 5 | 13 | 65 | 22 |
| Link Distance (ft) | 535 | 487 | 449 | 268 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 2: Glen Creek Road \& Millertown Pike

| Movement | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | R | LT | LR |
| Maximum Queue (tt) | 16 | 91 | 32 |
| Average Queue (tt) | 1 | 12 | 30 |
| 95th Queue (tt) | 7 | 53 | 31 |
| Link Distance (ft) |  | 218 | 5 |
| Upstream Blk Time (\%) |  | 0 | 42 |
| Queuing Penalty (veh) |  | 0 | 73 |
| Storage Bay Dist (ft) | 100 |  |  |
| Storage Blk Time (\%) |  |  |  |

Intersection: 12: Sable Point Lane/Mary Emily Lane \& Millertown Pike

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (tt) | 61 | 44 | 74 | 33 |
| Average Queue (ft) | 4 | 2 | 33 | 6 |
| 95th Queue (ft) | 31 | 19 | 61 | 27 |
| Link Distance (ft) | 535 | 487 | 449 | 268 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |

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Phone (865) 556-0042
ajaxengineering@gmail.com
September 9, 2018

## PROJECT NAME: The Highlands at Clear Spring

## TO: Knoxville/Knox County Metropolitan Planning Commission (MPC) City of Knoxville Engineering Department <br> Knox County Engineering Department

SUBJECT: TIS Comment Response Document for The Highlands at Clear Spring Review Comments Dated September 4, 2018 (9-G-18-UR \& 9-SE-18-C)

Dear MPC, City of Knoxville, and Knox County Staff,
The following comment response document is submitted to address comments dated September 4, 2018. Below, the first set of reviewer comments is from John Sexton, PE with Knox County Engineering and the second set of reviewer comments is from Tarren Barrett with the MPC.

## John Sexton, PE, Knox County Engineering:

Reviewer Comment: Page 2: 2nd paragraph, last line- add "or not" after "whether".
Response: On Page 2, in the 2nd paragraph, last line - "or not" was added after "whether".

Reviewer Comment: Page 7: Table 1 indicates that Glen Creek Road is 2-lane undivided road 26 feet wide. However, it is a boulevard cross-section.

Response: On Page 7, Table 1 was revised to show Glen Creek Road as a 2-lane boulevard with a road width of 46 feet.

Reviewer Comment: Page 10: 1st paragraph, last line- Please verify if the 36 SF lots are east of the roundabout or west of it.

Response: On Page 10, in the $1^{\text {st }}$ paragraph on the last line, the wording was changed for the 36 single-family residential detached lots and was corrected to state that they are west of the roundabout.

Reviewer Comment: Page 31: The reported HCM delay for the AM peak at Millertown Pike/Glen Creek Road is 7.7 seconds instead of 7.6 seconds.

Response: On Page 31 in Table 4, the reported HCM delay for the AM peak at Millertown Pike/Glen Creek Road for the westbound left turn movement was changed to 7.7 seconds instead of 7.6 seconds.

Reviewer Comment: Page 34: The last paragraph references 36 single-family lots east of the roundabout and 75 to the west. Are these reversed? See page 10 comment above.

Response: On Page 34 in the last paragraph, the location of the single-family detached lots was corrected to reflect the proper existing distribution of lots to the east and west of the roundabout.

Reviewer Comment: Page 36: Please add a traffic volume bubble at the intersection of Millertown Pike/Sable Point Lane/Mary Emily Lane showing the through traffic generated by the project.

Response: On Page 36, Figure 7, a traffic volume "bubble" was added at the intersection of Millertown Pike/Sable Point Lane/Mary Emily Lane showing the through traffic generated by the project.

Reviewer Comment: Page 38: The AM peak northbound left-turn volume on Glen Creek Road at Millertown Pike should be 172 instead of 169. Also make this correction in the affected capacity analysis and any affected reports of LOS, delay, and $\mathrm{v} / \mathrm{c}$.

Response: On Page 38, Figure 8, the AM peak northbound left-turn volume on Glen Creek Road at Millertown Pike was changed to 172 instead of 169. This volume revision also resulted in updates to Table 6, Table 8 and the LOS reports in Appendix G.

Reviewer Comment: Page 39: The AM peak LOS for eastbound Old Millertown Pike at Glen Creek Road should be B instead of A.

Response: On Page 39, the AM peak LOS for eastbound Old Millertown Pike at Glen Creek Road in Table 6 was changed to B instead of A.

Reviewer Comment: Page 40: The section title, "Discussion of Vehicle Crashes on Millertown Pike" should be bulleted but not underscored to match other subheading formats.

Response: On Page 40, the section title, "Discussion of Vehicle Crashes on Millertown Pike" was changed from underscored to a bulleted format.

Reviewer Comment: Page 45: Please provide actual field measurements of the available sight distance at Millertown Pike/Glen Creek Road. Based on County measurements, the available sight distance is 330 feet to the left and 350 feet to the right.

Response: The sight distance at the intersection of Glen Creek Road at Millertown Pike was measured on September 5th, 2018 by Scott Williams, PE, RLS. The following results were obtained from Glen Creek Road at Millertown Pike: the sight distance looking to the west (left) is 362 feet and the sight distance looking to the east (right) is 478 feet. These measurements were taken on Glen Creek Road 15 feet away from the edge of pavement of Millertown Pike. The surveyor believes that 400 feet of sight distance is potentially available looking to the west (left) if tree limbs are removed from the cedar trees located on the north side of Millertown Pike (and west of the intersection). It is believed that the cedar tree limbs are within the right-of-way, however, the trees themselves are located on private property. This new information is included on Pages 45-46 and 48 in the revised report.

Reviewer Comment: Page 51: Section 2C- Change the intersection road names to Old Millertown Pike at Glen Creek Road.

Response: On Page 56 (previously Page 51), in Section 2C - the intersection road names were changed to Old Millertown Pike at Glen Creek Road.

Reviewer Comment: Appendix I: Please highlight or otherwise identify which factors from the TDOT tables were used in the crash rate calculations.

Response: In Appendix I, the TDOT factors are highlighted that were used in the crash rate calculations.

## Tarren Barrett, MPC:

1. Reviewer Comment: In the first full paragraph on page 8, please rephrase the first sentence. It is unclear what is meant by a "straight horizontal and vertical road alignment."

Response: On Page 8, in the first full paragraph, the first sentence was rephrased by splitting the original sentence into 2 sentences.
2. Reviewer Comment: On page 25 half-way through the continued paragraph, correct "cutting thru" to "cutting through."

Response: On Page 25, half-way through the continued paragraph, the wording was corrected to "cutting through" from "cutting thru."
3. Reviewer Comment: On page 34 third paragraph, please rephrase the first sentence since it is too long and is unclear on the point that is trying to be made.

Response: On Page 34 in the third paragraph, the sentence was re-worded to make the discussion point clearer.
4. Reviewer Comment: On page 39, the table references a LOS of $F$ for the Northbound Left/Right of Millertown Pike at Glen Creek Road and the Northbound Left/Thru/Right of Millertown Pike at Sable Point Lane/Mary Emily Lane, but there are no recommendations on how to improve the internal street structure. Please look at providing recommendations for these. There was no mention of this in the Conclusions and Recommendations section.

Response: Further discussion of the internal street structure of the Millertown Pike at Glen Creek Road intersection is provided on Pages 54-55. Further discussion of the internal street structure of the Millertown Pike at Sable Point Lane / Mary Emily Lane intersection is provided on Pages 58-59.
5. Reviewer Comment: On page 46 last paragraph, please mention the right-turn lane requirement in the previous approval from 2005. It was mentioned that a right-turn lane was needed "by the time the next 40 homes are constructed in the Clear Springs development (either in Phase 1 or 2)." There are homes currently being constructed for previous phases. What does this mean, and what lot number out of the whole does it trigger the right-turn lane?

Response: On Page 48 (previously Page 47), the discussion involving the timing of the construction of the right turn lane has been removed. The developer has stated that they will begin design and construction of the
right turn lane immediately once The Highlands at Clear Spring has been approved by the County.
6. Reviewer Comment: On page 47, please give what the measured sight distance is.

Response: As stated earlier in this response letter, the sight distance at the intersection of Glen Creek Road at Millertown Pike was measured on September 5, 2018 by Scott Williams, PE, RLS. The following results were obtained from Glen Creek Road at Millertown Pike: the sight distance looking to the west (left) is 362 feet and the sight distance looking to the east (right) is 478 feet. These measurements were taken on Glen Creek Road 15 feet away from the edge of pavement of Millertown Pike. The surveyor believes that 400 feet of sight distance is potentially available looking to the west (left) if tree limbs are removed from the cedar trees located on the north side of Millertown Pike (and west of the intersection). It is believed that the cedar tree limbs are within the right-of-way, however, the trees themselves are located on private property. This new information is included on Page 45-46 and 48 in the revised report. In addition, a recommendation has been added on Page 51 that states a Side Road Sign (W2-2) should be installed for eastbound traffic on Millertown Pike.
7. Reviewer Comment: The study needs to reflect a connection to and evaluation of Parasol Lane from Autumn Creek Drive, which the developer has agreed to connect to.

Response: In addition to the existing discussion of this road connection on Pages 57-58, an additional discussion was added on Pages 59-60.
8. Reviewer Comment: Include a detailed figure with dimensions of the rightturn lane of Millertown Pike at Glen Creek Road per the 100 ft storage length and 150 ft taper length. If a full right-turn lane is not feasible given the utility pole, close proximity of the adjacent property owner's driveway, severe grades and guard rail, then please work with Knox County Engineering to determine a better solution given the constraints.

Response: Scott Williams, PE, RLS has designed a rough layout for a right turn lane on Millertown Pike at Glen Creek Road. This layout does not consider right-of-way, existing utilities, grading, and drainage but does provide a conceptual level layout. This layout has been provided in the revised report and is labeled as Figure 10 on Page 49.
9. Reviewer Comment: Please refer to John Sexton's (Knox County Engineer) attached comments for further revisions.

Response: The response to the comments made by John Sexton are provided at the beginning of this response letter.

In addition to the requested revisions, other changes in the report include the following:

- Updated Page Footers
- Updated Title Page
- Updated Table of Contents
- Updated Recommendations on Page 2
- Added Figure 10
- Added Appendix L

If you have any questions or further comments, please feel free to contact me at any time. I look forward to your review and approval.

Sincerely,
Ajax Engineering, LLC
Robert W. Jacks, P.E.



[^0]:    ${ }^{1}$ Major Road Plan - May 2011 by Knoxville/Knox County Metropolitan Planning Commission
    ${ }^{2}$ Edge of curb to edge of curb or edge of pavements near project site
    ${ }^{3}$ According to Knoxville Area Transit System Map

[^1]:    Revised September 2018
    The Highlands at Clear Spring
    Transportation Impact Study
    Knoxville, TN

